Evidence of Surface Loss as Ubiquitous Limiting Damping Mechanism in SiN Micro- and Nanomechanical Resonators

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Silicon nitride (SiN) micro- and nanomechanical resonators have attracted a lot of attention in various research fields due to their exceptionally high quality factors (Qs). Despite their popularity, the origin of the limiting loss mechanisms in these structures has remained controversial. In this Letter we propose an analytical model combining acoustic radiation loss with intrinsic loss. The model accurately predicts the resulting mode-dependent Qs of low-stress silicon-rich and high-stress stoichiometric SiN membranes. The large acoustic mismatch of the low-stress membrane to the substrate seems to minimize radiation loss and Qs of higher modes ($n \land m \ge 3$) are limited by intrinsic losses. The study of these intrinsic losses in low-stress membranes reveals a linear dependence with the membrane thickness. This finding was confirmed by comparing the intrinsic dissipation of arbitrary (membranes, strings, and cantilevers) SiN resonators extracted from literature, suggesting surface loss as ubiquitous damping mechanism in thin SiN resonators with $Q_{\text{surf}} = \beta h$ and $\beta = 6 \times 10^{10} \pm 4 \times 10^{10}$ m⁻¹. Based on the intrinsic loss the maximal achievable Qs and Qf products for SiN membranes and strings are outlined.

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Since the discovery of the exceptionally high quality factors (Q) of nanomechanical silicon nitride (SiN) resonators [1,2], SiN strings and membranes have become the centerpiece of many experiments in the fields of cavity optomechanics [3–14] and sensor technology [15–20]. For example, in cavity optomechanics a high Q at high frequencies is required in order to advance towards the quantum regime of the mechanical resonators, and in resonant sensors a high Q enables a better resolution. Despite the continuous effort to understand and optimize Q of SiN resonators, the underlying source of the limiting mechanism has remained controversial. On the one hand, it has been suggested by several groups that SiN resonators are limited by intrinsic losses [21–23]. Conversely, it has recently been suggested that radiation loss is the limiting factor for Q in SiN membranes [24]. In this Letter we show that a model which combines intrinsic and acoustic radiation losses accurately predicts the mode-dependent Qs of low- and high-stress SiN membranes. Finally, we show that the intrinsic loss in thin arbitrary SiN resonators scales with thickness. This is evidence that surface loss is the ubiquitous limiting damping mechanism in micro- and nanomechanical SiN resonators.

The exceptionally high Qs of SiN resonators originate from the high intrinsic tensile stress σ which increases the stored energy without significantly increasing the energy loss during vibration [21,22,25]. Assuming the energy loss to be coupled to the local out-of-plane bending during vibration, the intrinsic quality factor of a square membrane under tensile stress $Q_{\text{intr},\sigma}$ is given by [25]

$$Q_{\text{intr.}\sigma} \approx Q_{\text{intr}} [2\lambda + (n^2 + m^2)\pi^2\lambda^2]^{-1}, \tag{1}$$

with $\lambda = (h/L)\sqrt{E/(12\sigma)}$ where Q_{intr} is the intrinsic quality factor of the relaxed resonator without the tensile stress (like, for example, a cantilever), n, m are the mode numbers, E the Young's modulus, h the thickness, L is the side length, and σ is the tensile stress. The expression for strings can also be developed and the final result is (1) with m = 0 and n as the mode number, which is equal to an earlier model for Q of loaded wires [26]. The value in square brackets in (1) is a Q-enhancing factor that comprises two terms. The left term is independent of the mode number and comes from the local curvature of the resonator at the clamped ends. The right term is dependent on the mode numbers and originates from the curvature of the antinodes. As per definition of a string or membrane $\lambda \ll 1$ [27]. Hence, the left term is a lot larger, that is, the damping due to the membrane curvature at the clamped ends usually dominates $Q_{\text{intr.}\sigma}$. The local bending at the clamping is decreasing exponentially with a decay length $L_c = L\lambda$ [25,26,28]. For stoichiometric SiN $L_c \approx 5 \times h$ and the peak intrinsic damping for a 30 nm thick resonator thus happens within a 150 nm wide band at the resonator ends close to the clamping.

Besides the intrinsic energy loss, the resonators can lose energy through phonons tunneling into the substrate, so-called acoustic radiation loss. It has been suggested that acoustic radiation loss in SiN membranes is strongly mode dependent and that modes with low mode numbers typically are limited by radiation loss [29]. An analytical model based on the coupling of membrane modes to free modes of the substrate has been fully developed [29,30]. For the sake of simplicity, we provide here the asymptotic limit for a square membrane

$$Q_{\rm rad} \approx 1.5 \alpha \frac{\rho_s}{\rho_r} \eta^3 \frac{n^2 m^2}{(n^2 + m^2)^{3/2}} \frac{L}{h}$$
 (2)

with the "acoustic mismatch" (phase velocity ratio) between a semi-infinite substrate and the resonator $\eta \approx \sqrt{(E_s/\sigma)(\rho_r/\rho_s)}$ with the mass densities ρ_s and ρ_r of the substrate and resonator, respectively, and the Young's modulus of the substrate E_s . The prefactor α is a fitting parameter correcting for substrate imperfections resulting from the specific chip mounting conditions. Under ideal conditions of a semi-infinite substrate $\alpha = 1$. Equation (2) is valid under the condition $n, m \gg \sqrt{n^2 + m^2}/\eta$. Typically, $\eta \gg 1$ for SiN membranes and thus the radiation loss model is valid for all $n \sim m$. Destructive interference of the waves radiating into the substrate can lead to a suppression of the acoustic radiation loss for increasing harmonic modes (n = m) [29]. From (2) it can be seen that acoustic radiation loss is minimal for harmonic modes n=m and the envelope of maximal values is increasing linearly with the mode numbers $Q_{\rm rad} \propto n$. For strings, $Q_{\rm rad} \propto L/w$ is predicted to be a function of the string width w [31]. This effect has been observed with SiN strings where Q increased with decreasing width and approached an asymptotic limit given by intrinsic losses [21].

According to (2), $Q_{\rm rad}$ is a function of the acoustic mismatch η between the resonator and a semi-infinite substrate. This has recently been demonstrated with nanomechanical SiN strings whose Qs deteriorate when the acoustic mismatch is reduced by touching the anchor area with an AFM tip [32]. It has repeatedly been shown that especially lower mode Qs are sensitive to the chip mounting conditions and that these Qs can be increased by minimizing the contact between chip and support [7,21,24,33]. A successful way of suppressing radiation losses is to locate the mechanical structure within a well-designed phononic band gap structure. This removes the free frame modes around the membrane and suppresses the probability of phonon tunneling, i.e., radiation loss [34,35]. The measured maximal Os of modes with negligible radiation loss of such a SiN membrane had maximal Q values that correspond to expected values obtained with similar membranes without the phononic band gap. This is strong evidence that Qs in SiN membranes ultimately can be limited by intrinsic losses if the chip is mounted carefully. This notion is supported by the comparison of specific examples of Q values of stoichiometric SiN strings [22] and membranes [24] from literature to the intrinsic (1) and acoustic radiation loss (2) models (see Supplemental Material [36]). It suggests that intrinsic loss is limiting Q in both cases, which contradicts the conclusions made in [24] that radiation loss is the limiting mechanism.

There are strong indications that the overall mode dependence of Q is best described by a combination of both models. In order to test this we compare low-stress silicon-rich SiN (SR-SiN) (from Norcada) and high-stress stoichiometric SiN (fabricated in-house) membrane Q data

to a combined model that takes into account both intrinsic and acoustic radiation losses

$$Q^{-1} = Q_{\text{infr}\,\sigma}^{-1} + Q_{\text{rad}}^{-1}.$$
 (3)

The membranes were characterized in the frequency domain with a lock-in amplifier (Zurich Instruments HF2PLL) in high vacuum (pressure $< 10^{-5}$ mbar) at room temperature. The membrane motion was actuated in the linear regime with a piezoelectric shaker and detected with a laser vibrometer (MSA-500 Polytec GmbH).

Figures 1(a) and 1(b) show the measured Qs for various modes of a SR-SiN and stoichiometric SiN membrane, respectively, with equal dimensions. The combined model (3), based on the exact solution of the radiation loss model [30], predicts the measured values of both membranes with good accuracy for a single chosen set of parameters $Q_{\rm intr}$ and α . These parameters resulted in the best possible fit for both membranes. All the modes in Fig. 1 fulfill the conditions required for the validity of the radiation loss model. The maximal Qs of the low-stress membrane Fig. 1(a) produce an envelope of maximal Q values which

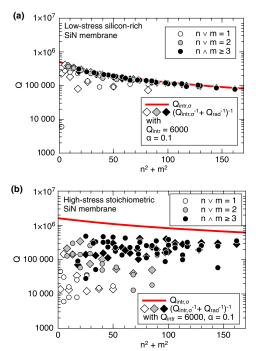


FIG. 1 (color online). Qs for modes $(n \land m \le 9)$ of a (a) square SR-SiN membrane $(L \approx 250 \ \mu\text{m}, \ \sigma = 92 \ \text{MPa}, \ h \approx 100 \ \text{nm})$ and (b) square stoichiometric SiN membrane $(L \approx 250 \ \mu\text{m}, \ \sigma = 988 \ \text{MPa}, \ h \approx 100 \ \text{nm})$. The chips were fixed with a double sticky carbon disc (Agar Scientific). The red line represents the highest quality factor value envelope due to intrinsic loss (1). The diamonds represent the fit of all quality factor values with (3), combining intrinsic and acoustic radiation loss based on the exact model developed by Wilson-Rae *et al.* [30]. The material properties of silicon were used for $E_s = 130 \ \text{GPa}$ and $\rho_s = 2300 \ \text{kg/m}^3$. (\land : AND, \lor : OR).

is accurately described by the intrinsic damping model (1) (red line). Hence, the maximal Qs of the SR-SiN membrane seem to be clearly limited by intrinsic losses. In contrast, the peak Os of the high-stress membrane are below the intrinsic loss envelope and they thus seem to be limited by radiation loss. The combined model (3) is shown as diamonds. In both membranes, modes with $n \vee m \leq 2$ are suppressed strongest by acoustic radiation loss, as predicted by the model, and as it was suggested by [25]. Both Si chips were fixed to the piezoelectric actuator with a double sticky carbon tape. The resonance frequencies are in the MHz regime, which results in wavelengths in the Si that are larger than the Si chip thickness. Hence, the carbon tape and the piezoshaker become part of the substrate. The lower Young's modulus of the tape reduces the acoustic mismatch compared to a pure Si substrate, which is reflected in the fit parameter $\alpha = 0.1 < 1$. The lower stress in the SR-SiN membrane results in a better acoustic mismatch η and a lower Q_{intr} envelope so that the maximal Qs are limited by intrinsic losses, which entails Qs that are less scattered compared to the high-stress membrane. SR-SiN membranes are thus the optimal structures to investigate the origin of the intrinsic loss, which is presented in the following part.

Figure 2(a) shows the extracted $Q_{\rm intr}$ from the maximal Q envelope given by intrinsic losses (1) from a set of square SR-SiN membranes with varying thicknesses h and lengths L. The complete set of measured $Q_{\rm intr}$ are plotted in the Supplemental Material [36]. The $Q_{\rm intr}$ values increase steadily with membrane thickness h, independent of the membrane size L. For low h the increase is following a linear trend (see linear slope line). A similar linear trend has been observed with Qs of SiN microcantilevers and was assigned to surface loss $Q_{\rm surf}(h) = \beta h$, with a slope β [37]. Hence, the observed linear relationship in Fig. 2(a) of $Q_{\rm intr}$ with h is strong evidence of surface loss. For structures with a reduced surface-to-volume ratio, surface loss will become obsolete and the intrinsic loss will be dominated by volume loss $Q_{\rm vol}$. This can be summarized by the formula

$$Q_{\text{intr}}^{-1}(h) = Q_{\text{surf}}^{-1}(h) + Q_{\text{vol}}^{-1}.$$
 (4)

In order to get more data to test the model (4), we extract $Q_{\rm intr}$ values for diverse SiN resonators from the literature. The values are obtained directly from maximal $Q_{\rm S}$ of unstressed cantilevers, and calculated by means of (1) from prestressed strings and membranes. All $Q_{\rm intr}$ values are listed in Fig. 2(b) together with the average values from Fig. 2(a). All values are fitted with (4). Apparently, the trend of all $Q_{\rm intr}$ s of all different SiN structures is described accurately by a combination of surface and volume loss. Our membranes had relatively large variations in h, L, and σ of $\pm 15\%$, $\pm 25\%$, and $\pm 75\%$, with respect to their nominal values, which propagates to a total uncertainty in the extraction of $Q_{\rm intr}$ of $\pm 60\%$. We took this as our error estimation for all values (thin red lines). From the fit, an

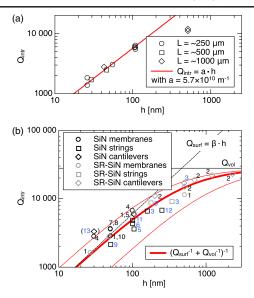


FIG. 2 (color online). (a) Intrinsic quality factors $Q_{\rm intr}$ as a function of membrane thickness h of SR-SiN membranes. The values represent the maximal values within the asymptotic Q_{intr} envelope. The tensile stress varied strongly between 60 MPa < σ < 253 MPa (determined by means of resonance frequency). The lowest values are fitted with a linear slope. (b) Q_{intr} values at room temperature extracted from literature and this work as a function of structure thickness h. The red line represents (4) fitted to all values with $\beta=6\times 10^{10}\pm 4\times 10^{10}~{\rm m}^{-1}$ and a volume loss related $Q_{\rm vol}=28\,000\pm 2000$. The fine red lines represent the estimated error of β of $\pm 60\%$. The values are taken from 1: this work; 2: [37]; 3: [21]; 4: [24]; 5: [1]; 6: [22]; 7: [34]; 8: [7]; 9: [38]; 10: [25]; 11: [4]; 12: [39] (13: [40]—h has a high uncertainty as it was only estimated from the HF etch rate; the initial thickness was 110 nm). All values were extracted assuming E = 240 GPa and $\rho = 3000 \text{ kg/m}^3$. The blue numbered values represent SiN resonators that were in contact with hydrofluoric acid.

average surface loss parameter of $\beta=6\times 10^{10}\pm 4\times 10^{10}~{\rm m}^{-1}$ and a volume loss related $Q_{\rm vol}=28\,000\pm 2000$ can be extracted. It seems that all different structure types made from either SR-SiN or stoichiometric SiN are ultimately limited by surface loss. Volume loss starts to significantly contribute in thicker resonators.

The origin of the observed surface loss could be manifold, e.g., surface impurities or surface roughness. The chemical analysis with x-ray photoelectron spectroscopy of the surface of two SiN membranes [one commercial stoichiometric low-pressure chemical vapor deposition (LPCVD) SiN membrane from Norcada, and one stoichiometric LPCVD SiN membrane fabricated in-house] revealed a high concentration of oxygen and carbon (see Supplemental Material [36]). The same finding was made earlier by Yang *et al.* [41] who found oxygen and carbon concentration on the surface of LPCVD SiN of 22 and 10 at. %, respectively. It has further been shown that these specific SiN surface impurities remain after cleaning with hydrofluoric acid (HF) and 3–7 at. % of F impurities are added [42]. Hence, surface impurities seem to be ubiquitous in LPCVD SiN films and can even be increased,

e.g., with an HF dip. In Fig. 2(b) all the SiN resonators that were exposed to HF are listed with blue numbers and their $Q_{\rm intr}$ values are generally below the average. It seems that an HF dip could increase surface loss. Another possible origin of surface losses could be related to surface roughness which was found to be in the range of 0.3–3 nm [41,43] of untreated LPCVD SiN. Hence, surface roughness can become a significant fraction of the total SiN thin film thickness.

Based on the Q_{intr} master curve for SiN from Fig. 2(b), it is now possible to predict the maximal obtainable Qs for harmonic modes n = m of square SiN membranes that are limited by intrinsic loss. From Fig. 3(a) it becomes evident that the thickness does not significantly influence Q of thin membranes at low mode numbers, an effect that has been observed experimentally [23]. This is a direct effect of the $Q_{\rm intr}$ that decreases with thickness and hence counteracts the Q-enhancing effect of a small h in (1). Thinner membranes only result in higher Os at higher modes. For Fig. 3(b) the thickness is fixed to 30 nm. It is not surprising that larger membranes result in higher Qs. But Q starts to deteriorate with mode numbers when λ becomes large as, e.g., it was observed with short SiN strings [22]. In quantum cavity optomechanics a figure of merit is the Qfproduct. $Qf > 6 \times 10^{12}$ Hz is the minimum requirement for room-temperature quantum optomechanics [44]. In that case the thermal decoherence rate $(k_BT)/(2\pi Q\hbar)$ at temperature T is smaller than the resonance frequency f. The maximal *Qf* product obtainable with a SiN membrane at room temperature is shown in Fig. 3(c). It seems that the limit cannot be overcome in the fundamental mode

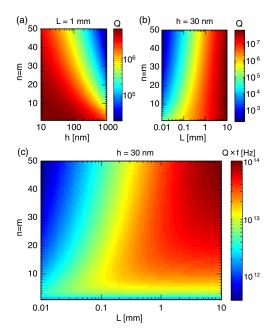


FIG. 3 (color online). Prediction of maximal Q and Qf values obtainable with a square SiN membrane at room temperature for harmonic modes (n=m) that are limited by intrinsic loss. A value error of 60% has to be assumed.

independent of membrane size, confirming the experimental findings from Wilson *et al.* [7]. For SiN string resonators, the maximal Q values for low mode numbers are equal to the ones displayed in Figs. 3(a) and 3(b), but the Qf product values have to be divided by $\sqrt{2}$. It has been shown that intrinsic damping is reduced at cryogenic temperatures, which means that all predicted values in Fig. 3 will increase accordingly [34,40,45].

In conclusion, Q in prestressed SiN micro- and nanomechanical resonators is limited by a combination of intrinsic and acoustic radiation loss. In membranes, both respective Os scale linearly with the dimensions (L/h). Hence, the limiting damping mechanism is mainly determined by the acoustic mismatch of the membrane to the substrate (η). In high-stress SiN membranes, η is reduced and the maximal intrinsic loss Q limit is increased; hence, the resulting Q values are strongly mode dependent and are scattered due to radiation loss. The maximal Qs can become limited by intrinsic loss by maximizing the acoustic mismatch, e.g., by mounting the chip freely or with a phononic band gap structure. In contrast, low-stress SiN membranes have a higher acoustic mismatch to the substrate and the maximal intrinsic Q limit is lower. Hence, the resulting Qs of higher mode numbers $(n \land m \ge 3)$ reach an upper envelope that is limited by intrinsic losses, while lower mode numbers $(n \lor m \le 2)$ can be limited by radiation loss. Generally, radiation loss is minimal for symmetric modes $(n \sim m)$. In SiN strings, radiation loss scales inversely with width and narrow strings can become limited by intrinsic loss.

The intrinsic quality factors $Q_{\rm intr}$ of thin low-stress SiN membranes scale linearly with the membrane thickness, which is strong evidence of surface loss. The same linear scaling of $Q_{\rm surf}=\beta h$ has been confirmed by independent SiN Q data taken from literature (cantilevers, strings and membranes) which is evidence that surface loss is the ubiquitous limiting damping mechanism in thin arbitrary SiN resonators with a scaling factor $\beta=6\times 10^{10}\pm 4\times 10^{10}~{\rm m}^{-1}$. For thin prestressed resonators that are limited by intrinsic loss, the thickness dependent surface loss is counteracting the Q enhancement at low mode numbers and Q can only significantly be increased with the size L. Finally, it seems that $Qf>6\times 10^{12}~{\rm Hz}$ required for quantum cavity optomechanics at room temperature cannot be reached with the fundamental mode, independent of resonator length.

The framework of Q analysis presented here is readily applicable to other emerging thin film mechanical string or membrane-type resonators made of materials such as SiC [46,47], InGaP [48], C (graphene) [49–51], C (diamond) [52], or MoS₂ [53,54].

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