

## Monte Carlo Calculation of Free Energy, Critical Point, and Surface Critical Behavior of Three-Dimensional Heisenberg Ferromagnets

M. P. Nightingale

*Department of Physics, University of Rhode Island, Kingston, Rhode Island 02881*

and

H. W. J. Blöte

*Laboratorium voor Technische Natuurkunde, 2600 GA Delft, The Netherlands*

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A transfer-matrix Monte Carlo technique is developed to compute the free energy of three-dimensional, classical Heisenberg ferromagnets. From the free energy of systems with periodic and antiperiodic boundary conditions, helicity moduli are calculated. From these the critical couplings for simple cubic (sc) and face-centered cubic lattices are estimated, by use of finite-size scaling. For the sc lattice, the critical dimension of the surface magnetization is estimated with standard Monte Carlo methods, yielding a result in excellent agreement with the  $\epsilon$ -expansion work of Diehl and Nüsser.

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Transfer matrices are widely used in numerical studies of statistical mechanical systems in two dimensions with discrete microscopic degrees of freedom.<sup>1</sup> In three dimensions, numerical calculation of eigenvalues of transfer matrices become intractable already for small systems: a  $5 \times 5 \times \infty$  Ising model in  $2+1$  dimensions seems to be the current upper limit.<sup>2</sup> Systems with continuous degrees of freedom, with the exception of linear chains, are even more of a challenge.

Here, we combine Monte Carlo (MC) and transfer-matrix techniques to tackle a three-dimensional Heisenberg model and directly calculate free energies in terms of the transfer-matrix eigenvalues for lattices up to  $10 \times 10 \times \infty$ . The method is a variant of the Green's-function MC method,<sup>3</sup> of which there have been some preliminary applications to the three-dimensional Ising model.<sup>4</sup>

Consider a lattice in three dimensions with  $N$  sites:  $n_z$  layers of  $m = n_x n_y$  sites each. We chose helical boundary conditions to obtain a single, sparse transfer matrix, and label the sites with one index  $i = 1, \dots, N$ . Sites  $1, \dots, m$  and  $N - m + 1, \dots, N$  form the bottom and top surfaces. For a general lattice, each nearest-neighbor bond features precisely once in the list  $(i, i - d_\alpha)$ ,  $i = 1, \dots, N$ , and  $\alpha = 1, \dots, c$ , up to end effects. The  $c$  displacements  $d_\alpha$  define the lattice:  $c = 3$  with  $d_1 = 1$ ,  $d_2 = n_x$ , and  $d_3 = m$  yields the simple cubic (sc) lattice; for the face-centered cubic (fcc) lattice, add  $d_4 = m - 1$ ,  $d_5 = m - n_x$ , and  $d_6 = m - n_x - 1$ . At each site  $i$  there is a spin, a three-component unit vector  $\mathbf{s}_i$ . The reduced Hamiltonian is

$$-\beta \mathcal{H} = \sum_{i=1}^N \sum_{\alpha=1}^c \mathbf{s}_i' \cdot \mathbf{s}_{i-d_\alpha}' \quad (1)$$

where  $\mathbf{s}_i' = \mathbf{s}_i \sqrt{K}$  for coupling constant  $K$  ( $\mathbf{s}_i' = 0$  for

$i < 0$ ). Integration of the Boltzmann weights over all  $\mathbf{s}_i$  with  $i \leq N - m$  gives a partition function:

$$Z_N(S_N^{N-m+1}) = \int \dots \int dS_1^{N-m} e^{-\beta \mathcal{H}}, \quad (2)$$

where  $S_i^j = (\mathbf{s}_i, \dots, \mathbf{s}_j)$ . With general  $m$ -uples of spins  $U = (\mathbf{u}_1, \dots, \mathbf{u}_m)$  and  $V$ , we define a transfer matrix  $\mathbf{T}$  that adds one site to the lattice:

$$\mathbf{T}(U|V) = \exp \left[ \mathbf{u}_1 \cdot \sum_{\alpha} \mathbf{v}_{d_\alpha} \right] \prod_{i=2}^m \delta(\mathbf{u}_i, \mathbf{v}_{i-1}),$$

where the  $\delta$  functions are normalized such that

$$Z_{N+1}(U) = \int \dots \int \mathbf{T}(U|V) Z_N(V) dV. \quad (3)$$

As  $N \rightarrow \infty$ , the dimensionless free energy ( $f$ ) per site is given in terms of the dominant eigenvalue ( $\lambda_0$ ) of  $\mathbf{T}$  by  $f = -\ln \lambda_0$ .

To implement the power method to obtain this eigenvalue, the matrix multiplication in Eq. (3) is represented by a random process, the so-called transfer-matrix MC method. Introduce a sequence of random walkers  $R_t = (S_t, w_t)$ ,  $t = 1, \dots, r$ :  $S_t = (\mathbf{s}_1^t, \dots, \mathbf{s}_m^t)$  represents a layer configuration of statistical weight  $w_t \geq 0$ . We maintain  $r$  within a few percent of a target  $r_0$ ; the weights are kept in the range  $b_l < w_t < b_u$ , with  $b_l \approx \frac{1}{2}$  and  $b_u = 2$ . Rewrite  $\mathbf{T}(S'|S) = P(S'|S)D(S)$ , with a normalization  $D(S)$  independent of  $S'$ , such that  $P(S'|S)$  is a probability density for a transition from  $S$  to  $S'$ . An MC run consists of sweeps  $t = 1, \dots, M$  over all random walkers. At time  $t$  there are two steps. Affixing primes to variables at time  $t+1$ , we define step (1): For  $t = 1, \dots, r$  change  $R_t$  to  $R_t' = (S_t', w_t')$  according to  $P(S_t'|S_t)$ , with  $w_t' = D(S_t)w_t/c'$ . With  $\hat{\lambda}_0$  a running estimate of  $\lambda_0$ , choose  $c' = \hat{\lambda}_0 r / r_0$  to maintain  $r$  close to  $r_0$  in step (2): From the  $R_t'$  construct a new sequence

using each walker precisely once: (a) If  $w'_i > b_u$ , add two random walkers ( $S'_i, \frac{1}{2} w'_i$ ) to the new sequence; (b) form pairs ( $S'_i, w'_i$ ) and ( $S'_k, w'_k$ ) with  $w'_i < b_l$  and  $w'_k < b_l$ , and add ( $S'_\lambda, w'_i + w'_k$ ), where  $S'_\lambda = S'_i$  or  $S'_\lambda = S'_k$  with relative probabilities  $w'_i$  and  $w'_k$ ; (c) if  $b_l < w'_i < b_u$ , or if  $R_i$  is left unpaired in step (b) add  $R'_i$ . The walkers represent a vector  $\Phi$  with components

$$\Phi(U) = \sum_{i=1}^r w_i \delta(s_i, u_1) \cdots \delta(s_m, u_m). \quad (4)$$

Denote the vector realized in sweep  $t$  by  $\Phi_t(U)$ . The crux of the method is that

$$\left\langle \prod_{b=1}^{\tau} c_{t+b} \Phi_{t+b}(U) \right\rangle = T^{\tau} \Phi_t(U), \quad (5)$$

where the angle brackets denote the average over all processes starting from the vector  $\Phi_t(U)$ . An estimator<sup>5</sup> of the dominant eigenvector  $\Psi_0$  of the transfer matrix is

$$\Psi_0(U, \tau) = \frac{1}{M} \sum_{t=1}^M \left[ \prod_{b=0}^{\tau} c_{t-b} \Phi_t(U) \right]. \quad (6)$$

This is the iterate of order  $\tau$  in the power method, and as such it has a bias for any  $\tau < \infty$ ; its variance increases with  $\tau$ . As a compromise we chose the largest  $\tau$  with a statistically significant nonzero estimate of the autocorrelation at lag  $\tau$  of  $c_t$ . The dominant eigenvalue of the transfer matrix is given by  $\lambda_0 \approx W_0(\tau+1)/W_0(\tau)$ , where  $W_0$  is the integral of  $\Psi_0(U, \tau)$  over  $U$ . As  $\Psi_0(U)$  for  $N \rightarrow \infty$  is the probability density of a surface configuration  $U$ , the multiplication of Eq. (6) through by a spin function and integration over  $U$  yields surface correlations.

We applied the same method to systems with antiperiodic boundary conditions: Each of the  $n_z$  planes had two seams related by translations by a vector between sites 0 and  $n_x n_y$ . One seam was in the  $y$  direction, the other in the  $x$  direction, except for a single step in the  $y$  direction forced by the helical boundary conditions. Along bonds across the seam the coupling was  $-K$ , instead of  $K$ .

The critical coupling  $K_c$  was obtained as follows. Denote the dimensionless free energies per site of the periodic and antiperiodic systems by  $f_+$  and  $f_-$ ; write  $\Delta = K_c - K$ . For  $n_x = n_y = n$  and small  $|\Delta|$  one has the scaling relation

$$n^d (f_+ - f_-) = H(n^{\nu_T} \Delta) \approx H_0 + H_1 n^{\nu_T} \Delta$$

in  $d=3$  dimensions<sup>6</sup>;  $H$  is the helicity scaling function, and the correlation length diverges as  $\Delta^{-\nu}$ , where  $\nu_T = \nu^{-1}$ . With  $K_c$ ,  $H_0$ , and  $H_1$  as parameters, we made least-squares fits to data for several  $K$  and  $n$  values. In most runs the target number  $r_0$  was 2500. With a number of sweeps that added roughly 5000 layers, this amounts to  $12.5 \times 10^6$  flips per spin in total.

Figure 1 shows  $H$  vs  $n$  on an  $n^{\nu_T}$  scale for various  $K$ ,

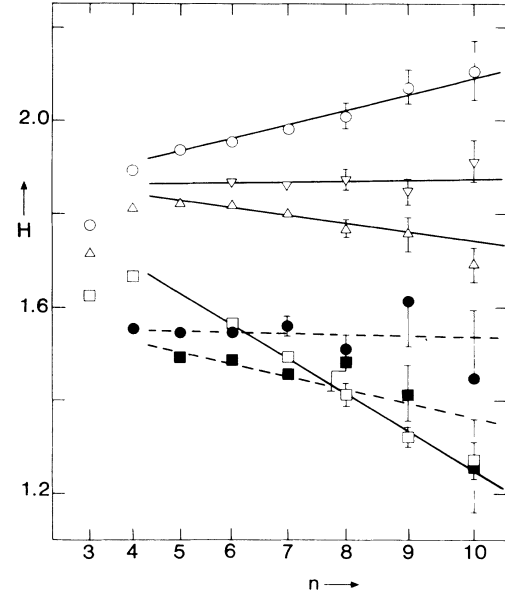


FIG. 1. Helicity modulus scaling function vs  $n^{1.418}$  for various coupling strengths  $K$ . Open symbols represent data for the sc lattice:  $K=0.695$  (circles),  $0.6922$  (inverted triangles),  $0.6904$  (triangles), and  $0.68236$  (squares); filled symbols are fcc data:  $K=0.316$  (circles) and  $0.31489$  (squares). For  $n=10$ , two squares almost coincide; the fcc datum point has the longer error bars. Solid (sc) and dashed (fcc) lines illustrate linear behavior near criticality for  $n > 5$ .

for both the sc and fcc lattices. To check for finite-size effects, we systematically increased the size of the smallest system included in the fits. The results (and standard errors) are as follows: For the sc lattice,  $K_c = 0.6922(2)$  and  $0.6925(3)$ , for sizes 5 and up and 6 and up, respectively; for the fcc lattice,  $K_c = 0.3162(3)$ ,  $0.3160(2)$ , and  $0.3170(5)$ , for sizes 4 and up, 5 and up, and 6 and up. In the fits we used<sup>7</sup>  $\nu_T = 1.418$ . The  $K_c$  for the sc case agrees well with results of Ritchie and Fisher,<sup>8</sup> and of Ferer<sup>9</sup> obtained from eight- and twelve-term series. Agreement is less satisfactory with a ten-term-series estimate of Ohno, Okabe, and Morita<sup>10</sup> who find  $K_c \approx 0.68236$ . For the fcc lattice the agreement with the result<sup>11</sup>  $K_c = 0.3149(2)$  is reasonable. The values of  $K$  around  $K_c$  were not chosen optimally to estimate the bulk thermal exponent, yet we have data for the sc lattice over a sufficiently wide range of couplings to obtain least-squares estimates:  $\nu_T = 1.406(55)$  and  $1.396(78)$  for sizes 5 and up and 6 and up, respectively.

The transfer-matrix method was also used to calculate surface correlations for the Heisenberg system. Only for small systems was a variance obtained smaller than with a standard MC algorithm,<sup>12</sup> and so only results of the latter will be discussed here. We used finite sc lattices with sites  $(x, y, z)$ , with  $x$ ,  $y$ , and  $z$  ranging from 1 to  $n_x = n_y = n$  and  $n_z = 2n$ , respectively, free boundaries at  $z=1$  and  $z=n_z$ , and helical or periodic boundary condi-

tions in  $x$  and  $y$  directions. Up to boundary effects, the Hamiltonian was that of Eq. (1). Also, couplings with and within the surface were redefined via  $s'_i = s_i \sqrt{K_s}$ , where  $K_s = \epsilon K$  with enhancement factor  $\epsilon$ . We calculated the surface susceptibility

$$\chi_{11} = n^{-2} \left\langle \sum \mathbf{s}_{x,y,z} \cdot \mathbf{s}_{x',y',z} \right\rangle,$$

summing over all sites  $(x,y,z)$  and  $(x',y',z)$  on one surface; the angle brackets denote the thermal average. We also calculated the surface correlation  $g_n$  halfway across the system:

$$g_n = n^{-2} \sum_x \sum_y \langle \mathbf{s}_{x,y,z} \cdot (\mathbf{s}_{x+n/2,y,z} + \mathbf{s}_{x,y+n/2,z} + \mathbf{s}_{x+n/2,y+n/2,z}) \rangle,$$

identifying sites  $(x,y,z)$  and  $(x',y',z)$ , if  $|x-x'|=n$ , or  $|y-y'|=n$ . With  $\chi_{11}$  and  $g_n$  we estimated the surface critical exponent  $y_{H_1}$ , which, e.g., yields the surface susceptibility exponent with  $\gamma_{11} = (d' - 2y_{H_1})/y_T$ , where  $d' = 2$ .

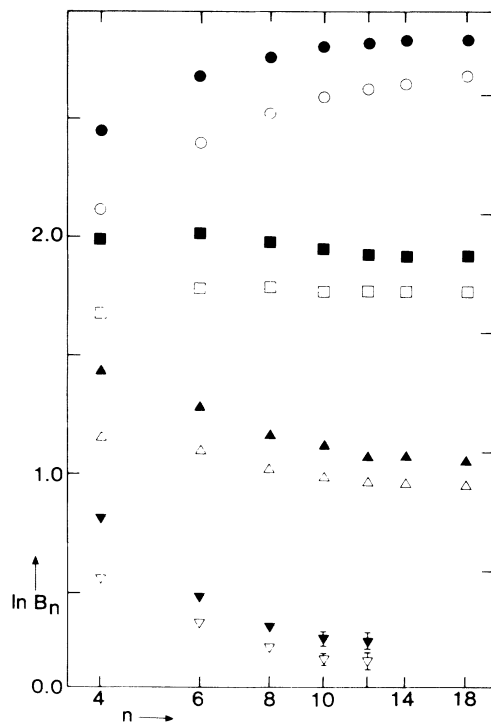


FIG. 2. Scaling behavior of surface correlation function  $g_n$ :  $\ln B_n$  vs  $n$  on a  $\ln n$  scale for several values of the surface enhancement  $\epsilon$ , where  $B_n = g_n \exp[(4 - 2y_{H_1}) \ln n]$ , with  $y_{H_1} = 0.8$  from our numerical analysis. According to scaling,  $B_n$  is finite and nonzero for  $n \rightarrow \infty$ . Filled and open symbols are for cylindrical and helical boundary conditions, respectively:  $\epsilon = 1.0$  (circles),  $0.83$  (squares),  $0.66$  (triangles), and  $0.5$  (inverted triangles). To avoid overlap, data points for cylindrical systems are shifted upward by  $0.1$  (see tick marks on the right-hand side). Error bars are shown where they exceed the size of the symbols.

The MC estimates were obtained from one or several runs of  $2 \times 10^5$  flips per spin. To obtain a vectorizable algorithm, spins were flipped sequentially on sublattices, such that nearest neighbors were on different sublattices. For periodic lattices of even size this is simple: They are bipartite. Helical systems had  $p$  sublattices  $L_i$ :  $L_i$  consists of sites  $i + kp$  ( $k = 0, 1, \dots$ ), with  $p$  the smallest integer relatively prime to  $n$  and  $n^2$ .

The MC data (see Figs. 2 and 3) were analyzed with finite-size scaling. The  $\gamma_{11}$  were fitted<sup>13</sup> with  $\chi_{11}(n) \approx \chi_{11}(\infty) + An^g$ , where  $g = d' - 2y_{H_1}$ . The  $g_n$  have strong corrections to scaling and were fitted with  $g_n \approx (B + C/n)n^h$ , where  $h = 2(y_{H_1} - d')$ . A renormalization-group argument suggests the origin and sign of this correction. Simply assume that the surface fixed point<sup>14</sup> is characterized by a single, nearest-neighbor interaction  $K_s^*$ . At bulk criticality  $K_s$  will tend towards  $K_s^*$  under renormalization. As the number of renormalizations required to calculate correlations grows with distance, they will decay with an effective exponent  $y_{H_1}$  which decreases with distance for  $K_s > K_s^*$  and vice versa. Scaling<sup>15</sup> and  $\epsilon$ -expansion<sup>16</sup> arguments suggest the naive

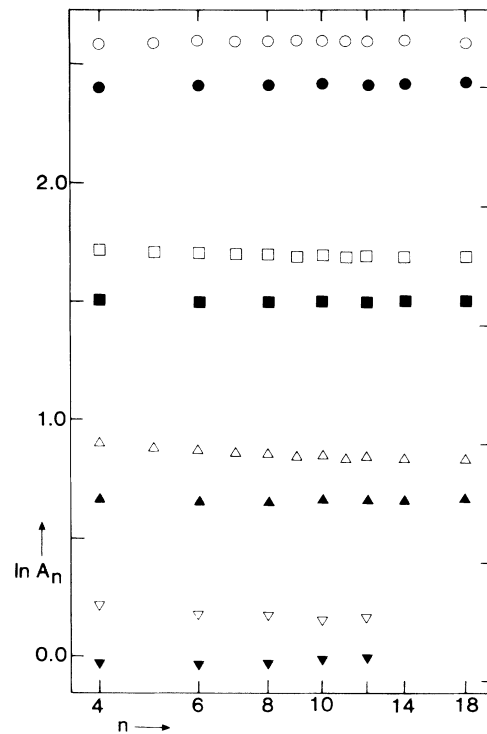


FIG. 3. Scaling behavior of surface susceptibility  $\chi_{11}$ :  $\ln A_n$  vs  $n$  on a  $\ln n$  scale for several values of the surface enhancement  $\epsilon$ , where  $A_n = [\chi_{11}(\infty) - \chi_{11}(n)] \exp[(2y_{H_1} - 2) \ln n]$ , with  $y_{H_1} = 0.8$  and  $\chi_{11}(\infty) = 11.25, 6.05, 3.65,$  and  $2.50$  for  $\epsilon = 1.0, 0.83, 0.66,$  and  $0.5$  from our numerical analysis. For the key to the symbols see Fig. 2. To avoid overlap, data points for cylindrical systems are shifted upward by  $0.1$  (see tick marks on the right-hand side). The statistical errors in the data do not exceed the size of the symbols.

TABLE I. Estimates of surface critical exponent  $y_{H_1}$  obtained from least-squares fits to surface susceptibility and correlation data for both helix and cylinder boundary conditions. Results are labeled by  $n$ , the smallest system size included in the various fits.

$n$	$\chi_{11}$		$g_n$	
	Helix	Cylinder	Helix	Cylinder
4	0.804(11)	0.778(07)	0.696(11)	0.685(12)
5	0.809(10)			
6	0.792(11)	0.806(11)	0.753(14)	0.770(18)
7	0.793(17)			
8	0.774(21)	0.791(24)	0.785(23)	0.784(32)
9	0.801(36)			
10	0.776(50)	0.699(49)	0.823(36)	0.821(72)

value  $-1$  for the correction-to-scaling exponent. The analysis of  $\chi_{11}$  required no such correction. Estimates of  $y_{H_1}$  were obtained from  $\chi_{11}$  and  $g_n$  for several enhancements  $\epsilon$ , both for cylinders and helices. Table I summarizes the results. We attribute the deviations at the top and bottom of Table I to finite size and too small a range of system sizes, respectively, and find  $y_{H_1} = 0.80 \pm 0.03$ . This confirms the  $\epsilon$ -expansion value<sup>17</sup>  $y_{H_1} = 0.809 \pm 0.014$ , the series estimate<sup>10</sup>  $y_{H_1} = 0.85 \pm 0.06$ , a previous MC result<sup>18</sup>  $y_{H_1} = 0.87 \pm 0.14$ , and the experimental value<sup>19</sup>  $y_{H_1} = 0.83 \pm 0.06$ .

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