## Periodically Driven Quantum Thermal Machines from Warming up to Limit Cycle

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Theoretical treatments of periodically driven quantum thermal machines (PD-QTMs) are largely focused on the limit-cycle stage of operation characterized by a periodic state of the system. Yet, this regime is not immediately accessible for experimental verification. Here, we present a general thermodynamic framework that handles the performance of PD-QTMs both before and during the limit-cycle stage of operation. It is achieved by observing that periodicity may break down at the ensemble average level, even in the limit-cycle phase. With this observation, and using conventional thermodynamic expressions for work and heat, we find that a complete description of the first law of thermodynamics for PD-QTMs requires a new contribution, which vanishes *only* in the limit-cycle phase under rather weak system-bath couplings. Significantly, this contribution is substantial at strong couplings even at limit cycle, thus largely affecting the behavior of the thermodynamic efficiency. We demonstrate our framework by simulating a quantum Otto engine building upon a driven resonant level model. Our results provide new insights towards a complete description of PD-QTMs, from turn-on to the limit-cycle stage and, particularly, shed light on the development of quantum thermodynamics at strong coupling.

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Introduction.—A tantalizing goal of quantum thermodynamics is to investigate, analyze, and ultimately design thermal machines on the quantum scale  $[1-11]$  $[1-11]$  $[1-11]$  $[1-11]$ . Among the various routes towards this vision, devising periodically driven quantum thermal machines (PD-QTMs) in which work can be extracted through externally driving a quantum working substance represents a paradigmatic one. This field has attracted much attention in recent years with intriguing theoretical proposals [[12](#page-4-2)–[26](#page-5-0)] together with delicate experimental realizations in various platforms [\[27](#page-5-1)–[36\]](#page-5-2).

Existing theories on PD-QTMs are largely carried out in the limit-cycle stage of operation, where the working substance should recoil to its original state after a driving cycle (see, e.g., Refs. [\[12](#page-4-2)–[14](#page-4-3),[18](#page-4-4)[,25,](#page-4-5)[37](#page-5-3)–[40](#page-5-4)]). Although the limit-cycle regime enables theoretical simplicity, it faces potential challenges. On the one hand, recent studies have pointed out that the state of the working substance needs not inherit the periodicity of external drivings at finite times [\[20](#page-4-6)[,24](#page-4-7),[40](#page-5-4)], namely, there may exist a transient warming-up phase for the operation of PD-QTMs before a limit cycle sets in. On the other hand, the limit-cycle stage is not immediately accessible experimentally, which may lead to discrepancy between theoretical predictions and experimental measurements. Addressing these challenges requires a unified thermodynamic description of both the warming-up and limit-cycle phases of PD-QTMs, which is, however, still missing.

In this work, we present a thermodynamic framework that deals with cycle-number dependent thermodynamic quantities. As such, it allows us to characterize in a unified manner the performance of PD-QTMs from the warmingup to the limit-cycle phases. Our theory relies on the observation that periodicity can break down at the ensemble average level, namely,  $\langle \mathcal{O}(t) \rangle \neq \langle \mathcal{O}(t + \mathcal{T}) \rangle$  with  $\mathcal O$ being a periodic observable  $\mathcal{O}(t) = \mathcal{O}(t+T)$  and T the driving period. This breakdown is trivial in the transient warming-up phase where even the state of the working substance does not behave in a periodic manner. However, nontrivially, this breakdown can show up in the limit-cycle phase if  $\mathcal O$  involves bath degrees of freedom, a scenario which is frequently encountered in studies of quantum thermodynamics (see recent discussions [\[41,](#page-5-5)[42\]](#page-5-6) and reference therein).

Building upon this observation, we find that the thermodynamic characterization of PD-QTMs generally acquires a new contribution in both the warming-up and limit-cycle phases, besides the conventional notions of work and heat. Particularly, through completing the first law of thermodynamics [cf. Eq. [\(4\)](#page-1-0)] and ensuring its validity across the whole parameter space at all times, we identify this extra term (denoted as A hereafter) as the change of an ensemble average  $\langle H_S(t) + H_I(t) \rangle$  within a cycle [cf. Eq. [\(5\)](#page-1-1)];  $H_{S(I)}$ denotes the Hamiltonian for the working substance (system-bath coupling). Intriguingly, this  $A$  term vanishes only in the limit-cycle phase provided that the system-bath

<span id="page-1-2"></span>

FIG. 1. Schematic of a driven resonant level engine operating with a quantum Otto cycle. The cycle consists of isochoric heating (stroke 1) and cooling (stroke 3) processes and two workextracting processes [strokes 2 and 4 with  $\epsilon(t)$  tuned from  $\epsilon_1$  to  $\epsilon_2$ and from  $\epsilon_2$  to  $\epsilon_1$ , respectively].

coupling is rather weak. We further uncover that contributions from the  $A$  term play a nontrivial role in shaping behavior of the thermodynamic efficiency [cf. Eq. [\(6\)\]](#page-2-0) in both the warming-up and limit-cycle phases, especially at strong coupling, compared with existing characterizations, which largely neglect it.

We illustrate our general framework using the quantum Otto heat engine (Fig. [1](#page-1-2)), with a driven electronic level as the working substance. Based on simulations, we show that conventional definitions without  $A$  fail to capture the correct thermodynamics, especially at strong coupling where the  $A$  term is substantial in both warm-up and limit-cycle regimes. The framework presented here allows the description of PD-QTMs even before the limit cycle stage, and at strong coupling, both aspects crucial for describing experimental systems and advancing the field of quantum thermodynamics.

<span id="page-1-3"></span>Quantum thermodynamics of generic PD-QTMs.— Generally, PD-QTMs can be modeled as  $(h = 1, k_B = 1)$ hereafter)

$$
H(t) = H_S(t) + H_B + H_I(t).
$$
 (1)

Here,  $H<sub>S</sub>(t)$  denotes a semiclassically driven working substance with the understanding that the working substance exchanges work with an external agent that we do not explicitly include within the quantum description.  $H_B = \sum_{v=h,c} H_B^v$  consists of a hot (h) and a cold (c) thermal<br>both and  $H_1(t) = \sum H^v(t) = \sum A(t)H^v$  denotes a time bath and  $H_I(t) = \sum_v H_I^v(t) \equiv \sum_v \lambda_v(t) H_I^v$  denotes a time-<br>dependent system-bath coupling. Here  $\lambda_v(t)$  is a timedependent system-bath coupling. Here,  $\lambda_v(t)$  is a timedependent coefficient describing the contact switching of the  $v$  reservoir, used to implement thermodynamic strokes (see, e.g., Refs. [[24](#page-4-7),[25](#page-4-5),[43](#page-5-7)]). We assume periodic protocols  $H_{S,I}(t) = H_{S,I}(t+T)$  such that  $H(t) = H(t+T)$  with T the period of the driving. Here, we do not enforce a limitcycle mode of operation for the PD-QTM *a priori* by any type of renewal mechanism for states. Instead, the cyclic behavior of the system's state arises naturally due to the periodic protocol described by Eq. [\(1\)](#page-1-3).

To analyze the quantum thermodynamics of the PD-QTM, we utilize the definitions of heat and work based on the complete Hamiltonian dynamics,  $H(t)$  [\[24,](#page-4-7)[44](#page-5-8)–[46](#page-5-9)]. This approach naturally avoids the problem of the partitioning of the system-bath interaction. Denoting by  $\rho_{\text{tot}}$  the total density matrix of the composite system, the integrated injected work  $W(m)$  and absorbed heat  $Q_n(m)$  from the v bath during the *m*th cycle  $[mT, (m+1)\overline{T}]$  with a non-<br>negative integer  $m > 0$  are uniquely defined as [24,44–46] negative integer  $m \ge 0$  are uniquely defined as [\[24](#page-4-7)[,44](#page-5-8)–[46\]](#page-5-9)

<span id="page-1-4"></span>
$$
\mathcal{W}(m) \equiv \int_{mT}^{(m+1)T} dt \text{Tr}[\dot{H}(t)\rho_{\text{tot}}(t)],\tag{2}
$$

<span id="page-1-5"></span>
$$
\mathcal{Q}_{v}(m) \equiv -\int_{mT}^{(m+1)T} dt \text{Tr}[H_{B}^{v} \dot{\rho}_{\text{tot}}(t)]. \tag{3}
$$

Here,  $\mathcal{X}(t) \equiv d\mathcal{X}(t)/dt$  for an arbitrary operator  $\mathcal{X}(t)$ , the trace is performed over system and bath degrees of freedom. The introduction of the cycle-number  $(m)$  dependent thermodynamic quantities allows us to characterize the performance of PD-QTMs in both the warming-up and limit-cycle stages. Note that the expression for absorbed heat  $\mathcal{Q}_v$  is consistent with the definition employed in quantum transport scenarios [\[47](#page-5-10)–[49](#page-5-11)]. For the work definition, it naturally incorporates work costs for implementing a time-dependent system-bath coupling [\[15\]](#page-4-8). In our convention, a heat engine corresponds to  $W < 0$ ,  $Q_h > 0$ and  $\mathcal{Q}_c < 0$ .

Since the integrand in Eq. [\(2\)](#page-1-4) is just  $d\langle H(t)\rangle/dt$ with  $\langle H(t) \rangle \equiv \text{Tr}[H(t)\rho_{\text{tot}}(t)]$  the internal energy of the composite system we can express Eq. (2) as  $\mathcal{W}(m)$  – composite system, we can express Eq. [\(2\)](#page-1-4) as  $W(m) =$  $\text{Tr}\left\{\hat{H}(t)[\rho_{\text{tot}}((m+1)T)-\rho_{\text{tot}}(mT)]\right\}$ . This immedia-<br>tely leads to an intriguing observation:  $\rho_{\text{tot}}(mT) \neq$ tely leads to an intriguing observation:  $\rho_{\text{tot}}(mT) \neq$  $\rho_{\text{tot}}((m+1)T)$ , generally valid since  $W(m) \neq 0$  for a PD-QTM. Note that this difference does not prevent the existence of a limit-cycle phase for the reduced system density matrix  $\rho_S$ ,  $\rho_S(mT) = \rho_S((m+1)T)$  [\[12](#page-4-2)– [14,](#page-4-3)[18,](#page-4-4)[25](#page-4-5)[,37](#page-5-3)–[40\]](#page-5-4), since the bath state needs not be a periodic function at all. This simple observation has a profound consequence: An operator  $\mathcal O$  involving bath degrees of freedom generally shows  $\langle \mathcal{O}(mT) \rangle \neq$  $\langle \mathcal{O}((m+1)\mathcal{T})\rangle$ , even when  $\mathcal{O}(m\mathcal{T}) = \mathcal{O}((m+1)\mathcal{T})$ . Namely, the periodicity can break down at the ensemble average level.

<span id="page-1-0"></span>We now turn to the first law of thermodynamics for PD-QTMs. In terms of our definitions for heat and work, it takes the following exact form [[50](#page-5-12)],

$$
W(m) + \sum_{v} \mathcal{Q}_{v}(m) - \mathcal{A}(m) = 0.
$$
 (4)

<span id="page-1-1"></span>Crucially, besides the conventional notions of work and heat, an extra quantity appears,  $\mathcal{A}(m)$ ,

$$
\mathcal{A}(m) \equiv \operatorname{Tr}\{H_{SI}(m\mathcal{T})[\rho_{\text{tot}}((m+1)\mathcal{T}) - \rho_{\text{tot}}(m\mathcal{T})]\}.
$$
 (5)

Here, we denote by  $H_{SI}(mT) \equiv H_S(mT) + H_I(mT)$ . In arriving at the first law Eq. [\(4\)](#page-1-0), we emphasize that no approximations were invoked. The  $A$  term reflects the change to  $\text{Tr}\lbrace H_{SI}\rho_{\text{tot}}\rbrace$  after a cycle, highlighting the nontrivial role of the system-bath coupling in quantum engines [[25](#page-4-5),[41](#page-5-5)]. In the warming-up phase where even the system density matrix  $\rho_s$  does not inherit the periodicity of the driving protocol, one naturally expects a nonzero  $\mathcal{A}(m)$ . In the limit-cycle phase,  $A(m)$  vanishes only when the system-bath coupling is negligible compared to the system energy scale since then  $\mathcal{A}(m) \simeq \text{Tr}_{S} \{ H_{S}(mT)$  $[\rho_S((m+1)T) - \rho_S(mT)]$ } = 0. Otherwise, at strong<br>counting we still have  $A(m) \neq 0$  as  $(H_1(mT)) \neq$ coupling, we still have  $\mathcal{A}(m) \neq 0$  as  $\langle H_1(mT) \rangle \neq 0$  $\langle H_1((m+1)T) \rangle$  [see discussion before Eq. [\(4\)\]](#page-1-0). This result contradicts previous studies (see, e.g., Ref. [\[24\]](#page-4-7)), which neglected the contribution from  $\mathcal{A}(m)$  regardless of system-bath coupling strength. This first law and the nontrivial behavior of  $\mathcal{A}(m)$  represent our first main result. As for the second law of thermodynamics, we still observe the conventional Clausius inequality [\[13](#page-4-9)[,42,](#page-5-6)[51](#page-5-13)],  $S(m) \equiv \left[ S_S((m+1)T) - S_S(mT) \right] - \sum_v \hat{\beta}_v \hat{Q}_v(m) \ge 0$ <br>with  $S_c(m) = -\text{Tr}[\hat{Q}_c(mT) \ln \hat{Q}_c(mT)]$  the von Neumann with  $S_S(m) = -\text{Tr}[\rho_S(mT) \ln \rho_S(mT)]$  the von Neumann<br>entrony of the working substance. Here  $\beta$  are the inverse entropy of the working substance. Here,  $\beta<sub>v</sub>$  are the inverse temperatures of the heat baths.

<span id="page-2-0"></span>Using Eq. [\(4\),](#page-1-0) the averaged thermodynamic efficiency over a cycle,  $\eta(m) \equiv -[\mathcal{W}(m)/\mathcal{Q}_h(m)]$ , reads

$$
\eta(m) = \eta_0(m) - \frac{\mathcal{A}(m)}{\mathcal{Q}_h(m)}.
$$
\n(6)

Here,  $\eta_0 = 1 + \mathcal{Q}_c/\mathcal{Q}_h$  is the common definition of efficiency [\[16,](#page-4-10)[18,](#page-4-4)[21](#page-4-11)–[23](#page-4-12)], which has been applied to strong coupling scenarios [\[17](#page-4-13)[,24\]](#page-4-7). Intriguingly,  $\eta(m)$  gains an additional contribution  $\mathcal{A}(m)/\mathcal{Q}_h(m)$ , compared to  $\eta_0(m)$ . We point out that Eq. [\(6\)](#page-2-0) is completely general: It can be applied to arbitrary PD-QTMs in both the warming-up and limit-cycle phases, regardless of the system-bath coupling strength. On the contrary,  $\eta_0(m)$  can only be applied to the weak-coupling scenario in the limit-cycle phase where  $\mathcal{A}(m)$  vanishes [see discussion below Eq. [\(5\)\]](#page-1-1). This working definition for the efficiency is our second main result.

<span id="page-2-1"></span>Example: Driven resonant level engine.—To substantiate and exemplify our main results [cf. Eqs. [\(4\)](#page-1-0)–[\(6\)](#page-2-0)] we present a numerical example of a quantum Otto heat engine (see Fig. [1](#page-1-2)) that extracts work from heat baths with a resonant level model [[44,](#page-5-8)[45](#page-5-14),[47](#page-5-10),[48](#page-5-15),[52](#page-5-16)–[57](#page-5-17)],

$$
H_S(t) = \epsilon(t)c_d^{\dagger}c_d,
$$
  
\n
$$
H_B^v = \sum_k \epsilon_{kv}c_{kv}^{\dagger}c_{kv},
$$
  
\n
$$
H_I^v(t) = \lambda_v(t)\sum_k t_{kv}(c_{kv}^{\dagger}c_d + c_d^{\dagger}c_{kv}).
$$
\n(7)

Here, the working substance consists of a single spinless electronic level with the annihilation operator  $c_d$  and timedependent energy  $\epsilon(t)$ . The dot is alternating its coupling to two fermionic baths (leads)  $v = h$ , c of different temperatures.  $c_{kv}$  annihilates an electron with energy  $\epsilon_{kv}$  in the v lead that couples to the central level with  $t_{kv}$  as the tunneling rate. The  $v$  lead is occupied according to the Fermi-Dirac distribution with an inverse temperature  $\beta_v$ and a chemical potential  $\mu_{\nu}$ ; for our purpose, we set  $\beta_h \neq \beta_c$  and  $\mu_{h,c} = 0$ . The coupling of the central level to the leads is given by the spectral densities  $\Gamma_{v}(\epsilon) = 2\pi \sum_{k} t_{kv}^{2} \delta(\epsilon - \epsilon_{kv})$ . In what follows, we consider the wideband limit  $\Gamma(\epsilon) = \Gamma$  and adopt symmetric the wideband limit,  $\Gamma_v(\epsilon) = \Gamma_v$  and adopt symmetric couplings,  $\Gamma_{hc} = \Gamma$ . The time-dependent coefficients  $\lambda_{v}(t)$  equal 1 when the coupling to the v lead is turned on and 0 otherwise, thus enabling thermalization strokes in the standard Otto cycle.

The complete Otto cycle with period  $\mathcal T$  consists of four strokes; see Fig. [1](#page-1-2) for an illustration: (i) Stroke 1  $(0 \le t < t_1)$ : In this isochoric thermalization step, the central level with a fixed energy  $\epsilon_1$  is coupled to the hot lead. (ii) Stroke 2 ( $t_1 \le t < t_1 + t_2$ ): The energy of the isolated central level is shifted from  $\epsilon_1$  to  $\epsilon_2$ . (iii) Stroke 3  $(t_1 + t_2 \le t < t_1 + t_2 + t_3)$ : In this isochoric thermalization step, the central level with a fixed energy  $\epsilon_2$  is coupled to the cold lead. (iv) Stroke 4 ( $t_1 + t_2 + t_3 \le t < T$ ): The energy of the isolated central level is tuned back from  $\epsilon_2$  to  $\epsilon_1$ . We remark that the adopted cycle protocol does not enforce a periodicity on the system density matrix *a priori*. The engine needs a transient warming-up process before settling into a limit-cycle operation mode. We note that the amount of work generated during strokes 2 and 4 is independent of the detailed functional form of  $\epsilon(t)$  connecting fixed end points  $\epsilon_{1,2}$  as the charge occupation of the central level during these two strokes remains fixed; in Ref. [[58](#page-5-18)], we exploit this fact together with an equilibrium charge occupation expression [[59](#page-5-19)] (note that we attach the central level to two leads alternately in the Otto cycle) to estimate the heat-engine operation regime.

The cycle number-dependent thermodynamics is simulated by employing the driven Liouville von Neumann equation method [[60](#page-6-0)–[64](#page-6-1)] whose performance for addressing quantum thermodynamics up to strong coupling has been carefully assessed [[45](#page-5-14),[56](#page-5-20)]; we relegate simulation details, including numerical implementation, initial condition at  $t = 0$  and adopted parameter values, to [[58](#page-5-18)]. A typical set of thermodynamic results is depicted in Fig. [2](#page-3-0).

The behavior of  $\mathcal{A}(m)$  along with the work  $\mathcal{W}(m)$  is presented in Fig. [2\(a\);](#page-3-0) results for the heat exchange can be found in Ref. [[58](#page-5-18)]. We find that as the coupling strength increases, the magnitude of  $\mathcal{A}(m)$  becomes more pronounced. From this it is evident that based on our heat and work definitions, the complete first law of thermodynamics at all times should read  $W + \sum_{v} Q_v - A = 0$  as depicted in Fig. [2\(b\)](#page-3-0). In contrast, the sum  $W + \sum_{v} Q_v$  considered in other studies (see, e.g., Refs. [\[18](#page-4-4)[,24\]](#page-4-7)) approaches zero only in the weak-coupling scenario, and in the limit-cycle stage [see red line for  $\Gamma = 0.02$  in Fig. [2\(b\)](#page-3-0) at  $m = 5$  where the

<span id="page-3-0"></span>

FIG. 2. (a)  $\mathcal{A}(m)$  [cf. Eq. [\(5\)\]](#page-1-1) as a function of the number of cycles m (note  $m + 1$  is the number of completed cycles) while varying the coupling strengths,  $\Gamma = 0.02$  (red circles),  $\Gamma = 0.05$  (blue squares),  $\Gamma = 0.2$  (purple left-triangles) and  $\Gamma = 0.5$  (green right-triangles). Inset: Net injected work  $W(m)$  [cf. Eq. [\(2\)\]](#page-1-4) as a function of m while varying coupling strengths. (b) Comparison between the function  $\mathcal{F}(m) \equiv \mathcal{W}(m) + \sum_{v} \mathcal{Q}_v(m) - \mathcal{A}(m)$  (empty symbols), which constitute the correct first law, and its incomplete counterpart  $\mathcal{F}_0(m) \equiv$  $W(m) + \sum_{v} Q_v(m)$  (solid symbols) as a function of m for  $\Gamma = 0.02$  (red squares) and  $\Gamma = 0.5$  (green triangles). (c) Thermodynamic efficiency  $\eta(m)$  defined for a cycle  $[mT, (m+1)T]$  [cf. Eq. [\(6\)\]](#page-2-0) as a function of m with varying coupling strengths  $\Gamma = 0.02$  (red<br>circles)  $\Gamma = 0.05$  (blue squares)  $\Gamma = 0.2$  (purple left-triangles) and  $\Gamma = 0.5$  (green circles),  $\Gamma = 0.05$  (blue squares),  $\Gamma = 0.2$  (purple left-triangles) and  $\Gamma = 0.5$  (green right-triangles). Inset: The incomplete efficiency  $\eta_0(m) = 1 + \mathcal{Q}_c(m)/\mathcal{Q}_h(m)$  as a function of m. Lines in the main plots are drawn for guidance. Other dimensionless parameters are  $\beta_h = 0.2$ ,  $\beta_c = 1.5$ ,  $\mu_h = \mu_c = 0$ ,  $\epsilon_1 = 2$ ,  $\epsilon_2 = 1$ ,  $t_1 = t_3 = \mathcal{T}/3$ , and  $t_2 = t_4 = \mathcal{T}/6$  with  $\mathcal{T} = 60$ .

engine is reaching the limit-cycle phase; this is confirmed in Ref. [[58](#page-5-18)] with a long-time simulation for  $\Gamma = 0.02$ ]. Importantly, beyond the weak coupling regime, the faulty first law that neglects the  $A$  term deviates from zero  $at$  all times. Perhaps most surprisingly, Fig. [2\(c\)](#page-3-0) reveals that if one adopts the incomplete definition of efficiency, i.e., Eq. [\(6\)](#page-2-0) without  $\mathcal{A}$ , at strong coupling one would predict no heat engine behavior in this regime [see inset of Fig. [2\(c\)](#page-3-0)]. However, by properly including the  $A$  contribution, thus accounting for the effect of system-bath coupling, we find that the system does operate as a heat engine, consistent with the negative injected work value reported in the inset of Fig. [2\(a\)](#page-3-0).

Besides the aforementioned basic features that reinforce the validity of our general theory, there are a few points worth discussing further: (i) Weak coupling scenarios need more transient cycles to warm up than the strong coupling counterparts before a limit-cycle phase sets in. Comparing the behaviors of  $\mathcal{A}(m)$  and  $\eta(m)$  as a function of m, we argue that the former can assess the number of transient cycles based on its magnitude variation with increasing m. For instance, from Fig. [2\(a\)](#page-3-0), we observe that an engine of  $\Gamma = 0.05$  requires at least 4 transient cycles; note  $m + 1$  is the number of completed cycles. In contrast, an engine with  $\Gamma = 0.5$  needs just one cycle to warm up. We have verified that the number of transient cycles is independent of the initial charge occupation of the central level. (ii) The thermodynamic efficiency  $\eta(m)$  does not reach a stationary value at strong couplings with increasing  $m$  [see curve for  $\Gamma = 0.5$  in Fig. [2\(c\)](#page-3-0)], noting that the heat  $\mathcal{Q}_{h,c}(m)$  depends on the state of the bath, which needs not be a periodic function; see [\[58\]](#page-5-18) for the behavior of  $\mathcal{Q}_{h,c}(m)$  while varying  $m$  and the coupling strength. This finding implies that a characterization based on a single cycle in the limitcycle phase may not be applicable at strong couplings. (iii) In our simulations,  $\eta(m)$  increases as the coupling strength increases. This seems at odds with some studies [\[17](#page-4-13)[,65\]](#page-6-2), which have observed the opposite trend. However, we point out that these studies used the incomplete definition  $\eta_0$ . Indeed, the inset of Fig. [2\(c\)](#page-3-0) shows that  $\eta_0$  $decreases$  as  $\Gamma$  increases, until it becomes invalid for very large coupling strength. This suggests that interactions with the baths are in fact helpful in the heat-work conversion process [\[25\]](#page-4-5). The dramatic qualitative difference between  $\eta_0$  and  $\eta$  highlights that the incomplete definition  $\eta_0$ , which only involves heats, should be used with caution in analyzing the performance of PD-QTMs.

Discussion.—One may argue that the  $\mathcal A$  term [cf. Eq. [\(5\)\]](#page-1-1) can be absorbed by redefining heat and work (see discussions in Refs. [\[44](#page-5-8)[,53](#page-5-21)[,55](#page-5-22)]). We would like to point out that (i) the work definition we adopted [cf. Eq.  $(2)$ ] already comprises the internal energy change of the total composite system, and (ii) introducing an effective bath Hamiltonian with the replacement  $H_B^v \to H_B^v + H_I^v/2$  [[44](#page-5-8),[53](#page-5-21),[55](#page-5-22)] and<br>accordingly modifying the heat definition [cf. Eq. (3)] one accordingly modifying the heat definition [cf. Eq. [\(3\)](#page-1-5)], one is still not able to eliminate the  $A$  term, by comparing the definitions Eqs. [\(3\)](#page-1-5) and [\(5\).](#page-1-1) After all, as we argued, the  $A$ term originates from the fact that periodicity breaks down at the ensemble average level even in the limit-cycle phase.

Recognizing the generic presence of  $A$ , it is tempting to explore whether the inclusion of work costs for the attachment and detachment of the working substance to and from the baths can affect the behavior of A. While here we switched between strokes by tuning  $\lambda_n(t)$  [see Eq. [\(7\)\]](#page-2-1) using a sharp step function alternating between 0 and 1, one could adopt a smooth function. We leave this point to future investigations.

A *direct* measurement of  $A$  is experimentally challenging since it requires measuring energy change associated with system-bath coupling. However, if we focus on the standard Otto cycle as adopted here, an indirect measurement scheme for inferring  $A$  is possible based on the first law of thermodynamics [cf. Eq. [\(4\)](#page-1-0)]: Work is fully determined by the driven system and heat can be evaluated via a two-time measurement scheme right before and after the thermalization strokes at which the system-bath interaction is turned off;  $A$  is the sum of work and two heats terms. In this sense, the efficiency  $\eta$  is also experimentally measurable, as it is just the ratio between work and heat from the hot bath. This indirect measurement scheme is fully compatible with current experimental capabilities, an example being a quantum Otto engine based a driven spin- $1/2$  [[32](#page-5-23)] in which work was evaluated using an interferometric approach and the averaged heat was accessed by a two-time measurement protocol. Hence, our framework, which provides a complete characterization of the efficiency as a function of the cycle number, can be experimentally verified.

In summary, we presented a unified, consistent thermodynamic theory with cycle-number dependent thermodynamic quantities. The framework describes the operation of generic PD-QTMs both before and during the limit-cycle phase, and it properly treats strongly coupled thermal machines. We expect this framework to promote the development of PD-QTMs.

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