## Activation of Topological Defects Induces a Brittle-to-Ductile Transition in Epithelial Monolayers

<span id="page-0-0"></span>Yixia Chen [,](https://orcid.org/0000-0002-4624-2764) Qigan Gao , Jingchen Li, Fangtao Mao, Ruowen Tang, and Hongyuan Jiang  $\bullet$ Hefei National Laboratory for Physical Science at the Microscale, CAS Key Laboratory of Mechanical Behavior and Design of Materials, CAS Center for Excellence in Complex System Mechanics, Department of Modern Mechanics, University of Science and Technology of China, Hefei, Anhui 230026, China

(Received 7 June 2021; accepted 8 December 2021; published 5 January 2022)

Epithelial monolayers are subjected to various mechanical forces, such as stretching, shearing, and compression. Thus, its mechanical response to external loadings is essential for its biological functions. However, the mechanism of the fracture failure of the epithelial monolayer remains poorly understood. Here, by introducing a new type of topological transition, i.e., detach transition or T4 transition, we develop a modified cellular vertex model to investigate the rupture of the cell monolayer. Interestingly, we find a brittle-to-ductile transition in epithelial monolayers, which is controlled by the mechanical properties of single cells and cell-cell contacts. We reveal that the external loadings can activate cell rearrangement in ductile cell monolayers. The plastic deformation results from the nucleation and propagation of "pentagonheptagon defects" in analogy with the topological defects commonly seen in 2D materials. By using a simplified four-cell model, we further demonstrate that the brittle-to-ductile transition is induced by the competition between cell rearrangement and cell detachment. Our work provides a new theoretical framework to study the rupture of living tissues and may have important implications for many other biological processes, such as wound healing and tissue morphogenesis.

DOI: [10.1103/PhysRevLett.128.018101](https://doi.org/10.1103/PhysRevLett.128.018101)

An epithelial monolayer, a single-cell-thick tissue that covers most surfaces of animal organs, is subjected to various internal or external mechanical forces and thus undergoes large deformations during embryonic morphogenesis [[1](#page-4-0)–[3\]](#page-4-0) and many physiological activities such as respiration, digestion, and cardiac pulses [[4](#page-4-0)–[6\]](#page-4-0). For example, the typical strain of human skin during posture changes or sports is about 25% [[7\]](#page-4-0). Cyclic changes in blood pressure can stretch blood vessel walls circumferentially and induce a strain up to 15% [\[8](#page-4-0)]. The maximum strain and strain rate of mitral valve during the beating of human hearts can reach 30% and 400% s<sup>-1</sup>, respectively [[9,10\]](#page-4-0). Furthermore, the compressive forces during embryonic development are big enough to buckle and fold tissues [[11\]](#page-5-0) and drive the morphogenesis of brain cortex [[12](#page-5-0)], gut villi [\[13](#page-5-0)], and optic cup [\[14\]](#page-5-0). Thus, the mechanical properties of epithelial monolayers must be excellent enough to maintain their integrity under these mechanical loadings.

Despite the fact that epithelial monolayers can dissipate mechanical stress to maintain epithelial homeostasis through cell division, intercalation, and extrusion [\[15](#page-5-0)–[19\]](#page-5-0), tissue fracture may still occur when cell-cell adhesion is impaired or excessive stretch is applied. For example, patients with mutations in adherens junction proteins, desmosomal proteins, or actin regulators suffer from tissue fragility defects and disrupted barrier functions [\[20\]](#page-5-0). Mechanical ventilation is known to cause acute lung injury because of the overstretching to alveoli during the treatment of acute respiratory distress syndrome [\[21](#page-5-0),[22](#page-5-0)]. Interestingly, the motility of Trichoplax adhaerens, a highly dynamic simple organism, can lead to the fracture of its epithelial tissue [\[23\]](#page-5-0). Moreover, cracks may appear around the location of weak adhesion between neighboring cells in confluent epithelial sheets, causing woundlike holes [\[24](#page-5-0)] and even fracture failure [[25](#page-5-0)]. Similarly, monolayers can release the excessive hydraulic pressure through the breakage of cell-cell adhesion [\[26,27](#page-5-0)]. Although the mechanics of epithelial monolayers is an essential part of its functions, little is known about how fracture failure occurs in response to mechanical stress and large deformation, and a simple theoretical model to characterize monolayer fracture is still lacking.

First, we treat each cell as an individual polygon containing several vertices [Figs.  $1(c)$  and  $1(d)$ ] based on the two-dimensional vertex model [\[28](#page-5-0)–[33](#page-5-0)]. For simplicity, here we assume the properties of each cell are identical. The energy of the system is

$$
U = \sum_{I:\text{cell}} \frac{1}{2} K(A_I - A_0)^2 + \sum_{I:\text{cell}} \frac{1}{2} \Gamma L_I^2 + \sum_{ab:\text{edge}} \Lambda I_{ab}.
$$
 (1)

The first term in Eq. (1) is the energy of cell area elasticity with areal stiffness K [\[29,34\]](#page-5-0), where  $A_I$  and  $A_0$  are the current and preferred area of the Ith cell. The second term represents the perimeter elasticity originating from actomyosin contractility, where  $\Gamma$  is the contractile modulus [[35](#page-5-0)].

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FIG. 1. Topological transitions in cell monolayers. (a) The fracture failure (scale bar,  $1 \text{ mm}$ ) and (b)  $T1$  transition under uniaxial tensile loading in experiments (scale bar:  $25 \mu m$ ). See Supplemental Material [\[37\]](#page-5-0) for details. (c)  $T1$  transition in vertex model. (d) Detach transition (T4 transition) we defined.

The third term is the interfacial energy with a line tension  $\Lambda$ , which originates from the competition between cortical tension and intercellular adhesion [[29,36\]](#page-5-0). Λ can be negative if adhesion energy is bigger than cortical tension or positive if cortical tension dominates.  $L<sub>I</sub>$  denotes the perimeter of the Ith cell and  $l_{ab}$  is the length of the contact edge connected by adjacent vertices  $a$  and  $b$ . The morphological changes of the monolayer can be described by  $d\mathbf{r}_a/dt = \mathbf{F}_a/\eta$ , where  $\eta$  is the viscous coefficient,  $\mathbf{r}_a$  and  $\mathbf{F}_a = -\frac{\partial U}{\partial \mathbf{r}_a}$  are the coordinates and force acting on vertex a, respectively.

The topological transitions in the classical vertex model are based on geometrical criterions, such as length (T1 transition, to model cell intercalation  $[49]$ ), area (T2 transition, to describe cell death  $[50]$  $[50]$  $[50]$ , and distance  $(T3$  transition, to model cell merging process [[44](#page-5-0)]). For example, when the edge between two neighboring cells is shorter than a threshold, the edge will shrink to a point and another two cells become new neighbors, so that T1 transition occurs (see Fig. 1). However, the above geometrical criteria are not relevant to fracture and cannot be used to describe monolayer fracture since they do not allow for the creation of intracellular spacing. To solve this problem, we propose a failure criterion and define a detach transition  $(T4$  transition) [Fig. 1(d)], based on the calculation of intercellular stress on each edge (Supplemental Material [\[37](#page-5-0)] and Fig. S1). The 2D normal stress on an edge is

$$
s_{ab} = F_{ab}^n / l_{ab},\tag{2}
$$

where  $l_{ab}$  is edge length, and  $F_{ab}^n$  is the normal component of the traction force on this edge. The cell-cell adhesion will break when  $s_{ab} > s_{cr}$ , where  $s_{cr}$  is the critical stress as a material property of cell-cell contact (e.g., the adhesive links including E-cadherin [[51](#page-6-0)] and tricellular junction proteins [\[45\]](#page-5-0)). After this detach transition occurs, a crack between two cells appears, and new short edges are created in some cells so that the edge number of these cells increases [Fig. 1(d)]. Similar failure criteria has been used in the system of soft sticky balls connected by springs [\[23](#page-5-0)], and nonconfluent epithelium can also be obtained through replacing the original vertex by a small triangular extracellular space in a vertexlike model [\[46](#page-6-0)] or through energy minimization in a simple four-cell model [\[52\]](#page-6-0).

We can normalize all the equations with characteristic length  $\sqrt{A_0}$  and characteristic time  $\eta/KA_0$  and obtain three dimensionless parameters:  $\tilde{\Gamma} = \Gamma/KA_0$ ,  $\tilde{\Lambda} = \Lambda/KA_0^{3/2}$ , and  $\tilde{s}_{cr} = s_{cr}/KA_0$ . Thus, we have

$$
\tilde{U} = \sum_{I:\text{cell}} \frac{1}{2} (\tilde{A}_I - 1)^2 + \sum_{I:\text{cell}} \frac{1}{2} \tilde{\Gamma} \tilde{L}_I^2 + \sum_{ab:\text{edge}} \tilde{\Lambda} \tilde{I}_{ab}.
$$
 (3)

The intracellular stress  $\tilde{\sigma}_{xx}^{\text{cell}}$  and tissue stress  $\tilde{\sigma}_{xx}^{\text{tissue}}$  can be derived (Supplemental Material [[37](#page-5-0)]).

Now, we can investigate the uniaxial stretching of cell monolayers. If the loading is very quick, there is not enough time for cell rearrangement, which is the case in most experiments [\[25,26\]](#page-5-0). In contrast, here we consider a quasistatic displacement-controlled uniaxial tensile test, where the loading is slow enough to allow the system to reach the equilibrium at each loading step and allow cell rearrangement to happen, but fast enough to eliminate the influence of cell division and death. Notice that epithelial cells usually take more than 10 h to finish cell cycle [[53](#page-6-0)], while a typical  $T1$  transition occurs in tens of minutes [[54](#page-6-0)]. Therefore, here we neglect cell division and death and only consider T1 transition and detachment transition (Fig. 1).

Confluent cell monolayer can undergo a solid-to-liquid transition (SLT) at  $\tilde{\Lambda} = -4\tilde{\Gamma} \sqrt{n \tan(\pi/n)}$  [\[30\]](#page-5-0), where *n* is the number of cell sides (Fig. S2 [[37](#page-5-0)]). Here, we focus on the solid phase (jammed monolayers) and first consider a hexagonal lattice (Figs. 2 and [3](#page-2-0)), which is known as the ground state of the solid phase [\[30](#page-5-0)[,55\]](#page-6-0). Although hexagonal lattice sounds ideal, it is quite common in tissues, such as marginal cells of stria vascularis [\[56](#page-6-0)], Drosophila wing disk [[57](#page-6-0)], and lens fiber cells [[58](#page-6-0)]. Here we perform the uniaxial tensile test in the zigzag direction of hexagonal



FIG. 2. A brittle monolayer ( $\tilde{\Gamma} = 0.16$ ,  $\tilde{\Lambda} = -0.7$ , and  $\tilde{s}_{cr} = 3$ ) under displacement-controlled uniaxial tensile loading. (a) Time evolution of monolayer morphology. (b) Corresponding time evolution of intracellular stress  $\tilde{\sigma}_{xx}^{\text{cell}}$ . To induce failure in the middle, a nick is made to concentrate stress [[25](#page-5-0)].

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FIG. 3. A ductile monolayer ( $\tilde{\Gamma} = 0.16$ ,  $\tilde{\Lambda} = -1.19$ , and  $\tilde{s}_{cr} = 3$ ) under displacement-controlled uniaxial tensile loading. (a) Time evolution of monolayer morphology. The plastic deformation is induced by the nucleation and propagation of pentagon-heptagon defects, which are usually seen in graphene. (b) Corresponding time evolution of intracellular stress  $\tilde{\sigma}_{xx}^{\text{cell}}$  shows obvious distortions of stress field around pentagon-heptagon defects.

lattice [[59](#page-6-0)]. Interestingly, we find different parameters in this solid region can yield completely different mechanical responses.

Figure [2](#page-1-0) and Videos S1 and S2 (in the Supplemental Material [[37](#page-5-0)]) show a clearly catastrophic brittlelike failure without observable plastic elongation, which is further demonstrated by the sharp fracture surface, negligible cell rearrangement [Fig. 4(b)], and plastic strain [Fig. 4(c)]. The corresponding stress-strain curve further confirms its brittlelike nature, in which the sudden fracture occurs at a large elastic strain of 33.4% [blue curve in Fig. 4(a)]. Depending on parameters, the breaking elongation of brittle monolayers can vary greatly from 30% to more than 100% (Fig. S8). In fact, due to their soft nature, a good indicator of brittleness and ductility of soft materials (e.g., tissues and hydrogels) is not the elongation at break, but the plastic deformation before rupture.

Strikingly, as  $\tilde{\Lambda}$  decreases to  $-1.19$  in Fig. 3 and Videos S3 and S4 [\[37\]](#page-5-0), apparent plastic elongation with classical characteristics of ductile fracture are observed. Monolayer rupture occurs at a large strain of 109% with a permanent plastic elongation of 60%. Notably, an apparent necking and rough fracture surfaces are also observed, suggesting significant plastic flow occurs before fracture [Figs. S4(a),  $S4(b)$ , and  $S4(d)$  [\[37\]](#page-5-0) ]. This is further confirmed by its stress-strain relationship [the green curve in Fig. 4(a)].



FIG. 4. Brittle-to-ductile transition (BDT) of the epithelial monolayer is controlled by the mechanical properties of single cells and cell-cell contacts. (a)–(d) Hexagonal cell lattice. (a) Stress-strain relationship for various  $\tilde{\Lambda}$ . (b) The accumulated number of T1 transitions during stretching. Dashed lines indicate where curves stop. (c) The elastic strain, plastic strain, elastic modulus, and fracture strength as the function of  $\Lambda$ . (d) Phase diagram of BDT. (e)–(g) Irregular monolayers. (e) Stress-strain relationship for various  $\tilde{\Lambda}$ . (f) The proportion of cells with n cell sides before loading begins and after monolayer rupture occurs. (g) Irregular monolayer morphology during brittle and ductile fracture. Left, a brittle case at 35% strain [blue curve in (e)]. Right, a ductile case at 90% strain [green curve in (e)].

Therefore, Figs. [2](#page-1-0) and [3](#page-2-0) together reveal a clear brittle-toductile transition as  $\tilde{\Lambda}$  decreases, which is also confirmed by the stress-strain curves in Fig. [4\(a\).](#page-2-0)

The plastic deformation in Fig. [3](#page-2-0) is very similar to the germ-band elongation during Drosophila morphogenesis [\[47,48\]](#page-6-0). This plastic deformation results from  $T1$  transition, which is also known as cell rearrangement or cell intercalation  $[17,60-62]$  $[17,60-62]$  $[17,60-62]$  $[17,60-62]$  $[17,60-62]$  as shown in Fig. [1](#page-1-0). We find if T1 transition occurs inside the monolayer, two pair of pentagon-heptagon defects will appear [Fig. [1\(c\)](#page-1-0)]. In contrast, if T1 transition occurs on the boundary, only one pair of pentagon-heptagon defects and one pentagonal cell will appear [Fig. [1\(c\)\]](#page-1-0). Similar to many 2D materials, e.g., graphene [[63](#page-6-0)], a pentagon-heptagon defect resembles a disclination dipole, which can be regarded as an edge dislocation. We find dislocations keep nucleating on the boundaries, especially near the crack tip, and then propagate to the interior of the cell monolayer and finally end up at another boundary (Fig. [3](#page-2-0), Videos S3 and S4, and Fig.  $S5$  [\[37\]](#page-5-0)). The number of T1 transitions increase as the stretching continues [Fig. [4\(b\)](#page-2-0)], indicating permanent plastic deformation is accumulating. Thus, we conclude that the external loadings can activate cell rearrangement in ductile cell monolayers.

We also find, besides the stress concentration at the crack tip, that there are obvious distortions of stress field around each pentagon-heptagon defect [Fig. [3\(b\)](#page-2-0)], which is quite similar to the theoretical description of a disclination dipole in graphene [\[63](#page-6-0)]. Furthermore, as the monolayer becomes more ductile, it will also become softer (indicated by elastic modulus) and more fragile (indicated by fracture strength), yet the elastic range is approximately the same (indicated by maximum elastic strain) as shown in Fig. [3\(c\)](#page-2-0).

Similar to the effects of  $\tilde{\Lambda}$  [Fig. [4\(a\)\]](#page-2-0), as  $\tilde{\Gamma}$  decreases, there also exists a brittle-to-ductile transition (Fig. S6 [\[37\]](#page-5-0)). Furthermore, we find that the closer to the solid-fluid transition curve [Fig. [4\(d\)](#page-2-0)], i.e., the lower  $\tilde{\Lambda}$  and  $\tilde{\Gamma}$  [\[29,30](#page-5-0)], the more ductile the cell monolayer becomes, indicated by the increase of the cumulative number of  $T1$  transitions [Figs. [4\(b\)](#page-2-0), [4\(d\)](#page-2-0), S6, and S7]. Therefore, we conclude that the brittle-to-ductile transition of the epithelial monolayer is controlled by the mechanical properties of single cells and cell-cell contacts, such as the relative contractile modulus  $(nf), relative line tension  $($  $\tilde{\Lambda}$  $),$  and relative intercellular$ strength  $(\tilde{s}_{cr})$ .

Given that in many tissues the cell monolayer is not a regular hexagonal lattice [\[54,60,64\]](#page-6-0), we also investigate the uniaxial stretching of irregular cell monolayers. The irregular lattice with a diverse number of cell sides is generated through Voronoi tessellation and undergoes a local minimization of free energy, i.e., the annealing process, before stretching. The irregular lattice we obtained through this method [the gray column in Fig.  $4(f)$ ] is quite similar to the experimental samples where hexagonal cells are about 40% [\[64\]](#page-6-0).

We find that the brittle-to-ductile transition also exists in the irregular cell monolayer [Fig. [4\(e\)](#page-2-0), Videos S5 and S6 [\[37\]](#page-5-0)), and its mechanical responses are qualitatively the same as the hexagonal cell monolayer (Figs. S6 and S7). However, since the irregular cell monolayers have more preexisting disclination- and dislocationlike defects compared to the regular hexagonal monolayer, cell rearrangements occur more easily, more frequently, and earlier [[55\]](#page-6-0), so that the yield stress and fracture strength of the cell monolayer are smaller. Furthermore, the nonuniform nature of irregular lattice leads to local stress concentration, so that many detachment transitions occur and many small cracks are created during stretching, especially in brittle monolayers [Fig. [4\(g\),](#page-2-0) left]. Eventually, these small cracks may coalesce to form woundlike holes, which is in good agreement with the crack morphology observed in experiments [\[24,25](#page-5-0)].

Interestingly, in ductile cell monolayers, the irregular lattice becomes more regular, i.e., the proportion of hexagonal cells increases [Fig. [4\(f\)](#page-2-0), Video S7 [\[37](#page-5-0)] ] under uniaxial tensile loading, which is consistent with the prominent increase of topological order of tissues during development [[54](#page-6-0),[57,60,65](#page-6-0)]. This hexagonal ordering becomes inapparent as the monolayer becomes more brittle, since there is negligible cell rearrangement in brittle monolayers [Fig. [4\(f\)](#page-2-0)]. Therefore, these results indicate that the brittle-to-ductile transition can also affect the evolution of topological order of epithelial tissues during development.

To get more insight into brittle-to-ductile transition, we investigate T1 transition and detachment transition by using a simple four-cell model [\[36](#page-5-0)[,66\]](#page-6-0). Without external force  $(F = 0)$ , the total energy of the four-cell system has two local minimums, i.e., two equilibrium states before and after T1 transition, as the length of shared edge changes [Fig.  $5(a)$ ]. We find, in this case, the energy barrier for T1 transition  $\Delta U_0$  becomes smaller as the parameters approach the solid-to-liquid transition boundary [Fig. S10(a)  $[37]$ ], which is consistent with previous studies [\[36,](#page-5-0)[66](#page-6-0)]. When a tensile force  $\tilde{F}$  is applied along the zigzag direction, the total energy becomes higher, yet the energy barrier  $\Delta U_{\tilde{F}}$ and the equilibrium length of the shared edge before T1 transition  $\tilde{l}_{\tilde{F}}$  decreases, so that T1 transition will happen more easily [Figs.  $5(a)$ ,  $5(b)$ , and  $S10(b)$ ].

On the other hand, as the external force  $\tilde{F}$  increases, the stress along the shared edge  $\tilde{s}_{ab}$  will become larger due to the decrease of the equilibrium length of the shared edge [see Eq.  $(2)$ ] so that the detachment transition is also more likely to occur. Thus, T1 transition and detachment transition compete with each other to determine which process will happen first. We find T1 transition will occur first for small  $\tilde{\Lambda}$  or  $\tilde{\Gamma}$ , while detachment transition will occur first for large  $\tilde{\Lambda}$  or  $\tilde{\Gamma}$  [Figs. [5\(c\)](#page-4-0) and S11(b) [[37](#page-5-0)]] during the loading process. Further calculation shows that T1 transition will occur first near the boundary of solid-toliquid transition in the phase diagram, so that the cell monolayer is ductile [Fig. [5\(d\)\]](#page-4-0), which well explains the

<span id="page-4-0"></span>

FIG. 5. Competition between  $T1$  and detach transition leads to the observed brittle-to-ductile transition. (a) Energy landscape with or without external force  $\tilde{F}$  on the left and right boundaries, showing energy barrier and equilibrium length of shared edge (red line) before and after T1 transition ( $\tilde{\Gamma} = 0.12$ ,  $\tilde{\Lambda} = -0.6$ ). (b) Normalized energy barrier  $\Delta \tilde{U}_{\tilde{F}} / \Delta \tilde{U}_0$  and normalized equilibrium length of shared edge  $(\tilde{l}_{\tilde{F}} - \tilde{l}_0)/\tilde{l}_0$  change with  $\tilde{F}$ . (c) Competition between T1 and detachment transition under tensile loading ( $\ddot{\Gamma} = 0.12$ ,  $\ddot{s}_{cr} = 2$ ). (d) Phase diagram of four-cell system under stretching ( $\tilde{s}_{cr} = 5$ ).

brittle-to-ductile transition we found in Fig. [4.](#page-2-0) We further demonstrate that the boundary of brittle-to-ductile transition is mainly determined by  $\tilde{s}_{cr}$ , and the decrease of  $\tilde{s}_{cr}$ leads to a larger brittle region in the phase diagram [Fig. S11(c)], which is similar to the effect of ethylenediamine tetra-acetic acid, a chelating agent that disrupts the adhesive links at the cell-cell interface and causes the monolayer to be more fragile [\[25\]](#page-5-0). Therefore, we conclude that the competition between  $T1$  transition and detachment transition leads to the observed brittle-to-ductile transition of the cell monolayer.

In summary, we define a new type of topological transition, i.e., detach transition or T4 transition, so that the fracture failure can be studied in the framework of a vertex model. We show that there exists a brittle-to-ductile transition in epithelial monolayers when the mechanical properties of individual cells and cell-cell contacts change, and the transition is attributed to the competition between cell rearrangement and cell detachment. Interestingly, in ductile monolayers, cell intercalation can lead to the plastic deformation characterized by the nucleation and propagation of pentagon-heptagon defects that are commonly seen in 2D materials. Our results demonstrate how the mechanical properties of individual living cells and their interaction determine the mechanical response of larger scale tissues. The brittle-to-ductile transition still exists even when the healing process is present (Fig. S9 [[37](#page-5-0)]). Similar brittle-toductile transitions were also observed in amorphous solids when attraction (similar to the line tension in our work) [\[67\]](#page-6-0) and annealing degree changed [[68](#page-6-0),[69](#page-6-0)]. Our findings provide a new theoretical framework to study the mechanics of cell monolayers and may also have important implications for other relevant biological processes accompanied by significant cell rearrangement and detachment.

This work was supported by the National Natural Science Foundation of China (Grants No. 12025207 and No. 11872357), the Fundamental Research Funds for the Central Universities, the Strategic Priority Research Program of the Chinese Academy of Sciences (Grant No. XDB22040403). This work was partially carried out at the University of Science and Technology of China Center for Micro and Nanoscale Research and Fabrication.

[\\*](#page-0-0) Corresponding author. jianghy@ustc.edu.cn

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