

Strong Single-Photon Coupling in Superconducting Quantum Magnetomechanics

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We show that the inductive coupling between the quantum mechanical motion of a superconducting microcantilever and a flux-dependent microwave quantum circuit can attain the strong single-photon nanomechanical coupling regime with feasible experimental parameters. We propose to use a superconducting strip, which is in the Meissner state, at the tip of a cantilever. A pickup coil collects the flux generated by the sheet currents induced by an external quadrupole magnetic field centered at the strip location. The position-dependent magnetic response of the superconducting strip, enhanced by both diamagnetism and demagnetizing effects, leads to a strong magnetomechanical coupling to quantum circuits.

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In quantum nanomechanics, the strength of the radiation-pressure interaction between a single electromagnetic mode of frequency ω and a micromechanical mode of frequency Ω and effective mass M is denoted by g_0 , the so-called single-photon coupling rate [1]. This is the cavity frequency shift due to a zero-point motion displacement of the mechanical oscillator, given by $z_{zp} = [\hbar/(2M\Omega)]^{1/2}$, namely, $g_0 = z_{zp} \partial\omega/\partial z|_{z=0}$. The single-photon coupling, being nonlinear, could be exploited to observe non-Gaussian physics in micromechanical oscillators [2–7], a goal that would represent a milestone in the field [1]. However, this is today experimentally very challenging. The mechanical mode (electromagnetic mode) suffers decoherence with a rate Γ (κ) whose origin depends on the particular experimental implementation. To fully exploit the non-Gaussian character of the single-photon nanomechanical coupling, one would like to operate in the strong-coupling regime $g_0 \gtrsim \Gamma, \kappa$ as well as in the resolved sideband regime $\Omega/\kappa \gtrsim 1$. The latter is required to sideband cool the mechanical mode into the ground state [8–10]. While $g_0/\Gamma \gtrsim 1$ and $\Omega/\kappa \gtrsim 1$ has been achieved simultaneously in several experiments [1], the so-called single-photon strong coupling regime $g_0/\kappa \gtrsim 1$ is much more challenging. Indeed, according to [1], the highest values of g_0/κ obtained so far with solid mesoscopic objects are $\sim 10^{-3}$ [11,12] (with cold gases one achieves $g_0/\kappa \sim 1$ [13,14] but not in the resolved sideband regime).

In this Letter, we propose a microwave optomechanical scenario, see Fig. 1, where we show that the strong single-photon regime $g_0/\kappa \gtrsim 1$ can be achieved in the resolved sideband regime with feasible experimental parameters. Contrary to most of the current experiments in microwave optomechanics [1,12], where the optomechanical coupling is implemented capacitively, here, we motivate to use an inductive coupling to a flux-dependent quantum circuit as a

way to obtain 3 orders of magnitude stronger couplings. Such a strong quantum *magnetomechanical* (MM) coupling is achieved via the magnetic response of a superconducting (SC) strip in an inhomogeneous external field that is strengthened by the large diamagnetic and demagnetizing effects of superconducting strips in the Meissner state [15,16]. This contrasts to other experiments and proposals on quantum magnetomechanics that do not exploit this fact and thus, do not achieve such strong couplings, see, for instance, [17–21].

The quantum MM coupling to a flux-dependent quantum circuit can be obtained as follows. While, in principle, one just requires a quantum circuit with a SQUID loop, here,

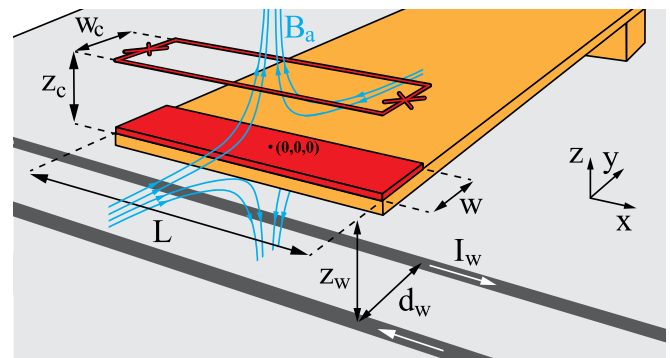


FIG. 1 (color online). Schematic illustration of the proposal (not to scale). A superconducting strip of length L and width w is deposited on the tip of the cantilever. At a distance z_c above the cantilever, a pickup coil of the same length and width w_c , which is fabricated on a wafer not shown for clarity, collects the flux generated by the currents in the strip induced by an external quadrupole field B_a . The B field is generated by two parallel wires with opposite current of intensity I_w , separated by a distance d_w , and placed below the cantilever at a distance z_w . An additional perpendicular bias field creates a zero field at the strip position.

we use the particular example of a transmon qubit [22] that operates as a slightly anharmonic inductance-capacitance (LC) oscillator with creation (annihilation) mode operators \hat{a}^\dagger (\hat{a}). The Hamiltonian can be written as $\hat{H} = \hbar\omega(z_m)\hat{a}^\dagger\hat{a} + \hbar\beta\hat{a}^\dagger\hat{a}^\dagger\hat{a}\hat{a}/2$, where $\hbar\omega(z_m) = [8E_J(z_m)E_C]^{1/2} - E_C$, $E_J(z_m) = 2E_{J_1} \cos[\pi\Phi(z_m)/\Phi_0]$, $\hbar\beta = -E_C$, Φ_0 is the flux quantum, and z_m is the position of the superconducting strip along the z axis, as described in more detailed below. Here, E_C is the charging energy of a single electron stored in the capacitance, and E_{J_1} is the energy associated with an electron tunneling across one of the two identical junctions. The transmon regime requires $E_J/E_C \gg 40$. Hereafter, we will not use the anharmonic term, which can be a resource for many applications, and will only focus on the flux-dependent microwave harmonic oscillator. The flux threading the pickup coil $\Phi(z_m)$ depends on the z displacement of the mechanical oscillator from the equilibrium position $z_m = 0$, which is given by $z_m = z_{zp}(\hat{b}^\dagger + \hat{b})$. By expanding $\omega(z_m)$ around $z_m = 0$, one arrives at the standard single-photon coupling nanomechanical Hamiltonian [1] $\hat{H} = \hbar\omega\hat{a}^\dagger\hat{a} + \hbar\Omega\hat{b}^\dagger\hat{b} - \hbar g_0\hat{a}^\dagger\hat{a}(\hat{b}^\dagger + \hat{b})$ with $\omega = \omega(0)$ and $g_0 = \phi\omega_0\eta$, where $\hbar\omega_0 \equiv [8E_{J_1}E_C]^{1/2}$, $\phi \equiv \pi \sin(\pi\Phi(0)/\Phi_0)/[2\cos(\pi\Phi(0)/\Phi_0)]^{1/2}$, and

$$\eta \equiv \left. \frac{z_{zp}}{\Phi_0} \frac{\partial \Phi(z)}{\partial z} \right|_{z=0}. \quad (1)$$

The dimensionless parameter η quantifies the MM coupling to any quantum circuit since it is the variation of flux (in units of Φ_0) in the pickup coil due to a zero-point motion displacement of the mechanical oscillator. The decoherence rate of the quantum circuit can be generally expressed as $\kappa = \omega_0/Q$, where Q is the circuit quality factor. Therefore, the ratio between the single-photon coupling and κ is given by $g_0/\kappa = \phi Q\eta$. The parameter ϕ can be tuned by varying $\Phi(0)$. Consequently, the MM coupling can be switched on (switched off) by operating at the linear (quadratic) regime, e.g., $\Phi(0)/\Phi_0 \sim 1/4$ (e.g., $\Phi(0)/\Phi_0 = 0$), where $\phi \sim 2$ ($\phi = 0$). Note that since values of $Q \sim 10^6$ have been measured [23,24], the strong single-photon regime $g_0/\kappa \gtrsim 1$ could be thus achieved provided $2\eta \gtrsim 10^{-6}$. In the following, we propose and analyze a setup where such regime could be achieved.

We consider a thin SC strip occupying the region $x \in [-L/2, +L/2]$, $y \in [-w/2, +w/2]$, and $z \in [z_m - t/2, z_m + t/2]$, with $L \gg w \gg t$, see Fig. 1. The SC strip is assumed to harmonically oscillate along the z axis, with equilibrium position at $z_m = 0$ and harmonic frequency Ω . This can be achieved, for instance, by depositing the SC strip at the tip of a nonmagnetic micromechanical cantilever of thickness t_0 , width L , and mass density ρ_0 , see Fig. 1. In the calculation of the single-photon radiation pressure coupling, the effective mass of the mechanical oscillator

can be approximated by [25] $M = Lw(\rho t + \rho_0 t_0)$, where ρ is the mass density of the SC material. A rectangular pickup coil covering the area $x \in [-L/2, +L/2]$, $y \in [-w_c/2, +w_c/2]$ is placed at $z = z_c$ on a second wafer. The SC strip, which is considered to be in the Meissner state, fulfills that either the London penetration depth $\lambda \ll t$ or, if $\lambda \gtrsim t$, the two-dimensional screening length $\Lambda \equiv \lambda^2/t \ll w$ [15,16]. It is also assumed that $t > \xi$, where ξ is the superconducting coherence length. Under these standard conditions, one can treat the magnetic response of the SC strip using London theory [15,16].

The MM coupling is established by applying an external \mathbf{B} field to the SC strip in the Meissner state. Due to the diamagnetic response of the SC strip, currents are induced to have a zero total \mathbf{B} field in the interior of the sample [15,16]. The flux threading the pickup coil generated by the induced strip currents depends on the strip z position of the cantilever. Stronger couplings are obtained when an inhomogeneous field with a gradient along z is applied. The reason is that the induced currents depend in this case on the position of the cantilever and therefore, η scales as $1/z_c$ for $z_c \gtrsim w$. This contrasts with the case of a homogenous applied field since then the position-dependent flux only arises because the distance between the cantilever and the pickup coil changes, thereby leading to $\eta \propto 1/z_c^2$. A convenient inhomogeneous magnetic field, with a gradient along z , and uniform along the x axis (the long axis of the strip), is given by the quadrupolar field $\mathbf{B}_a(y, z) = b(-y\mathbf{e}_y + z\mathbf{e}_z)$, where the gradient b is constant, and its maximum value is limited to ensure field strengths in the strip are below its critical field.

The induced currents in the SC strip in the presence of the applied field \mathbf{B}_a can be calculated as follows. Since one needs the field generated by the induced currents at a distance $z_c \gg t$, one can use the average sheet current $\mathbf{K}(y, z_m) \equiv \int_{z_m-t/2}^{z_m+t/2} \mathbf{J}(y, z) dz$, where \mathbf{J} is the volume current density. The currents are assumed to be independent on x since the applied field is homogeneous in x , $L \gg w$, and when $t \ll w$ the current distribution is not affected by the y component of the external field [26]. Moreover, we show in the Supplemental Material (SM) [27] that although \mathbf{B}_a is not uniform across t , the induced K_x only depends on the thickness-averaged external vector potential under the thin film approximation. Hence, when the strip is at some height $z = z_m$, K_x will be well approximated to that induced by a uniform out-of-plane field $\mathbf{B}_a = bz_m\hat{\mathbf{z}}$, namely, [15,16]

$$\mathbf{K}(y, z_m) = \frac{bz_m}{\mu_0} \frac{2y}{\sqrt{(w/2)^2 - y^2}} \mathbf{e}_x, \quad (2)$$

where μ_0 is the vacuum permeability. This current distribution expels the out-of-plane \mathbf{B} field from the interior of the sample, depends on the position of the cantilever z_m and is zero when $z_m = 0$.

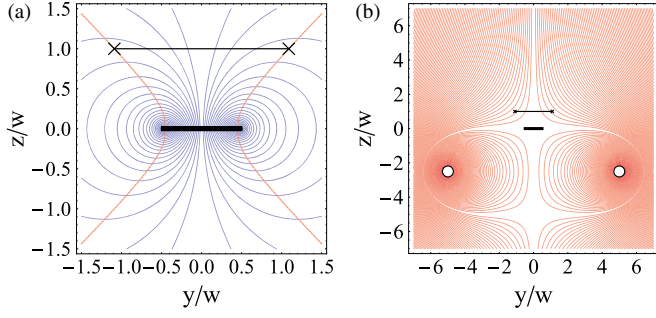


FIG. 2 (color online). **B**-field lines corresponding to the (a) field created by the induced currents \mathbf{B}_K and (b) the applied field created by two antiparallel wires (marked as white circles) and a bias field, see text. The SC strip (pickup coil) is illustrated to scale in both plots with a solid rectangle (solid line segment delimited by crosses). The dashed red line in (a) marks the optimal pickup coil width w_c^* for each pickup coil height z_c .

To obtain an analytical expression for η , one needs the vector potential generated by the strip currents. This can be calculated by integrating across the strip width the contributions from the infinitesimal narrow straight filaments that compose it, namely, $\mathbf{A}_K(y, z) = \int_{-w/2}^{w/2} d\mathbf{A}_K(y, y', z)$, where, using Ampère's law,

$$d\mathbf{A}_K(y, y', z) = -\frac{\mu_0 dI}{2\pi} \ln[(y - y')^2 + (z - z_m)^2] \hat{\mathbf{x}}, \quad (3)$$

with $dI = K_x(y', z_m) dy'$. Using Eq. (2), one obtains that $\mathbf{A}_K(y, z) = A_K(y, z) \mathbf{e}_x$ is given by

$$\frac{A_K(y, z)}{bz_m} = y - \frac{y}{|y|} \operatorname{Re} \left\{ \sqrt{[y + i(z - z_m)]^2 - \left(\frac{w}{2}\right)^2} \right\}. \quad (4)$$

In this particular longitudinal geometry, one can use the contour lines of the vector potential to plot the magnetic **B**-field lines [29] of $\mathbf{B}_K = \nabla \times \mathbf{A}_K$, as shown in Fig. 2(a). The magnetic flux threading the pickup coil is given by the contour integral of the vector potential along the coil wire.

This leads to $\Phi(z_m) = 2L_c A_K(w_c/2, z_c)$. Using Eq. (4) and recalling Eq. (1), one obtains $\eta = \eta_* \chi$, where

$$\chi \equiv \frac{w_c}{w} - \operatorname{Re} \left\{ \sqrt{\left(\frac{w_c}{w} + i \frac{2z_c}{w}\right)^2 - 1} \right\}. \quad (5)$$

The maximum value of η is given by $\eta_* \equiv z_{zp} b L_c w / \Phi_0$, which corresponds to the limit $w_c \rightarrow w$ and $z_c \rightarrow 0$. Given a coil distance z_c , the value of η is maximized for an optimal w_c^* which corresponds to the width for which the lateral long wires of the pickup coil coincide with the lines of $B_K^z = 0$ [see Fig. 2(a)]. Using w_c^* , η/η_* can be plotted as a function of z_c/w , see Fig. 3(a). At an experimentally feasible distance $z_c = w$, $\eta/\eta_* \approx 1.2 \times 10^{-1}$. At the same distance, an homogeneous external field would lead to $\eta/\eta_* \approx 1.9 \times 10^{-2}$, nearly an order of magnitude less, see SM [27] and Fig. 3(a).

The value of η_* , and thus of g_0/κ , is maximized when the maximum gradient b^{\max} allowing for superconductivity in the strip is used. That is, one requires $|\mathbf{B}_a + \mathbf{B}_K| < B_c$ at any point in the sample, where B_c is the first critical field from the SC strip material. By taking into account the demagnetizing effects [15,16], it is shown in the SM [30] that this leads to $b^{\max} = f(t/w) 2B_c/w$, where $f(x) = [1 + (\sqrt{2x} + x)(1 + x)]^{-1/2}$. Taking $L_c = L$, one arrives at

$$\eta_* = \frac{2B_c}{\Phi_0} f(t/w) \sqrt{\frac{\rho t}{\rho t + \rho_0 t_0} \frac{\hbar}{2\rho\Omega}} \sqrt{\frac{L_c}{tw}}, \quad (6)$$

that together with Eq. (5) gives an analytical expression for η and thus, g_0/κ . Hereafter, we consider niobium for the SC strip, with $B_c \approx 140$ mT and $\rho = 8.57 \times 10^3$ kg/m³, the strip dimensions $t = 50$ nm, $w = 1$ μ m, and $L_c = 100$ μ m, the cantilever to be made of silica with $\rho_0 = 2.3 \times 10^3$ kg/m³, $t_0 = 0.5$ μ m, and $\Omega = 2\pi \times 10^6$ Hz. Using $z_c = w$, $w_c = w_c^* \approx 2.2$ μ m, and $b^{\max} \approx 2.4 \times 10^5$ T/m, one obtains $2\eta \sim 20.4 \times 10^{-6}$. This is the main result of

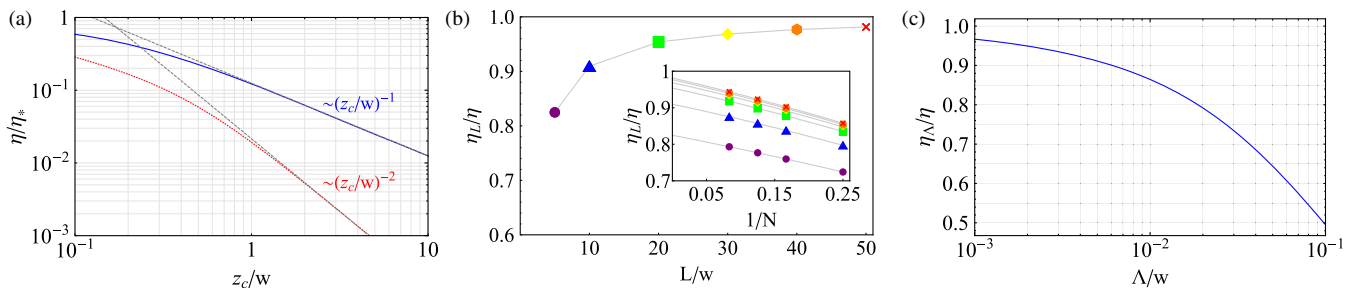


FIG. 3 (color online). (a) η/η_* as a function of z_c/w for the case of the quadrupole field (red blue line) corresponding to Eq. (5) and for a homogeneous field (dotted red line) corresponding to the expression given in the SM [27]. Dashed grey lines indicate the asymptotic scaling for $z_c/w \gtrsim 1$. (b) η_L/η values computed with MEM [30–32] for different finite strip lengths L/w . Inset shows the values obtained by extrapolating the results for different number of cells N in the MEM method. (c) η_L/η as a function of Λ/w calculated using the expression for the sheet currents given in [33] (see also SM [27]).

the Letter because $Q \approx 10^6$ has been experimentally measured [23,24], and thus, using the maximum gradient b_{\max} , this would lead to $g_0/\kappa \approx 20.4$, well within the single-photon strong coupling regime. Mechanical dampings of $\gamma \sim 2\pi \times 1$ Hz have been measured in low frequency mass-loaded cantilevers [34–36]. This would lead to mechanical decoherence rates of $\Gamma \approx \gamma K_b T / (\hbar \Omega) \sim 2\pi \times 6.5$ kHz at $T = 50$ mK, and hence, to a single-photon cooperativity $C = g_0^2 / (\kappa \Gamma) \sim 400$ (using the maximum gradient b^{\max}).

Let us now discuss two approximations that were used to calculate η : the distributions of fields and currents were those of (i) an infinite strip length with (ii) $\Lambda = 0$. Regarding (i), we have numerically computed η for $z_c = w$ and $w_c = w_c^*$ for finite L/w values. In Fig. 3(b), the ratio of η_L (computed with a finite L) with η (obtained with an infinite length) as a function of L/w is plotted. This has been done using the magnetic energy minimization (MEM) method [30–32]. As expected, η_L/η approaches unity as one increases L/w , with $\eta_L/\eta \sim 0.98$ already at $L/w = 50$ (with the values discussed above, one has $L/w = 100$). Regarding (ii), a finite Λ can be taken into account by using an approximated expression for the current distribution, see [33] and SM [27]. Using this, η_Λ/η (with η_Λ being the value of η for a finite Λ) can be plotted as a function of Λ/w , see Fig. 3(c). For niobium, $\lambda = 39$ nm and therefore, $\Lambda/w = 3 \times 10^{-2}$. This leads to $\eta_\Lambda/\eta \approx 0.73$ at $z_c = w$ and $w_c = w_c^*$. This validates approximations (i) and (ii).

To generate the ideal quadrupole \mathbf{B} field given by $\mathbf{B}_a = b(-y\mathbf{e}_y + z\mathbf{e}_z)$, we propose to use two thin long straight wires placed along the x axis, at some height $z = -z_w$ and $y = \pm d_w/2$, with $d_w = 4z_w$, see Fig. 2(b). The wire at $y = d_w/2$ ($y = -d_w/2$) has a positive (negative) current I_w , namely, along \mathbf{e}_x ($-\mathbf{e}_x$), see Fig. 1. An expression for the \mathbf{B} field generated by the wires \mathbf{B}_w can be straightforwardly obtained, see SM [27]. To have a zero field at the position of the strip, namely, at $z = 0$ and $y = 0$, one should add an out-of-plane bias field $\mathbf{B}_b = 4\mu_0 I_w / (5\pi z_w) \mathbf{e}_z$. The total field $\mathbf{B}_w + \mathbf{B}_b$ is very similar to the quadrupole field \mathbf{B}_a , see Fig. 2(b). In particular, the gradient along z is given by $\partial_z B_z|_{z=0} = b[1 + \alpha(2y/z_w)^2 + \mathcal{O}(y/z_w)^4]$, with $b = 16\mu_0 I_w / (25\pi z_w^2)$, and $\alpha = 72/100$. Since $|y| < w/2$, one can choose w/z_w to set the maximum inhomogeneity $\epsilon = [\partial_z B_z|_{y=w/2, z=0} - \partial_z B_z|_{y=0, z=0}] / b \ll 1$ to be as small as desired by using $w/z_w < \sqrt{\epsilon/\alpha}$. Restricting the maximum current intensity to the experimentally feasible value of $I_w = 1$ A, one has that for $z_w = 5.4 \mu\text{m}$ the gradient is $b \approx 4.1 \times 10^4$ T/m $\approx 0.17b^{\max}$ and therefore, $g_0/\kappa \approx 3.5$ and $C \sim 12$, still well within the single-photon coupling regime. We have numerically validated that the inhomogeneity in the gradient field leads to negligible corrections. With this configuration, the total \mathbf{B} field at the wire of the pickup coil at $z_c = 1 \mu\text{m}$ and $y = w_c^*/2 = 1.1 \mu\text{m}$ is ~ 62 mT.

The intensity in the wires and the strength of the bias field might fluctuate as $I_w(t) = I_w + \delta I_w(t)$ and $\mathbf{B}_b(t) = [B_b + \delta B_b(t)]\mathbf{e}_z$. The fluctuations of the intensity (bias field) are characterized by a power spectrum $S_{I(B)}(\omega)$, where $S_f(\omega) \equiv 2 \int_0^\infty \langle \delta f(t) \delta f(0) \rangle \cos(\omega t) dt$. Consequently, the flux threading the pickup coil will also fluctuate as $\Phi(t) = \Phi + \delta\Phi(t)$. It is shown in the SM [27] that $S_\Phi(\omega)/\Phi_0^2 = a_I^2 S_I(\omega)/I_w^2 + a_B^2 S_B(\omega)/B_b^2$, where the noise amplification dimensionless parameters are $a_I = 6.4 \times 10^3$ and $a_B = 1.4 \times 10^4$ (their exact expression is given in the SM [27]). To reduce the flux noise, one should thus use persistent currents and gradiometric configurations. The fluctuations on the external field might also lead to decoherence in the mechanical oscillator. As shown in the SM [27], the magnetic Lorentz force $\mathbf{F} = \int_V \mathbf{J}(\mathbf{r}) \times \mathbf{B}_a(\mathbf{r}) d\mathbf{r}$ for the external quadrupole trap leads to $\mathbf{F} = -M\Omega_m^2 z_m \mathbf{e}_z / 2$, where $\Omega_m = bw[L\pi/(4M\mu_0)]^{1/2} = 2\pi \times 59$ kHz $< \Omega$ [37]. Since the gradient fluctuates due to the wire intensity fluctuations, so does Ω_m . As shown in [38] and in the SM [27], this leads to Fock state transitions from level n to $n \pm 2$ with a rate given by $R_{0 \rightarrow 2} = \pi\Omega^2 S_I(2\Omega)/(4I_w^2) \sim 2\pi \times 0.5$ kHz for $[S_I(2\Omega)]^{1/2}/(I_w) = 10^{-5}/\text{Hz}^{1/2}$. This is 2 orders of magnitude smaller than g_0 and therefore should not compromise the strong-coupling regime.

In conclusion, we have shown that a very strong inductive coupling can be achieved between a SC strip in the Meissner state and a flux-dependent quantum circuit. This might allow us to attain the so-far experimentally challenging single-photon coupling regime in quantum nanomechanics. Such a strong coupling could also be used to exploit a linearized nanomechanical coupling to a superconducting qubit. This proposal might be employed as an experimental test bed for quantum magnetomechanics with levitated superconducting microspheres [39]. An interesting further direction for research is the possibility of exploiting type-II SC strips with controlled SC vortices to achieve even larger couplings. In this respect, this experimental scenario might offer an alternative tool to probe the rich physics of type-II superconductivity using the high sensitivity of microcantilevers near the quantum regime.

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