## Improved Energy Confinement in Spheromaks with Reduced Field Errors

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An increase in the global energy confinement time  $(\tau_E)$  was obtained in the CTX spheromak by replacing the high-field-error mesh-wall flux conserver with a low-field-error solid-wall flux conserver. The maximum  $\tau_E$  is now 0.18 ms, an order of magnitude greater than previously reported values of  $\leq 0.017$ ms. Both  $\tau_E$  and the magnetic energy decay time  $(\tau_W)$  now increase with central electron temperature, which was not previously observed. These new results are consistent with a previously proposed energyloss mechanism associated with high edge helicity dissipation.

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A spheromak' is a toroidal magnetic configuration with large internal plasma currents and self-generated internal magnetic fields. This configuration has been studied for many years with the hope that it would make an attractive fusion reactor. However, an apparent condemning feature of the spheromak for reactor use was the short global energy confinement times  $(\tau_F)$  previously reported,  $2.3$  in the 5-20- $\mu$ s range. It has been proposed that the dominant energy loss has been a consequence of enhanced helicity dissipation in the edge region of the spheromak induced by magnetic-field errors.<sup>2-4</sup> (Helicity<sup>5</sup> K is the quantitative measure of the "knottedness" of magnetic-field lines, i.e., flux linkage.) In the case of CTX with a mesh-wall flux conserver,  $2.6$ the field errors were due to the bridges crossing the midplane gap, the coarseness of the mesh, and the nonzero resistivity of the copper rods. Edge field lines either contacted the rods themselves, or the vacuum tank surrounding the flux conserver. It was estimated that approximately 25% of the poloidal flux intersected metal, and it appears that the resistivity of the open field lines was dominated by electron-neutral collisions<sup>2</sup> ( $\eta_{e,n}$  is much higher than  $\eta_{Spitzer}$  in this region). These field lines are influenced by the minimum-energy principle,  $7$ which states that  $\lambda = \mu_0 \mathbf{J} \cdot \mathbf{B} / ||\mathbf{B}||^2$  (where **J** is the current density and B is the magnetic field) should be a spatial constant. Therefore, current is driven on the highresistance open field lines, primarily by instabilities in the bulk plasma induced by  $\nabla \lambda$ . The exact nature of these instabilities is not yet understood, but it is generally accepted that they cause direct ion heating at the expense of magnetic energy  $(W)$ , giving<sup>2,3,6</sup> ion temperatures  $(T_i)$  higher than the electron temperature  $(T_e)$ . The enhanced decay rate of  $W$  (due to instabilities and direct ion heating) must be accompanied by an approximately equal helicity decay rate  $(\tau_K^{-1} \equiv -\dot{K}/K)$ , because  $W/K \propto \langle \lambda \rangle$  (volume-averaged  $\lambda$ ), which changes only slightly with  $\nabla \lambda$ . Enhanced  $\dot{K}$  is a direct result of large edge  $\eta$ **J**, since  $\overrightarrow{K} \propto \int_{\text{vol}} \eta \mathbf{J} \cdot \mathbf{B} d^3x$ . (One can think of this as enhanced "untying" of the "magnetic knot" in the resistive edge.) The severe impact on  $\tau_E$  came from high charge-exchange rates involving the hot, directly

heated, ions.  $2,3,6$  Another observation consistent with edge-dominated helicity decay was that both  $\tau_E$  and the global magnetic energy decay time  $(\tau_W)$  did not depend on the central electron temperature.<sup>2</sup> Observations and conditions in other spheromak devices are also consistent with this model.  $3,9$ 

In this Letter, we report the  $\tau_E$  results from CTX with a solid-wall flux conserver specifically designed to minimize magnetic-field errors. The significantly improved confinement, now as high as 0.18 ms, the observation that both  $\tau_W$  and  $\tau_E$  now depend on central electron temperature, and the apparent reduction of  $T_i/T_e$  by a factor of  $\approx$  3 (based on the  $T_d$  measurements discussed below) are all consistent with the above model. Reduced edge volume of high  $nJ$  lowers K to the point where central conditions have a significant contribution. The accompanying reduction in enhanced W reduces  $T_i/T_e$ , and  $\tau_E$  is improved by the reduction of charge exchange of hot ions.

The new flux conserver, shown in Fig. 1, is cylindrical with 0.61 m radius and 0.62 m length, and has 6.4-mmthick solid oxygen-free high-conductivity (OFHC) copper walls. All surface diagnostics (i.e.,  $B_{\text{wall}}$  probes) are recessed in the flux conserver wall, so that the plasma "sees" a very nearly smooth surface. In addition, the midplane gap (through which most of the optical diagnostics view) was carefully designed to minimize field errors in this region. As shown in Fig. 1, the solid-copper flanges on each flux conserver half are radially extended a distance equal to the midplane gap width, and connected by 48 evenly spaced "C clamps." This ensures that the small amount of spheromak flux that bulges into the midplane gap is still relatively far from the symmetrybreaking clamps. (Note that previous solid-wall ffux conservers<sup>10</sup> used in CTX were not designed for low field errors.) Clean discharges are obtained by depositing titanium on the plasma side of the flux conserver.<sup>11</sup> A small amount of bias field<sup> $12$ </sup> is applied (the bias flux inside the 0.61 m radius of the flux-conserver midplane is  $\leq$  5% of the spheromak poloidal flux), which was empirically found to increase the number of high-quality discharges obtainable  $(> 25)$  before regettering was



FIG. 1. The CTX low-field-error flux conserver. The entrance region, center plug, and flux conserver are all made from OFHC Cu. The electrodes are W-coated stainless steel. The Ti ball is shown in the position used for coating; it is retracted into the gun for spheromak operation. The positions of the  $B<sub>wall</sub>$  probes are indicated; the seven positions to the right of the "midplane" in the figure are replicated at four torodial angles. Also indicated is the probe installation method minimizing field errors. The equilibrium shown was calculated with a typical value of bias flux.

necessary. Satomi et al. have used solid-wall (potentially low-field-error) flux conservers with Ti gettering,  $13$ but  $\tau_F$  values have not been reported. The "center plug" (see Fig. I) was first installed with the mesh-wall flux conserver, and no differences in confinement were observed for those conditions.

The CTX diagnostics include an array of 32 wall poloidal magnetic-field probes used to determine both the magnetic equilibrium and any current-driven modal activity;<sup>14</sup> multipoint Thomson scattering absolutely calibrated for density using Raman scattering; an eightchord  $CO<sub>2</sub>$  interferometer with impact parameters (b) measured from the geometric symmetry axis ranging from 0 to 0.54 m; four bolometers for measuring radiation power; three monochromators typically used to measure time-dependent oxygen line radiation; and a polychromator for measuring impurity-ion Dopplerbroadened line emission.

A typical time evolution of a low-field-error CTX discharge is shown in Fig. 2. The plasma gun is energized at  $t = 0$  (H<sub>2</sub> gas is puffed into the gun beginning at  $t \approx -0.24$  ms), helicity injection begins at  $t \approx 0.15$  ms, and the spheromak energy is built up and sustained  $15$  until  $t \approx 0.7$  ms when the gun voltage is removed. Unlike previous operation, no backfill of neutral gas is used. The plasma continues to heat during the decay phase of the discharge, until the pressure gradient  $(\nabla P)$  becomes too large, and a  $\nabla P$ -driven instability expels the central plasma<sup>16</sup> (at  $t \approx 1.67$  ms in Fig. 2). To delay this instability as long as possible,  $H_2$  gas is puffed at the spheromak edge (see Fig. <sup>1</sup> for location of the valve) to



FIG. 2. A typical CTX discharge. Indicated are the toroidal plasma current as inferred from the  $B<sub>wall</sub>$  data, and line-averaged electron density from the central-beam  $(b=0.32)$ m) and edge-beam  $(b = 0.54 \text{ m})$  interferometer data. For this discharge,  $\tau_E$  was 0.15 ms at  $t = 1.51$  ms.

raise the edge density, thus reducing  $\nabla P$ . The timing of the valve opening is adjusted so that the edge density begins to rise just prior to the typical instability time without the edge puff (at  $t \approx 1.04$  ms in Fig. 2). Because the valve has a fixed plenum size, this technique is effective only in delaying the  $\nabla P$ -driven instability. The long-term spheromak behavior after the instability varies. If substantial plasma density is lost, extremely rapid decay of the plasma current begins  $\approx 0.1$  ms later. However, the spheromak can recover (and again have high  $\tau_E$ ) if sufficient density remains, but repeaking of the pressure profile will eventually trigger another event. Under some conditions, no large events are observed, but many small successive events leads to a complete loss of density in  $\approx 0.2$  ms.

In this Letter,  $\tau_E$  is reported for spheromak decay only, and  $\tau_E$  would be accurately determined by  $\dot{E} = -W - E/\tau_E$ , where  $E = \frac{3}{2} \int_{\text{vol}} (P_e + P_i) d^3x$ ,  $P_e$  $=n_e k T_e$ ,  $P_i = n_i k T_i$ , W is the total magnetic energy, and  $-\dot{W}$  is the total input power. Radiation losses, which might be as high as 80% of  $-\dot{W}$  (discussed below), have not been subtracted from the input power. It is customary to measure  $\tau_E$  during a steady-state phase of the discharge where  $\dot{E} \approx 0$ . In the discharges considered here, no clear steady state is reached; the plasma either is in a heating phase or is suffering or recovering from a  $\nabla P$  instability. Also, there are no diagnostics on CTX which can be used to estimate  $E$  as a function of time on a single discharge. A composite of Thomson scattering from many discharges is inaccurate because the data set is limited, and covers a large variation in discharge details. In this Letter, E is simply ignored, and  $\tau_E$  $\approx \frac{3}{2} \beta_{\text{vol}} \tau_W$ , where  $\beta_{\text{vol}} \equiv 2\mu_0 \sqrt{P_e + P_i} \sqrt{\frac{9}{\text{vol}}}/\sqrt{B^2} \sqrt{\frac{1}{\text{vol}}}$  is the volume-averaged beta, and  $\tau_W = -W/W$ . The error introduced is estimated to be no greater than  $\pm 25\%$  by noting that the inclusion of  $\dot{E}$  gives  $\frac{3}{2} \beta_{\text{vol}} \tau_W$ /

 $[1 + \frac{3}{2} (\beta_{\text{vol}} - \tau_W \beta_{\text{vol}})]$ , and the Thomson-scattering data indicate the "limits of plausibility' for an instantaneous  $\dot{\beta}_{\text{vol}}$  as  $-0.1 < \dot{\beta}_{\text{vol}} < 0.2$  ms<sup>-1</sup>.

The value of  $W(t)$  is obtained by doing a leastsquares-error fit of the  $B<sub>wall</sub>$  data by zero- $\beta$  equilibria calculated with the linear  $\lambda$  model.<sup>14</sup> The input power is obtained by applying (in order) a O. 1-ms square-window smoothing to  $W(t)$ , a simple two-point time derivative, and then a second 0.1-ms square-window smoothing.

The electron contribution to  $\beta_{\text{vol}}$  is determined from multipoint Thomson scattering, which gives  $n_e(r)$  and  $T_e(r)$  for r between 0.347 and 0.560 m [see Ref. 16 for typical  $P_e(r)$  profiles]. For typical equilibrium configuration, the function  $dV/dr$  vs r was calculated figuration, the function  $dV/dr$  vs r was calculated<br>for  $r_{\text{mag axis}} \le r \le r_{\text{wall}}$  along the midplane, where  $dV$  is the incremental volume between flux surfaces intersecting the midplane at r and  $r+dr$ , and  $\langle P_e \rangle_{\text{vol}} = V^{-1}$  $\frac{\partial f}{\partial r_{\text{max}}} P_e(r) (dV/dr) dr$ . Since half the volume is contained between 0.567 and 0.610 m, care must be taken in the extrapolation of  $P_e$  in this region. A linear extrapolation with the same slope as the last two data points is used (clipping at zero if this gives negative  $P_e$ ), unless this slope is positive, in which case a linear extrapolation from the last point to  $P_e(r_{\text{wall}}) = 0$  is used. The highest  $\tau_E$  values reported are insensitive to these details, because the measured  $P_e$  goes to essentially zero at some  $r \le 0.560$  m, and  $P_e = 0$  is used for larger r.

An accurate measure of the ion contribution to  $\beta_{\text{vol}}$  is not easily determined. The only  $T_i$  diagnostic available on CTX is a single-chord polychromator measuring Doppler-broadened impurity radiation<sup>6</sup> (usually  $Ov$ ), which gives a "temperature"  $(T_d)$ . Because of the lack of spatial profiles for  $T<sub>d</sub>$ , and the uncertainties introduced by associating  $T<sub>d</sub>$  with the true bulk ion temperature, the assumption  $T_i(x) = T_e(x)$  is made (same as-



FIG. 3. The global energy confinement time for all available data with the exception of five data points (see the text). The open circles represent data with  $P_{\text{max}}/\langle P\rangle_{\text{vol}} > 7$ . The line is a least-squares proportional fit to the solid-circle data. Radiation losses have not been subtracted from the input power.

sumption made in Ref. 2), and  $\langle P \rangle_{\text{vol}} = 2 \langle P_e \rangle_{\text{vol}}$ . The effects of correcting  $\tau_E$  based on measured  $T_d$  will be discussed below.

Figure 3 shows the obtained  $\tau_E$  values vs  $T_e$  at the magnetic axis for all available multipoint Thomsonscattering data with the low-field-error flux conserver, except those data points which are less than 0.015 ms after major VP-driven events, or within time periods of many small successive events (eliminates five data points with  $\tau_E \le 0.03$  ms). Figure 4 shows  $\tau_W$  for the same set of data. These data show a clear, approximately linear dependence of both  $\tau_E$  and  $\tau_W$  on the central value of  $T_e$ , in extreme contrast with the data from the mesh-wall flux conserver, where no dependence was found. Comparison with Spitzer resistivity is made by defining  $Z_{\text{eff}} = \mu_0/2\langle \lambda \rangle^2 \langle \eta_{\text{Spitzer}}^{Z=1} \rangle_{\text{vol}} \tau_W$ , and using  $\langle T_e^{3/2} \rangle_{\text{vol}}$  determined from the data. The  $Z_{\text{eff}}$  is  $\lt$  2 for 45% of the data, and  $\leq 4$  for 90% of the data, which is probably consistent with the impurity fraction (not measured directly).

In both figures, data which have a pressure peaking parameter  $(P_{\text{max}}/P_{\text{vol}})$  greater than 7 are indicated. The  $\tau_E$  for this subset of data correlate with  $T_e$ , but with reduced magnitude. For these data,  $\langle P \rangle_{\text{vol}}$  was calculated using  $P_e = 0$  in more than 55% of the volume. This may be an overly pessimistic calculation, or reduced  $\tau_E$ may be a real effect associated with large  $\nabla P_e$ . Note that there is no detriment to the  $\tau_W$  values for these cases. Resolution of this issue is beyond the scope of this Letter.

There has been a significant reduction of  $T<sub>d</sub>$  in the low-field-error discharges compared to the mesh-wall flux-conserver data. For mesh-wall flux-conserver discharges,<sup>6</sup> the only simultaneous measurements of  $T_d$ and  $T_e$  were at  $t = t_s = 0.3$  ms in condition 15804 from Ref. 2, giving  $T_d \approx 200$  eV,  $T_e \approx 30$  eV, and  $T_d/T_e \approx 7$  $(t<sub>s</sub>$  is the time at which sustainment ends and decay be-



FIG. 4. The global magnetic energy decay time for the same data as Fig. 3. The line is a least-squares proportional fit to all the data.

gins). Subsequently,  $T_d$  rose to  $\approx 350$  eV by  $t = t_s$  $\approx 0.6$  ms, and remained approximately constant thereafter. Data from other conditions in Ref. 2 indicate that  $T<sub>e</sub>$  increased in time, but measured values never exceeded  $\approx$  70-80 eV. Combined with an assumed  $T_d \approx 350$ eV, it is plausible that  $T_d/T_e$  dropped in time from  $\approx$  7 to  $\approx$  4. Simultaneous measurements of  $T_d$  and  $T_e$  during decay of low-field-error discharges show a maximum  $T_d/T_e$  of  $\approx$  4 at  $t - t_s \approx 0.4$  ms, which drops steadily to  $\approx$  1 by  $t - t_s \approx 0.7$  ms, and stays  $\approx$  1 thereafter. Further interpretation of  $T_d$  is beyond the scope of this Letter.

In principle, the  $\tau_E$  values should be corrected for the actual bulk ion temperature. The data discussed above give one limit;  $T_i = T_e$  (divide by 2 for the limit  $T_i = 0$ ). For another (upper) limit, the  $T_d$  value can be substituted, correcting  $\tau_E$  by the factor  $0.5(1 + \langle n_e \rangle_{\text{vol}} k T_d$  $\langle P_e \rangle_{\text{vol}}$ , which gives  $\tau_E \ge 0.2$  ms for 30% of the data, and a maximum  $\tau_E$  of 0.26 ms. The largest corrections are for data with  $\tau_E \lesssim 0.1$  ms in Fig. 3.

The substantial improvements in  $\tau_E$  and  $\tau_W$  indicate that enhanced edge helicity dissipation, and the accompanying consequences, have been overcome by careful design and construction of the flux conserver. The dependence of  $\tau_W$  on central  $T_e$  shows the edge volume no longer dominates in determining the plasma resistance. Hot-ion charge exchange no longer dominates in determining  $\tau_E$ . The bolometer data indicate that 70% to 80% of the magnetic energy dissipated before the onset of large negative  $I_{\text{tor}}$  (at  $t \approx 1.76$  ms in Fig. 2) appears as radiation. (The remaining magnetic energy does not appear as radiation.) Since the plasma continually heats during this time, this level of radiation loss does not represent an important limitation for the achievable plasma temperature in these discharges. Reduced radiation power would lead to a faster heating rate, and the VP-driven instability threshold would be reached quicker. (This instability has been observed as early as  $t \approx 1.1$  ms.<sup>16</sup>) Only the **VP**-driven instability

presently limits further heating, and thus, further increases in  $\tau_W$  and  $\tau_E$ . The theoretical  $\beta$  limits can be increased considerably by proper shaping of the spheromak boundary.<sup>9</sup> Experiments using a properly shaped lowfield-error flux conserver are needed to further test confinement limits in spheromaks.

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