

Polymer translocation through a nanopore assisted by an environment of active rods

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We use a combination of computer simulations and isoflux tension propagation (IFTP) theory to investigate the translocation dynamics of a flexible linear polymer through a nanopore into an environment composed of repulsive active rods in two dimensions. We demonstrate that the rod activity induces a crowding effect on the polymer, leading to a time-dependent effective net force that facilitates translocation into the active environment. Incorporating this force into the IFTP theory for pore-driven translocation allows us to characterize translocation dynamics in detail and derive a scaling form for the average translocation time as $\bar{\tau} \sim N_{01}^{1+\nu} \bar{L}_r^\nu / \bar{F}_{SP}$, where N_{01} , \bar{L}_r , and \bar{F}_{SP} are the initial contour length of the *cis*-side subchain, rod length, and self-propelling force acting on the rods, respectively, and ν is the equilibrium Flory scaling exponent.

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I. INTRODUCTION

Translocation dynamics of biopolymers through nanopores has been one of the most active research areas in soft matter during the past few decades (see, e.g., Refs. [1–4] and references therein). The most relevant examples include DNA and mRNA translocation through nuclear pores, protein transportation across a membrane, and DNA injection by a virus. There are many applications from DNA sequencing to gene therapy and controlled drug delivery [5], and forced translocation was originally suggested as an inexpensive and fast method for DNA sequencing. Motivated by these applications, many experimental as well as theoretical works [6–41] have been performed since the seminal works by Bezrukov *et al.* [42] and by Kasianowicz *et al.* [43]. To date, most studies have focused on the dynamics of polymer translocation facilitated by external driving in the pore or by pulling the polymer from the head bead by optical tweezers, both of which are experimentally feasible [20–30].

In biological systems, however, polymer translocation processes often occur in crowded environments [5]. Such environments may be composed of diffusive and randomly distributed spherical static obstacles [44–47] or chaperones that assist transport across membranes [48–50]. Crowded environments consisting of active particles (APs) have introduced a new out-of-equilibrium-dynamics field of research with rich physics [51,52]. Examples include synthetic motile objects from molecular scale to microns [53,54], micro-

scopic living organisms [55,56], and artificial swimmers from nanometer to millimeter scales [57–69]. The presence of APs has a strong influence on polymer chains in equilibrium and can lead to significant conformational and dynamical changes (collapse or swelling) depending on the system parameters [70–76].

An interesting open question pertains to the influence of APs on polymer translocation dynamics. Pore-driven polymer translocation in the presence of spherical APs has been considered using computer simulation methods [77] and it was found that with high activity, there is a crowding effect in two dimensions (2D) that leads to a speed-up of translocation. An interesting and unanswered question remains concerning the effect of the APs on the dynamics of unforced or nondriven translocation. In many cases active objects such as bacteria are not spherical, but assume rodlike shapes. The combination of anisotropy in the shape of the APs and the presence of a self-propelling (SP) force that makes the objects active leads to interesting collective dynamics. In the case of rodlike APs, there is orientational alignment of the active rods (ARs) along the walls in a two-dimensional confining channel [78] and also in their collective motion [79]. The presence of a translocating polymer in such an environment thus warrants closer examination.

To this end, we perform here extensive computer simulations of unforced polymer translocation dynamics in the presence of ARs on the *trans* side of the pore. We demonstrate that when the chain is initially placed in such a way that a part of the chain is in the *trans* compartment, the presence of ARs induces a net effective force from the *cis* to the *trans* side that overcomes entropic forces and facilitates translocation. The presence of a time-dependent driving force allows us to use the isoflux tension propagation (IFTP) theory, which is benchmarked against the simulation data. As our main theoretical result, we find that the mean translocation time $\bar{\tau}$ scales with the initial contour length of the *cis*-side subchain N_{01} , rod length \bar{L}_r , and SP force \bar{F}_{SP} as $\bar{\tau} \sim N_{01}^{1+\nu} \bar{L}_r^\nu / \bar{F}_{SP}$, where ν is the

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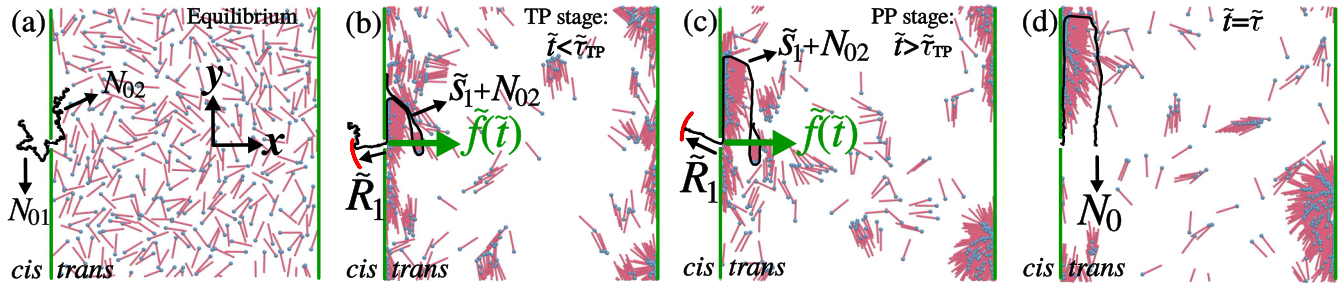


FIG. 1. (a) Configuration of the system after equilibration with passive rods with the chain fixed inside the pore. The compartment dimensions are $L_x = 2L_y = 400$ (equally partitioned by a membrane in the y direction), $L_r = 16$ (16 beads), and the number of rods $N_r = 320$, which gives a number density of 0.128. Translocation is initiated from this state at $\tilde{t} = 0$ by making the rods active with $F_{SP} = 32$ and releasing the chain. Here N_{01} and N_{02} are the initial contour lengths of the *cis*- and *trans*-side subchains, respectively. (b) Snapshot of the system during the tension propagation (TP) stage, i.e., $\tilde{t} < \tilde{\tau}_{TP}$. The location of the tension front is denoted by \tilde{R}_1 , and $\tilde{s}_1 + N_{02}$ is the translocation coordinate (the number of monomers on the *trans* side). The SP force F_{SP} acts on the blue head monomer of each rod and is directed parallel to its axis from tail to head. The effective force imposed by the rods on the chain $\tilde{f}(\tilde{t})$ originates from the interaction between the active rods and the *trans*-side subchain. (c) Same as in (b) but for the postpropagation stage, i.e., $\tilde{t} > \tilde{\tau}_{TP}$, where the tension has already reached the *cis*-side subchain end. (d) Final configuration of the system at the end of the translocation process.

equilibrium Flory exponent. This scaling form for the translocation time is valid in the limit of long chains ($N_{01} \gg 1$) and its dependence on \tilde{L}_r and \tilde{F}_{SP} comes from the effective net force acting on the monomer(s) at the pore induced by the APs with the *trans*-side subchain. This leads to scaling of $\tilde{\tau}$ with N_{01} identical to that of a pore-driven chain without APs.

The structure of the paper is as follows. In Sec. II we present details of the Langevin dynamics (LD) computer simulations for a coarse-grained model of active rods and a translocating polymer chain. The IFTP theory is introduced in Sec. III. Section IV is devoted to presentation and discussion of our main results. A summary and conclusions are in Sec. V.

II. LANGEVIN DYNAMICS SIMULATIONS

Our system comprises a flexible, self-avoiding polymer chain of length N_0 modeled by the bead-spring model [80] with beads having a pairwise shifted repulsive Lennard-Jones (SRLJ) interaction $U_{LJ}(r) = 4\epsilon[(\frac{\sigma}{r})^{12} - (\frac{\sigma}{r})^6] + \epsilon$ if $r \leq 2^{1/6}\sigma$ and zero otherwise. Here σ is the LJ radius, ϵ is the potential well depth, and r is the distance between two monomers. In addition, the consecutive monomers are connected by the finitely extensible nonlinear elastic interaction $U_{FENE}(r) = -\frac{1}{2}kR_0^2 \ln[1 - r^2/R_0^2]$, where k and R_0 are the string constant and the maximum allowed distance between the consecutive monomers, respectively. The polymer is put into a container of size $L_x = 2L_y = 400$ in units of σ and there is a membrane in the middle (see Fig. 1) with a nanopore of radius 1.5σ allowing only one bead in the pore at a time. The container has walls in the x direction and periodic boundary conditions in the y direction, and its walls and the membrane interact with the chain with the same SRLJ potential. In the *trans* side there are N_r rigid rods comprising SRLJ beads of radius σ whose length is $L_r\sigma$. To model self-propulsion, a SP force with magnitude of F_{SP} is added to the head bead of each rod along its main axis and from its tail to its head.

For the simulations we employ LD, where for the position of the i th monomer of the polymer $M\dot{\tilde{r}}_i = -\eta\dot{\tilde{r}}_i - \tilde{\nabla}U_{mi} + \tilde{\xi}_i(t)$. Here η is the friction coefficient, U_{mi} is the sum of all interactions, and $\tilde{\xi}_i(t)$ is white noise with $\langle \tilde{\xi}_i(t) \rangle = 0$ and

$\langle \tilde{\xi}_i(t)\tilde{\xi}_j(t') \rangle = 2\eta k_B T \delta_{ij} \delta(t - t')$, where k_B is the Boltzmann constant, T is the temperature, and δ_{ij} and $\delta(t - t')$ are the Kronecker and Dirac delta functions, respectively. For the i th bead of each rod we add the SP force as $M\dot{\tilde{r}}_i = -\eta\dot{\tilde{r}}_i + F_{SP}\delta_{ih}\hat{e} - \tilde{\nabla}U_{ri} + \tilde{\xi}_i(t)$, where h picks the head bead, \hat{e} is the unit vector parallel to the vector connecting the tail to the head, and U_{ri} is the sum of all interactions on the i th bead. We use M , σ , and ϵ as the units for mass, length, and energy, respectively, where $M = 1$ is the mass of each monomer in the polymer and the rods and $\epsilon = 1$. The temperature is kept at $k_B T = 1.2$, the solvent friction coefficient is $\eta = 0.7$, and $\tau_0 = \sqrt{M\sigma^2/\epsilon}$ is the simulation time unit. In our simulations, the integration time step is $dt = 0.001\tau_0$. Finally, the spring constant is set to $k = 30$ and $R_0 = 1.5$. The simulations were performed using the LAMMPS [81] package.

Before the translocation process, the polymer is fixed in the pore such that there are N_{01} and N_{02} beads in the *cis* and *trans* compartments, respectively, where $N_0 = 1 + N_{01} + N_{02}$. The polymer-rod system is equilibrated for $t_{eq} = 5 \times 10^4 \tau_0$ without the SP force, and at the beginning of translocation the polymer is released and F_{SP} is turned on for all rods simultaneously. The rod lengths used in the LD simulations are $L_r = 8, 12, 16$, and 20 , which correspond to the number of rods in the *trans* domain $N_r = 640, 426, 320$, and 256 , respectively. For the SP force we have $F_{SP} = 16, 24$, and 32 , the initial *cis*-side contour lengths are $N_{01} = 50, 100$, and 150 , and finally the initial *trans*-side contour length is $N_{02} = 100$. For all sets of parameters the value of the rods' volume fraction is fixed at about 0.1 in 2D. The density of the ARs here are chosen low enough such that the equilibrated system has a uniformly random orientational distribution. For the particular system with $N_{01} = N_{02} = 100$, $\tilde{L}_r = 16$, and $\tilde{F}_{SP} = 32$ the results are averaged over 3000 uncorrelated trajectories, while for the other cases we use at least 1000 trajectories.

We use dimensionless quantities throughout and a tilde denotes units within the IFTP theory. They are defined as $\tilde{Q} \equiv Q/Q_u$, where the denominator denotes the units of length, time, velocity, monomer flux, friction, and force as $s_u \equiv \sigma$, $t_u \equiv \eta\sigma^2/(k_B T)$, $v_u \equiv \sigma/t_u = k_B T/(\eta\sigma)$, $\phi_u \equiv k_B T/(\eta\sigma^2)$, $\Gamma_u \equiv \eta$, and $f_u \equiv k_B T/\sigma$, respectively.

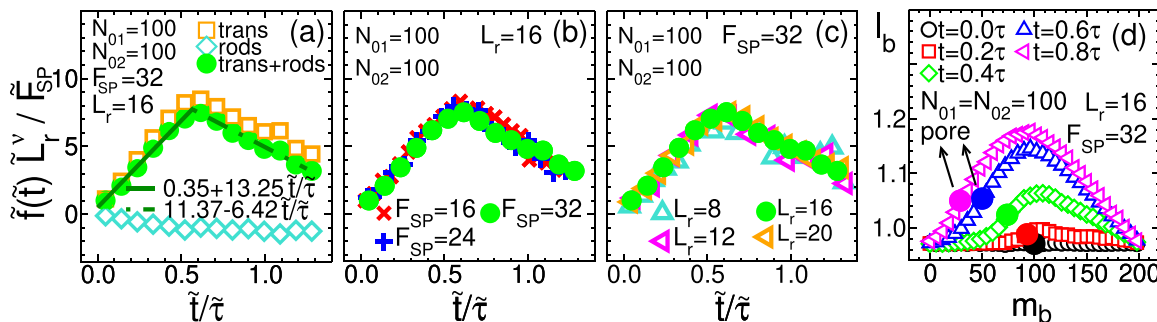


FIG. 2. (a) Plot of $\tilde{f}(\tilde{t})\tilde{L}_r^\nu/\tilde{F}_{SP}$ as a function of the normalized time $\tilde{t}/\tilde{\tau}$, where $\tilde{f}(\tilde{t})$ is the effective force experienced by the monomer inside the pore in the x direction from the LD simulations, ν is the Flory exponent, and $\tilde{\tau}$ is the translocation time (as obtained from LD) for $L_r = 16$, $N_r = 320$, and $F_{SP} = 32$. Open orange squares and open turquoise diamonds are data for the contributions of the tension due to the *trans*-side subchain and the interactions of ARs with the monomer inside the pore, respectively. The effective force which is the sum of the tension due to the *trans*-side subchain and the AR interactions with the monomer inside the pore is given by green circles. The solid and the dashed green lines are the fitting curves for the effective force in the TP and PP stages, respectively. Here $N_{01} = 100$ and $N_{02} = 100$ are the initial contour lengths of the *cis*- and *trans*-side subchains, respectively. (b) Same as in (a) but for fixed $L_r = 16$ and for different values of $F_{SP} = 16, 24$, and 32 . (c) Same as in (b) but for fixed $F_{SP} = 32$ and different values of $L_r = 8, 12, 16$, and 20 corresponding to the number of rods $N_r = 640, 426, 320$, and 256 , respectively. (d) Bond length l_b as a function of the bond index m_b with the same system parameters as in (a) for different time instants during the translocation process $t/\tau = 0-0.8$. The bond indices $m_b = 1$ and 200 identify the tail and head bonds in the *cis* and *trans* sides, respectively.

Figure 1(a) presents a typical snapshot of the system after equilibration at $\tilde{t} = 0$. We find that the activity of the rods induces an effective force $\tilde{f}(\tilde{t})$ on the monomer in the pore, directed from *cis* to *trans* such that it facilitates translocation as depicted in Fig. 1(b). This causes tension propagation along the backbone of the *cis*-side subchain. The distance between the tension front on the *cis* side from the pore is denoted by \tilde{R}_1 . This stage is called the tension propagation (TP) stage ($\tilde{t} < \tilde{t}_{TP}$). The number of the monomers on the *trans* side $\tilde{s}_1 + N_{02}$ defines a translocation coordinate and is equal to N_{02} at time zero. Eventually the tension reaches the end of the *cis*-side subchain and the postpropagation (PP) stage starts ($\tilde{t} > \tilde{t}_{TP}$), which is presented in Fig. 1(c). Finally, Fig. 1(d) shows the last snapshot of the system at the end of the translocation process which defines the translocation time $\tilde{\tau}$.

III. ISOFUX TENSION PROPAGATION THEORY

Over the past few years a consistent and quantitatively accurate theory of driven polymer translocation has been developed based on isoflux tension propagation. Due to the effective force $\tilde{f}(\tilde{t})$ induced by the SP forces of the rods, we can generalize the IFTP theory to the present case too. To obtain the time evolution of the translocation coordinate \tilde{s}_1 , which is the number of monomers that have passed from the *cis* to the *trans* side, the isoflux approximation for the monomer flux $\tilde{\phi}_1(\tilde{t}) = d\tilde{s}_1/d\tilde{t}$ means that it is constant in space but evolves in time within the mobile subchain on the *cis* side. The tension force on the backbone of the chain at distance \tilde{x} from the pore on the *cis* side $\tilde{F}(\tilde{x}, \tilde{t})$ is obtained by integration of the local tension force balance relation $d\tilde{F}(\tilde{x}', \tilde{t}) = -\tilde{\phi}_1(\tilde{t})d\tilde{x}'$ from the pore entrance at $\tilde{x}' = 0$ to the distance \tilde{x} as $\tilde{F}(\tilde{x}, \tilde{t}) = \tilde{F}_0 - \tilde{x}\tilde{\phi}_1(\tilde{t})$ [here the tension force at the entrance of the pore on the *cis* side is $\tilde{F}_0 = \tilde{f}(\tilde{t}) - \tilde{\eta}_p\tilde{\phi}_1(\tilde{t})$]. Then, as the tension force vanishes at \tilde{R}_1 , i.e., $\tilde{F}(\tilde{R}_1, \tilde{t}) = 0$, one can write $\tilde{F}_0 = \tilde{R}_1\tilde{\phi}_1(\tilde{t})$. Finally, using the above definitions of the monomer flux and \tilde{F}_0 , the equation of motion for the translocation coordinates is

cast in the form [26,27]

$$\tilde{\Gamma}_1(\tilde{t})\frac{d\tilde{s}_1}{d\tilde{t}} = \tilde{f}(\tilde{t}), \quad (1)$$

where $\tilde{\Gamma}_1(\tilde{t}) = \tilde{R}_1(\tilde{t}) + \tilde{\eta}_p$, with $\tilde{\eta}_p$ and $\tilde{R}_1(\tilde{t})$ the pore friction and the tension front distance from the nanopore, respectively.

In Fig. 2(a) we plot $\tilde{f}(\tilde{t})\tilde{L}_r^\nu/\tilde{F}_{SP}$, where $\tilde{f}(\tilde{t})$ is the effective force (closed green circles) (is the sum of the tension due to the *trans*-side subchain and the AR interactions with the monomer inside the pore) in the horizontal direction from *cis* to *trans* as a function of the normalized time $\tilde{t}/\tilde{\tau}$ for $N_{01} = N_{02} = 100$, $F_{SP} = 32$, and $L_r = 16$. It is the sum of the tension force due to the *trans*-side subchain (open orange squares) and the force due to the interactions of the ARs with the monomer inside the pore (open turquoise diamonds). The effective force first grows almost linearly and then decreases. Its largest magnitude in LJ units is of the same order as that of F_{SP} . In Figs. 2(b) and 2(c) we show the corresponding data for varying either F_{SP} or L_r . The remarkable finding here is that all the data collapse onto two master curves, namely, $\tilde{f}_{TP}(\tilde{t})\tilde{L}_r^\nu/\tilde{F}_{SP} = 0.35 + 13.25\tilde{t}/\tilde{\tau}$ [solid green line in Fig. 2(a)] and $\tilde{f}_{PP}(\tilde{t})\tilde{L}_r^\nu/\tilde{F}_{SP} = 11.37 - 6.42\tilde{t}/\tilde{\tau}$ [dash-dotted green line in Fig. 2(a)] in the TP and PP stages, respectively, and they intersect at $\tilde{t}/\tilde{\tau} = 0.56$. We have independently verified from the bond lengths that the maximum of the effective force curve exactly corresponds to the TP time where the tension front reaches the end of the *cis*-side subchain. To this end, in Fig. 2(d) we plot the bond length l_b as a function of the bond index m_b . The bond indices $m_b = 1$ and 200 identify the tail and head bonds on the *cis* and *trans* sides, respectively. It can be seen from the figure that the tension front reaches the tail bond ($m_b = 1$) at about $\tilde{t}/\tilde{\tau} = 0.56 \approx 0.6$ (open blue triangles), which defines the TP time. We have checked this for all the sets of parameters here.

Solving Eq. (1) gives the translocation coordinate \tilde{s}_1 provided that the time evolution of the location of the tension front \tilde{R}_1 is known. Using the end-to-end distance \tilde{R}_{1e}

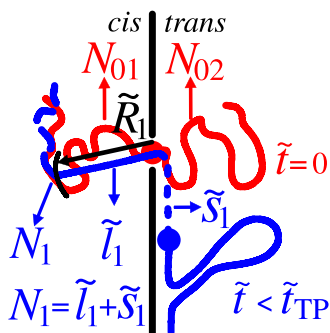


FIG. 3. Schematic of polymer configurations at time zero (in red) and at time $\tilde{t} < \tilde{t}_{TP}$ (in blue), where \tilde{t}_{TP} denotes the tension propagation time. For the sake of clarity, the active rods in the *trans* side have not been depicted. The initial contour lengths of the *cis*- and *trans*-side subchains at time zero are N_{01} and N_{02} , respectively, and the polymer is in its equilibrium state while the monomer (closed red circle) that identifies the border between the initial *cis*- and *trans*-side subchains is fixed at the pore. At time \tilde{t} , \tilde{s}_1 is the number of monomers that was initially in the *cis* side and has traversed the pore (dotted blue line), \tilde{l}_1 is the number of mobile monomers in the *cis* side (solid blue line in the *cis* side), and the equilibrium part of the subchain in the *cis* side is the dashed blue line. Here N_1 is the number of all monomers that have experienced the tension force by time \tilde{t} and thus $N_1 = \tilde{l}_1 + \tilde{s}_1$. The closed blue circle separates the initial *cis*-side subchain from the *trans*-side side subchain. The location of the tension front is shown by \tilde{R}_1 .

corresponding to the extent of the mobile part of the *cis*-side subchain at time zero just before the translocation process, wherein the chain is in its equilibrium state, the location of the tension front \tilde{R}_1 and its equation of motion can be obtained. To understand why \tilde{R}_1 is equal to \tilde{R}_{1e} we just need to compare the *cis*-side subchain configurations at time zero with the ones at time \tilde{t} as depicted in Fig. 3. For visualization purposes, in Fig. 3 the polymer configurations at time zero (in red) and at time $\tilde{t} < \tilde{t}_{TP}$ (in blue) are depicted, where \tilde{t}_{TP} denotes the tension propagation time. For the sake of clarity, the active rods on the *trans* side are not depicted. The initial contour lengths of the *cis*- and *trans*-side subchains at time zero are N_{01} and N_{02} , respectively, and the polymer is in its equilibrium state while the monomer (closed red circle) that identifies the border between the initial *cis*- and *trans*-side subchains is fixed at the pore. As time passes, at time \tilde{t} a part of the subchain that was initially in the *cis* side has traversed the pore (dotted blue line) and \tilde{s}_1 monomers have gone through. At time \tilde{t} , \tilde{l}_1 is the number of mobile monomers on the *cis* side (solid blue line in the *cis* side) and the equilibrium part of the subchain in the *cis* side is the dashed blue line. In addition, N_1 is the number of all monomers that have experienced the tension force by time \tilde{t} and thus $N_1 = \tilde{l}_1 + \tilde{s}_1$. The closed blue circle separates the initial *cis*-side subchain from the *trans*-side subchain. The location of the tension front is shown by \tilde{R}_1 . As mentioned above, the number of monomers affected by the tension front on the *cis* side at time \tilde{t} is N_1 . On the other hand, at time zero these N_1 monomers are accommodated in the space between the nanopore and the current location of the tension front at time \tilde{t} . The linear size of this accommodating space, on the one hand, at time zero is given by the end-to-end distance of

the N_1 monomers as $\tilde{R}_{1e} = A_\nu N_1^\nu$ and, on the other hand, at time \tilde{t} it is identified as the distance between the tension front and the nanopore \tilde{R}_1 . Therefore, $\tilde{R}_1 = \tilde{R}_{1e} = A_\nu N_1^\nu$. Moreover, as $N_1 = \tilde{l}_1 + \tilde{s}_1$, where \tilde{l}_1 is the number of monomers in the mobile domain (affected by the tension front) on the *cis* side and \tilde{s}_1 is the translocation coordinate as defined above, we can simply write $\tilde{R}_1 = A_\nu (\tilde{l}_1 + \tilde{s}_1)^\nu$. Here $A_\nu = 1.1$ for the present LD model and $\nu = 3/4$ is the equilibrium Flory scaling exponent in 2D. Assuming that the mobile part of the *cis*-side subchain is fully straightened corresponding to the strong stretching (SS) regime of polymer translocation dynamics, we can write $\tilde{l}_1 = \tilde{R}_1$ [19,24]. Together with the definition of the monomer flux $\dot{\tilde{\phi}}_1 = d\tilde{s}_1/d\tilde{t}$ and differentiating both sides of $\tilde{R}_1 = A_\nu (\tilde{R}_1 + \tilde{s}_1)^\nu$ in time, the equation of motion for \tilde{R}_1 in the TP stage is

$$\dot{\tilde{R}}_1(\tilde{t}) = \frac{\nu A_\nu^{1/\nu} \tilde{R}_1(\tilde{t})^{(\nu-1)/\nu} \dot{\tilde{\phi}}_1(\tilde{t})}{1 - \nu A_\nu^{1/\nu} \tilde{R}_1(\tilde{t})^{(\nu-1)/\nu}}. \quad (2)$$

In the PP stage the tension has already reached the *cis*-side subchain. Differentiating the closure $N_1 = \tilde{l}_1 + \tilde{s}_1 = N_{01}$ gives the time evolution of \tilde{R}_1 as

$$\dot{\tilde{R}}_1(\tilde{t}) = -\dot{\tilde{\phi}}_1. \quad (3)$$

To have the full solution of the IFTP theory in the TP stage both Eqs. (1) and (2) must be self-consistently solved, while in the PP stage one has to solve Eqs. (1) and (3).

IV. RESULTS

A. Waiting time distribution

To validate the IFTP theory it is useful to investigate the waiting time (WT) distribution w , which is the time that each bead spends in the pore during the translocation process. In the IFTP theory, to obtain the WT we need to calculate the inverse of $\tilde{s}(t)$, i.e., $t(\tilde{s})$. Then the WT is obtained as $w(\tilde{s}) = t(\tilde{s} + 0.5) - t(\tilde{s} - 0.5)$. On the other hand, in the LD simulations the WT can be obtained directly by recording the time that each bead spends in the pore during the translocation process. In Fig. 4(a) we plot $w(\tilde{s})$ as a function of the total translocation coordinate $\tilde{s} = \tilde{s}_1 + \tilde{s}_2$ (\tilde{s}_1 and \tilde{s}_2 correspond to the *cis*- and *trans*-side subchains, respectively) for $N_{02} = 100$, $F_{SP} = 32$, $L_r = 16$, the pore friction coefficient in the IFTP theory $\tilde{\eta}_p = 8$ (which can be obtained by comparing the WT from IFTP with LD simulations and once it has been obtained it is fixed), and for different values of the initial *cis*-side contour lengths $N_{01} = 50$ (open turquoise squares), $N_{01} = 100$ (open green circles) and $N_{01} = 150$ (open orange diamonds). The solid blue, dashed green, and dash-dotted red lines present the IFTP results for $N_{01} = 50, 100$, and 150 , respectively. Regions with $0 < \tilde{s} \leq N_{02}$ and $N_{02} < \tilde{s} \leq N_0$ identify the monomers initially in the *trans*- and the *cis*-side subchains, respectively. Here $N_{02} = 100$ has been fixed in order to have the same initial configuration for the *trans*-side subsystem. This allows us to investigate only the effect of the initial contour length of the *cis*-side subchain on the translocation process. We find good agreement between the LD simulation results and the IFTP theory. The simulation data show that the *trans*-side subchain ($0 < \tilde{s} \leq N_{02}$) contributes to the WT (see Fig. 4) due to the small magnitude of $\tilde{f}(\tilde{t})$ at the beginning of translocation

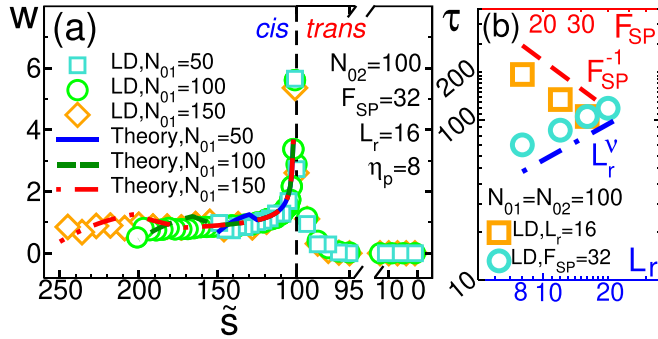


FIG. 4. (a) Waiting time w as a function of the total translocation coordinate \tilde{s} for fixed values of the initial *trans*-side contour length $N_{02} = 100$, SP force $F_{SP} = 32$, rod length $L_r = 16$, and pore friction in the IFTP theory $\eta_p = 8$ and for different values of the initial *cis*-side contour lengths $N_{01} = 50$ (open turquoise squares), $N_{01} = 100$ (open green circles), and $N_{01} = 150$ (open orange diamonds). The solid blue, dashed green, and red dash-dotted lines are the IFTP results for $N_{01} = 50$, 100, and 150, respectively. (b) Translocation time τ (from LD simulations) plotted as a function of rod length L_r for fixed $F_{SP} = 32$ (open turquoise circles from the bottom horizontal blue axis). Open orange squares are the LD data for the translocation time as a function of F_{SP} (from the top horizontal red axis) for fixed $L_r = 16$. Dashed red and dash-dotted blue lines are guides to the eye.

process because a short section of the *trans*-side subchain is temporarily retracted to the *cis* side. The IFTP theory thus slightly underestimates the WT as it considers the dynamics of the *cis*-side subchain only.

B. Scaling of translocation time

Next we consider the average translocation time $\bar{\tau}$ for the polymer needs to pass through the nanopore. Its scaling form can be written as $\bar{\tau} \propto \tilde{L}_r^\beta \tilde{L}_r^\gamma N_{01}^\alpha$, where α , β , and γ are the translocation, SP force, and rod length exponents, respectively. Combining mass conservation in the TP and PP stages, i.e., $N_1 = \tilde{s}_1 + \tilde{l}_1$ and $N_1 = \tilde{s}_1 + \tilde{l}_1 = N_{01}$, respectively, with Eq. (1), the TP time is obtained by integration of N_1 from zero to N_{01} , while the PP time is calculated by integration of \tilde{R}_1 from $\tilde{R}_1(N_{01})$ to zero [24]. The sum of the TP and PP times leads to

$$\int_0^{\tilde{\tau}_{TP}} \tilde{f}_{TP}(\tilde{t}) d\tilde{t} + \int_{\tilde{\tau}_{TP}}^{\tilde{\tau}} \tilde{f}_{PP}(\tilde{t}) d\tilde{t} = \int_0^{N_{01}} dN_1 [\tilde{R}_1(N_1) + \tilde{\eta}_p], \quad (4)$$

where the effective forces in the TP and PP stages of this relation are obtained from fitting to the simulation data in Fig. 2(a) for TP (solid green line) and PP (dash-dotted green line) stages, respectively, as

$$\begin{aligned} \tilde{f}_{TP}(\tilde{t}) \tilde{L}_r^\nu / \tilde{F}_{SP} &= a + b\tilde{t}/\tilde{\tau}, \\ \tilde{f}_{PP}(\tilde{t}) \tilde{L}_r^\nu / \tilde{F}_{SP} &= c - d\tilde{t}/\tilde{\tau}, \end{aligned} \quad (5)$$

with $a = 0.35$, $b = 13.25$, $c = 11.37$, and $d = 6.42$. Using $\tilde{f}_{TP}(\tilde{t} = \tilde{\tau}_{TP}) = \tilde{f}_{PP}(\tilde{t} = \tilde{\tau}_{TP})$, the TP time is then given by $\tilde{\tau}_{TP} = Q\tilde{\tau}$, where $Q = (c - a)/(b + d) \approx 0.56$ here, as mentioned earlier. Combining $\tilde{\tau}_{TP} = Q\tilde{\tau}$ with the effective forces in the TP and PP stages in Eq. (5) together with Eq. (4) gives

the total translocation time as

$$\bar{\tau} = \tilde{L}_r^\nu \int_0^{N_{01}} dN_1 [\tilde{R}_1(N_1) + \tilde{\eta}_p] / G\tilde{F}_{SP}. \quad (6)$$

Using $\tilde{R}_1(N_1) = A_\nu N_1^\nu$, where $\nu = 3/4$ in 2D and $A_\nu = 1.1$ (from LD data), the scaling of the translocation time is

$$\bar{\tau} = \frac{\tilde{L}_r^\nu}{G\tilde{F}_{SP}} \left[\frac{A_\nu N_{01}^{1+\nu}}{1+\nu} + N_{01} \tilde{\eta}_p \right], \quad (7)$$

where $G = -0.5(c - a)^2/(b + d) + c - d/2 \approx 11.25$. Equation (7) reveals that the SP force and rod length exponents are $\beta = -1$ and $\gamma = \nu$, respectively, and the translocation exponent varies within $1 < \alpha \leq 1 + \nu$, where the upper bound holds in the long-chain limit $N_{01} \gg 1$. The SP force and translocation exponents are in agreement with purely pore-driven translocation in the SS regime [24]. In Fig. 4(b) we plot the translocation time as a function of the SP force (open orange squares from the top red horizontal axis) and the rod length (open turquoise circles from the bottom blue horizontal axis). Dashed red and dash-dotted blue lines are guides to the eye. The SP force and rod length exponents obtained from IFTP theory are in good agreement with the LD data.

V. CONCLUSION

In summary, we have shown here that active rodlike particles on the *trans* side of a membrane can efficiently overcome entropic losses and facilitate translocation of a polymer chain through a nanopore. The SP force induces a crowding effect of the rods close to the membrane and the polymer, and as a net result there is an effective driving force making translocation possible even without explicit driving. We have used a combination of LD simulations and IFTP theory in the SS regime to characterize the waiting time distribution w and the average translocation time τ . Neglecting the explicit contribution of N_{02} to the dynamics allowed us to derive a scaling form for $\bar{\tau}$ as a function of N_{01} , SP force, and rod length. The scaling exponents for τ and the SP force are in agreement with those of the purely pore-driven translocation case. Here we have only focused on systems wherein the initial values of the contour lengths for the *trans*-side subchain are long enough to lead to successful translocation events. Moreover, even for the system composed of 50% of the chain already on the *trans* side, for a successful translocation there would be a threshold for the value of \tilde{F}_{SP} in order to overcome the entropic force. On the other hand, at a constant value of \tilde{F}_{SP} , there exists a threshold value for N_{02}/N_0 in order to overcome the entropic force. For this case the threshold value of the N_{02} depends on the density of the ARs as well as the value of \tilde{F}_{SP} . Our work provides insight into our knowledge about the role of APs in living cells that may assist translocation of biomolecules and may be used as a method to control translocation dynamics, which is crucial for DNA sequencing applications.

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