

## Itinerant Conductance in Fuse-Antifuse Networks

Cesar I. N. Sampaio Filho,<sup>1,\*</sup> André A. Moreira,<sup>1</sup> Nuno A. M. Araújo,<sup>2</sup> José S. Andrade Jr.,<sup>1,3</sup> and Hans J. Herrmann<sup>1,3</sup>

<sup>1</sup>*Departamento de Física, Universidade Federal do Ceará, 60451-970 Fortaleza, Ceará, Brazil*

<sup>2</sup>*Departamento de Física, Faculdade de Ciências, Universidade de Lisboa, P-1749-016 Lisboa, Portugal, and Centro de Física Teórica e Computacional, Universidade de Lisboa, P-1749-016 Lisboa, Portugal*

<sup>3</sup>*Computational Physics for Engineering Materials, IfB, ETH Zurich, Schafmattstrasse 6, 8093 Zurich, Switzerland*

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We report on a novel dynamic phase in electrical networks, in which current channels perpetually change in time. This occurs when the elementary units of the network are fuse-antifuse devices, namely, become insulators within a certain finite interval of local applied voltages. As a consequence, the macroscopic current exhibits temporal fluctuations which increase with system size. We determine the conditions under which this exotic situation appears by establishing a phase diagram as a function of the applied field and the size of the insulating window. Besides its obvious application as a versatile electronic device, due to its rich variety of behaviors, this network model provides a possible description for particle-laden flow through porous media leading to dynamical clogging and reopening of the local channels in the pore space.

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Fluid flow through a porous medium is frequently described in terms of a complex network system of steady-state flow channels, which are more or less tortuous depending on the strength of the disorder [1,2]. Preferential channeling in these systems is a result of minimizing the dissipated energy or flow resistance and is thus typically unique. When the fluid erodes and deposits material, however, the clogging and reopening of channels depends on the evolution of local conditions. We will show here using an electrical analog model that, under certain conditions, a new itinerant state can be attained in which these preferential channels constantly change their locations.

A plausible electrical analog for this complex fluid dynamical system is a network in which each link contains a reversible fuse-antifuse device [3–7], as described in Fig. 1(a). In an electrical circuit, a typical fuse behaves as a conductor if the voltage drop is below a given threshold  $v_I$  and becomes irreversibly an insulator otherwise. In the case of an antifuse, if the voltage drop exceeds a threshold  $v_C$ , its behavior changes abruptly from an insulator to a conductor. This type of switch has been widely used in programmable elements, in order to configure logic circuits and create customized designs [3,4]. As depicted in Fig. 1(b), more sophisticated devices, like programmable read-only memories [5], can intrinsically couple in their bits both fuse and antifuse behaviors in a reversible fashion, which are triggered one or another depending on the applied potential drop [5,8,9].

As shown in Fig. 1, our electrical analog model for particulate transport in a fluid flowing through a clogging-reopening pore space consists of a regular lattice where each link is a reversible fuse-antifuse device. More precisely, as described in Fig. 1(a), these elementary units have the same conductance  $g = 1$  while in the conducting state, namely for  $v < v_I$  and  $v > v_C$ , but are associated to

randomly distributed insulating and conducting threshold voltages,  $v_I$  and  $v_C$ , respectively [10–18]. The values of  $v_I$  are chosen from a uniform distribution in the interval  $[\epsilon, \epsilon + \Delta]$ , with  $\epsilon = 0.10$  and  $\Delta = 0.1$  or  $\Delta = 1.0$ . The conducting threshold is defined as  $v_C = sv_I$ , where  $s$  is a model parameter describing how much the insulating and

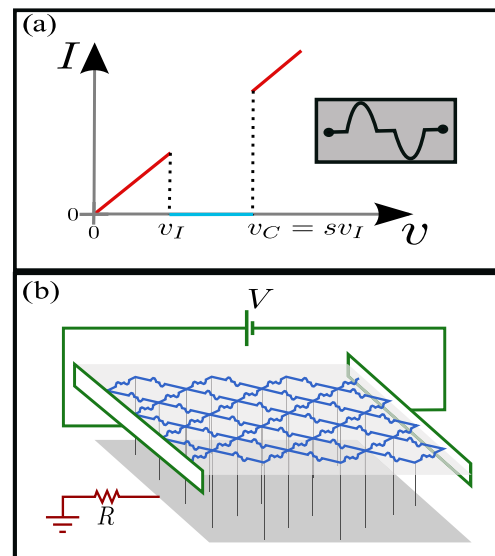


FIG. 1. (a) The  $I$ - $V$  behavior of the fuse-antifuse channel driven by a voltage drop  $v$ . If the voltage drop  $v$  is below the insulating threshold  $v_I$ , the channel has unitary conductance. If  $v_I < v < v_C$ , the channel is an insulator, and its conductance is set to zero. Finally, if the voltage drop is above the conducting threshold  $v_C$ , the channel is recovered with unitary conductance. (b) Representation of the fuse-antifuse network with each site of the lattice connected with nearest neighbors through a fuse-antifuse channel and connected to the ground through a link of high resistance  $R \gg 1$ .

conducting events are separated. Moreover, all sites of the lattice, except those at which the overall voltage drop is applied, are connected to the ground through a link of very high resistivity,  $R \gg 1$ . Therefore, sites that become eventually isolated during the dynamics will have zero potential.

We performed simulations with an initially filled tilted square lattice and apply a voltage drop  $V$  across it. Next, at each step, we solve Kirchoff's law [19] on each site in order to determine the voltage drop  $v_k$  on each bond  $k$ . After determining  $v_k$ , we proceed to identify which bonds will be insulators or conductors, by calculating for each bond the ratio,

$$R_k = \frac{|v_k|}{v_I}. \quad (1)$$

Any bond  $k$  with  $1 < R_k < s$  will be removed, that is, will have its conductivity set to zero in the following step. Note that this removal is reversible, that is, if the voltage drop between the end points of a removed bond changes and  $R_k$  becomes larger than  $s$ , the bond will be recovered to the system with original conductivity. Since the removal or recovery process is synchronous, that is, several bonds may change state at the same step, it is possible that entire regions of the system disconnect from both terminals. In this case, the potential in these regions becomes zero. Here, a time unit is defined in terms of a model iteration in which Kirchoff's law is simultaneously solved for all sites. After the corresponding voltage drops are computed, we can further identify which ones remain as insulators or conductors.

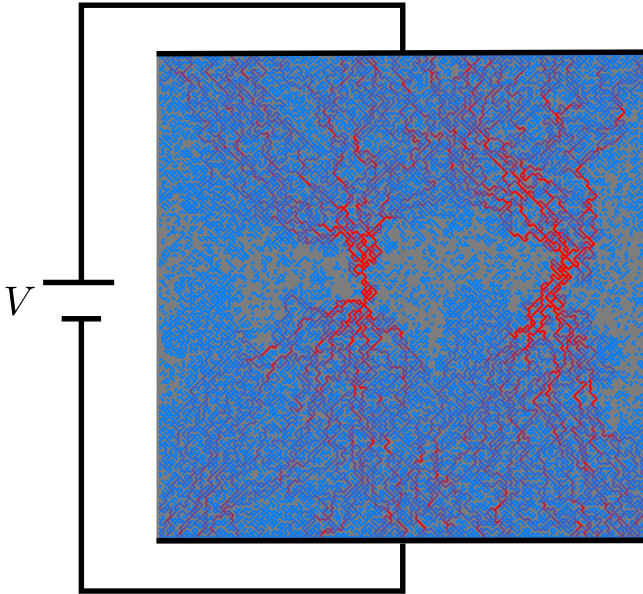


FIG. 2. Typical snapshot of the itinerant phase of the system at steady state, for a tilted square lattice with  $L = 96$ , voltage drop  $V = 192$  applied from top to bottom, and periodic boundary conditions from left to right. We used  $\Delta = 0.1$  and  $s = 384$ . Isolating bonds are represented in brown while conducting bonds are colored according to their local current intensity, from blue to red corresponding to low and high values, respectively.

A snapshot of the system at the steady state of the itinerant phase is shown in Fig. 2, where the bonds represent conducting channels colored according to their associated values of electrical currents. In order to quantify the macroscopic behavior of the system, we calculate the global conductance  $G = \sum_k v_k g_k / V$ , where  $V$  is the global voltage drop applied to the system, the summation stands for all fuse-antifuse elements along any line perpendicular to the direction where  $V$  is applied, and  $g_k$  is the conductance of the  $k$ th bond, here considered unitary.

Next, we consider the dependence of the global conductance  $G$  on the parameter space, defined in terms of the variables  $V \times s$ . As shown in Fig. 3, the time dependence of the conductance  $G$  can exhibit a rich variety of behaviors, depending on the applied voltage drop  $V$ . By fixing the values of  $\Delta = 0.10$ ,  $s = 12.8$ , and  $L = 128$ , for sufficiently low ( $V = 26$ ) and high ( $V = 1024$ ) values of the voltage drop, since all elements of the network remain in the conducting state, the system operates under an invariant and maximal conductance,  $G_{\max} = 1$ . For  $V = 32$  and  $64$ , the fuse-antifuse elements can dynamically change from insulators to conductors and vice versa in the network. As a consequence, after a transient period, the conductance is always finite,  $G > 0$ , but fluctuates around an approximately constant mean value. For  $V = 256$ ,  $G$  exhibits periodic peaks of maximal conductance at a frequency that is proportional to  $L^{-1}$ . Finally, for a larger voltage drop,  $V = 512$ , fluctuations are again observed in  $G$ , but now with episodes of insulator behavior,  $G = 0$ , due to eventual losses of global connectivity.

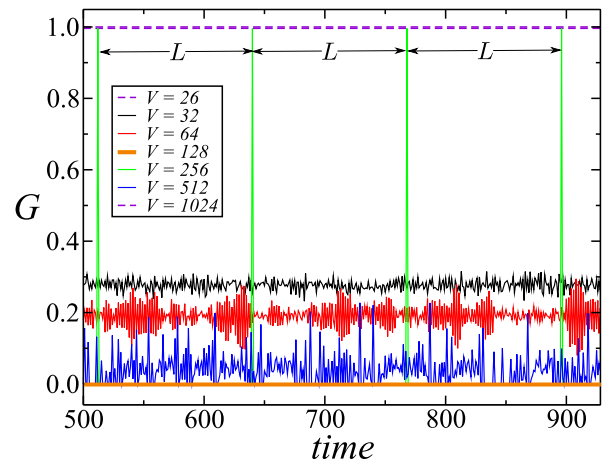


FIG. 3. The time dependence of the global conductance  $G$ . By fixing the values of  $\Delta = 0.10$ ,  $s = 12.8$ , and  $L = 128$ , for sufficiently low ( $V = 26$ ) and high ( $V = 1024$ ) values of the voltage drop, all elements of the network remain in the conducting state. For  $V = 32$  and  $64$ , the conductance is always finite,  $G > 0$ , but fluctuates around mean values. For  $V = 256$ ,  $G$  exhibits periodic peaks of maximal conductance at a frequency that is proportional to  $L^{-1}$ . Finally, for a larger voltage drop,  $V = 512$ , fluctuations are again observed in  $G$ , but now with episodes of insulator behavior,  $G = 0$ , due to eventual losses of global network connectivity.





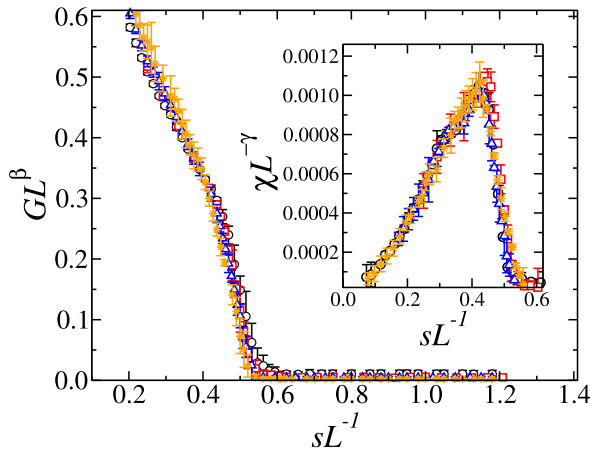


FIG. 7. Data collapse of the mean conductance for different lattice sizes  $L$  as a function of the parameter  $sL^{-1}$ , considering  $\Delta = 0.10$  and  $L = 32$  (circles), 48 (rectangles), 64 (triangles), and 96 (stars). Each data point is measured at the steady state during  $10^5$  time steps and averaged over 100 samples. The inset shows the data collapse of the weighted variance, defined as  $\chi_G = N(\langle G^2 \rangle - \langle G \rangle^2)$ , where  $N = 2L^2$  is the number of sites on the lattice. The best data collapse is obtained for  $\beta = 0.58$  and  $\gamma = 1.70$ . Both results suggest that the fuse-antifuse model undergoes a continuous phase transformation from a conductive to an insulating phase.

Along the line  $V = V_a$  of the phase diagram, as we increase the parameter  $sL^{-1}$ , the system undergoes a phase transformation from the itinerant (nonperiodic) to the insulating phase (the horizontal dashed line in Fig. 4). In order to characterize this transformation, we analyze the global conductance and its fluctuations near the transition point between the phases, by fixing  $V = V_a$  and changing the parameter  $sL^{-1}$ . In the main plot of Fig. 7, we show the data collapse of the global conductance as a function of  $sL^{-1}$ , considering  $L = 32, 48, 64,$  and  $96$ . Each data point is measured at steady state during  $10^5$  time steps and averaged over 100 samples. The best data collapse is obtained using the exponent  $\beta = 0.58$ . The results shown in Fig. 7 suggest that the fuse-antifuse model undergoes a continuous transition from an itinerant to an insulating phase, at a specific scale invariant value  $s_c L^{-1}$ . This is corroborated by the results presented in the inset of Fig. 7, where we show the data collapse of the weighted variance  $\chi_G$ , with  $\chi_G = N(\langle G^2 \rangle - \langle G \rangle^2)$ , using the exponent  $\gamma = 1.70$ .

In summary, we have introduced a fuse-antifuse network model which exhibits a regime of itinerant conductivity. At fixed external potential, the conductance spontaneously fluctuates with an amplitude that increases with system size. This novel itinerant regime is in some sense similar to the dynamics of braiding rivers [30] and might help to understand flicker noise [31–33] and similar phenomena where spontaneous macroscopic fluctuations appear. Concerning the eroding and depositing fluid flowing through a porous medium, very recent experiments do

indeed seem to show, under certain conditions, intermittently fluctuating permeabilities [34].

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\*Corresponding author.

cesar@fisica.ufc.br

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