## **Saturation of Laser Imprint on Ablatively Driven Plastic Targets**

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The imprinting of areal density perturbations on thick planar plastic targets has been studied numerically and analytically. Simulations predict that the target modulation saturates while still in a small-amplitude regime. General scaling laws relating saturation times and amplitudes to mean laser drive and wavelength, and perturbation amplitude and wavelength, are summarized from the simulations. A linear gasdynamic model is used to study the physical mechanisms responsible for the saturation, and provides strong evidence that mass ablation is the dominant stabilizing influence. [S0031-9007(97)03946-X]

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When a laser-driven inertial confinement fusion (ICF) pellet is imploded, the ablative Rayleigh-Taylor Instability (RTI) [1] produces exponential growth of any initial mass perturbations on the pellet. The seed for the ablative RTI is provided by limitations in target fabrication, and by the imprint [2-4] of inevitable spatial nonuniformities in the laser beams. If the laser has been optically smoothed, then the imprint can be very small, but it can never be completely eliminated and is generally larger than target nonuniformities resulting from the manufacturing process. This means that imprint is the dominant seed of the RTI in direct-drive ICF, and so understanding and control of the process is of paramount importance. During the majority of a laser-driven implosion the laser absorption region is radially farther out than the high-density ablation surface, and so the driving pressure nonuniformities are rapidly smoothed out by thermal conduction [5]. However, in the very early part of the laser pulse the plasma corona is thin, and nonuniformity of the laser beam has a larger effect on the target. Laser imprinting is thus primarily an impulsive effect whose duration is short compared to a shock transit time through the pellet shell.

Thermal smoothing stops the lateral *acceleration* of the material, but does nothing to remove the lateral *velocity* perturbation field already in place. Thus a situation akin to the Richtmyer-Meshkov instability (RMI) [6] can be expected, where the passage of a nonuniform shock perturbs an interface, and subsequent linear amplification of these perturbations is due to the velocity field thereby generated. However, a more complex phenomenon is observed in numerical simulations of laser imprinting. An early period of growth of the target mass perturbations is

followed by small amplitude saturation and subsequent decay. This is a clear indication that some stabilizing process is at work.

Both the early-time growth and the saturation of the areal mass perturbation amplitude  $\delta m$  in a laser-driven target have been observed numerically, in isolated instances [7], but there were no general scaling rules, and the saturation was not understood. In this Letter we present scalings for imprint from numerical simulations, and a plausible model to explain the observed  $\delta m$  saturation. The scalings apply over a wide range of conditions relevant to the direct-drive laser-fusion problem, and agree for the most part with those predicted by a linear analytical model similar to that describing the classical RMI [8]. Moreover, by means of comparison between the numerical and analytical results, we demonstrate for the first time that the small-amplitude saturation of  $\delta m$  is primarily due to mass ablation, which removes perturbed material from the unstable target surface. Although the importance of mass ablation for the RTI has been understood for many years [9], this is the first evidence of its relevance to early-time RMI-like mass imprinting.

The simulations reported here use the FAST code [10], which has previously proved effective at reproducing experimental observations of imprinting [3]. The code includes: FCT advection; inverse bremsstrahlung laser energy deposition; Spitzer-Härm thermal conduction; variable Eddington multigroup radiation transport with STA-NRL [11] opacities and tabulated Henke [12] opacities at low temperatures; and, a tabulated equation of state (EOS). In all cases, simulations are of semi-infinitely thick, planar polystyrene (CH) targets irradiated with a

laser beam modulated by a sinusoidal perturbation in a transverse (y) direction. There are at least twenty grid points per modulation wavelength in y, and the laser-direction axial (x) grid was designed such that  $\delta x = 0.2 \ \mu m$  from 5  $\mu m$  in front of the ablation front through the entire ablation front region in the target.

The parameters that were independently varied in this study for each of the relevant laser wavelengths  $\lambda_L =$ 0.249, 0.35, and 0.53  $\mu$ m include: the mean laser intensity  $I_o$  from 1 × 10<sup>12</sup> to 9 × 10<sup>13</sup> W/cm<sup>2</sup>; the laser spatial perturbation amplitude  $\delta I/I$  from 0.5 to 10.0%; and, perturbation wavelengths  $\lambda_s$  typical of laser speckle scales, from 7.5 to 60  $\mu$ m. Following an initial 250 ps linear ramp from  $3 \times 10^9 \text{ W/cm}^2$  to  $I_o$ , the irradiance is held constant in time. For a given run, both  $\delta I/I$  and  $\lambda_s$  are also held fixed in time. The scalings reported here confirm many of those obtained with the hydrocode POLLUX [13,14]. The temporal scalings are also observed in ISI simulations, where laser perturbation amplitudes fluctuate statistically in y and t. The scalings are qualitatively independent of both the EOS and radiation transport details, and are computationally robust.

The extent of the laser imprinting is measured by the modulation in target areal density,  $\delta m(t) =$  $\delta[\int_{x_1}^{x_2} \rho(x, y, t) dx]$ , where  $\rho$  is the mass density and  $\delta[]$ denotes the y rms variation of the enclosed quantity. The point  $x_1$  is far to the interior of the target, ahead of the shock front. The point  $x_2$  is taken  $\sim 12 \ \mu m$  beyond the critical surface so as to include all significantly modulated plasma. The pressure perturbations  $\delta P$  at the ablation front are smoothed out by thermal conduction by about t = 500 ps. Long after that, the perturbation growth slows down until  $\delta m$  saturates and subsequently decays; see Fig. 1(a). This imprint saturation is not caused by the modulation entering a nonlinear regime, which is characteristic for both the RTI and the RMI. Rather, it is a linear, small-amplitude phenomenon. For all time through "saturation,"  $\delta m(t) \propto \delta I/I$  while the time scale is independent of  $\delta I/I$ . Therefore, the final amplitude



FIG. 1. Target areal density modulation,  $\delta m$ , for  $I_o = 3 \times 10^{12} \text{ W/cm}^2$ ,  $\lambda_s = 30 \ \mu\text{m}$  and  $\lambda_L = 0.249 \ \mu\text{m}$ . (a)  $\delta m \ (\mu\text{m g/cm}^3)$  as a function of time, for rms  $\delta I/I = 0.05$ ; (b)  $\delta m$  maximum as a function of rms  $\delta I/I$ . Saturation time  $t_{\text{sat}}$  in ns (solid line, symbols) is independent of  $\delta I/I$ , and saturation amplitude  $A_{\text{sat}}$  in  $\mu\text{m g/cm}^3$  (dashed line and open symbols) varies directly as  $\delta I/I$ .

of saturation  $A_{sat}$  also varies linearly with the same quantity, whereas the saturation time  $t_{sat}$  is independent of it. This is illustrated by Fig. 1(b), which is a typical sample from our database. Thus, a reduction in the beam nonuniformity generates a corresponding reduction in the target imprint in all cases.

From our database of more than 200 simulations, we have generated a predictive saturation scaling law that agrees with the observed  $\delta m$  amplitude ( $A_{sat}$ ,  $\mu m g/cm^3$ ) and time ( $t_{sat}$ , ns) saturation values to an accuracy of better than ~20% on average for both  $t_{sat}$  and  $A_{sat}$ . These are

$$t_{\rm sat} \simeq 0.06 \lambda_s^{1.1} I_0^{-3/8},$$
 (1)

$$A_{\rm sat} \simeq 0.052 \lambda_s^{f_1} I_o^{f_2} \lambda_L^{f_3} \delta I / I \,, \qquad (2)$$

with

$$f_i = \alpha_{i1}\lambda_s + \alpha_{i2}\lambda_L + \alpha_{i3}I_o + \alpha_{i4},$$

where the parameters in the scaling are as follows: perturbation wavelength  $(\lambda_s, \mu m)$ ; mean intensity  $(I_o, 10^{13} \text{ W/cm}^2)$ ; laser wavelength  $(\lambda_L, \mu \text{m})$ ; rms perturbation amplitude  $(\delta I/I)$ ; and, with coefficients  $\alpha_{13} = -0.067, \ \alpha_{14} = 1.49, \ \alpha_{21} = 0.004, \ \alpha_{22} = -0.94,$  $\alpha_{24} = 0.408, \, \alpha_{31} = 0.0037, \, \alpha_{33} = -0.07, \, \alpha_{34} = -1.13,$ and  $\alpha_{11}$ ,  $\alpha_{12}$ ,  $\alpha_{32}$ , and  $\alpha_{23}$  all zero. The scaling law is a good fit, with errors exceeding 20% only for runs at the high- $I_o$ , long- $\lambda_s$ , and short- $\lambda_L$  edges of the parameter space. In these equations  $t_{sat}$  is defined as the time just prior to saturation when the time derivative of  $\delta m$  is 0.1 of its maximum value, and  $A_{sat}$  is  $\delta m$  at that time. This definition reduces the statistical variation introduced by the sonic waves in the solution. In all cases,  $\delta m$  fully saturates, as can be seen by the representative curve, Fig. 1(a). The temporal saturation scaling, Eq. (1), is shown as a function of  $\lambda_s$  and  $I_o$  in Fig. 2. The  $t_{\text{sat}}$  dependence on  $I_o$ ,  $I_o^{-3/8}$ , is approximately  $P_a^{-1/2}$ . A balance between the differences in mass ablation and thermal smoothing accounts for the lack of laser wavelength variation in Eq. (1). Figure 3 shows the scaling of



FIG. 2. Temporal  $\delta m$  saturation (ns) variation as functions of  $I_o$  (10<sup>13</sup> W/cm<sup>2</sup>) and  $\lambda_s$  ( $\mu$ m), for rms  $\delta I/I = 0.01$ . (a) Contour plot of Eq. (1); (b) Eq. (1) for  $\lambda_s = 30 \ \mu$ m. For (b), simulation datapoints overlay the Eq. (1) scaling curves for: 0.249  $\mu$ m (crosses); 0.35  $\mu$ m (circles); and, 0.53  $\mu$ m (diamonds)  $\lambda_L$ .



FIG. 3. Amplitude  $\delta m$  saturation ( $\mu$ m g/cm<sup>3</sup>) variation as functions of  $I_o$  (10<sup>13</sup> W/cm<sup>2</sup>) and  $\lambda_s$  ( $\mu$ m), for  $\lambda_L = 0.35 \ \mu$ m. (a) Contour plot of Eq. (2), for rms  $\delta I/I = 0.01$ ; and, (b) Eq. (2) scaling curve with simulation datapoints overlaid, for  $\lambda_s = 45 \ \mu$ m, and rms  $\delta I/I = 0.05$ .

 $A_{\text{sat}}$ , Eq. (2), as a function of  $I_o$  and  $\lambda_s$  for the three laser wavelengths. Despite the complexity of the expression in Eq. (2), the essentially simple nature of the scaling is apparent from the contour plot, which is similar over the range of  $\lambda_L$  investigated. For the relevant parameter ranges considered, 1% KrF (0.249  $\mu$ m), blue (0.35  $\mu$ m), and green (0.53  $\mu$ m) laser light imprint saturate at a maximum amplitude of about 0.7, 0.5, and 0.3  $\mu$ m g/cm<sup>3</sup>, respectively, with  $t_{\text{sat}}$  between 2 and 10 ns.

In order to investigate the influence of the various processes at work in imprinting, the problem was examined analytically with a gasdynamic model similar to that presented in [8]. Consider a half space filled with uniform ideal gas whose density is  $\rho_0$ . At time t = 0, a shock wave is driven into the gas by an ablative pressure  $P_a$  so that the shock propagates at constant speed D, compressing the gas to the density  $\rho_1$ . The velocity of the shock front with respect to the shocked material is thus  $D_1 = \rho_0 D / \rho_1$ . A single-mode pressure perturbation is imposed upon  $P_a$  at the ablation front:  $\delta P[x = x_a(t), t] = \delta P_a f(t) \exp(iky)$ , where  $\delta P_a / P_a =$  $0.75\delta I/I$ , and the decaying function f(t) describes thermal smoothing as the corona develops. For this we use the expression  $f(t) = \exp(-t/t_1)$ , with  $t_1 = 500$  ps, as taken from the simulation. The effect of mass ablation is modeled by removing the fluid particles from the ablation front at the velocity  $v_a = \dot{m}/\rho_1$  relative to the fluid, where  $\dot{m} [g/(cm^2 s)]$  is the mass ablation rate. The important parameter of the model with mass ablation becomes the ratio of the two velocities  $\mu = v_a/D_1 = \dot{m}/\rho_0 D$ and  $0 \le \mu < 1$ . The limiting case  $\mu = 0$  corresponds to absence of mass ablation, whereas the larger  $\mu$ , the more important  $\dot{m}$  is. Values for  $\mu$  are extracted from the simulation. In the simulation, the unperturbed axial  $\rho$  and P profiles are not flat and steady, as assumed in the model, so that the estimate of  $\dot{m}$  should refer to a certain density level. For our baseline case (Fig. 4, solid line with closed circles),  $D = 1.24 \times 10^6$  cm/s, and the mass flow rate through the surface  $\rho = 1 \text{ g/cm}^3$ is about  $1.25 \times 10^5$  g/(cm<sup>2</sup> s), hence  $\mu \approx 0.1$ . Choosing  $\rho$  closer to the actual value of  $\rho_1 = 2.5$  g/cm<sup>3</sup> would increase the effective value of  $\mu$  up to 0.2–0.3.



FIG. 4. Time evolution of  $\delta m$  ( $\mu m g/cm^3$ ) for  $P_a = 1$  Mbar ( $I_o = 3 \times 10^{12}$  W/cm<sup>2</sup> for simulations), rms  $\delta I/I = 0.05$ ,  $\lambda_s = 30 \ \mu m$ , and  $t_1 = 0.5$  ns from: simulations: with radiation transport (solid line with solid circles); without radiation transport (solid line with squares); and, by the gasdynamic model for the same conditions and:  $\mu = 0$  (dashed line);  $\mu = 0.1$  (chain-dashed line); and,  $\mu = 0.3$  (dotted line with open circles).

The linearized perturbation problem is solved analytically as in [8] for the classical RMI. In Fig. 4, the analytical results for  $\delta m$  are compared to the simulation. Without  $\dot{m}$  ( $\mu = 0$ ) the model predicts typical RM behavior unlimited linear growth of  $\delta m$ , with superimposed sonic oscillations. However, the late time evolution is qualitatively different with  $\dot{m}$  included, in that the model predicts saturation of  $\delta m$ , as observed in the simulations. To explain it, we note that, in the absence of lateral pressure gradient, the linear growth of the RM-like instabilities is essentially due to vorticity  $\omega$ , both initially deposited at the interface and generated by the rippled shock front; see [8,15]. Since the fluid particles carrying  $\omega$  are constantly removed from the flow through the ablation front, and  $\omega$ production at the shock front decreases as the ripples decay, the shock-compressed plasma at the ablation front eventually becomes irrotational, stopping the perturbation growth. Both the model  $A_{sat}$  and  $t_{sat}$  agree well with the simulation, although the decay after saturation is not observed. These discrepancies result from the omission of a vortical flow effect similar to that described in [10]. The early-time  $\delta P$  accelerates the plasma in the lateral direction, producing  $\omega$  that supports lateral motion long after the lateral pressure gradient is smoothed out. This motion generates a more intense downstream axial plasma outflow through the pressure valleys. In both cases of classical RMI and RTI, the mass is driven laterally from the bubble area and then falls axially into the spike, increasing areal mass. In our case, however, the mass driven to the spike (pressure valley) is lost from there at higher rate through the outer boundary of the  $\delta m$  integration surface. Thus  $\delta m$  decays instead of growing, and the bubble-spike structure flattens instead of sharpening. Our analytical model does not account for the lateral nonuniformity of effective  $\dot{m}$ , nor for the vortical flow in the low-density plasma. It describes only the effect of lateral mass redistribution in

the dense plasma and predicts its saturation solely due to the uniform loss of the  $\omega$ -carrying fluid particles. For the conditions of Fig. 4, the nonuniformity of the axial mass losses and the vortical flow of the low density mass from spike to bubble, which both act to decrease the rms  $\delta m$ , are responsible for the decay of  $\delta m$ .

Some of the scalings mentioned above can be explained by the gasdynamic model. In the linear theory, all the perturbations are proportional to the external driving perturbation, that is, to  $\delta I/I$ . The only time scale in the linear theory is  $\lambda_s/D$ , hence  $t_{sat}$  varies as  $\lambda_s$ , all other parameters being constant. Since in the relevant range of the parameter  $\mu$ , the dimensionless  $t_{sat}$  is relatively insensitive to the choice of values of  $\mu$  and  $t_1$ , and for strong shock waves  $P_a$  scales as  $\rho_0 D^2$ , we conclude that  $t_{sat}$  scales as  $P_a^{-1/2}$ , in general agreement with the simulation results.

In summary, saturation of laser imprinting has been observed in single-mode imprint simulations across a broad range of parameters relevant to ICF. In this Letter we have summarized the saturation scalings in approximate scaling laws, and we have used a highly idealized model of the flow to demonstrate that  $\dot{m}$  is the fundamental hydrodynamic mechanism which produces the numerically observed imprint stabilization. This mechanism is the same as that which provides reduction to the rate of the ablative RTI [9]. In neither case is the ablation front really a contact surface formed by a fixed set of the fluid particles, but instead is a surface through which mass ablates. With a constant outflow of the perturbed fluid particles, continuous perturbation growth requires additional energy. In the case of the RTI, the acceleration, or effective gravity, provides such an energy source, and  $\dot{m}$ generally serves to reduce the ablative RT growth rate by a term proportional to the wave number [9]. However, the RMI, in contrast to the RTI, develops without any permanent energy source. Thus, introducing an outflow of perturbed fluid particles provides a permanent sink for energy (and  $\omega$ , see above), which results in full saturation of perturbation growth for all wavelengths. We note that the same stabilizing mechanism stops the RM-like perturbation growth in planar targets with surface ripples [16] and would saturate the perturbation growth due to initial target nonuniformity. In the simulations, thermal and radiative heat conduction both contribute to increasing the effects of saturation by effectively increasing  $\dot{m}$ . However, the fundamental result, that  $\delta m$  saturates in a finite time, is independent of such particulars, as is demonstrated by Fig. 4. We have verified that the contribution of those mechanisms is to shape the axial  $\rho$  and P profiles rather than to damp the perturbation directly. Generically,

both  $t_{sat}$  and  $A_{sat}$  are determined by a finite surface layer within a finite time interval. This provides us with an interesting concept that may prove extremely useful in the development of an ablator for high-gain direct-drive laser fusion, i.e., mass ablation is the dominant control parameter in the problem of laser imprinting.

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