



Long-Distance Transfer and Routing of Static Magnetic Fields

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We show how the static magnetic field of a finite source can be transferred and routed to arbitrary long distances. This is achieved by using transformation optics, which results in a device made of a material with a highly anisotropic magnetic permeability. We show that a simplified version of the device, made by a superconducting-ferromagnet hybrid, also leads to an excellent transfer of the magnetic field. The latter is demonstrated with a proof-of-principle experiment where a ferromagnet tube coated with a superconductor improves the transfer of static magnetic fields with respect to conventional methods by a 400% factor over distances of 14 cm.

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Magnetism is a fundamental interaction shaping our physical world, at the basis of technologies such as magnetic recording or energy generation. Guiding and transferring magnetic fields is essential in many technologies, from large scale transformers to nanoscale magnetic logic devices [1,2]. Unlike electromagnetic waves, which can be routed and transmitted with waveguides or optical fibers to long distances, static magnetic fields rapidly decay [3]. The conventional way to transfer magnetic fields is by using a ferromagnetic (FM) material with high magnetic permeability μ , as in the transfer of magnetic field from the primary to the secondary circuits of a transformer [1]. However, the transferred field rapidly decays with distance. We show in Fig. 1 a demonstration of this fact for a cylindrical geometry, which will be employed throughout the work. The reason for this is that the isotropic μ yields high values of magnetic induction \mathbf{B} not only in the direction of the cylinder axis but also in the radial direction, so field escapes through the cylinder lateral surface and the value at its end decreases drastically with increasing length. Alternatively, one could consider guiding magnetic field lines through a hollow superconducting (SC) tube. However, the transferred field rapidly decreases with increasing tube length (see Fig. 1 and Ref. [4]). Hence, in contrast to time-dependent electromagnetic fields, which can be transmitted and routed to long distances with, e.g., optical fibers, a device capable of doing so with static magnetic fields does not exist.

In this Letter we theoretically design and experimentally demonstrate such a device, which we call a magnetic hose. The design of the magnetic hose is based on transformation optics [5–8], which has already enabled the realization of invisibility cloaks [7,9,10], perfect lenses [11], and waveguides operating in the subwavelength regime [12]. Transformation optics has been successfully applied also

to static fields [13–20] and has allowed us to experimentally implement magnetic cloaks [14,15]. The application of transformation optics to static magnetic fields allows us to find that an infinitely wide slab of thickness t made of a homogenous material with $\mu_{\parallel} = \infty$ along the thickness, and $\mu_{\perp} = 0$ along the width, exactly transfers the magnetic field from the lower surface of the slab to the upper surface [see Figs. 2(a) and 2(b) for the case of a dipolar source and also Sec. I of the Supplemental Material [21]]. This material effectively transforms the space such that the region below the slab is unaltered and the space within

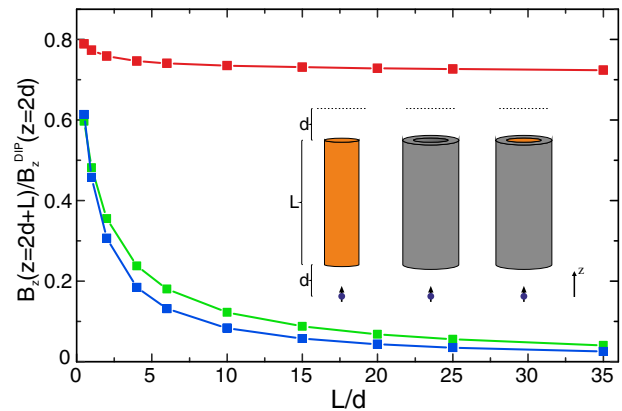


FIG. 1 (color online). The maximum field at a distance d of the top surface $B_z(z = 2d + L)$, normalized to the maximum field of the isolated dipole at a distance $2d$, $B_z^{\text{DIP}}(z = 2d)$, is plotted for an ideal FM cylinder (middle green line), an ideal SC tube (lower blue line), and a bilayer magnetic hose (upper red line), when a dipolar source is placed at a distance d below them as a function of the cylinder lengths L . In the inset, sketches of the three cases are shown, with the FM in orange and the SC in gray. In all these calculations the radius of the FM cylinder is $r = 0.8d$ and the thickness of the SC tube $w = 0.5d$.

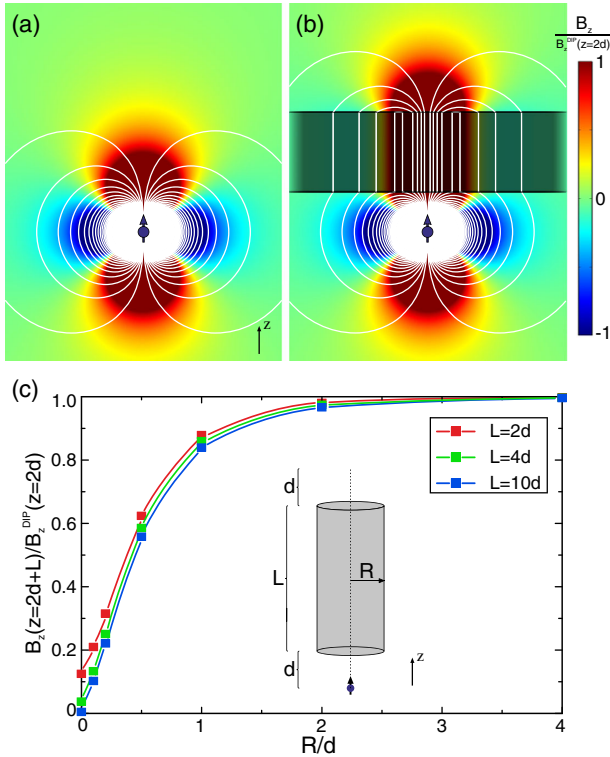


FIG. 2 (color online). The field of a magnetic source, e.g., a point dipole (a) (field lines in white and vertical field B_z in colors), is exactly transferred to an arbitrary distance, (b), through an infinite slab of ideal material (shaded region) having $\mu_{\parallel} = \infty$ along the thickness and $\mu_{\perp} = 0$ along the width. (c) Maximum vertical field at a distance d above a magnetic hose made of the ideal material, when a vertical dipole is placed at a distance d below the hose, as a function of the radius R . The field is normalized to the maximum field created by an isolated dipole at a vertical distance $2d$, $B_z^{\text{DIP}}(z=2d)$. Different hoses of length $L = 2d, 4d$ and $10d$ are plotted (from top to bottom).

the slab is shifted to the region above it. Such a slab has other remarkable properties. First, magnetic induction \mathbf{B} is vertical and magnetic field \mathbf{H} horizontal in the material volume. Because \mathbf{B} is perpendicular to \mathbf{H} , the magnetic energy is zero in the material [16]. Second, \mathbf{B} and \mathbf{H} —and thus magnetic energy—are not modified in the region containing the sources. The magnetic energy originally in the material volume is thus transferred to the other end. This is valid for any magnetic source and, remarkably, for any slab thickness t . However, this ideal design is not feasible, both because (i) the slab is infinitely wide and because (ii) no materials exist with such extreme anisotropy.

Let us address these difficulties separately. To circumvent (i), we consider a cylindrical piece of material with finite radius R , length L , radial permeability $\mu_{\rho} = 0$, and axial permeability $\mu_z = \infty$. We numerically study the transfer of magnetic field when a vertically aligned magnetic dipole is placed at a distance d below its bottom end

[inset in Fig. 2(c)]. In Fig. 2(c) we show the maximum vertical field B_z (always found at $\rho = 0$) at a distance d above the top end as a function of L and R . B_z decreases only slightly when the material length increases and rapidly saturates to a certain value that depends on R . It can be demonstrated (based on magnetic poles, see Sec. II of the Supplemental Material [21]) that this saturated value is not zero; hence, a part of the magnetic field is always transferred through the hose to arbitrary distances. For $R = 4d$ and lengths up to $L = 10d$ the material transfers the field from one end of the hose to the other, similarly to the ideal infinite slab. This property is approximately maintained even for radii as small as $R = 2d$.

To circumvent difficulty (ii) we follow a similar strategy used in the context of magnetic cloaks and concentrators [16,18]. The extreme anisotropic medium with $\mu_{\rho} = 0$ and $\mu_z = \infty$ can be approximated using existing isotropic materials: a series of n alternated superconducting (ideally with $\mathbf{B} = 0$ in their volume) and soft ferromagnetic (ideally with $\mathbf{H} = 0$) concentric cylindrical layers (see Sec. VIII of the Supplemental Material [21] for a discussion of the adequacy of the materials). Ferromagnetic parts provide a large axial permeability and the alternated superconductors prevent radial \mathbf{B} components. In Fig. 3 we show calculated results for several discretized versions of the magnetic hose into n concentric cylindrical shells, half of them superconducting and half ferromagnetic. The field of the dipole, located at one end of the hose, that is transferred to the opposite end tends to the ideal behavior with increasing n . More than 90% of the transfer can be achieved with $n = 20$. Remarkably, even with the simplest configuration ($n = 2$) the transfer can be as high as 75% (as in Fig. 1). In this bilayer scheme the SC has to be the outer layer, surrounding the FM, in order to prevent the field lines attracted by the inner FM core from leaking outside through the lateral surface.

We concentrate hereinafter on the simplest hose discretization, a SC shell of thickness w surrounding a FM core of radius r ($R = r + w$). The field transmitted by this simple bilayer hose strongly depends on its sizes r and w , because they determine the amount of field lines that goes into the hose. In Sec. IV of the Supplemental Material [21] we show that an optimum transmission is obtained with $r = 0.6d$ and $w = 1.4d$. In Fig. 4 we show numerical calculations illustrating the routing of the magnetic field of a dipolar source through hoses with different topologies with open and closed exits; many combinations of sources, branching geometries, and open and closed ends can be made following these examples. Results provide a clear verification of the capabilities of the magnetic hose—even in its simplest discretization—for routing and long-distance transfer of magnetic fields (see Sec. VI of the Supplemental Material [21] for further examples). As mentioned above, we emphasize that this cannot be obtained with only the FM or the SC (see a comparison in Fig. 1).

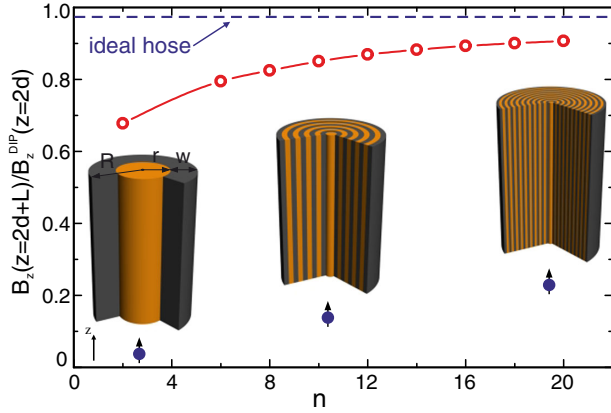


FIG. 3 (color online). Maximum field transferred by hoses discretized into different number of layers n . A point dipole is placed at a distance d below the bottom end and the field is calculated at a distance d above the top. SC and FM layers have all the same thickness, as shown in the insets (FM in light orange and SC in gray). The field transferred by an ideal hose with the same geometry is plotted with a blue dashed line. The total radius of the hose is $R = 2d$ and its length $L = 4d$.

For the case of closed hoses [as in Fig. 4(b)], we have validated the numerical results, from first principles, by analytically solving magnetostatic Maxwell equations with the boundary conditions: \mathbf{B} is zero in the SC and the scalar magnetic potential is constant in the FM. As shown in Sec. V of the Supplemental Material [21], the field of the dipolar source with magnetic moment m in the left branch is transferred towards the air gap (right), and builds up there according to the expression

$$B_z = \frac{\mu_0 m}{2\pi r^2 (l_s + l_a)}. \quad (1)$$

Here r is the radius of the FM core, μ_0 the vacuum permeability, and l_s (l_a) the length of the source (air) gap. Equation (1) shows that the field in the whole air gap is uniform and vertical [22] and, remarkably, does not depend on the hose length.

We have experimentally confirmed the magnetic field transferred through bilayer SC-FM magnetic hoses. We constructed two hoses with lengths 60 and 140 mm, each consisting of a FM cylinder and a SC shell made by adjacent pieces of YBCO superconducting tape (see Sec. VII of the Supplemental Material [21]). A constant current loop was placed at one end of the hoses and the transferred magnetic field was measured at the opposite end by a Hall probe. Results in Fig. 5(a) show the measured transferred field for the SC only, the FM only, and the magnetic hose. We also show the calculated transferred field by the FM only (upper green curve), showing excellent agreement with the experiments, and the field of the bare coil (lower purple curve). The field transferred along the hose is much larger than that with only the FM or the SC and the ratio between the fields

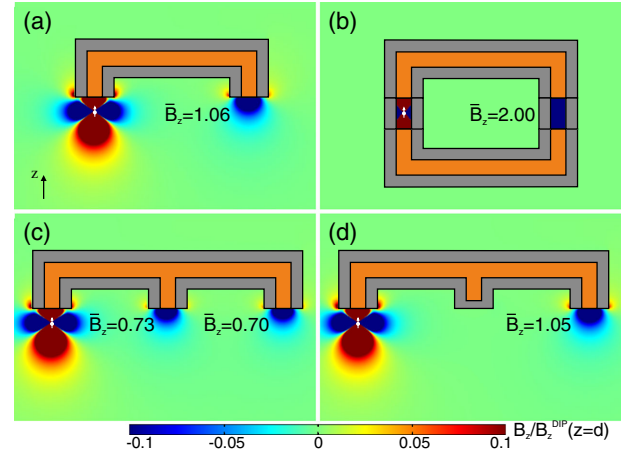


FIG. 4 (color online). Vertical field component B_z (in color scale) in the middle plane of different 3D geometries. The field source is a point dipole (sketched in white) placed at a vertical distance d from the hoses. The FM cylindrical core (light orange) has a radius $r = 0.5d$ and the surrounding SC (gray) a thickness $w = 0.75d$. In each simulation the average output field \bar{B}_z is calculated as the quotient between the flux that exits each hose end and the area of the ferromagnetic section and normalized to the maximum vertical field created by an isolated dipole at a distance d , $B_z^{\text{DIP}}(z = d)$. Analytical and numerical values of \bar{B}_z fully agree for the closed hose (b). Case (c) shows a hose divided into two branches; when one of its ends is closed with the SC, (d), we recover the case of a hose with a single branch (a). See Sec. VI of the Supplemental Material [21] for further discussions of the results.

transferred by the hose and the FM increases with increasing length, confirming our theoretical ideas. The field transferred by the hose is less than the theoretical value and slightly decreases with increasing length because of a imperfect sealing of SC parts, which can be improved by better manufacturing. This is supported by numerical calculations, which agree with the experimental results, see Sec. VII of the Supplemental Material [21]. Even with these imperfections in such a proof-of-principle experiment, the measured transferred field ratio of the hose with respect to the FM increases from 200% to 400% between the short and long studied lengths.

Because the magnetic hose operates with static fields, associated with an infinite wavelength, our ideas can be implemented at any scale [8,13,15,16]. This hints at the possibility of miniaturizing the magnetic hose to the nanoscale. Such a magnetic nanohose could open new possibilities to increase the magnetic coupling between nanomagnets in magnetic logic schemes, which has been identified as an important issue in some spintronic proposals [2,23–25]. A magnetic nanohose could also be used as a new tool to harness quantum systems, as required, for instance, in quantum information processing [26]. In particular, such a device would permit us to address, control, and manipulate the internal state of individual quantum systems, even if they are separated by distances of

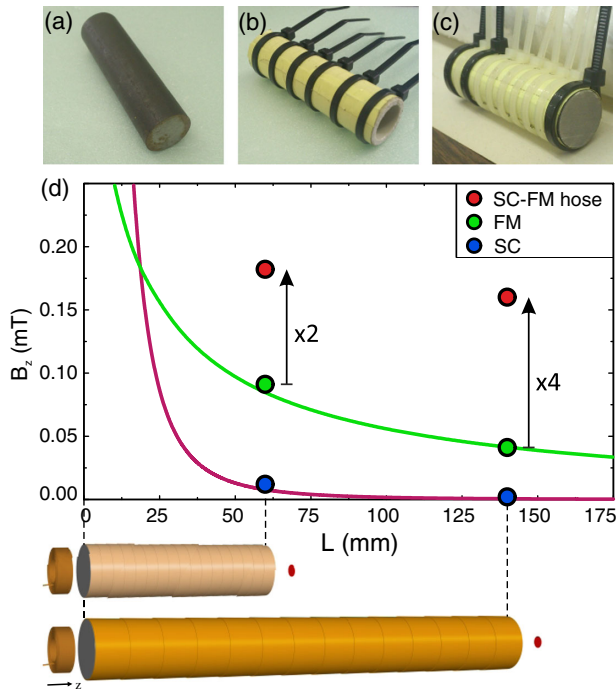


FIG. 5 (color online). Pictures of the construction of the experimental devices (of length 60 mm): (a) the FM cylinder, (b) the SC shell wrapped around a plastic former, and (c) the SC + FM bilayer magnetic hose. (d) Measured transferred magnetic field at one end of cylinders of length 60 and 140 mm. At the other end the field source is a coil fed with 1 A direct current (see the sketches below). Three cases are measured: SC only, FM only, and the SC + FM bilayer magnetic hose. Lines are calculated results for the field of the bare coil (purple curve) and that transferred by the FM only (green).

the order of few tens of nanometers, where optical methods are no longer available. This could be particularly relevant in the context of nitrogen-vacancy (NV) color defect centers in a diamond nanocrystal [27], identified as promising systems for the implementation of quantum information processors [28], or quantum repeaters [29]. Beyond the transfer of classical magnetic fields, one could also envision a system similar to the one considered here to couple distant quantum systems magnetically, allowing us to separate them by relatively long distances and still strongly interact with each other. This would provide us with a very powerful alternative to existing methods that directly couple NV centers at the quantum level [30]. The characterization of such a system, however, requires a full quantum treatment, something that is out of the scope of the present work.

In conclusion, we have theoretically proposed and experimentally demonstrated a magnetic hose to transfer the static magnetic field of a given source to distant positions along chosen paths. The hose is designed to operate with static magnetic fields and it is the actual magnetostatic field lines that are guided. We remark that other approaches recently used for manipulating and guiding electromagnetic waves,

even at subwavelength scales, such as epsilon-near-zero (ENZ) materials [31–33] or hyperbolic metamaterials [34], cannot be used with static fields. The reason is that these approaches are based on the coupling of electric and magnetic fields, whereas in our static case the displacement current coupling electric and magnetic field is negligible. Moreover, as discussed in Ref. [13], ENZ metamaterials at zero frequency do not exist. The magnetic hose proposed here thus brings a new tool to control magnetic fields, which complements the possibilities offered by metamaterials for the case of electromagnetic waves.

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