Fluctuation-driven dynamics in nanoscale thin-film flows: Physical insights from numerical investigations

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The effects of thermal fluctuations on nanoscale flows are captured by a numerical scheme that is underpinned by fluctuating hydrodynamics. A stochastic lubrication equation (SLE) is solved on nonuniform adaptive grids to study a series of nanoscale thin-film flows. The Fornberg scheme is used for high-resolution spatial discretization and a fully implicit time-marching scheme is designed for numerical stability. The accuracy of the numerical method is verified against theoretical results for thermal capillary waves during the linear stage of their development. The framework is then used to study the nonlinear behavior of three bounded thin-film flows: (1) droplet spreading, where power laws are derived; (2) droplet coalescence, where molecular dynamics results are reproduced by the SLE at a fraction of the computational cost and it is discovered that thermal fluctuations decelerate the process, in contrast to previously investigated phenomena; and (3) thin-film rupture, where, in the regime considered, disjoining pressure dominates the final stages of rupture.

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I. INTRODUCTION

Bounded planar thin-film flows are common in both nature and technology. A variety of interesting flow behaviors fall into this class, including rupture [1], dewetting [2], droplet spreading [3], and sessile droplet coalescence [4]. Dynamics of these processes can often be well described by lubrication equations (LEs), derived using a long-wave approximation to the Navier-Stokes equations [5], which reduces the modeling problem to solving a single partial differential equation. Motivated by emerging technologies in micro- and nanoscale fluid dynamics [6], thin-film nanoflows have attracted considerable interest recently and challenged conventional theories, due

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to the emergence of new dominant physics at these scales. An important physical factor at the nanoscale is thermal noise, which has been shown experimentally to influence interfacial dynamics through the observation of thermal capillary waves on interfaces of (ultra-low surface-tension) colloid-polymer mixtures [7]. Recently, with the use of molecular dynamics (MD) simulations, it has been discovered that fluctuation-driven nanowaves dominate a range of nanoscale interfacial-flow phenomena, such as nanothread breakup [8], nanojet instability [9], nanodroplet coalescence [10], and development of rough interfaces on nanoscale thin films [11]. Notably, the observations of nanothread breakup in MD were further confirmed by an analytical model [12] and experiments with colloid-polymer mixtures [13,14].

To model thin-film flows with thermal noise mathematically, Grün *et al.* [15] derived a stochastic lubrication equation (SLE) by applying a long-wave approximation to the Landau-Lifshitz-Navier-Stokes equations (the fluctuating hydrodynamics equations) [16]. Linear instability analysis was then conducted on the SLE by Mecke and Rauscher [17] to obtain an evolving spectrum for thermal capillary waves of the film interface. It was shown that thermal noise changes the spectrum of thermal capillary waves from an exponential decay to a power law for large wave numbers, which was then confirmed by the experimental observations on the dewetting of polymer films [18]. The same spectrum behavior was also confirmed in MD simulations, first done by Willis and Freund [19] in 2010 and recently, followed by Zhang *et al.* [20], who showed that interfacial roughening falls into a universality class [11]. However, theories based on small deviations from equilibrium cannot, inevitably, describe inherently nonlinear events such as film breakup.

Besides the theoretical analysis, numerical studies of the fully nonlinear SLE have also been carried out with uncorrelated noise [21] and a spatially correlated noise model [22], whose solutions at the linear stage are confirmed by the theory for thermal capillary waves and experimental data, respectively. The nonlinear dynamics was also investigated in these numerical studies with particular attention paid to thin-film rupture time [22] and droplet size distribution after dewetting [21]. However, analytic results for these nonlinear behaviors are nontrivial. The only successful attempt is on nanodroplet spreading [23,24], where a similarity solution was derived for "fluctuation-dominated spreading" and then verified numerically. Therefore, numerical investigations have become an important approach to better understand the nonlinear behaviors of thin-film flows. Interestingly, the spatial discretization in previous works [21,22,25] was developed only on uniform grids, meaning that the locally nonlinear behaviors (e.g., multiscale rupture dynamics) could not be easily resolved with high accuracy, while, in the deterministic cases (LE), these local behaviors have been captured accurately on nonuniform grids in a range of different numerical schemes [26–29].

In this work, we develop an accurate and efficient numerical scheme (on nonuniform grids) to overcome the aforementioned drawbacks and employ it to investigate different kinds of bounded thin-film flows; in particular for flows where we expect locally nonlinear dynamics (such as in rupture and coalescence).

The article is laid out as follows. In Sec. II the SLE is introduced, the numerical scheme is proposed and the correlated-noise model is presented. In Sec. III numerical solutions for the SLE are verified against known analytical results (Sec. III). In Sec. IV we use the SLE solver to study three different kinds of thin-film flows with nonlinear dynamics: (1) droplet spreading on a precursor film verified by theories developed (Sec. IV A), (2) bounded droplet coalescence, validated by MD (Sec. IV B), and (3) thin-film rupture (Sec. IV C).

II. MATHEMATICAL MODELING AND NUMERICAL APPROACH

In this section, we introduce the mathematical model which describes nanoscale thin-film flows and then propose a numerical framework for solving the associated system of equations. We first present the nondimensionalised SLE.



FIG. 1. Schematic of a thin film with a perturbed interface.

A. Stochastic lubrication equations

The SLE for a two-dimensional bounded film was first derived by Grün *et al.* [15] and Davidovitch *et al.* [23], who applied a long-wave approximation to the fluctuating hydrodynamics equations to describe the dynamics of the interface by the film height h(x, t) (see Fig. 1). Recently, Zhang *et al.* [30] proposed a more general SLE using a slip boundary condition, which is crucial at the nanoscale, so this approach is employed here.

To identify the governing dimensionless parameters, we nondimensionalize the SLE with the following characteristic scales:

$$h = \tilde{h}/h_0, \quad t = \tilde{t}/(3\mu h_0/\gamma), \quad \Pi = \tilde{\Pi}/(\gamma/h_0), \quad \mathcal{N} = \tilde{\mathcal{N}}\sqrt{3\mu h_0^2/\gamma},$$

where \tilde{h} , \tilde{t} , Π , and \tilde{N} represent the dimensional interface height, time, disjoining pressure, and normally distributed random variable (the model for thermal fluctuations), respectively. Note that the dimensional material parameters are not given tildes. h_0 is the characteristic film height, μ is the liquid's dynamic viscosity and γ is surface tension. Following Zhang *et al.* [30], the dimensionless SLE is given by

$$\frac{\partial h}{\partial t} = -\frac{\partial}{\partial x} \left[M(h) \left(\frac{\partial^3 h}{\partial x^3} - \frac{\partial \Pi}{\partial x} \right) - \sqrt{2\varphi M(h)} \mathcal{N} \right].$$
(1)

Here the mobility $M(h) = h^3 + 3 l_s h^2$, so that the slip length $l_s = 0$ the "orginal SLE" from Ref. [15] is recovered. The disjoining pressure $\Pi = A/(6\pi h^3)$, where A is the dimensionless Hamaker constant, reflecting the strength of the van der Waals forces between liquid and a substrate [20]. The noise term \mathcal{N} has zero mean and covariance $\langle \mathcal{N}(x,t)\mathcal{N}(x',t')\rangle = \delta(x-x')\delta(t-t')$. The dimensionless parameter $\varphi = l_T^2/(Wh_0)$ relates to the intensity of interface fluctuations, where $l_T = \sqrt{k_B T/\gamma}$ is the characteristic thermal fluctuation length and W is the initial thickness of the film (z direction). When $\varphi = 0$, the deterministic LE [5] is recovered. In this work, periodic boundary conditions are considered in all cases and the initial conditions depend on the type of thin-film flow we simulate. The remaining parts of this section are concerned with the numerical scheme for solving Eq. (1).

B. Spatial discretization on nonuniform grids

To resolve locally large gradients in flow variables, without slowing down the computation dramatically, we use a nonuniform grid for spatial discretization. We choose the well-known scheme proposed by Fornberg [31] to approximate spatial derivatives using finite differences,

$$\frac{d^k}{dx^k}h(x) \approx \sum_{j=0}^n \mathcal{L}_{j,n}^k(x)h(x_j),\tag{2}$$

where $\{x_j\}_{j=0}^s$ are the grid points chosen for approximation and $\mathcal{L}_{j,s}^k(x)$ are the Fornberg coefficients calculated at *x*. Details of the calculation and error estimate of the Fornberg coefficients can be found in Appendix A.

To apply the Fornberg scheme for spatial discretization we first rearrange the SLE into a conservative form:

$$\frac{\partial h}{\partial t} = -\frac{\partial F(h)}{\partial x}, \quad \text{where } F(h) = M(h) \left(\frac{\partial^3 h}{\partial x^3} + \frac{A}{2\pi h^4} \frac{\partial h}{\partial x}\right) - \sqrt{2\varphi M(h)} \mathcal{N}. \tag{3}$$

The film height h(x, t) is to be solved at the *m*th step, t^m , according to a certain spatial discretization $\{x_i\}_{i=0}^n$ to give an array $\{h_i^m\}_{i=0}^n$. We use 3 (n = 2) and 5 (n = 4) points to approximate the first-order and the third-order derivatives, respectively, with the target point located at the center to provide second-order accuracy. The expression for the spatial discretization of Eq. (3) at the *i*th node is then written as

$$\partial_t h_i = -\sum_{j=0}^2 \mathcal{L}_{j,2}^1 F_{i-1+j}, \tag{4}$$

where

$$F_{i} = M(h_{i}) \left(\sum_{j=0}^{4} \mathcal{L}_{j,4}^{3} h_{i-2+j} + \frac{A}{2\pi h_{i}^{4}} \sum_{j=0}^{2} \mathcal{L}_{j,2}^{1} h_{i-1+j} \right) - \sqrt{2\varphi M(h_{i})} N_{i}.$$
(5)

Here $\mathcal{L}_{j,2}^1(x_i)$ using $\{x_{i-1}, x_i, x_{i+1}\}$ and $\mathcal{L}_{j,4}^3(x_i)$ using $\{x_{i-2}, x_{i-1}, x_i, x_{i+1}, x_{i+2}\}$ are the Fornberg coefficients for the first and third derivatives, respectively.

C. Implicit time-marching method

Equation (4) is of the form

$$\frac{\partial \mathbf{h}}{\partial t} = \mathbf{D} \, \mathbf{h},\tag{6}$$

where **h** is the solution vector and **D**(**h**) is a matrix representing the nonlinear differential operator and has size $(n + 1) \times (n + 1)$. Employing the implicit Euler time-marching method [32] to Eq. (6) gives

$$\frac{\mathbf{h}^{m+1} - \mathbf{h}^m}{\Delta t} = \mathbf{D}(\mathbf{h}^{m+1}) \, \mathbf{h}^{m+1},\tag{7}$$

where the superscript m denotes the time-step level. This is equivalent to

$$\mathbf{G} = \left[\mathbf{I} - \Delta t \, \mathbf{D}(\mathbf{h}^{m+1})\right] \mathbf{h}^{m+1} - \mathbf{h}^m = \mathbf{0},\tag{8}$$

and this root-finding problem, $\mathbf{G}(\mathbf{h}^{m+1}) = \mathbf{0}$, can be solved by the Newton-Kantorovich method [33], using an initial guess of the solution \mathbf{h}^g (the superscript *g* denotes "guess") obtained by an explicit Euler time-marching method:

$$\mathbf{h}^{g} = \mathbf{h}^{m} + \Delta t \, \mathbf{D}(\mathbf{h}^{m}) \, \mathbf{h}^{m}. \tag{9}$$

If \mathbf{h}^g is a distance \mathbf{q} away from the solution, $\mathbf{h}^{m+1} = \mathbf{h}^g + \mathbf{q}$, so that $\mathbf{G}(\mathbf{h}^g + \mathbf{q}) = \mathbf{0}$, then in the linear approximation one has

$$\mathbf{G}(\mathbf{h}^g + \mathbf{q}) \approx \mathbf{G}(\mathbf{h}^g) + \frac{\partial \mathbf{G}(\mathbf{h}^g)}{\partial \mathbf{h}^g} \mathbf{q} = \mathbf{0}.$$
 (10)

From Eq. (8) we have

$$\frac{\partial \mathbf{G}(\mathbf{h}^g)}{\partial \mathbf{h}^g} = \mathbf{I} - \Delta t \mathbf{J},\tag{11}$$

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where the **J** is the Jacobian of $D(h^g)$. Combining Eqs. (10) and (11) yields a linear approximation of **q**,

$$\mathbf{q} \approx -(\mathbf{I} - \Delta t \mathbf{J})^{-1} \mathbf{G}(\mathbf{h}^g), \tag{12}$$

so that we can update \mathbf{h}^g as $\mathbf{h}^g + \mathbf{q}$ and repeat the process. If the iteration converges, both \mathbf{q} and $\mathbf{G}(\mathbf{h}^g)$ will decrease quadratically, eventually to zero. The final solution, $\mathbf{h}^{m+1} = \mathbf{h}^g$.

To control numerical errors caused by the temporal discretization, we implement the following criteria:

(1) The solution is not negative at any point, $h_i > 0$

(2) The maximum value of the time derivative error has to be smaller than a prescribed upper limit, where the error can be computed using the second-order derivative in the Taylor expansion, $\max_{1 \le i \le n} \left(\left| \frac{(\Delta t^m)^2}{h_i^m} \frac{d^2 h_i^m}{dt^2} \right| \right) < 10^{-3}$

(3) The iteration process converges, i.e., specifically, $|q_i|/h_i$ decreases monotonically to below 10^{-4}

(4) The number of iteration steps is smaller than 100.

If any condition is not satisfied, we go back to the initial value $(h_i^g = h_i^m)$ and restart the iteration process with a reduced time step. If Δt is smaller than 10^{-16} , the iteration halts and the code ends in a failed state. Unavoidably, the implicit Euler scheme applied to stochastic differential equations converges slower with reducing time steps than the equivalent deterministic system [32], forcing a smaller time step for the SLE (compared to the LE) that significantly increases the computational costs.

D. Correlated-noise model

The covariance of uncorrelated fluctuations are described by a Dirac delta function. The delta function could be approximated by a two-dimensional rectangular (boxcar) function (in t and x) that is nonzero over a time step (Δt) and grid spacing (Δx), i.e., $\mathcal{N}(x, t) \approx N_i^t / \sqrt{\Delta t \Delta x}$. Here N_i^t represents computer-generated random numbers and follows a normal distribution with zero mean and unit variance. However, this model has been shown prone to numerical instability for the SLE [34]; problems that are exacerbated as Δx and Δt become smaller and the amplitude of noise becomes larger.

To achieve a robust numerical scheme with nonuniform spatial and temporal discretization, we combine the spatially correlated noise model from Ref. [15] and the temporal one from Ref. [34], so that the noise becomes correlated beneath the spatial correlation length L_c and the time correlation length T_c . Uncorrelated behavior can then be approximated by taking the limit of these lengths to zero, ensuring they are numerically well resolved throughout the limiting process.

Following [15], the stochastic term, $\mathcal{N}(x, t)$ is expanded using separation of variables in the *Q*-Wiener [$\mathcal{W}(x, t)$] process as

$$\mathcal{N}(x,t) = \frac{\partial \mathcal{W}(x,t)}{\partial t} = \sum_{q \to -\infty}^{q \to +\infty} \chi_q \dot{c}_q(t) g_q(x).$$
(13)

Here the constant χ_q are the eigenvalues of the correlation function $F_{\rm cor}$,

$$\chi_q = \int_{-L/2}^{L/2} F_{\rm cor}(x) e^{-i2\pi qz/L} \, dx \,, \tag{14}$$

where q represents an integer sequence. The expressions for F_{cor} and details about this model can be found in Appendix B. The coefficient $\dot{c}_q(t)$ represents a temporally correlated noise process in our setup, in contrast to [15] where uncorrelated noise is considered, modeled by a simple linear interpolation between uncorrelated random noise at the endpoints of the temporal correlation interval [34] (see Fig. 17). As the full implicit time-marching method usually provides stable



FIG. 2. Interface profiles at two time instants ($t_1 = 20$ and $t_2 = 70$) from numerical solutions of the SLE with different values of the noise strength φ . Note that the same random numbers are employed in all the cases.

numerical performance with large time steps ($\Delta t > T_c$), this temporally correlated model will be only activated and is only practically necessary, when capturing local dynamics near singularities for very small Δt , e.g., for the final stage of film rupture (see more details in Appendix B).

E. Grid-size convergence

To test the grid-size convergence of the numerical approach above, we consider the simulation of a relatively short film L = 15 with an initial perturbation $h(x, 0) = -0.7 \cos(2\pi x/L)$, which relaxes to a relatively flat film in the absence of disjoining pressure (A = 0). We set $L_c = 1.5$ and run the simulations with an increasingly fine grid spacing for different values of the noise strength φ , whose influence is shown in Fig. 2.

Notably, besides numerical errors caused by discretizations in the simulation, statistical errors are also introduced by the stochastic term in the SLE. To better demonstrate the convergence, we measure two different kinds of errors.

The first one comes from the numerical discretization scheme. To exclude the influence of statistical variability, we perform simulations with the same $\mathcal{N}(x, t)$ for all cases, which is generated before the simulations by fixing N_q^t (see Appendix B) at each time instant. Figure 3(a) shows simulation results with $\varphi = 10^{-2}$ at three time instances for varying grid size. These interface profiles in Fig. 3(a) agree well with each other, indicating that the numerical errors indeed converge. We check the average deviation of each interface profile to that with the finest resolution calculated ($\Delta x = 0.0094$) shown in Fig. 3(b), where the second-order convergence, as expected, is confirmed, with the prefactor depending, unsurprisingly, on noise strength.

Since convergence studies for noisy systems are naturally stochastic, the second target quantity to test convergence is ensemble-averaged; here the ensemble consists of 200 independent simulations. The ensemble-averaged profiles at three-time instances are plotted in Fig. 4(a) for varying grid size. Here all profiles are presented relative to the minimum point (i.e., we plot *h* against $x - x_{min}$). Then we check the average deviation of each ensemble-averaged profile to that with the finest resolution ($\Delta x = 0.0094$); see Fig. 4(b), where the convergence is confirmed. Note the deterministic result (black lines) follow second-order convergence, while, as also expected, the stochastic cases converge with approximately first-order convergence.



FIG. 3. (a) Interface profiles obtained with different grids at three time instances: $t_1 = 20$, $t_2 = 40$, and $t_3 = 70$. Here $\varphi = 10^{-2}$. (b) Convergence characteristics for decreasing grid size, where Dev. is average deviation of interface profiles to the finest resolution profile in (a).

III. NUMERICAL VERIFICATION: THERMAL CAPILLARY WAVES

In this section, the numerical scheme is verified by comparison to analytical results known for thermal capillary waves, with particular attention paid to the effect of the nonuniform grid, which are known to create spurious effects in some stochastic partial differential equation systems [35].

The fluctuations of the interface in thermal equilibrium [11,17] can be described by the classical theory for thermal capillary waves [7,18] with the static spectra of each surface mode (wave number) derived from the equipartition theorem. To capture the development of thermal capillary waves towards the equilibrium state, more advanced theories that include the time evolution of wave spectra were derived by applying linear stability analysis to the SLE [20,22]; we will use the model from Ref. [20] to validate our numerical solutions. Starting with a smooth initial surface and neglecting disjoining pressure (A = 0), in dimensionless form the time evolution of the spectrum is given by (see Appendix C for derivation)

$$|H|_{\rm rms} = \sqrt{-\frac{\varphi L}{k^2}(e^{-2k^4t} - 1)},$$
(15)



FIG. 4. (a) Ensemble-averaged interface profiles obtained from 200 independent realizations at three time instances: $t_1 = 20$, $t_2 = 50$, and $t_3 = 80$. Here $\varphi = 10^{-2}$. (b) Convergence characteristics for decreasing grid size, where Dev. is average deviation of ensemble-averaged interface profiles to the finest resolution profile in (a).



FIG. 5. Interface profiles of a bounded film at four time instants, $t_1 = 0.0$ (purple dashed line), $t_2 = 0.001$ (black solid line), $t_3 = 0.1$ (blue dotted line), and $t_4 = 1.0$ (red dash-dotted line). The parameters chosen are $\varphi = 10^{-3}$ and L = 100. The inset shows how the waves develop on the nonuniform grid (with exponential distribution and markers representing nodal positions), with a higher density as one goes from left to right.

where $|H|_{\text{rms}}$ represents the root-mean square of wave perturbations in the frequency domain, k is the dimensionless wave number, and L is the dimensionless length of the film.

Figure 5 shows a typical simulation result of the development of thermal capillary waves, where perturbations, driven by thermal fluctuations, grow against time to generate significant capillary waves at the later stage (see the dash-dotted red line in Fig. 5). Note that, to test our nonuniform grid implementation, the grid nodes are nonuniformly distributed with the largest grid size $\Delta x_{\text{max}} = 0.1$ at x = 0 and the smallest grid size $\Delta x_{\min} = 0.001$ at x = L. We use the spatial correlated noise with $L_c = 0.1 \ge \Delta x$. The noise is uncorrelated in time with $\Delta t = 10^{-3}$.

To gather statistics, 50 independent simulations (or "realizations") are performed. The solution is divided into two regions: x < L/2 with coarse grids and x > L/2 with dense ones, to check the influence of the different grid sizes. On each region, a discrete Fourier transform of h(x, t) is applied to get the power spectral density. We then ensemble average the power spectral density at each time instant over the realizations and take the square root to produce the numerical results in Fig. 6 (dash lines with markers). Good agreement with the theory for thermal capillary waves [Eq. (15)] can be found for both regions (see red and blue line), validating the accuracy of our numerical scheme on extreme nonuniform grids.

IV. NUMERICAL SIMULATIONS FOR PHYSICAL INSIGHT

Having verified our numerical scheme, in this section we use the SLE solver established to explore three bounded thin-film flows with strong nonlinear dynamics: (1) droplet spreading on a precursor film, (2) sessile droplet coalescence, and (3) thin-film rupture, all of which are ubiquitous phenomena observed both in nature and many industrial processes [36,37].



FIG. 6. The root-mean square of (wave) disturbance amplitude vs the wave number at three time instants, $t_1 = 0.2$, $t_2 = 0.4$, and $t_3 = 0.6$; a comparison of ensemble-averaged SLE simulations (dashed lines with markers) and the analytical result (solid lines).

A. Droplet spreading on a precursor film

We now consider the nonlinear dynamics of a droplet spreading on a precursor film, for which the deterministic scaling is given by Tanner's law [3], and the more recent work of Davidovitch [23] resulted in a law that accounted for thermal fluctuations. In particular, these are given by

$$\begin{cases} \ell \sim t^{1/7}, & \text{Hydrodynamic (deterministic) spreading (Tanner's law) [3]} \\ \ell \sim t^{1/4}, & \text{Spreading driven by thermal fluctuations (Fluctuation-enhanced Tanner's law) [23].} \end{cases}$$
(16)

Here ℓ represents a characteristic lateral scale, which is estimated using the average second moment of *h* [see Eq. (D1) in Appendix D] [23]. The larger power law (1/4) in Davidovitch's theory demonstrates that the nanoscale spreading is enhanced by thermal fluctuations. However, these two theories are only valid for spreading with the no-slip boundary condition ($l_s = 0$), which is often inaccurate at the nanoscale. Therefore, we use the SLE with the slip boundary condition ($l_s \neq 0$) to derive "slip-modified" power laws for the spreading (see Appendix D for the detailed derivation):

$$\begin{cases} \ell \sim t^{1/6}, & \text{Slip-modified Tanner's law,} \\ \ell \sim t^{1/3}, & \text{Slip-modified fluctuation-enhanced Tanner's law.} \end{cases}$$
(17)

Note that the power laws are larger than those based on the no-slip boundary condition, predicting that the spreading is accelerated by slip, as we might expect.

The initial droplet profile for the numerical solutions is given by a section of a sinusoidal function with a precursor film set over the whole simulation domain. This approach has been widely used [22–24,38] and designed not only for numerical convenience, but also to circumvent the contact-line dynamics (which are fascinating, but not the focus of this article). To avoid rupture of the thin precursor film (the thickness of precursor film is less than one percent of the initial height of the droplet), we follow Ref. [23] and switch off the thermal fluctuations on it. Notably, it is unclear whether this "artificial limiter" modifies the numerical path in the stochastic process. More advanced approaches, like a Brownian bridge technique [39] or the inclusion of disjoining pressures, are certainly worthy of future investigation in this regard, but given the slightly artificial nature of the precursor film here they are considered beyond the scope of this article. When the droplet spreads to a precursor-film node and "pulls it up," namely, $h_i > h^*$, the fluctuations on this node are activated.



FIG. 7. Spreading profiles at three time instants, $t_1 = 10$ (black lines), $t_2 = 10^2$ (blue lines), and $t_3 = 10^3$ (red lines) with the no-slip boundary. where the solid lines represent one selected realization. The dash-dotted lines are the average from 50 realizations. The dotted lines are the (LE) solution of the deterministic equation. The inset shows the local behaviors of the selected realization (solid lines in the full plot). The lines symbols represent the adaptive grid nodes.

Moreover, since we are interested only in the spreading driven by surface tension and fluctuations in this work, the disjoining pressure is neglected (A = 0).

To accurately capture the spreading power laws, one needs to simulate the drop spreading for several decades of length. Thus it is computationally expensive to perform simulations on grids uniformly distributed in both the "drop" and "precursor film," in which the height of many nodes will vary very little over each time step. To reduce computational costs, we utilize our nonuniform adaptive grids with $\Delta x_{\min} = 0.01$ on the "drop" and $\Delta x_{\max} = 0.1$ on the "film," with the nodes in front of the advancing contact angles refined automatically ($\Delta x_i = \Delta x_{\min}$) to capture the spreading dynamics (see the inset in Fig. 7). Here each SLE realization on the uniform grids need about 4 core hours, while one simulation on the nonuniform adaptive grids costs less than 0.2 core hours; i.e., the speed-up is about 20.

Figure 7 shows the droplet profiles at different time steps, where the stochastic profiles are the average of the 50 independent realizations with $\varphi = 10^{-3}$. Note that the initial spreading is much "faster" than that at the later stage ($t_3 - t_2$ is much larger than $t_2 - t_1$) due to the initially stronger capillary forces (from the larger curvatures near where the drop meets the precursor), while at the later stage the thermal fluctuations play a significant role and accelerate the process (see the comparison between dotted lines and dash-dotted lines in Fig. 7).

The characteristic lateral scales (i.e., the drop's width) are plotted in Fig. 8, where the numerical solutions match not only previous analytical solutions with the no-slip boundary condition (black lines) [23], but also our "slip-modified" power laws (red lines) very well, giving us further confidence that our numerical scheme captures nanoscale flow physics both accurately and efficiently. Notably, in both boundary conditions, there exists a transfer from hydrodynamic spreading (Tanner's law) to the fluctuation-driven spreading (Davidovitch's law), showing that the noise dominates over deterministic relaxation only at the later stages of the spreading ($t \gg 1$).

B. Bounded droplet coalescence

Previous studies for droplet coalescence on a substrate have been carried out in the thin-film regime [4,40,41] without any influence of thermal fluctuations taken into account (i.e., using the



FIG. 8. Influence of the slip on the characteristic lateral scale, where black lines and red lines represent no-slip and slip results, respectively. The slip length $l_s = 1.0$. The dash-dotted lines are the solutions of the deterministic cases. The solid lines are the solutions of the stochastic cases with $\varphi = 10^{-3}$. Dashed lines represent similarity solutions in Eqs. (16) and (17).

LE), where surface tension is considered as the main driving force. However, Perumanath *et al.* [10] have shown that the fluctuations are crucial to the dynamics of coalescence of two "free" nanodroplets in a vacuum with MD. A similar influence of noise can be expected in the coalescence of two "bounded" nanodroplets, which will be explored by the SLE solver in this section. To verify our numerical predictions, we perform independent MD realizations for both symmetric-drop and asymmetric-drop coalescence (see details of MD settings in Appendix E). Note that we focus on two-dimensional cases here.

The MD results of two coalescence cases are presented in Fig. 9 with two separate droplets on the substrate set as the initial conditions. The initial distance between the two droplets is 50 nm.



FIG. 9. MD results for the coalescence. (a) Symmetric-drop coalescence with the same initial droplet radius (at $t = t_0 - 16.7$), R = 10 nm. (b) Asymmetric-drop coalescence with different initial droplet radii (at $t = t_0 - 12.2$): $R_1 = 15$ nm and $R_2 = 10$ nm.



FIG. 10. Asymmetric-drop coalescence profiles predicted in a representative simulation by the LE (dashdotted lines) and SLE (solid lines) at three time instants: $t_1 = 0.8$, $t_2 = 6.4$, and $t_3 = 13.8$. The inset shows the grid node distributions.

Because of the fully wettable substrate, both droplets spread first until their contact lines meet. The moment when the two droplets first connect and form a "molecular bridge" is defined as t_0 , shown in Fig. 9. After that, the liquid bridge grows and the two droplets eventually merge into one.

Similar to Sec. IV A, here the disjoining pressure is also neglected (A = 0). The dimensionless fluctuation intensity ($\varphi = 5.1 \times 10^{-3}$) is calculated from the liquid transport properties of MD (see the details in Appendix E). To set the initial configuration for the SLE, h(x, 0), the MD interface profile of each realization at t_0 is extracted from uniform bins along the x axis based on a threshold density. Then we shift all the coalescence points to the same position and use the averaged interface profiles as h(x, 0) for the SLE. Simulations are carried out on fixed nonuniform grids with more nodes interpolated near the coalescence point of h(x, 0) (see the inset in Fig. 10). The grids are exponentially distributed with $\Delta x_{\min} = 0.01$ at $h_{\min}(t_0)$ and $\Delta x_{\max} = 0.1$ on the precursor film on both sides to capture large gradients near the coalescence point. Additionally, we set the spatial correlation length $L_c = 0.1 \ge \Delta x$ and use a constant time step $\Delta t = 10^{-3}$. The numerical process is stable with this time step for the configuration of coalescence, so the temporally correlated noise model is not activated here.

The time evolution of the the minimum bridge height, $h_{\min}(t)$, is shown in Fig. 11, where the MD coalescence time, t_0 is set as zero for the comparison. From a theoretical aspect, $h_{\min}(t_0)$ is expected to be zero. However, in MD, with finite-sized particles, the thickness of the initial "molecular bridge," $h_{\min}(t_0)$, is approximately equal to the molecular scale. In both symmetric and asymmetric cases, good agreement between SLE and MD predictions is found at all times for the mean values, but also, importantly, for the standard deviation. Notably, the deterministic model (LE) is not able to accurately capture the dynamics at these scales, highlighting the significant role that thermal fluctuations must play. Moreover, the stochastic $h_{\min}(t)$ always appears smaller than that predicted by the (deterministic) LE for the same time, demonstrating that noise decelerates the coalescence. This finding is contrary to previous results for other nanoscale interfacial flows, where typically thermal fluctuations accelerate processes; such as in jet instability [9], thread rupture [34], and droplet spreading [23]. Therefore, it is concluded that the thermal noise cannot always assumed to be a driving force in the interface dynamics at the nanoscale, and its role is determined by the particular fluid configuration. Hernández-Sánchez et al. proposed a power law from the LE to describe coalescence dynamics and demonstrated their model with experiments in [4]. However, this power law is not found in Fig. 11, even in the LE solutions (black dashed lines in Fig. 11). At present, the reason is unclear and should be the subject of future investigation.



FIG. 11. Time evolution of the bridge height during drop coalescence: comparison between MD and the numerical solutions for the LE and SLE, for symmetric-drop coalescence in (a) and asymmetric-drop coalescence in (b). The SLE results are an average from 50 realizations and the MD ones come from 20 realizations. The error bars and shadows in (a) and (b) represent the standard deviations of the MD and the SLE, respectively.

The ensemble-averaged profiles plotted in Fig. 12 show good overall agreement between the MD results (solid lines) and the SLE solutions (dashed lines). For the asymmetric case, the averaged bottom point (h_{min}) moves towards the smaller droplet with time, driven by the surface tension. As noted above, the deterministic predictions (dash-dotted lines) do not capture the details of the profiles of the MD results, while the SLE results show remarkably good agreement. Moreover, the SLE solution can reproduce the MD result at a fraction of the computational cost of MD. For the asymmetric-drop coalescence simulation in this section, one MD realization takes more than 200 core hours, while one SLE simulation takes less than 0.2 core hour; i.e., the speed-up is about 10³.

C. Thin-film rupture

The bounded film can become unstable (and rupture) due to the van der Waals forces, as found in experiments with polymeric liquids [42]. This phenomenon has been successfully described by



FIG. 12. Coalescence profile predicted by the SLE/LE and the MD at three time instants, t_1 (black lines), t_2 (blue lines), and t_3 (red lines). (a) Symmetric-drop coalescence: $t_1 = t_0 + 0.83$, $t_2 = t_0 + 12.52$, and $t_3 = t_0 + 22.15$. (b) Asymmetric-drop coalescence: $t_1 = t_0 + 0.83$, $t_2 = t_0 + 6.37$, and $t_3 = t_0 + 13.85$.



FIG. 13. Thin-film rupture profiles at three time instants. The dashed lines are the (deterministic) LE result with $t_1 = 1.0$ (black), $t_2 = 51.0$ (red), and $t_3 = 52.6$ (blue). The solid lines are from one realization for the SLE ($\varphi = 10^{-3}$) with $t_1 = 1.0$ (black), $t_2 = 13.0$ (red), and $t_3 = 14.0$ (blue). The inset shows the adaptive grids at the rupture point.

the LE [42] with a similarity solution, $h_{\min}(t) \sim (t_b - t)^{1/5}$ [43], where the van der Waals forces are modeled by the disjoining pressure term $(\partial \Pi / \partial x)$ in Eq. (1). As the scale at the final stage of the rupture reaches several nanometers, thermal fluctuations are expected to play a significant role in rupture with a potentially modified similarity solution due to the fluctuations, which is, remarkably, not included in previous studies [21,22,38,42]. Therefore, we use our SLE solver in this section to investigate the influence of thermal fluctuations on the rupture dynamics.

We set the correlated length $L_c = 0.15$ and correlated time scale $T_c = 10^{-5}$. The dimensionless Hamaker constant A = 0.2. As $\Pi \sim 1/h^3$, the disjoining pressure term increases rapidly at the final stage of the rupture, resulting in two challenges for capturing the dynamics numerically: (1) the spatial derivatives are very large at the rupture point (see the sharp "spikes" in Fig. 13) and (2) the breakup happens extremely fast at the final stage (the time for the final breakup, $t_3 - t_2$, is much smaller than the time for the early perturbation development, $t_2 - t_1$, in Fig. 13). To overcome these challenges, we employ both spatial and temporal refinement with the simple criteria $\Delta x \sim h(x, t)$ and $\Delta t \sim h_{\min}(t)$. Initially, $\Delta x = 0.15$ and $\Delta t = 10^{-5}$, and they are decreased automatically to 1.5×10^{-4} and 10^{-8} respectively, to capture the dynamics at the length scale of $10^{-2}h_0$ (see the inset in Fig. 14).

Figure 14 shows the time evolution of the minimum film height with different fluctuation intensities. Since we focus on the dynamics near rupture, h_{\min} is plotted against time to rupture, $t_r - t$, where t_r is the time of rupture. The error bars represent the standard deviation from 50 independent SLE realizations. It is not surprising to find stronger fluctuations (larger φ) lead to larger standard deviations, but, it transpires that, these do not affect the "dynamic path" significantly in this regime (see the mean values in Fig. 14). A further interesting finding is that all numerical predictions (with different values of φ) match the similarity solution proposed by Zhang and Lister [43] fairly well to the instant of rupture (see inset in Fig. 14), indicating that van der Waals forces, rather than thermal fluctuations, dominate the final stages of thin-film rupture at the nanoscale. This finding is perhaps not surprising given the singular nature of the disjoining pressure term. The conclusion is also supported by the profiles in Fig. 13, where the stochastic spike is very similar to the deterministic one, despite the obvious oscillations located on two sides of the film. Therefore, in this particular regime, thermal fluctuations can play a role in accelerating instability generation,



FIG. 14. The temporal evolution of the minimum film height for different values of φ . Here green lines represent the simulation result of LE. Black, red, and blue lines are the average of 50 SLE realizations, where the error bars are the standard deviation. Inset shows the comparison with the similarity solution [43].

as described in Refs. [17,20,22], but once disjoining pressure become significant, it overwhelms the influence of fluctuations and dominates the dynamics.

V. CONCLUSIONS AND FUTURE WORK

In this work, a simple yet effective numerical scheme for the SLE has been developed to predict the interface dynamics of different classes of nanoscale bounded thin-film flows. The Fornberg scheme and correlated-noise model is employed in the solver for the nonuniform adaptive grids, offering the capability of capturing local dynamics accurately and efficiently. Based on verification with theoretical models and comparisons to MD results, this solver is demonstrated to be a powerful tool for studying both linear and nonlinear thin-film flows.

Potential directions for future research are related to the physics predicted by the SLE in spreading, coalescence, and rupture. In this article, thermal fluctuations are found to (1) accelerate the droplet spreading, (2) surprisingly decelerate the bounded droplet coalescence, and (3) not affect the final stages of film rupture. In the future, it will be interesting to see whether these findings can be verified experimentally by using colloid-polymer mixture with ultralow surface tension, which has been applied to generate significant thermal fluctuations in interfacial flows at several micrometers [7,13,14,18]. Additionally, the coalescence dynamics has been shown to be described by the analytical (similarity) solution in the deterministic (LE) cases [4]. So a similar analytical solution is expected to predict the "fluctuation-dominated" coalescence, which would be worthy of further investigations.

Moreover, the results presented in this paper are obtained for two-dimensional flows. Interesting dynamics in three-dimensional thin-film flows, such as different film-rupture patterns [42] and fingering instability in wetting and dewetting [2,44], has been thoroughly studied by the three-dimensional LE. Therefore, it would be interesting to extend our numerical scheme to the three-dimensional SLE and explore the influence of thermal fluctuations on these three-dimensional fluctuating hydrodynamics.

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APPENDIX A: THE FORNBERG SCHEME

Here we present a quick derivation of the Fornberg scheme [31] to show that the errors in the derivative approximations can be well controlled. Suppose we are given the values of target function h(x) at $x_0 < x_1 < \cdots < x_n$ and we would like to approximate the *k*th derivative of h(x) at $x \in \Omega$ where $\Omega = [x_0, x_n]$. The Lagrange interpolation polynomial of h(x) based on $h_i = h(x_i)_{i=0}^n$, $i = 0, 1, \ldots, j$ is given by

$$p_n(x) = \sum_{i=0}^n \mathcal{L}_{i,n} h_i, \tag{A1}$$

where $\{\mathcal{L}_{i,n}\}_{i=1}^{n}$ are the Lagrange polynomials defined by

$$\mathcal{L}_{i,n}(x) = \prod_{j=0, \, j \neq i}^{n} \frac{x - x_j}{x_i - x_j}.$$
 (A2)

It is then immediately known that if h(x) is n + 1 times continuously differentiable on Ω , then for each $x \in \Omega$,

$$\left\|h^{(k)}(x) - p_n^{(k)}(x)\right\| \le \|\pi^{(k)}(x)\| \frac{\|h^{(n+1)}(x)\|}{k!(n+1-k)!},$$
 (A3)

where $k \leq n$, $h^{(k)}$ is the *k*th derivative of h(x), $\pi(x) = (x - x_0)(x - x_1) \cdots (x - x_n)$ and || || denotes the supreme norm on Ω [45]. Thus $h^{(k)}(x)$ can be well approximated by $p_n^{(k)}(x)$ for $k \leq n$ if $|x_n - x_0|$ is small,

$$h^{(k)}(x) \approx p_n^{(k)}(x) = \sum_{i=0}^n \frac{d^k \mathcal{L}_{i,n}(x)}{dx^k} h_i = \sum_{i=0}^n \mathcal{L}_{i,n}^k(x) h_i,$$
(A4)

where $\mathcal{L}_{i,n}^k(x)$ is the expression for the Fornberg coefficients and can be calculated recursively. We know

$$\mathcal{L}_{i,n}(x) = \frac{x - x_n}{x_i - x_n} \mathcal{L}_{i,n-1}(x), \quad \text{for} \quad i \neq n$$
(A5)

and

$$\mathcal{L}_{n,n}(x) = \frac{\prod_{j=0}^{n-2} (x_{n-1} - x_j)}{\prod_{j=0}^{n-1} (x_n - x_j)} (x - x_{n-1}) \mathcal{L}_{n-1,n-1}(x).$$
(A6)

Then for $i \neq n$

$$\mathcal{L}_{i,n}^{k}(x) = \frac{d^{k}}{dx^{k}} \left[\frac{x - x_{n}}{x_{i} - x_{n}} \mathcal{L}_{i,n-1}(x) \right]$$
(A7)

$$=\frac{x-x_n}{x_i-x_n}\mathcal{L}_{i,n-1}^k(x) + \frac{k}{x_i-x_n}\mathcal{L}_{i,n-1}^{k-1}(x)$$
(A8)

and

$$\mathcal{L}_{n,n}^{k}(x) = \frac{d^{k}}{dx^{k}} \left[\frac{\prod_{j=0}^{n-2} (x_{n-1} - x_{j})}{\prod_{j=0}^{n-1} (x_{n} - x_{j})} (x - x_{n-1}) \mathcal{L}_{n-1,n-1}(x) \right]$$
(A9)

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$$= \frac{\prod_{j=0}^{n-2} (x_{n-1} - x_j)}{\prod_{j=0}^{n-1} (x_n - x_j)} \Big[(x - x_{n-1}) \mathcal{L}_{n-1,n-1}^k(x) + k \mathcal{L}_{n-1,n-1}^{k-1}(x) \Big].$$
(A10)

Since $\mathcal{L}_{0,0}$ represents a single point, it is natural to set $\mathcal{L}_{0,0}^0 = 0$. Further more $\mathcal{L}_{j,m}^s = 0$ for s > m because the *s*th derivative of a *m*th-order polynomial is always zero. Without loss of generality we set x = 0 to get

$$\mathcal{L}_{i,n}^{k} = \frac{1}{x_n - x_i} \left(x_n \mathcal{L}_{i,n-1}^{k} - k \mathcal{L}_{i,n-1}^{k-1} \right), \tag{A11}$$

$$\mathcal{L}_{n,n}^{k} = \frac{\prod_{j=0}^{n-2} (x_j - x_{n-1})}{\prod_{i=0}^{n-1} (x_j - x_n)} \Big[x_{n-1} \mathcal{L}_{n-1,n-1}^{k}(x) - k \mathcal{L}_{n-1,n-1}^{k-1}(x) \Big],$$
(A12)

$$\|h^{(k)} - p_n^{(k)}\| \leqslant \|\pi^{(k)}\| \frac{\|h^{(n+1)}\|}{k!(n+1-k)!} \simeq O(\delta x^{n+1-k}),$$
(A13)

where $\delta x = \max\{|x_0|, |x_n|\}$. Generally speaking the Fornberg scheme has at least accuracy of order n + 1 - k.

APPENDIX B: CORRELATED NOISE MODEL

In this Appendix, we introduce the spatially correlated noise model, proposed by Grün in [15], where an exponential correlation function is employed:

$$F_{\rm cor}(x, L_{\rm c}) = \begin{cases} X^{-1} \exp\{-\frac{1}{2} \left[\frac{L}{L_{\rm c}} \sin(\pi x/L)\right]^2\}, & \text{for } L_{\rm c} > 0, \\ \delta(x), & \text{for } L_{\rm c} = 0. \end{cases}$$
(B1)

Here L_c is the spatial correlation length, L is the domain length, and X is such that $\int_0^L F_{cor}(x, L_c) dx = 1$.

Diez *et al.* [22] calculated the integral and found that χ_q could be expressed by the Bessel function,

$$\chi_q = I_k(\alpha) / I_0(\alpha), \tag{B2}$$

where

$$\alpha = \left(\frac{L}{2L_c}\right)^2$$
 and $k = 2\pi q/L$.

Figure 15 shows the eigenvalue spectrum for several values of L_c . Note that for $L_c \rightarrow 0$ (i.e., $\alpha \rightarrow \infty$), we have $\chi_q \rightarrow 1$ for all q, leading to the limiting case of the white (uncorrelated) noise.

The term g_q corresponds to the set of orthonormal eigenfunctions according to

$$g_q(x) = \begin{cases} \sqrt{\frac{2}{L}} \cos(\frac{2\pi qx}{L}), & \text{for } q > 0\\ \sqrt{\frac{1}{L}}, & \text{for } q = 0.\\ \sqrt{\frac{2}{L}} \sin(\frac{2\pi qx}{L}), & \text{for } q < 0 \end{cases}$$
(B3)

Therefore, the discretized expression of the noise term is

$$N_{i}^{t} = \frac{1}{\sqrt{\Delta t}} \sum_{q=-\frac{M+1}{2}}^{q=\frac{M+1}{2}} \chi_{q} N_{q}^{t} g_{q}(x),$$
(B4)

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FIG. 15. Linear spectrum of eigenvalues for several values of L_c from Eq. (B2). Here the wave number $k = 2\pi q/L$.

where *M* is the number of nodes. Samples of N_i^t are illustrated in Fig. 16 with different spatial correlation lengths. Note that a larger L_c leads to smooth large-wavelength and small-amplitude noise.

The temporally correlated noise model proposed by Zhao *et al.* [34] is employed in this work, shown in Fig. 17, where T_c is the correlation timescale. When the adaptive time steps are reduced to less than T_c to capture local dynamics (e.g., for the final stage of the film rupture), this temporally correlated model is activated with time step added using linear interpolation. The discretized expression of the noise term becomes

$$N_i^t = \frac{1}{\sqrt{T_c}} \sum_{q=-\frac{M+1}{2}}^{q=\frac{M+1}{2}} \chi_q N_q^t g_q(x).$$
(B5)



FIG. 16. Spatially correlated noise with different L_c .



FIG. 17. The temporally correlated stochastic term N^t using linear interpolation.

APPENDIX C: DERIVATION OF THEORY FOR THERMAL CAPILLARY WAVES

Without the disjoining pressure term, Eq. (1) becomes

$$\partial_t h = -\partial_x \left(h^3 \partial_x^3 h - \sqrt{2\varphi h^3} \mathcal{N} \right). \tag{C1}$$

For the linear instability, we set $h = 1 + \hat{h}$ with $\hat{h} \ll 1$ to linearize Eq. (C1):

$$\partial_t \hat{h} + \partial_x^4 \hat{h}^4 = \sqrt{2\varphi} \,\partial_x \mathcal{N}. \tag{C2}$$

Then a finite Fourier transform is applied to Eq. (C2) to get

$$\partial_t H + k^4 H = ik\sqrt{2\varphi}N,\tag{C3}$$

where the transformed variables are defined as follows:

$$H(k,t) = \int_0^L \hat{h}(x,t)e^{-ikx} dx$$
 and $N(k,t) = \int_0^L \mathcal{N}(x,t)e^{-ikx} dx.$

The solution of Eq. (C3) is linearly decomposed into two parts:

$$H = H_{\rm LE} + H_{\rm fluc}.\tag{C4}$$

The first part is the solution to the homogenous form of Eq. (C3) (with $\varphi = 0$) with some stationary initial disturbances ($H=H_i$ at t = 0). Since we start from a smooth initial surface, $H_{LE}(k, t) = 0$. The second component of the solution arises from solving the full form of Eq. (C4) without any initial disturbances; this part of the solution is solely due to fluctuations and is thus denoted H_{fluc} . This is obtained by determining the homogeneous equation's impulse response,

$$H_{\rm res}(k,t) = e^{-k^4 t},\tag{C5}$$

which due to the linear, time-invariant nature of the system, allows us to write

$$\overline{|H_{\rm fluc}|^2} = \left(ik\sqrt{2\varphi}\right)^2 \left|\int_0^t N(k,t-\tau)H_{\rm res}(k,\tau)d\tau\right|^2.$$
 (C6)

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H is both a random and complex variable with zero mean. So the root mean square of H is sought, which from Eq. (C4) is given by

$$|H|_{\rm rms} = \sqrt{|H_{\rm LE} + H_{\rm fluc}|^2} = \sqrt{|H_{\rm fluc}|^2}.$$
 (C7)

Because N is uncorrelated Gaussian white noise, and the variance of the norm of the white noise $\overline{|N|^2} = L$, Eqs. (C5) and (C6) combine to give

$$\overline{|H_{\text{fluc}}|^2} = 2\varphi k^2 \int_0^t \overline{|N(k, t - \tau)|^2} H(k, \tau)^2 d\tau,$$

= $2\varphi k^2 L \int_0^t H^2 d\tau,$
= $-\frac{\varphi L}{k^2} (e^{-2k^4 t} - 1).$ (C8)

Equations (C7) and (C8) constitute the theory for thermal capillary waves used in Sec. III.

APPENDIX D: DERIVATION FOR THE SPREADING POWER LAWS

In this Appendix, we present the derivations for both no-slip and slip theories, i.e., $\ell \sim t^n$. The average second moment of *h* is applied to estimate the drop's width ℓ [23] whose explicit expression is

$$\ell(t) = \left\langle \left[\frac{1}{V} \int (x - X)^2 h(x, t) \, dx \right] \right\rangle,\tag{D1}$$

where $V = \int h dx$ is the constant volume of the droplet, $X = (\int xh dx)/V$ is the instantaneous position of the droplet center, and $\langle \cdots \rangle$ represents the ensemble average of all the realizations.

In order to decide the power law (n), a similarity transform is made with the change of variables:

$$x = b\breve{x}, \qquad h = b^{lpha}\breve{h}, \qquad t = b^{\eta}\breve{t},$$
 (D2)

where *b* is an arbitrary factor, and α and η are constants that remain to be fixed. The symbol "^{sym} means 'transformed' variables. According to the scaling relation above $[\breve{x} \sim \breve{h} \sim \breve{t} \sim O(1)]$, we can easily obtain $\ell \sim x \sim t^{1/\eta}$, namely, the power law is equal to $1/\eta$. For the value of η , we substitute the transform relations above into the SLE [Eq. (1)] and obtain

$$\frac{\partial \check{h}}{\partial \check{t}} = -(b^{3\alpha+\eta-4})\partial_{\check{x}}(\check{h}^{3}\partial_{\check{x}}^{3}\check{h}) + [b^{(\alpha+\eta-3)/2}]\sqrt{2\varphi}\partial_{\check{x}}[\check{h}^{3/2}\check{\mathcal{N}}(\check{x},\check{t})].$$
(D3)

Here we have two independent force terms on the right-hand side: (1) the deterministic term due to the surface tension and (2) the stochastic term due to the thermal fluctuations. To hold the "similarity" of the transform, the scaling powers of the arbitrary scaling factor b should always be zero, namely,

$$\begin{cases} 3\alpha + \eta - 4 = 0, & \text{for the deterministic term,} \\ \alpha + \eta - 3 = 0, & \text{for the stochastic term.} \end{cases}$$
(D4)

In addition, no matter which force drives the spreading, the droplet volume,

$$V = \int h \, dx = b^{\alpha+1} \int \check{h} \, d\check{x},$$

should always be conserved, requiring $\alpha = -1$. So, we can obtain the value of the left coefficient η from Eq. (D4), i.e., $\eta = 7$ in the surface tension term; and $\eta = 4$ in the stochastic term, implying

$\epsilon (\text{kJ mol}^{-1})$	σ (nm)	Α	В	р	q	χ	к	а	θ_0 (degree)
25.87	0.2390	7.050	0.6022	4	0	1.2	23.15	1.8	109.47

TABLE I. Parameters of the mW model.

two power-law spreading regimes:

$$\begin{cases} \ell \sim t^{1/7}, & \text{Tanner's law,} \\ \ell \sim t^{1/4}, & \text{fluctuation enhanced Tanner's law,} \end{cases}$$
(D5)

which have been proposed by Tanner [3] and Davidovitch et al. [23], respectively.

To take the slip effect into account, Eq. (D4) is modified:

$$\frac{\partial \check{h}}{\partial \check{t}} = -\left(b^{2\alpha+\eta-4}\right)\partial_{\check{x}}\left(3\tilde{\ell}_{\check{s}}\check{h}^{2}\partial_{\check{x}}^{3}\check{h}\right) + b^{(\eta-3)/2}\sqrt{2\varphi}\partial_{\check{x}}\left[\sqrt{3\tilde{\ell}_{\check{s}}\check{h}^{2}}\check{\mathcal{N}}(\check{x},\check{t})\right].$$
 (D6)

By the same approach, we get

$$\begin{aligned}
2\alpha + \eta - 4 &= 0, & \text{for the deterministic term,} \\
\eta - 3 &= 0, & \text{for the stochastic term,} \end{aligned}$$
(D7)

where α is still equal to -1. Therefore, we can obtain a "slip-modified" power law for the spreading:

$$\begin{cases} \ell \sim t^{1/6}, & \text{Slip-modified Tanner's law,} \\ \ell \sim t^{1/3}, & \text{Slip-modified fluctuation enhanced Tanner's law.} \end{cases}$$
(D8)

APPENDIX E: MD SETTINGS FOR THE DROPLET COALESCENCE

In this work, we choose the mW model [46] to simulate liquid water. The model mimics the hydrogen-bonded structure of water through the introduction of a non-bond-angular-dependent term that encourages tetrahedral configurations. The model contains two terms: (1) ϕ_{ij} depending on the distances between pairs of atoms (represented by r_{ij} and s_{ik}) and (2) ϕ_{ijk} depending on the angles formed by triplets of atoms (represented by θ_{ijk}). The full expression is given by

$$\mathcal{U} = \sum_{i} \sum_{j>i} \phi_{ij}(r_{ij}) + \sum_{i} \sum_{j\neq i} \sum_{k>j} \phi_{ijk}(r_{ij}, s_{ik}, \theta_{ijk}),$$

$$\phi_{ij}(r_{ij}) = A\epsilon \left[B\left(\frac{\sigma}{r_{ij}}\right)^{p} - \left(\frac{\sigma}{r_{ij}}\right)^{q} \right] \exp\left(\frac{\sigma}{r_{ij} - a\sigma}\right),$$

$$\phi_{ijk}(r_{ij}, s_{ik}, \theta_{ijk}) = \kappa \epsilon (\cos \theta_{ijk} - \cos \theta_{0})^{2} \exp\left(\frac{\chi \sigma}{r_{ij} - a\sigma}\right) \exp\left(\frac{\chi \sigma}{s_{ik} - a\sigma}\right), \quad (E1)$$

where A, B, p, q, χ , and κ , respectively, give the form and scale to the potential, and θ_0 represents the tetrahedral angles. All the parameters are presented in Table I.

The platinum substrate is assumed to be rigid with an atomic mass of 3.24×10^{-25} kg [47]. The liquid-solid interaction is modeled by the 12-6 LJ potential with $\epsilon_{ls}/k_B = 444$ K and $\sigma_{ls} = 0.28$ nm to create a fully wettable substrate (zero contact angle). The initial configurations of droplets are cut from a liquid bulk, created from equilibrium NVT simulations with a Nosé-Hoover thermostat at T = 400 K. The same ensemble and thermostat is used for the main simulations with the time step, 2.5 femtoseconds, and the entire domain width along the z axis, W = 2 nm and the length scale for nondimensionalization, $h_0 = 10$ nm.

To compare MD results with the predictions of the SLE, the liquid transport properties are calculated are required. Here dynamic viscosity is found to be $\mu = 1.64 \times 10^{-4} \text{ kg m}^{-1} \text{ s}^{-1}$ by the Green-Kubo method [48,49], which integrating the time-autocorrelation function of the off-diagonal

elements of the pressure tensor P_{ij} so that

$$\mu = \frac{V_{\text{bulk}}}{k_{\text{B}}T} \int_0^\infty \langle P_{ij}(t) P_{ij}(0) \rangle dt \quad (i \neq j),$$
(E2)

where V_{bulk} is the volume of the bulk fluid, k_{B} is the Boltzmann constant, and *T* is temperature. The pressure tensor components are obtained using the definition of [50] and the angular brackets indicate the expectation. The surface tension is calculated from the profiles of the components of the pressure tensor in a simple liquid-vapor system, using the mechanical definition [51]:

$$\gamma = \frac{1}{2} \int_0^{L_z} [P_{\rm n}(z) - P_{\rm t}(z)] dz, \tag{E3}$$

where L_z is the length of the MD domain, and subscripts 'n' and 't' denote normal and tangential components, respectively. Finally, we have $\gamma = 5.45 \times 10^{-2} \text{ N m}^{-1}$.

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