## Dynamical Model of Wall-Bounded Turbulence

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Three complex ordinary differential equations, modeling interactions in wall-bounded turbulent flow, are developed and studied. It is believed that the roll-wave interactions which are included are of fundamental importance to turbulence production. Integration of these triad equations is shown to be consistent with direct flow simulations and the Ruelle-Takens route to chaos.

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Wall-bounded turbulent flow is characterized by a sequence of events in which a relatively slow moving wall fluid bursts [1] into the fast moving core fluid, and the fast moving core fluid sweeps  $[2]$  into the wall region (see also Ref. [3]). These events, which occur roughly 20% of the time, have an overwhelming effect on force balance at the wall, accounting for roughly 80% of the Reynolds stress at low Reynolds number (Re). Fluctuating turbulent wall flow on average is mainly organized in streamwise counterrotating rolls. (On the basis of energy, 75% lie in such modes for low Re [4].) Roll patterns appear as streaks in experiments [5]. Theoretical models for their existence have been offered [6,7], but no generally accepted theory exists. The remaining turbulent fiuctuations appear as propagating modes which travel downstream at a speed close to the mean speed at the locus of maximal Reynolds stress [4,8]. For channel flow without spanwise constraints propagating modes are plane waves, and have been shown to act as triggers for the bursts and sweeps of the streaks  $[4,8]$ . A goal of this Letter is the construction and examination of a simple dynamical model which describes the interaction of key modes and which leads to bursting and sweeping, essential elements of wall-bounded turbulence.

For simplicity, we consider channel flow without spanwise constraint, driven by a constant streamwise pressure gradient,  $-k$ . If  $\rho$  denotes the density of the fluid and H the half channel width, then the friction velocity, In simulations, L and W are the periodic length and  $u^2 = kH/\rho$ , is representative of the rms fluctuations in width of the channel. For relatively low q, V to a goo  $u_*^2 = kH/\rho$ , is representative of the rms fluctuations in width of the channel. For relatively low q, V to a good ap-<br>the wall region. The wall scale is  $l_* = \nu/u_*$ , and the proximation is the mean velocity at the locus of the wall region. The wall scale is  $l_* = \nu/u_*$ , and the proximation is the mean velocity at the locus of maximal Kolmogorov scale is roughly  $5l_*$  in the sublayer. Ex-<br>Kolmogorov scale is roughly  $5l_*$  in the sublayer. Ex-Kolmogorov scale is roughly  $5l_*$  in the sublayer. Ex-<br>netiment [5] and simulation indicate that streaks are of tions of the two point correlation operator. m and n will periment [5] and simulation indicate that streaks are of a distribution of roll modes and with peak wavelength be referred to as streamwise and spanwise wave numbers close to  $100l_*$ . (Extension to the turbulent boundary and q as the vertical quantum number. The vertical delayer requires a slow streamwise dependence in  $u_*$  and pendence  $\psi^q_{mn}(x_2)$  is obtained from simulations [9], and  $l_*$ .) Integration of the mean flow equations yields

$$
U = \frac{1}{2}x_2\left(2 - \frac{x_2}{R_*}\right) + \int_0^{x_2/R_*} \overline{u_1 u_2} \, dx_2. \tag{1}
$$

Here and in the following we use the subscripts  $(1,2,3)$  to

denote the streamwise, wall normal, and spanwise directions and  $U$  is the mean flow (streamwise). All velocities are normalized by  $u_*$  and length scales by  $l_*$ , so that the Reynolds number is  $R_* = u_* H/\nu = H/l_*$ . The bar signifies the ensemble average obtained by averaging over the  $(x_1, x_3)$  plane. Velocity fluctuations are incompressible,  $\nabla \cdot \mathbf{u} = 0$  and satisfy

$$
\frac{\partial}{\partial t}u_i + U \frac{\partial}{\partial x_1}u_i + \delta_{i1} \left( u_2 \frac{dU}{dx_2} - \frac{d}{dx_2} \overline{u_1 u_2} \right) + u_{i,j} u_j + \frac{\partial p}{\partial x_i} - \nabla^2 u_i = 0. \tag{2}
$$

p has been normalized by  $\rho u_*^2$  and time by  $l_*/u_* = \nu/u_*^2$ .

Sreenivasan [7] has proposed that, in analogy with transition, the locus of maximal Reynolds stress plays a central role in wall turbulence. Confirmation of this assertion is to be found in the simulations of Sirovich et al. [4,8]. As shown there the flow can be optimally represented as a superposition of velocity modes each having the form

$$
a_{mn}^q(t)\psi_{mn}^q(x_2) \exp\left[\frac{2\pi im}{L}(x_1 - Vt) + \frac{2\pi iL}{W}n_3x_3\right]
$$

$$
= a_m^q(t) \exp\left[-\omega_m t\right] \mathbf{V}_{mn}^q(\mathbf{x}) .
$$
 (3)

in particular is discussed in Ref. [10].  $a_{mn}^q(t)$  is found to exhibit chaotic behavior typical of turbulence.

We will use the results of simulations in a nominal way to construct a simple physical model. We consider mode energies  $\lambda_{mn}^q = \langle |a_{mn}^q|^2 \rangle$  (brackets indicate the time average), the first fifteen of which are [4]



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The first line gives  $(m, n, q)$  and the second the percent of total energy in each mode. One must also consider degeneracies based on flow symmetries, e.g., (0,4,1) and  $(0,-4, 1)$  have the same energy, as do  $(1,2,1)$ ,  $(-1,2,1)$ ,  $(1-2, 1)$ , and  $(-1, -2, 1)$ . One member of a degenerate set will be used to represent all members of the (invariant) subspace. The energy in the table is the fraction of the total for the subspace.

The most energetic modes are  $m = 0$  modes (rolls);  $q = 1$  modes are more energetic than other quantum numbers, and  $m = 2$  modes are less energetic than the  $m = 1$  modes. Perturbations based only on roll modes  $(m = 0)$  can be rigorously shown to decay to Poiseuille flow [11]. A model [12] which is based on just such modes has been shown to lead to artifactual behavior [3].

 $V_{mn}^{q}(x)$  by construction satisfies continuity and hence any finite sum of such terms satisfies continuity. The pressure gradient is orthogonal to the space of such terms and need not be considered. The principal interaction term in (2) is quadratic, conservative, and governs the passage of energy among modes. In a Galerkin projection, the quadratic terms lead to triad interactions. For example, to follow the (0,4,1) roll, a possible triad interaction is  $(0,4,1) \otimes (1,2,1) \otimes (1,2,1)$ . (Other possible interactions are considered later.) To follow these modes the flow is assumed to have the form

$$
\mathbf{u} \approx A_1 \mathbf{V}_{0.4} + A_2 \mathbf{V}_{1.2} + A_3 \mathbf{V}_{1-2} + \text{c.c.}, \tag{4}
$$

where for simplicity we have left out the (quantum)  $q = 1$ dependence. The complex coefficients  $A_n$  are time dependent, and it remains to verify that these have secular temporal growth as in  $(3)$ . If  $(4)$  is substituted into  $(2)$ , then under Galerkin projection we obtain

$$
\dot{A}_1 = l_1 A_1 - q_1 \bar{A}_2 A_3 - A_1 [c_{11}|A_1|^2 + c_{12}(|A_2|^2 + |A_3|^2)],
$$
\n(5)

$$
\dot{A}_2 = l_2 A_2 + q_2 \bar{A}_1 A_3 - A_2 [c_{21}|A_1|^2 + c_{22}(|A_2|^2 + |A_3|^2)],
$$
\n(6)

$$
\dot{A}_3 = l_2 A_3 + q_2 A_1 A_2 - A_3 [c_{21}|A_1|^2 + c_{22}(|A_2|^3 + |A_3|^2)],
$$
\n(7)

where [10]  $l_1 = 19.91r - 1.640e/r$ ,  $l_2 = (13.81 - i17.82)r -$ 0.605e/r;  $q_1 = 0.910$ ,  $q_2 = 1.914 - i1.612$ ;  $c_{11} = 16.56r$ ,  $c_{12} = 10.59r, c_{21} = (10.59 - i12.58)r; c_{22} = (8.582$ i6.743)r. Here  $r = R_*/R_c$ .  $R_c = 180$  is the Reynolds number at which  $V_{kl}(x_2)$  were computed and the *eddy viscosity e* is chosen to be 2.7. Cubic terms arise from  $\overline{uv}$ in (1).

 $(5)-(7)$  have the form of a three-wave resonance. Such equations appear in wave interactions in shear flows [13], in plasmas [14), and in thermal convection to describe roll-hexagon competition [15]. Related equations without cubic terms appear in the interaction between oblique Tollmien-Schlichting (TS) waves and Taylor-Görtler vortices in curved channel flows [16].

Symmetries in the flow confer invariances on the dynamical system. Translational invariance in the stream-

wise and spanwise directions generates the trigonometric terms in  $V_0$ <sub>4</sub>,  $V_1$ <sub>2</sub>,  $V_{-1}$ <sub>2</sub>. In addition, (5)–(7) are invariant under the group  $A_1 \rightarrow A_1 e^{2a}$ ,  $A_2 \rightarrow A_2 e^{(b-a)i}$ ,  $A_3 \rightarrow A_3 e^{(b+a)i}$ , where a, b are arbitrary real constants. The flow geometry possesses a number of reflectional symmetries  $[17]$  and from these  $(5)-(7)$  are invariant under  $A_1 \rightarrow \overline{A}_1$ ,  $A_2 \rightarrow A_3$ ,  $A_3 \rightarrow A_2$ . From Lie theory [18] each invariance can reduce the order of the system by one.

To carry out this reduction we use the polar representation,  $A_i = r_i e^{i\theta_j}$ ,  $i = 1, 2, 3$ , which yields

$$
\dot{r}_1 = l_1 r_1 - q_1 r_2 r_3 \cos \psi - r_1 [c_{11} r_1^2 + c_{12} (r_2^2 + r_3^2)],
$$
  
\n
$$
\dot{r}_2 = l_2^r r_2 + q r_1 r_3 \cos(\psi + \theta_0) - r_2 R_2^r,
$$
  
\n
$$
\dot{r}_3 = l_2^r r_3 + q r_1 r_2 \cos(\psi - \theta_0) - r_3 R_2^r,
$$
\n(8)

$$
\dot{\theta}_1 = -q_1 \frac{r_2 r_3}{r_1} \sin \psi, \quad \dot{\theta}_2 = l_2^i + q \frac{r_1 r_3}{r_2} \sin(\psi + \theta_0) - R_2^i,
$$

$$
\dot{\theta}_3 = l_2^i - q \frac{r_1 r_2}{r_3} \sin(\psi - \theta_0) - R_2^i,
$$
(9)

where  $\psi = \theta_3 - \theta_2 - \theta_1$ ,  $R_2^r = c_{21}^r r_1^2 + c_{22}^r (r_2^2 + r_3^2)$ ,  $R_2^r$ where  $\psi = 0.3$   $\psi_2 = 0.1$ ,  $I_2 = -0.21$ ,  $I_1 + 0.22$ ,  $I_2 + I_3$ ,  $I_3 = -0.21$ ,  $I_1 + 0.22$ ,  $I_2 + I_3$ ,  $I_4 = -0.21$ ,  $I_1 + I_2 = -0.21$ ,  $I_1 + I_2 = -0.21$ ,  $I_2 + I_3 = -0.21$ ,  $I_3 + I_4 = -0.21$ ,  $I_4 + I_5 = -0.21$ ,  $I_5 + I_6 = -0.21$ ,  $I_$  $c_{21'}1 + c_{22'}(2 + 3), qe^- - q_2$ , and  $c_{2j}$ ,  $c_{2j}$  are the rea<br>and imaginary parts of  $c_{2j}$  with  $j = 1,2$ . The three equations of (9) can be reduced to

$$
\dot{\psi} = q \frac{r_2 r_3}{r_1} \sin \psi - q \frac{r_1 r_3}{r_2} \sin(\psi + \theta_0) - q \frac{r_1 r_2}{r_3} \sin(\psi - \theta_0).
$$
\n(10)

 $(5)-(7)$  can be reduced to  $(8)$  and  $(10)$ , in the variables  $r_1$ ,  $r_2$ ,  $r_3$ , and  $\psi$ .

Other possible interactions: Possible triads which can enter in the evolution of the  $(0,4,1)$  mode are  $(0,4,1)$   $\otimes$  $(0,2,1) \otimes (0,2,1)$  and  $(0,4,1) \otimes (0,1,1) \otimes (0,3,1)$ , which are pure roll mode interactions. By themselves such interactions cause relaminarization to Poiseuille flow and take place at a slow pace [4,8], and are not significant to the rapid dynamics of wall turbulence. Another possible triad interaction is  $(0,4,1) \otimes (1,3,1) \otimes (1,1,1)$ . This may be neglected since  $(1,1,1)$  (which does not appear in the table) is at a lower energy so the interaction is weak. Also in the evolutionary equation for  $a_{04}^{(1)}$  (i.e., for  $(A_1)$  this interaction leads, e.g., to a term  $\propto a_{13}^1a_{-11}^1,$  but the product is uncorrelated  $\langle a_{13} a_{-11} \rangle = 0$  in the exact interaction which is further evidence that this is weak.

To test such ideas we integrated the  $(0,3,1) \otimes (1,5,1)$  $\otimes$  (1,2,1) triad along with (5)–(7) and coupled through  $(1,2,1)$  to  $(5)$ – $(7)$  to numerical integration and found that  $(0,3,1)$  and  $(1,5,1)$  decayed to zero under normal initial conditions. Similarly  $(0,6,1) \otimes (1,3,1) \otimes (1,3,1)$  is an eligible triad of the table, and is coupled to  $(5)$ – $(7)$  through cubic terms; e.g.,  $A_{04} | A_{13} |^2$  appears in (5)–(7). If these coupled triads are numerically integrated, the modes in the second triad decay to zero. [If  $(0,6,1) \otimes (1,3,1) \otimes$ (1,3,1) is decoupled it supports nonzero solutions, which, however, are nonchaotic at the relatively low Re we consider.] Other numerical experiments further support the idea that the triads interact weakly. We regard  $(5)-(7)$ 



FIG. 1. Three-space of the fluid velocity. (a)  $R_* = 156$ , (b)  $R_* = 158.4$ , and (c)  $R_* = 168$ .

as being representative and now discuss their solutions

Steady solutions: (A)  $A_1 = A_2 = A_3 = 0$ , corresponding to plane Poiseuille flow, is stable if  $l_1, l_2^r < 0$  or if  $R_* < 62.2$ . Coincidentally, this is the value of  $R_2$  found in simulations and experiments [10] (B). sponding to plane Poiseuille flow, is stable if  $l_1, l_2^r < 0$  or if  $R_* < 62.2$ . Coincidentally, this is the value of  $R_*$  found in simulations and experiments [19]. (B):  $|A_1|^2 = l_1/c_{11}, A_2 = A_3 = 0.$  The condition that  $l_1 > 0$ implies that  $R_* > 84.9$ . Physically this solution corresponds to one steady roll in the flow, which may be shown to be unstable.

Periodic solutions: (A)  $A_1 = 0$ ,  $A_2 = 0$ ,  $A_3 = ae^{i\omega t}$ Periodic solutions: (A)  $A_1 = 0$ ,  $A_2 = 0$ ,  $A_3 = ae^{i\omega}$ <br>with  $a = \sqrt{l_2^r/c_{22}^r}$ ,  $\omega = l_2^t - c_{22}^t a^2$ , a single oblique wave By symmetry,  $A_2 = ae^{i\omega t}$ , and  $A_1 = A_3 = 0$  is also a solution. It may be shown that for  $62.2 < R_* < 130.7$ , both of these solutions are stable, and which solution appears depends on the initial conditions. (B) Another periodic solution can be found by letting  $A_1 = r_{10}$  $r_{20}e^{i\omega t}$ ,  $A_3 = \pm A_2$ ; here  $r_{10}$  and  $r_{20}$  are real, determine by  $l_1r_{10} \neq q_1r_{20}^2 - r_{10}(c_{11}r_{10}^2 + 2c_{12}r_{20}^2) = 0$ ,  $l_2^r \pm q_r r_{10} - (c_{21}^r r_{10}^2 + 2c_{22}^r r_{20}^2) = 0$  and the frequency by  $\omega = l_2^i \pm q_i r_{10} - (c_{21}^i r_{10}^2 + c_{22}^i r_{20}^2)$ , with  $q_r = \text{Re}(q_2)$ ,  $q_i = \text{$ This solution corresponds to two oblique waves and one steady roll. The stability can be investigated by means of the polar decomposition, (8) and (10). A  $4 \times 4$  Jacobi<br>matrix obtained at  $r_1 = r_{10}$ ,  $r_2 = r_{20}$ ,  $r_3 = r_{20}$ ,  $\psi = 0$ ,  $\pi$ determines the eigenvalues which in turn determine the stability. From this it is found that the solution is all unstable whenever it exists. This result is consistent with a simulation in which the flow field evolving from a pair of oblique waves is characterized by a rapid development into a turbulentlike state [20].

Quasiperiodic and chaotic solutions: For  $130.7 < R_*$ 157.5, we find *simple* quasiperiodic solutions, with  $A_1(t)$ ,  $r_2(t)$ , and  $r_3(t)$  periodic and  $A_2 = r_2(t)e^{i(\omega t + \beta)}$ ,  $A_3 =$  $r_3(t)e^{i(\omega t+\alpha)}$  quasiperiodic because of the appearance of the second frequency  $\omega$ . When 157.5  $< R_* < 166$ , we find complicated quasiperiodic solutions, meaning that  $A_1(t)$ is no longer periodic. The solutions appear complicated but some symmetries are preserved. In the interval 166  $\leq$  $R_*$  < 180, chaos and quasiperiodic solutions coexist.

n order to view the flow of these solutions in phase space we consider the three space of the fluid velocity itself  $(u, u_2, u_3)$  at some nominal location in space. Figure 1 depicts this behavior at three representative values of 157.5 the motion lies on a two-torus and this is seen in the control parameter  $R_*$ . In the range 130.7  $\lt R_*$ ig. 1(a). (This was calculated at Re= 156.) In the range 157.5  $R_*$  < 166 the motion lies on a three-torus. The orderliness of this motion is shown in Fig.  $1(b)$ (calculated at  $R_* = 158.4$ ). A typical example (drawn for  $R_* = 168$ ) of the chaotic range 166  $\lt R_* < 180$  is



FIG. 2. A comparison of the statistics with the full simulation; data from the original simulation are marked; the solid lines are from the model equations at  $R_* = 180$ . (a) A age Reynolds stress  $-\overline{uv}$ ; (b) root mean square velocity of streamwise component  $u_{\rm rms}$  and normal component  $v_{\rm rms}$ .



FIG. 3. The power spectrum at  $R_* = 180$ .

shown in Fig. 1(c). For special, nongeneric initial data quasiperiodic trajectories may also be found in this range. Although three-torus motion appears, it is not typical. The likely route to chaos follows the Ruelle-Takens scenario [21] in which three-torus motion experiences a symmetry breaking. This is in contrast with the heteroclinic cycle which is central to earlier models [12] and which is very likely an artifact of Galerkin projection [22].

The chaos which is found in this simple model shares a number of features found in large scale turbulent simulations. The amplitude and phase of propagating modes closely resembles typical curves found in the full simulation [4], and thus the propagation property is verifed. The components of  $(u)_{rms}$  and average Reynolds stress for the model are shown in Fig. 2 and although these are quantitatively different from what is found in the full simulation [4], the qualitative resemblance is striking. The temporal power spectrum shown in Fig. 3 also closely resembles that found in a more complicated model [10] and shows a second peak as indicated in recent experiments [23].

Real turbulence occurs as the result of countless interactions among roll-like and wavelike modes [4]. In the present investigations we have demonstrated a range of behavior for the basic triad interactions. This model is of a stereotypical type and captures fundamental features of wall-bounded turbulent flows. In a full simulation or a real experiment such triads may be regarded as interacting subsystems. Moreover, as we have argued in a limited sense these interactions appear to be relatively weak. If the table is expanded to include more modes, the interactions become more complex. Within a limited framework of computation we have shown that the interactions are relatively weak. We regard our model as a caricature or as being *impressionistic* [24]. Furthermore, it is a speculation that wall-bounded turbulence may be described by a (Re dependent) system of weakly interacting triads.

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