Quantum Enhanced Balanced Heterodyne Readout for Differential Interferometry

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Conventional heterodyne readout schemes are now under reconsideration due to the realization of techniques to evade its inherent 3 dB signal-to-noise penalty. The application of high-frequency, quadratureentangled, two-mode squeezed states can further improve the readout sensitivity of audio-band signals. In this Letter, we experimentally demonstrate quantum-enhanced heterodyne readout of two spatially distinct interferometers with direct optical signal combination, circumventing the 3 dB heterodyne signal-to-noise penalty. Applying a high-frequency, quadrature-entangled, two-mode squeezed state, we show further signal-to-noise improvement of an injected audio band signal of 3.5 dB. This technique is applicable for quantum-limited high-precision experiments, with application to searches for quantum gravity, searches for dark matter, gravitational wave detection, and wavelength-multiplexed quantum communication.

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Quantum enhancement techniques, such as the application of squeezed states of light, have improved the quantumlimited signal-to-noise ratio (SNR) in many precision measurements, including gravitational wave detection [1–4], magnetometry [5], biosensing [6], and plasmonics [7]. Squeezed states are also a major interest for quantum communication [8]. The long-developed ubiquitous methods of homodyne detection [9] and heterodyne detection [10] are critical to the success of applying squeezed states. Balanced homodyne detection, where the signal sidebands are symmetric around the local oscillator (LO) field, continues to be applied in many quantum metrology areas, including measuring highly squeezed states [11] and future gravitational wave detectors [12]. However, for low-frequency sensitivity, care is needed to avoid technical noise sidebands on the LO field affecting the measurement [13,14].

To circumvent the technical challenges of producing, controlling, and utilizing low (or audio-band) frequency squeezed light [13,15–17], several theoretical techniques have been proposed revolving around heterodyne readout schemes [10]. Heterodyning is commonplace in several experiments such as light detection and ranging (LIDAR) [18], vibrometry [19], spectroscopy [20], and laser stabilization [21]. Heterodyning offers an essential advantage of innate resistance to low-frequency technical noise on the LO due to the significant frequency separation between it

and the signals of interest. The sideband structure of a typical heterodyne experiment has a single-sided signal sideband and dual-sided vacuum noise sidebands [10]. Compared to homodyne detection techniques, where both signal and noise have a dual-sided sideband structure, heterodyne detection suffers from a 3 dB reduction in the overall SNR.

This SNR penalty can be evaded with a two-carrier approach, introducing coherent signals at positive and negative frequencies relative to the LO [9,22]. Further SNR improvement is possible using two-mode squeezed states [23]. Avoiding the LO noise coupling and challenges of low-frequency squeezing makes two-carrier heterodyning an attractive alternative to homodyne detection for quantum-enhanced interferometry-based sensors [24,25]. Additionally, two-carrier heterodyning can provide an all-optical differential readout method for twin sensors, such as those used for tests of quantum gravity in correlated space-time volumes [26–28] and searches for dark matter candidates [29,30].

Applying a two-mode squeezed state to a twin interferometer can increase the SNR, which has been theoretically investigated for gravitational wave detectors [24,25], and interferometric tests of quantum gravity [31,32]. Two-mode squeezed states have been experimentally investigated in application to twin-interferometer [28] and single interferometer designs [33–35]. These works rely on the use of homodyne readout and digital filtering.

In this Letter, we experimentally demonstrate a quantumenhanced heterodyne readout of two spatially distinct interferometers with direct optical signal combination.

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We circumvent the 3 dB heterodyne SNR penalty, showing further SNR improvements by applying two-mode squeezing generated with a frequency-nondegenerate optical parametric oscillator (OPO). We provide an alternative to the conventional homodyne readout without compromising on sensitivity, an approach that can reduce the complexity of real-time quantum communication experiments [36,37]. Our scheme is of particular interest for correlated interferometry experiments [26-28,31,32,38], dark matter detectors [29,30], and gravitational wave detectors [24,25], allowing flexibility in the choice of readout quadratures and quadrature combinations. In application to these detectors, this readout scheme may provide access to signal- and null-data streams simultaneously. Using a frequency-nondegenerate OPO to produce two-mode squeezing minimizes technical complexity compared to the widely used method in quantum teleportation [39] (via optical combination of two degenerate squeezed states), as highlighted in [40]. Additionally, our method of squeezed state generation reduces inherent losses compared to previous twin-interferometer demonstrations [28].

The experimental setup is illustrated in Fig. 1. Two spatially separate Michelson interferometers are probed with 40 uW *s*-polarized upper ($\omega_0 + \Delta$) and lower ($\omega_0 - \Delta$) carrier fields, frequency separated by $2\Delta = 850$ MHz, and operated close to the dark fringe. We generate the two carrier fields by strongly modulating a portion of the primary 1064 nm laser field with an electro-optic modulator (EOM), driven at $\Delta = 425$ MHz, then spatially separated for use in the interferometers. The carrier field preparation is not shown in Fig. 1. A signal ($\Omega = 25$ kHz) is introduced into each interferometer through piezoelectric-transducer (PZT) driven end mirrors, resulting in a frequency diagram as shown in Fig. 1(a). After spatial recombination on the combining cavity, the interferometers' output fields are simultaneously measured.

P-polarized auxiliary control fields (not shown in Fig. 1) are generated with birefringent optics before each interferometer. Further birefringent optics are used to break the degeneracy of *s* and *p* polarization in the interferometers. This allows us to lock the interferometers with a *p*-polarized field on the mid-fringe in reflection while simultaneously ensuring a dark fringe for the *s* polarization in transmission. The combining cavity is length controlled using the lower carrier auxiliary field, sensed on reflection. The frequency nondegeneracy between *s* and *p* polarization of the cavity is negligible by design. The auxiliary *p*-polarization fields are reflected from the Faraday isolator, and their beat note forms the control signal between the two carriers, and fed back to a PZT-actuated mirror, thus setting ϕ .

The carrier fields are measured using balanced detection, after combination with the LO (at ω_0) on a 50:50 beam splitter. Frequency diagrams of the fields after the beam splitter are shown in Figs. 1(b) and 1(c). The beam splitter outputs are then sent to a high-bandwidth balanced detector (similar to the one used in [41]). Our readout scheme electronically



FIG. 1. Simplified schematic of the experiment, showing the twin-Michelson interferometer (Twin Mich) outputs that are spatially overlapped with a combining cavity (CC), and phase locked (relative phase ϕ). The combined fields pass through a Faraday isolator (FI) towards the balanced detector. A two-mode squeezed state, produced by the optical parametric oscillator (OPO), is injected via the Faraday isolator, with each mode being reflected off an interferometer. A flipper mirror (FM) is used for direct squeezing measurement. Michelson carrier field preparation and polarization auxiliary fields are not shown for clarity. The LO phase (θ_{LO}) and squeezed quadrature angle (θ_{sq}) are also shown. (a) Frequency diagram of each interferometer carrier with $\pm \Omega$ signal sidebands. (b) and (c) Frequency diagrams of fields at the balanced detector with in-phase ($\phi = 0$) and out-of-phase ($\phi = \pi$) carriers.

demodulates the subtracted photocurrent at $\Delta = 425$ MHz, extracting the audio-frequency signals that modulate the highfrequency LO-carrier beat notes. The LO field is stabilized to a 550 kHz amplitude modulation sideband on the upper carrier. This beat note at the balanced detector provides a control signal to a PZT-actuated mirror on the LO path, setting the LO phase $\theta_{LO} = 0$. Control of both θ_{LO} and ϕ gives the choice of coherent signal addition or cancellation.

Electronically demodulating the heterodyne's subtracted photocurrent output yields information about the sum and difference of the two interferometers quadratures [37]. Defining the amplitude quadrature, \tilde{X}_1 , and phase quadrature, \tilde{X}_2 , of the upper and lower interferometers as $\tilde{X}_{(1,2)}^{\pm\Delta} = \tilde{X}_{(1,2)}(\omega_0 \pm \Delta)$, the in-phase photocurrent \tilde{i}_I is proportional to

$$\tilde{i}_I(\theta_{\rm LO} = 0, \phi = 0) \propto \frac{1}{2} \left(\tilde{X}_1^{-\Delta} + \tilde{X}_1^{+\Delta} \right), \tag{1}$$

$$\tilde{i}_I(\theta_{\rm LO} = 0, \phi = \pi) \propto \frac{1}{2} \left(\tilde{X}_1^{-\Delta} - \tilde{X}_1^{+\Delta} \right).$$
(2)

Conversely, when demodulating in-quadrature, the resulting photocurrent, \tilde{i}_Q , contains information about the difference or sum of the phase quadratures of the two interferometers:

$$\tilde{i}_{\mathcal{Q}}(\theta_{\rm LO}=0,\phi=0) \propto \frac{1}{2} \left(\tilde{X}_2^{-\Delta} - \tilde{X}_2^{+\Delta} \right), \tag{3}$$

$$\tilde{i}_{\mathcal{Q}}(\theta_{\rm LO}=0,\phi=\pi) \propto \frac{1}{2} \Big(\tilde{X}_2^{-\Delta} + \tilde{X}_2^{+\Delta} \Big). \tag{4}$$

Changes to θ_{LO} and ϕ result in a mixing of the carrier quadratures. The demodulated photocurrents in Eqs. (1)–(4) can be generalized with the substitutions $\tilde{X}_{(1,2)}^{-\Delta} \rightarrow \cos(\theta_{\text{LO}})\tilde{X}_{(1,2)}^{-\Delta} + \sin(\theta_{\text{LO}})\tilde{X}_{(2,1)}^{-\Delta}$ and $\tilde{X}_{(1,2)}^{+\Delta} \rightarrow \cos(\phi - \theta_{\text{LO}})\tilde{X}_{(1,2)}^{+\Delta} + \sin(\phi - \theta_{\text{LO}})\tilde{X}_{(2,1)}^{+\Delta}$.

For this work, we focus on analyzing the amplitude quadrature signal dynamics [Eqs. (1) and (2)], motivated by the preferential coupling of differential arm-length modulation to amplitude modulation in interferometers at a neardark fringe. For signals preferentially appearing in one quadrature, setting incorrect θ_{LO} or ϕ will result in loss of signal. For the remainder of this Letter, θ_{LO} is always set to zero.

A quantum-enhanced SNR can be achieved via the injection of a two-mode squeezed state, produced by a doubly resonant bow-tie OPO [42]. The two modes of the squeezed state are quadrature-entangled [43] and frequency separated by the OPO's free spectral range (FSR), 850 MHz. This is also the chosen frequency separation of the interferometer carrier fields (2 Δ). The squeezed state is injected towards the interferometers with the Faraday isolator. The combining cavity spatially separates the two-mode squeezed state, with one mode entering the anti-symmetric port of each interferometer. Upon reflection off each interferometer, the entangled modes copropagate with the upper and lower signal fields. They are spatially recombined at the combining cavity, and then measured with the balanced detector.

The quadrature-entangled squeezed state produced by our OPO contains correlations between the two amplitude quadratures and two phase quadratures of the modes. This state can be described by the relationship between each mode's amplitude and phase quadratures, $\tilde{S}_1^{\pm \Delta}$ and $\tilde{S}_2^{\pm \Delta}$ [43,44]. The noise variances of the combined quadratures of a two-mode amplitude-quadrature squeezed state are

$$\frac{1}{2}\operatorname{Var}(\tilde{S}_{1}^{-\Delta} + \tilde{S}_{1}^{+\Delta}) = \frac{1}{2}\operatorname{Var}(\tilde{S}_{2}^{-\Delta} - \tilde{S}_{2}^{+\Delta}) = V_{-}, \quad (5)$$

$$\frac{1}{2}\operatorname{Var}(\tilde{S}_{1}^{-\Delta} - \tilde{S}_{1}^{+\Delta}) = \frac{1}{2}\operatorname{Var}(\tilde{S}_{2}^{-\Delta} + \tilde{S}_{2}^{+\Delta}) = V_{+}.$$
 (6)

Where V_{-} is the squeezed, and V_{+} is the antisqueezed, noise variance:

$$V_{-} = 1 - \frac{4x}{(1+x)^2} = e^{-2r}, \quad V_{+} = 1 + \frac{4x}{(1-x)^2} = e^{2r}.$$
 (7)

The normalized down-conversion parameter x is experimentally measured as the ratio of pump power to the OPO's oscillation threshold power, $x = \sqrt{P/P_T}$. This is related to the squeezing parameter r by $x = -\tanh(r/2)$.

Equations (5) and (6) show that measurements of a twomode amplitude-quadrature squeezed state aligned to the LO, $\theta_{sq} = 0$, result in a squeezed noise variance in both simultaneously accessible demodulated photocurrents, Eqs. (1) and (3) [37,44].

Equations (1) and (2), with the inclusion of squeezing at $\theta_{sq} = 0$ ($\theta_{LO} = 0$), can be written as

$$\tilde{i}_I(\phi=0) \propto \frac{1}{2} \left(\tilde{X}_1^{-\Delta} + \tilde{X}_1^{+\Delta} + \tilde{S}_1^{-\Delta} + \tilde{S}_1^{+\Delta} \right), \quad (8)$$

$$\tilde{i}_I(\phi = \pi) \propto \frac{1}{2} \left(\tilde{X}_1^{-\Delta} - \tilde{X}_1^{+\Delta} + \tilde{S}_1^{-\Delta} + \tilde{S}_1^{+\Delta} \right).$$
(9)

If the squeezed quadrature angle is misaligned, $\theta_{sq} \neq 0$, the measured noise variance will be

$$V_{\theta_{sq}} = V_{-}\cos^2(\theta_{sq}) + V_{+}\sin^2(\theta_{sq}).$$
(10)

The squeezed quadrature angle changes with the pump field phase. In this work, the pump field phase is manually tuned and not actively controlled.

Experimental loss sets a fundamental limit to the possible improvements in SNR due to squeezing. The expected losses for components of the experiment are summarized in Table I, along with overall experimental efficiencies measured for the upper and lower, signal and squeezing modes. These losses were experimentally measured by propagating bright fields along individual segments of the optical path.

First, we characterize the squeezed light source, verifying the expected loss in the process. We measure degenerate and two-mode squeezing with the flipper mirror (FM) up, bypassing the interferometers, as well as characterizing the two-mode squeezed state while operating the experiment

TABLE I. The optical efficiency budget.

Component	Efficiency	
OPO escape efficiency	$98 \pm 1\%$	
Squeezing injection path	$97\pm1\%$	
Faraday isolator (single pass)	$95\pm1\%$	
Balanced detector contrast	$97\pm1\%$	
Photodiode quantum efficiency	$90\pm2\%$	
Individual interferometer	$95\pm2\%$	
Combining cavity (single pass)	$96\pm1\%$	
Signal efficiency, lower (upper)	$77 \pm 3\% \ (80 \pm 3\%)$	
Squeezing mode efficiency, η_1 (η_2)	$64 \pm 3\% \ (69 \pm 3\%)$	
Squeezing efficiency, flipper mirror up	$73\pm3\%$	

as a whole. Both states are produced by the same OPO, which has a threshold of $P_T = 66.3$ mW, locked to different pump resonance conditions. Degenerate low-frequency squeezed states are produced when the pump is coresonant with the fundamental resonance; the two-mode high-frequency squeezed state is produced when the pump is operated on its resonance at the midpoint of the OPO fundamental FSR. Measurements of noise power are shown in Fig. 2, plotted against *x*. Each point represents an average noise power within a shot-noise-limited frequency range (12 kHz–50 kHz), acquired over three measurements. For the degenerate squeezing measurement, we operate our balanced detector as a dc homodyne detector.

To model the noise power measurements, the effect of differential loss between the two modes of the squeezed state must be considered. This can be described with a parameter known as dephasing [1]. Dephasing acts similarly to phase noise, an effect well understood in degenerate squeezing measurements [45,46].

Degradation due to loss and dephasing on a state with squeezed and antisqueezed quadratures, V_{-} and V_{+} , results in the degraded noise variance, V'_{\pm} [1]:

$$V'_{\mp} = \eta_c [(1 - \Xi')V_{\mp} + \Xi'V_{\pm}] + (1 - \eta_c).$$
(11)

Here, η_c is the common efficiency,

$$\eta_c = \frac{\eta_1 + \eta_2}{2},$$
 (12)



FIG. 2. Measurements of squeezing ($\theta_{sq} = 0$) and antisqueezing [$\theta_{sq} = (\pi/2)$] over a range of the normalized down-conversion (pump) parameters. Photodetector dark noise has been subtracted from each measurement. We show three configurations, each fitted with Eq. (11): degenerate squeezing output from the OPO with dc homodyne measurement (black), two-mode squeezing output to balanced detector demodulated at 425 MHz (pink), and two-mode squeezing after injection into the twininterferometers and demodulated at 425 MHz (green). Each point represents an average of three measurements over a frequency range of 12 kHz–50 kHz.

which depends on η_1 and η_2 , the respective efficiencies of the lower and upper modes, and Ξ' is the effective dephasing parameter which encompasses the effect of differential loss and phase noise.

$$\Xi' = \Xi + \theta_{\rm rms}^2 - 2\Xi \theta_{\rm rms}^2 \tag{13}$$

Here, $\theta_{\rm rms}$ is the root-mean-square of the phase fluctuations, and

$$\Xi = \frac{\eta_1 + \eta_2 - 2\sqrt{\eta_1 \eta_2}}{2(\eta_1 + \eta_2)}.$$
 (14)

Figure 2 shows fitted models for each noise power measurement set. The fitting process utilizes Eq. (11). These models and measurements characterize squeezed state performance and validate our efficiency measurements. These modeling results are summarized in Table II.

For degenerate and two-mode squeezing measurements, without the dynamics of the interferometers (FM up), the expected effective dephasing will be only due to phase noise, as the loss is uniform at all sideband frequencies, i.e. $\Xi = 0$. For the degenerate squeezing measurements, the model returns an effective dephasing corresponding to phase noise of 8 mrad with an error range of 0 to 17 mrad. In the case of two-mode squeezing, it is 6 mrad with the bounds of 0 to 14 mrad. These measurements are consistent with previous characterization of this squeezing source indicating a phase noise of approximately 3 mrad [47]. The error for the modeled phase noise is relatively large because of the lack of data points close to the oscillation threshold of the OPO. At these higher pump parameters, phase noise limits the SNR improvement [45] and locking of the squeezed quadrature angle is required for accurate averaged measurement. Models for both squeezed states demonstrate a common loss consistent with measurements in Table I.

When characterizing the twin-interferometer system, the two-mode squeezed state experienced different losses incurred by the individual interferometers and combining cavity ($\Xi \neq 0$). With the returned fitted parameters, and assuming that phase noise is consistent with the prior measurements (8 mrad of phase noise), the remaining dephasing component corresponds with an efficiency of $\eta_1 = (62 \pm 2)\%$ and $\eta_2 = (66 \pm 2)\%$. These values align

TABLE II. Equation (11) fitted parameters that produce the models in Fig. 2.

Fitted model	Parameter	Value	Error
Degenerate squeezing	$\eta_c \ \Xi'$	72% 6×10^{-5}	$\pm 2\%$ $^{+2.6}_{-0.6} \times 10^{-4}$
Two-mode squeezing	$\eta_c \ \Xi'$	73% 5×10^{-5}	$\pm 2\%$ $^{+2.3}_{-0.5} \times 10^{-4}$
Two-mode squeezing with interferometers	$\eta_c \ \Xi'$	64% 3.7×10^{-4}	$\pm 1\%$ $^{4}_{-1.3}^{+1.3} \times 10^{-4}$



FIG. 3. Noise spectra showing the results of the twin-Michelson interferometer experiment normalized to the average shot noise value. The top row of spectra, (a) and (b), show a 25 kHz tone injected into a single interferometer, compared with the same tone simultaneously injected into both interferometers [with $\phi = (0, \pi)$]. The bottom row of spectra, (c) and (d), show the same twin-interferometer tone with the injection of the two-mode squeezed state, operating at a normalized pump parameter of x = 0.65, corresponding to a squeezing parameter of r = 1.55.

with the experimentally measured efficiencies in Table I, considering their uncertainties.

As a second step, an $\Omega = 25$ kHz signal was injected into the twin-interferometer system to characterize the SNR, and demonstrate the evasion of the 3 dB heterodyne penalty. Figure 3 shows measurements of shot-noiselimited spectra around the injected signal and quantumenhanced spectra when injecting the two-mode squeezed state. Figures 3(a) and 3(b) compare signal strengths between a single interferometer and the twin interferometer. Figures 3(c) and 3(d) demonstrate the quantum enhancement of the twin-interferometer signals when the two-mode squeezed state is injected. For both nonsqueezing and squeezing injection measurements, we show the sum $[\theta_{\rm LO} = 0, \ \phi = 0, \ {\rm Eq.} (1)]$ and difference $[\theta_{\rm LO} = 0, \ \phi = \pi, \ {\rm Eq.} (2)]$ condition of the Michelsons' amplitude quadratures. In our tabletop environment, the lower audio-band frequencies below 10 kHz were dominated by acoustic noise and vibrational modes coupled in via mirror mounts, cavities, and other optical elements. The signal and quantum enhancement technique we demonstrate has no fundamental limit in its low-frequency application, other than those technical noise challenges faced across similar experiments [13,15,16].

When the amplitude quadratures are coherently added $(\theta_{LO} = 0, \phi = 0)$, the signal strength increases by 6 dB, seen in Fig. 3(a). This is a result of having equal optical power across the two interferometers, such that when the second interferometer is introduced we have both doubled the total carrier power in the system (+3 dB) and introduced a dual-sided signal sideband structure (+3 dB). The latter explicitly demonstrates the successful experimental circumvention of the conventional 3 dB penalty associated with heterodyne readout.

Taking the difference of the amplitude quadratures $(\theta_{LO} = 0, \phi = \pi)$, we coherently cancel the injected signal, a point of interest for correlated interferometry experiments. In Fig. 3(b) we see a coherent signal suppression of more than 15 dB. Limits to coherent cancellation include carrier power balancing, interferometer lock points, error in signal calibration, the tuning of θ_{LO} and ϕ as well as any drifts in these values over time. In Fig. 3(d) this suppression increases to 17.5 dB, associated with drifts in the aforementioned parameters and the reduced shot noise level.

When we inject our two-mode squeezed state into the twin-interferometer system, we see either a reduced or increased overall noise floor level, depending on the squeezed quadrature angle. In Fig. 3(c) we directly observe a 3.5 dB average reduction when squeezing our readout quadrature ($\theta_{sq} = 0$), and an 11.5 dB increase in the noise floor when antisqueezing it [$\theta_{sq} = (\pi/2)$]. In Fig. 3(d) we see a similar reduction when $\theta_{sq} = 0$ however only a 10 dB increase with $\theta_{sq} = (\pi/2)$. These values, although varying, are consistent with the normalized pump parameter of x = 0.65, and long timescale pump-power drifts of 5% across the measurement period.

The presented results demonstrate a quantum-enhanced, dual Michelson sensor that employs balanced heterodyne readout. We show that a high-frequency quadratureentangled, two-mode squeezed state can improve the SNR of audio-band signals. Our readout scheme circumvents the conventional 3 dB penalty associated with heterodyne readout and can simultaneously obtain quantum-enhanced sum-amplitude and difference-phase quadrature information without introducing additional photodetectors. This flexibility opens opportunities for mixing and filtering amplitude and phase quadratures. Previous experiments [48–50] highlight these opportunities, for technical noise filtering and backaction evasion. Our scheme can provide these opportunities without additional signal loss. This proof-of-principle experiment underlines the potential for high-frequency two-mode squeezing, applicable not only to precision metrology, of which we highlight gravitational wave detection, dark matter detection, and quantum gravity tests, but also wavelength-multiplexed quantum communication. It experimentally demonstrates the SNR equivalence of balanced homodyne readout to dual-carrier heterodyne readout.

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Data availability—The data that support the plots within this Letter and other findings of this study are available from the contact author upon reasonable request.

The authors declare no competing interests.

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