[7]Preliminary results from the Magnetic Detector Group of the Stanford Linear Accelerator Center—Lawrence Berkeley Laboratory collaboration at SPEAR (W. Chinowsky, private communication).

[8]B. Knapp *et al.*, Phys. Rev. Lett. 34, 1040 (1975). Electroproduction has been observed at the Stanford Linear Accelerator Center and the two groups agree with each other (D. M. Ritson *et al.*, to be published).

[9]C. G. Callan and D. J. Gross, Phys. Rev. Lett. 22, 156 (1969).

[10]The same calculation can be done for two-φ production in NN collision. However, because of the φ mass being much smaller than the ψ mass $[m_\varphi^2 \simeq (\frac{1}{9})m_\psi^2]$, distinction between an elementary φ exchange and a Reggeized φ exchange is far less clear (different only by a factor of ~ 10 with $\eta_0 \simeq 2$), and no high-energy production data are available except for a loose upper bound indirectly set by a measurement of large-transverse-momentum muons. [J. A. Appel *et al.*, Phys. Rev. Lett. 33, 722 (1974)]. The Reggeized φ of normal slope ($\simeq 1$ GeV^{-2}) is fully consistent with this upper bound.

[11]Appel, Ref. 10.

[12]The lepton pairs from single-ψ production do not seem to explain all of the excess. L. M. Lederman, Columbia University Report (to be published).

[13]Production of ψ has been observed very recently in n-Be collision at Fermi National Accelerator Laboratory [B. Knapp *et al.*, Phys. Rev. Lett. 34, 1044 (1975)].

ERRATUM

NEW THEORY OF COERCIVE FORCE OF FERROMAGNETIC MATERIALS. R. Friedberg and D. I. Paul [Phys. Rev. Lett. 34, 1234 (1975)].

We correct a factor of 4 error in our normalization of the defect parameter $W[(\alpha_1/\alpha_2) - (\beta_2/\beta_2)]$ to the material Fe-Si4%. The revised table given below improves the theory inasmuch as the expansion parameter, h, is now less that 0.06 for all materials. Further, page 1236, line 7 should read that the constants C_1 and C_3 have the values $-2HS_1$ and $+2HS_1$, respectively.

TABLE I. Values of the coercive force due to grain boundaries. We assume the values $W = 6\times10^{-8}$ cm, $\alpha_1/\alpha_2 = 1.1$, $\beta_2/\beta_1 = 0.85$, and $S_1/S_2 = 1$.

Material	S_1 Magnetization	$(\frac{1}{2})\beta_1$ Anisotropy (ergs/cm^{3}x10^{-5})	$(\frac{1}{2})\alpha_1$ Exchange (ergs/cmx10^6)	$2\delta_1$ - Domain Wall Width (cmx10^6)	h Expansion Parameter	H_c-Coercive Force (Oersteds)	Observed Coercive Force
Supermalloy	630.	0.015	1.5	64.	0.0002	[a]0.0004	0.002
Permalloy	860.	0.02	2.0	64.	0.0002	[a]0.0006	0.05
[b]Iron-Si3%	1590.	3.7	2.2	4.8	0.0009	0.2	0.1
Iron-Si4%	1570.	3.2	2.1	5.2	0.003	0.5	0.5
Nickel	485.	0.7	0.5	5.2	0.003	0.3	0.7
Iron	1707.	4.8	2.4	4.4	0.003	0.7	1.
Cobalt	1400.	45.	4.7	2.0	0.007	20.	10.
[c]Alnico	915.	260.	2.0	[c]0.56	0.024	600.	600.
Co_5Sm	800.	1500.	2.0	0.24	0.056	9000.	10000.

[a]For these materials, the coercive force may be dominated by magnetostatic effects. In particular, for Permalloy, the rapid quenching of the disordered state should produce high stress fields and a Kondorsky-Néel-type contribution to the coercive force.

[b]This material is grain oriented. Therefore, we use $W = 2\times10^{-8}$ cm.

[c]Modern theory suggests a spin-rotation mechanism rather than domain-wall motion for Alnico. We have used an effective anisotropy taken from theoretical estimates of the intrinsic coercive force.