

## Comment on “Scaling of the Conductivity with Temperature and Uniaxial Stress in Si:B at the Metal-Insulator Transition”

Bogdanovich, Sarachik, and Bhatt [1] (BSB) recently employed uniaxial stress ( $S$ ) to tune Si:B through the metal-insulator transition and fit the data to the finite- $T$  scaling expression  $\sigma(t, T) = AT^x f[(t - t_c)/T^y]$  where  $t$  is a control parameter (dopant density or stress). BSB obtain  $x = 0.5$ ,  $y = 0.31$ , and find for  $\sigma(t, T \rightarrow 0) \propto (t - t_c)^\mu$  the surprising result  $\mu = x/y = 1.6$ . The scaling exponent  $\mu$  has been found to be 0.5 for unstressed Si:B, Si:P, Si:As [2] stressed Si:P [3] and Ge:Ga [4]. In addition, Itoh *et al.* [4] have found a good fit to the above scaling form with  $x = 0.27$ ,  $y = 0.54$ , and  $\mu = 0.50$  for the metallic side of the transition. This Comment suggests this large discrepancy is explained by stress inhomogeneity (SI) from sample bending.

$$\langle \sigma(T = 0) \rangle = \sigma_o (1 - \underline{S}/S_c)^\beta [1 - O\{(\langle \lambda \rangle \underline{S}/S_c)/(1 - \underline{S}/S_c)\}^2], \quad (1)$$

and the effect of SI is small. Experiment determines the resistance  $R$  between the voltage electrodes ( $z_1, z_2$ ) as  $R = A^{-1} \int_{z_1}^{z_2} \rho(z) dz$  [ $\rho(z) = 1/\sigma(z)$ ], hence  $\langle \sigma \rangle = (z_2 - z_1) / \int_{z_1}^{z_2} dz / \sigma(z)$ . In the limit  $1 - \underline{S}/S_c \ll \lambda \underline{S}/S_c$  for  $\underline{S} > S_c$

$$\langle \sigma(T = 0) \rangle = [\sigma_o S_c / 2 \underline{S} (1 + \beta)] (z_2 - z_1) / \int [dz \lambda(z) / [1 - \underline{S}/S_c + \lambda(z) \underline{S}/S_c]^{\beta+1}]. \quad (2)$$

At  $\underline{S} = S_c$  (2) yields  $\langle \sigma \rangle = [\sigma_o / 2(1 + \beta)] g(\lambda)$  with  $g(\lambda) = (z_2 - z_1) / \int dz \lambda^{-\beta}$  [ $z_2 - z_1 = L/8 = 1$  mm for the BSB case].  $\sigma(z) \rightarrow 0$  for  $\underline{S} = S_c / [1 - \lambda(z)]$  giving an apparent critical stress  $S_c^*(z) = S_c / [1 - \lambda(z)]$  so that  $\sigma(z) \propto [1 - \underline{S}/S_c^*(z)]^{\beta+1}$ . SI shifts  $S_c$  to  $S_c^*(z)$  and raises the scaling exponent to  $\beta + 1$  independent of  $z$ . The BSB data in Fig. 1 show  $\sigma(T = 0)$  vs  $\underline{S}$ . BSB infer  $S_c^* = 613$  bar and  $\mu = 1.6 = \beta + 1$  suggesting  $\beta \sim 0.6$ .

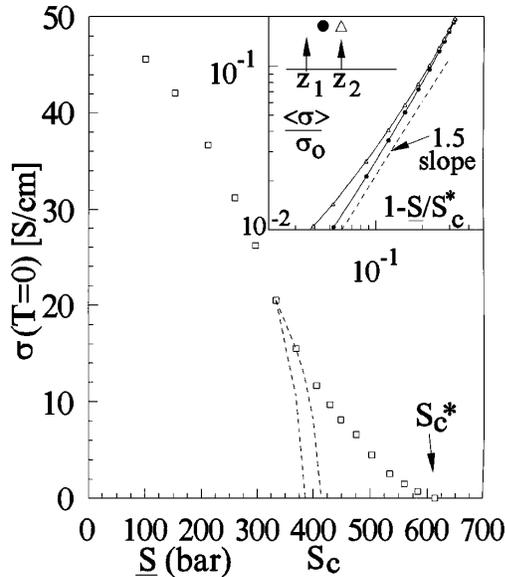


FIG. 1.  $\sigma(\underline{S}, T = 0)$  vs  $\underline{S}$  for Si:B.  $S_c$  is the actual critical point (CP).  $S_c^*$  is the apparent CP resulting from SI. The inset shows  $\langle \sigma(T = 0) \rangle / \sigma_o$  vs  $1 - \underline{S}/S_c^*$  for  $\lambda_m = 0.35$ .

For a column in static equilibrium  $EId^2y/dz^2 = M(z) = -Py$ , where  $E$  is Young's modulus,  $I$  is the cross section (area  $A = ab$ ,  $a < b$ ) moment-of-inertia, and  $M(z)$  is the bending moment for an axial force  $P$  and lateral deflection  $y$ . For a column of length  $L$  with free or pinned ends [5]  $y(z) = d_m \sin \pi z/L$  where the critical force  $P_c = \pi^2 EI/L^2$ . The deflection  $y$  depends on  $L/a$ , force eccentricity, load bearing surface defects, and the rigidity of the surfaces applying the forces.  $S$  varies linearly across the cross section at  $z$  between  $P/A(1 - 6y/a)$  and  $P/A(1 + 6y/a)$  with  $P/A$  the average stress  $\underline{S}$ .

For a stress distribution  $f(S, z)$  [ $\int f(S, z) dS = 1$ ] one finds  $f(S) = 1/2 \underline{S} \lambda$  for  $\underline{S}(1 - \lambda) < S < \underline{S}(1 + \lambda)$  [ $\lambda = 6y/a$ ] and zero outside this range. For a uniform stress  $\sigma(S, T = 0) = \sigma_o (1 - S/S_c)^\beta$ . For a nonuniform stress  $\sigma(z) = \sigma_o \int (1 - S/S_c)^\beta f(S, z) dS$ . Using this  $f(S)$  for  $1 - \underline{S}/S_c \gg \lambda \underline{S}/S_c$  one obtains

The data for  $\underline{S} < 333$  bar is a good fit to  $\beta \sim 0.5$  with  $S_c \sim 400 \pm 15$  bar corresponding to  $\langle \lambda \rangle \sim \frac{1}{3}$ .  $S_c^*/S_c = 1.53$  yields  $\lambda_m \sin \pi z_1/L = 0.347$  and  $\lambda_m = 0.354$  for  $z_1/L = 0.4375$ . The inset shows  $\langle \sigma \rangle / \sigma_o$  vs  $1 - \underline{S}/S_c^*$  for two positions of  $(z_1, z_2)$  relative to  $d_m$  from numerical integration of (2). It confirms SI from bending gives  $1.5 < \mu < 1.6$  for  $\beta = \frac{1}{2}$ , weakly dependent on the geometry for  $\langle \sigma \rangle / \sigma_o > 0.02$  [ $\langle \sigma \rangle > 1$  S/cm]. For  $\underline{S} > S_c^*$  the entire sample is insulating and  $\langle \sigma(\underline{S}, T) \rangle$  is a complex average of variable range hopping and activated conduction. The linear SI from bending produces a crossover from the true  $\mu \sim \frac{1}{2}$  to an apparent  $\mu \sim 1.6$ .

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