

## High-Sensitivity Optical Monitoring of a Micromechanical Resonator with a Quantum-Limited Optomechanical Sensor

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We experimentally demonstrate the high-sensitivity optical monitoring of a micromechanical resonator and its cooling by active control. Coating a low-loss mirror upon the resonator, we have built an optomechanical sensor based on a very high-finesse cavity (30 000). We have measured the thermal noise of the resonator with a quantum-limited sensitivity at the  $10^{-19}$  m/ $\sqrt{\text{Hz}}$  level, and cooled the resonator down to 5 K by a cold-damping technique. Applications of our setup range from quantum optics experiments to the experimental demonstration of the quantum ground state of a macroscopic mechanical resonator.

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*Introduction.*—Optomechanical coupling between a moving mirror and quantum fluctuations of light first appeared in the context of interferometric gravitational-wave detection [1,2] with the existence of the so-called standard quantum limit [3–5]. Since then, several schemes involving a cavity with a movable mirror subject to radiation pressure have been proposed either to create nonclassical states of both light [6,7] and mirror motion [8], to perform quantum nondemolition measurements [9], or to entangle two movable mirrors [10]. Recent progress in low-noise laser sources and low-loss mirrors has made the field experimentally accessible and has enlightened the unique sensitivity of interferometry, with conventional fused silica mirrors [11,12] or specially designed sensors such as a silicon torsion oscillator [13] or mirror-flexure system [14].

Micro- and nanoelectromechanical resonators play a great role in the quest to detect quantum fluctuations of a mechanical resonator [15–17] or for sensing purposes [18–20]. Detecting zero-point motion of a mechanical oscillator requires high resonance frequencies (up to the GHz band) and low temperature operation (in the mK regime). It also requires a sufficient sensitivity on the displacement measurement, which has not been reached yet by any setup based upon an electrical detection scheme.

The optomechanical monitoring of a micromechanical resonator therefore seems promising for the experimental observation of quantum effects of radiation pressure and to reach the quantum regime of a macroscopic oscillator [21]. The drastic improvement of sensitivity is made at the expense of a larger resonator and a correspondingly lower critical temperature, thus requiring an active cooling strategy such as cold damping [12] or cavity cooling [22].

In this Letter we demonstrate the experimental feasibility of these concepts. We present an experiment where the motion of a silicon micromechanical resonator is probed with an unprecedented sensitivity by an optical setup based on a very high-finesse optical cavity. We have observed the thermal noise spectrum of the resonator over a wide bandwidth, and we have cooled the resonator by a cold-damping technique. Quantum optics experiments possible with such a setup are discussed.

*Microresonator design and fabrication.*—We have developed silicon micromechanical resonators with typical transverse dimensions from 400  $\mu\text{m}$  to 1 mm and a thickness of a few tens of microns. With such dimensions, resonance frequencies are in the MHz range and the corresponding effective masses down to the  $\mu\text{g}$  level. Fabrication of the resonator proceeds as follows: we use 1 cm-squared chips, cut in a 4-inch SOI wafer (60  $\mu\text{m}$  Si || 2  $\mu\text{m}$  SiO<sub>2</sub> || 500  $\mu\text{m}$  Si), each with up to 4 microresonator structures. The structures are obtained by double-sided lithography and etched by deep reactive ion etching [23], which insures sharp edges. We have fabricated resonators with different geometries but the results presented here are all obtained with a 1 mm  $\times$  1 mm  $\times$  60  $\mu\text{m}$  doubly clamped beam (Fig. 1). Each resonator chip is coated on the upper side with a very high-reflectivity and low-loss dielectric coating for 1064 nm.

*Optomechanical sensing.*—The optical monitoring setup is based upon a single-ended Fabry-Perot cavity composed of the microresonator as a totally reflecting back mirror, and an input coupling mirror with a 5 cm curvature radius (Fig. 2). The cavity length is 2.4 mm, yielding an optical waist of 60  $\mu\text{m}$ . The resonator is

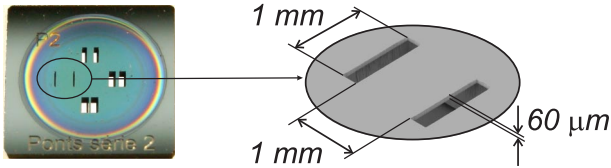


FIG. 1 (color online). Picture of a coated chip with 4 microresonators and scheme of the microresonator used throughout the Letter.

inserted in a mechanical structure which both guarantees optical parallelism and allows for accurate translation of the resonator perpendicularly to the optical axis in order to provide a fine centering of the resonator. Because of the very good coating made on the resonator, we have experimentally obtained a very high finesse  $\mathcal{F} = 30\,000$ . From the input mirror transmission  $T = 70$  ppm, this corresponds to overall losses (residual transmission of the microresonator and losses of both mirrors) equal to  $L = 140$  ppm.

The laser source is a highly stabilized Nd:YAG laser at  $\lambda = 1064$  nm. The laser beam is sent through a wide-band electro-optic modulator (EOM) used as an intensity-modulation device, and a triangular spatial filtering cavity, locked onto resonance with the tilt-locking technique [24]. Our laser source therefore delivers a perfect  $\text{TEM}_{00}$  Gaussian mode with well-defined intensity and wavelength, and mode matched to the high-finesse cavity by focusing lenses.

In order to eliminate the drift between the laser and the optical cavity, the cavity is temperature stabilized with residual temperature fluctuations below 10 mK. The laser frequency is finally locked at resonance by the Pound-

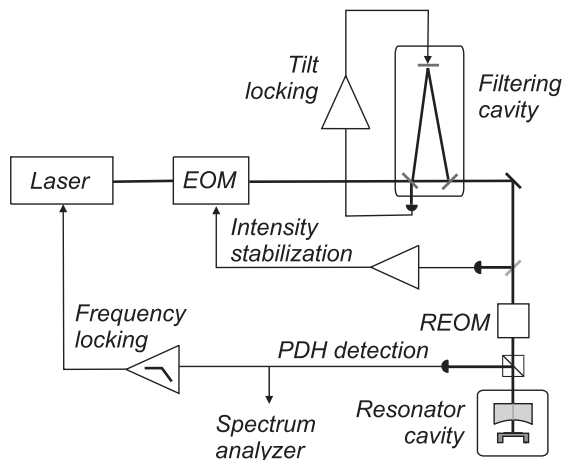


FIG. 2. Experimental setup used to monitor the displacements of the micromechanical oscillator. A Nd:YAG laser is intensity stabilized with an electro-optic modulator (EOM) and spatially filtered before entering the resonator cavity. The displacement signal is extracted by means of a Pound-Drever-Hall phase modulation scheme using a resonant electro-optic modulator (REOM). The low-frequency part of the signal is used to lock the laser frequency to the cavity resonance.

Drever-Hall (PDH) technique via a resonant electro-optical modulator (REOM) which provides a phase modulation of the incident beam at the sideband frequency of 12 MHz. The resonator displacements are monitored by the high-frequency part of the PDH error signal, and the displacements are calibrated by comparison with the effect of a frequency modulation of the laser beam [11].

*Noise levels and sensitivity.*—Curve (a) of Fig. 3 presents the resulting calibrated noise spectrum obtained at room temperature with a resolution bandwidth of 20 Hz and for an incident laser intensity of 1.5 mW. The spectrum exhibits sharp peaks with high dynamics, associated to the acoustic modes of the microresonator.

Curves (b)–(d) of Fig. 3 represent other relevant noises. The frequency noise of the laser has been independently characterized with the filtering cavity. Curve (b) presents an overestimated envelope. Frequency noise does not affect the sensitivity of our experiment for frequencies higher than 500 kHz and its effect could be further reduced by using a shorter cavity. The optical cavity is operated in vacuum (with a residual pressure below  $10^{-2}$  mbar) in order to minimize the effect of optical index fluctuations. Curve (d) presents the expected noise level deduced from the measurement made at ambient pressure, in agreement with a simple theoretical model [25].

At frequencies above 1 MHz, the sensitivity is only limited by the quantum phase noise of the reflected field [curve (c)] to a level [11,13]

$$\delta x_{\min} = \frac{\lambda}{16\mathcal{F}\sqrt{I}} \frac{F(m)}{\sqrt{\eta\eta_{\text{ph}}}} \frac{T+L}{T} \sqrt{1 + \left(\frac{f}{\Delta\nu}\right)^2}, \quad (1)$$

where  $I$  is the mean incident intensity (counted as photons/s),  $f$  the analysis frequency,  $\Delta\nu = 1.05$  MHz the cavity bandwidth,  $\eta = 91\%$  the mode matching of the beam to the cavity,  $\eta_{\text{ph}} = 93\%$  the detection efficiency,

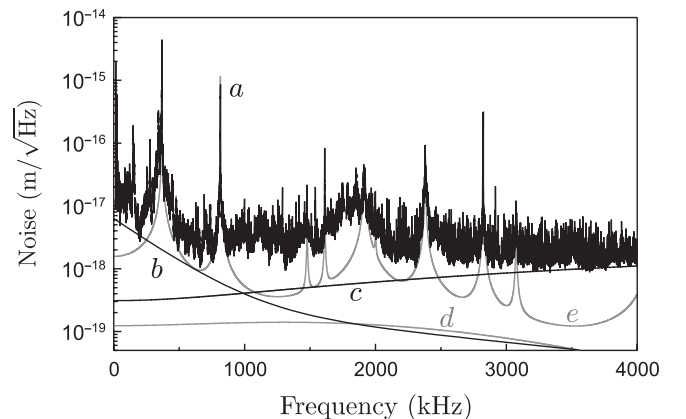


FIG. 3. Noise amplitude of the Pound-Drever-Hall signal, calibrated as microresonator displacements, over a 4 MHz span (a). Other curves represent relevant noises: maximum frequency noise level (b), shot-noise level (c), and optical index fluctuations due to the residual pressure (d). Curve (e) is the thermal noise spectrum expected from FEM simulations.

and  $F(m)$  a function of the modulation index  $m$  of the PDH scheme. With our parameters, the quantum-limited sensitivity is equal to  $4 \times 10^{-19} \text{ m}/\sqrt{\text{Hz}}$  at 1 MHz and back-action noise due to quantum effects of radiation pressure is not visible. It can be estimated at the  $10^{-22} \text{ m}/\sqrt{\text{Hz}}$  level except at mechanical resonances where it may be as large as  $10^{-18} \text{ m}/\sqrt{\text{Hz}}$  and would become visible if thermal noise is reduced.

*Single-mode optomechanical characterization.*—The elasticity theory and the fluctuation-dissipation theorem [26] allows one to account for the observed thermal noise spectrum, which can be seen as the sum of thermal peaks and off-resonance tails of the vibration modes. Our setup allows to study every vibration mode in great detail. As an example, curve (a) of Fig. 4 presents the noise spectrum acquired over a 4 kHz span centered around the mechanical resonance at 814 kHz. A Lorentzian fit of the resonance gives access to the optomechanical characteristics of the mode: resonance frequency  $f_m \approx 814 \text{ kHz}$ , effective mass  $m_{\text{eff}} \approx 190 \mu\text{g}$ , in good agreement with the expected values (890 kHz and  $130 \mu\text{g}$ ), computed with a finite element method (FEM). The discrepancy decreases quickly and is below 5% for higher frequency modes. It appears to be mainly due to the coupling of the resonator modes with the wafer modes, as shown by the dependence of the computed frequencies with the location of the resonator over the chip. The mechanical quality factor  $Q$  varies from 5000 to 15 000 among the modes, notably enhanced by the vacuum operation.

An external force can be applied onto the resonator: we have used an electrostatic force via a voltage modulation

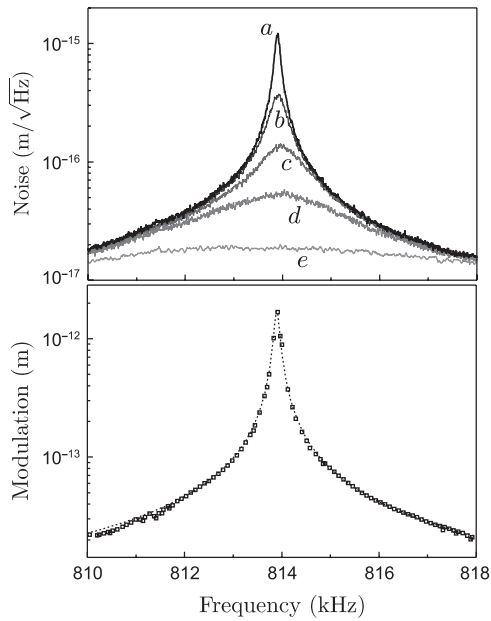


FIG. 4. Top: thermal noise amplitude spectra around a mechanical resonance of the oscillator at room temperature (a), and at lower effective temperatures obtained by cold damping (b)–(e). Bottom: mechanical response to a modulated electrostatic force ( $\square$ ) and corresponding Lorentzian fit (dashed line).

and an offset applied between the resonator and a tip. The resulting force is on the order of 1 nN. The bottom curve of Fig. 4 shows the corresponding mechanical response and confirms the mechanical origin of the resonance, along with the values of the parameters ( $f_m, m_{\text{eff}}, Q$ ).

*Spatial profiles.*—As the observed displacements depend on the overlap between the spatial structure of the mode and the optical intensity profile inside the cavity [27], the spatial profile can be mapped by translating the resonator with respect to the laser beam: Fig. 5 presents the measured thermal noise level as a function of the transverse displacement between the resonator and the laser waist. The results are in excellent agreement with the noise levels expected from the computed spatial structure of the mode. This sheds new light onto the variations of the mechanical quality factors observed between the various modes: one gets a low value for a mode where the vibration evolves along the longitudinal direction of the beam, whereas the value is higher for a “transverse” mode with a low displacement at the clamping location [28].

*Multimode spectrum.*—Performing an individual study of each acoustic mode of the resonator allows us to quantitatively explain the observed multimode noise spectrum of Fig. 3. Curve (e) presents the expected thermal noise spectrum of the resonator: only modes predicted by the FEM were taken into account, with the experimental values ( $f_m, m_{\text{eff}}, Q$ ) obtained by fitting the individual thermal noise spectra.

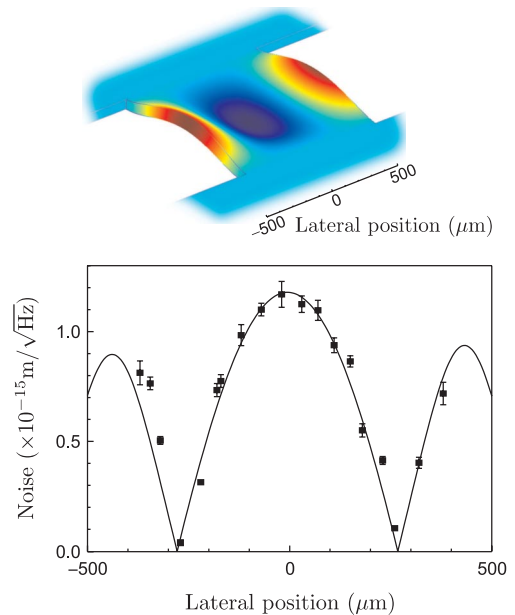


FIG. 5 (color online). Top: computed spatial profile of the 814 kHz vibration mode of the resonator. Bottom: variations of the observed displacement noise level as a function of the lateral position of the optical spot. Dots: experimental points; full line: fit with the expected spatial profile. The vertical error bars are mainly due to the optical finesse variation, especially at the edge of the resonator.

The yet unmodeled discrepancy, for example around 1800 kHz, appears to be due to the coupling between the resonator modes and neighboring modes of the silicon chip. This can be further accounted for by a noise spectrum monitored outside the resonator, on the wafer surface, which clearly exhibits the same vibration modes, along with a number of smaller peaks due to the modes of the silica input coupling mirror, which also constitute the quasicontinuum observed at higher frequencies.

*Cold damping.*—We have finally demonstrated the possibility to cool the resonator by a cold-damping feedback mechanism [12]. The monitoring signal is used in a feedback loop to apply a controlled electrostatic viscous force to the resonator, without any additional noise. According to the fluctuation-dissipation theorem, this yields a lower effective temperature. Curves (b)–(e) of Fig. 4 present the thermal noise spectra of the resonator obtained for increasing feedback gains. Because of the additional damping, the Lorentzian shapes are widened, whereas the amplitudes are strongly reduced. The reduction of the curve area is directly related to the effective temperature by the equipartition theorem. We have reached a temperature of 5 K, corresponding to a cooling factor of 60.

*Conclusion.*—We have presented an experiment where the motion of a micromechanical resonator is monitored at the  $10^{-19}$  m/ $\sqrt{\text{Hz}}$  level with a setup based upon a stabilized laser source and a very high-finesse optical cavity. The motion and the optomechanical behavior have been fully studied and accounted for, both at and off resonance, at frequencies of interest for quantum optics experiments ( $\geq 500$  kHz). This is to our knowledge the first monitoring of the motion of a micromechanical resonator over such a large frequency band. Our setup also presents a thousand-fold improvement in sensitivity over any previous detection scheme used to monitor the displacement of a microresonator, either electrical or optical [16,17,29,30]. The sensitivity is in principle large enough to detect the quantum effects of radiation pressure and the zero-point fluctuations of the resonator at the mechanical resonance, both estimated in the  $10^{-19}$ – $10^{-18}$  m/ $\sqrt{\text{Hz}}$  range, as far as the thermal noise is made small. There is still room for improvement, both optical and mechanical: the cavity finesse achieved so far is mainly limited by the roughness of the commercial silicon wafer, and higher values have already been obtained for the mechanical quality factor [31]. The design of a resonator with smaller size and with a lower impact of the wafer upon its motion is currently under investigation.

Low temperature operation of such a resonator opens the way to quantum optics experiments, as well as the experimental observation of the quantum ground state of a macroscopic mechanical resonator. As our resonator operates in the MHz range, it requires a more stringent condition on the temperature, below 1 mK. The sensitivity achieved is, however, promising since a specific scheme based upon active cooling by a cold-damping mechanism [12] has

already been proposed [21]. The single-mode resonant behavior observed over more than 40 dB with our resonator and the corresponding cooling by 2 orders of magnitude we have obtained seem especially promising in that purpose.

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