## Solid-Liquid Interfacial Premelting

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We report the observation of a premelting transition at chemically sharp solid-liquid interfaces using molecular-dynamics simulations. The transition is observed in the solid-Al—liquid-Pb system and involves the formation of a liquid interfacial film of Al with a width that grows logarithmically as the bulk melting temperature is approached from below, consistent with current theories of premelting. The premelting behavior leads to a sharp change in the temperature dependence of the diffusion coefficient in the interfacial region and could have important consequences for phenomena such as particle coalescence and shape equilibration, which are governed by interfacial kinetic processes.

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The term premelting refers to the formation of thermodynamically stable liquid films at solid interfaces subjected to temperatures below but near the bulk melting temperature  $(T_m)$  [1,2]. Surface premelting (SP), the formation of a premelting layer at a solid-vapor interface, was first observed experimentally by Frenken and van der Veen [3] using proton scattering. Since then, advances in experimental techniques have provided powerful tools for direct atomic-resolution observations of this surface phase transition [4–10]. These experimental studies have been complemented by a number of detailed atomistic simulations probing the existence and atomic-level mechanisms of SP (Refs. [11–18] and references therein). Premelting at solid-solid interfaces has also been reported in the literature and can take two basic forms: premelting at solid-solid heterophase boundaries and grain-boundary premelting. Examples of the former are found at interfaces between Pb and Al [19], SiO and Al<sub>2</sub>O<sub>3</sub> [20], as well as in ice at solid substrates, which plays a role in frost heave [11,21-23]. Premelting at grain boundaries has been the subject of numerous continuum modeling studies [24–30], atomistic simulations (Ref. [18] and references therein), and experimental [31] studies.

In this work, we report molecular-dynamics (MD) simulation results on Al-Pb solid-liquid interfaces that predict the existence of a third class of premelting transition, namely, solid-liquid premelting (SLP). In this process, a premelting liquid layer forms at a solid-liquid interface, below  $T_m$  of the solid. Such a transition should, in principle, be possible at chemically heterogeneous solid-liquid interfaces in which the melt phase of the solid and the liquid phase are mutually immiscible, as is the case with Al and Pb near  $T_m$  for Al. To the best of our knowledge, solidliquid premelting has not been previously reported under ambient pressures, either experimentally or by simulation, although some evidence of SLP has been reported in simulations of solid-liquid interfaces under extremely high pressures (diamond anvil) [32,33]. As we will demonstrate, the process of SLP leads to a sharp change in the temperature dependence of the diffusion coefficient in the interfacial region, which is expected to have important consequences for the kinetics of interface-controlled processes such as particle shape equilibration or coalescence of liquid nanoparticles in solids governed by interface-mediated Brownian motion [34,35].

Thermodynamically, premelting occurs near  $T_m$  when the interfacial free energy  $\gamma_{s\alpha}$  between the solid and another phase  $\alpha$  ( $\alpha$  = solid, liquid, or gas) is larger than the sum of that for the solid-melt ( $\gamma_{sl}$ ) and melt- $\alpha$  ( $\gamma_{l\alpha}$ ) interfaces,

$$\Delta \gamma = \gamma_{s\alpha} - [\gamma_{sl} + \gamma_{l\alpha}] > 0. \tag{1}$$

Thus, if the undercooling ( $\Delta T = T_m - T$ ) is not too great, it is thermodynamically favorable to form a thin film of metastable liquid because the increase in bulk free energy is more than compensated for by a lowering of the total interfacial free energy. The width of the interface as a function of undercooling depends on  $\Delta \gamma$  and  $\Delta T$  as well as the nature of the potential of interaction between the two interfaces, the so-called "disjoining potential." The pioneering theoretical studies by Kikuchi and Cahn [36] on grain-boundary premelting and Lipowsky [37] on SP both predict a logarithmic dependence [38] of the width of the premelting layer with respect to the undercooling [39],

$$w(\Delta T) = -w_0 \ln[\Delta T/T_0], \qquad (2)$$

where  $w_0$  and  $T_0$  are constants specific to the given interface.

*The system.*—The Al-Pb system is an ideal model alloy for the study of chemically heterogenous solid-liquid interfaces. The phase diagram is a simple monotectic that has a broad liquid-liquid miscibility gap, negligible solubility of Pb in the Al solid phase, and a large melting point separation (600 K for Pb and 933 K for Al). We have previously reported results from MD simulations on this system at 625 K, a temperature just above the melting point of Pb [40]. The simulation results are consistent with an *in situ* transmission-electron-microscopy (TEM) study of liquid Pb inclusions embedded in a crystalline Al matrix [41] in that the (111) interface is shown to be faceted, while (110) and (100) are rough at this temperature. The experiments also show that the (111) interface undergoes a roughening transition about 100 K below the melting point of Al.

Simulation details.—In our simulations of the Al-Pb solid-liquid interface, we employ a classical many-body potential developed by Landa *et al.* [42] to model the interatomic interactions. This potential predicts mutual immiscibility of Pb and Al in the solid state and a large-liquid state miscibility gap consistent with the experimental phase diagram up to 1200 K. The melting points of this potential [40] are 615.2(2) K and 922.4(2) K for Pb and Al, respectively. The MD simulations are performed using LAMMPS [43]. Equilibrated solid-liquid interfaces are set up at varying temperatures *T* ranging from 625 to 900 K, separated by 25 K up to 900 K with additional simulations at 912, 920, 921, and 922 K. Three crystallographic orientations for the Al-Pb interfaces are examined: (100), (110), and (111).

To produce the equilibrated interfaces, constant-area, constant-normal-pressure MD ( $NP_zAT$ ) simulations up to 50 ns in length are used to yield the appropriate equilibrium number density,  $\rho$ , pressure (1 bar), and composition. These are followed by constant *NVT* simulations to collect production data. Five replica systems (each containing two independent interfaces) are used at each temperature and orientation to improve statistics. For additional details as to the methods of interface setup, equilibration, and analysis, see the Supplemental Material [44] and Ref. [40].

Characterization.—The solid-liquid interfaces are characterized through the determination of interfacial profiles, which show the change in specific properties (e.g., density, local structural order, composition, and diffusion constant) as functions of the distance normal to the interfacial plane, defined as the z direction. The z coordinate is measured relative to a Gibbs dividing surface, defined here such that the excess number of Al atoms  $\Gamma_{Al}$  is zero (Supplemental Material [44]). To determine the extent of the premelting layer, we utilize two different order-parameter (OP) profiles. The first profile uses a local structure OP that distinguishes solid from liquid phases [45] and is normalized to 1 in the solid phase and 0 in the liquid phase. The second is a compositional order parameter equal to 1 in a pure Al system and 0 for pure Pb. For an Al-Pb solid-liquid interface without a premelting layer, these two order-parameter profiles will be approximately coincident; however, in the presence of a premelting layer (a liquid Al layer separating solid Al from liquid Pb), the interfacial position indicated by these two OP profiles will be separated by the width of the premelting layer w.

Figure 1 shows *NVT* snapshots of equilibrated (111) Al-Pb interfaces at increasing temperature for three different temperatures (625, 850, and 922 K), together with the corresponding time-averaged structural and composition OP profiles. For low *T* (top panel) just above  $T_{pb}^{Pb}$ , the



FIG. 1 (color online). Snapshots of Al-Pb (111) solid-liquid interfaces at three different temperatures. Top panel: 625 K, interface is faceted [40]; middle panel: 850 K, interface is rough; bottom panel: 922 K, interface is premelted. In the image, the crystalline Al atoms (as determined from the structural OP) are black (dark blue online), the liquid Al atoms (premelted layer) are light gray (green online), and the liquid Pb atoms are shown in dark gray (red online). In each image, the average structural OP and chemical OP are plotted as dotted and solid lines, respectively. The premelting width w is defined as the distance between the two OPs (at half value).

(111) interface is faceted [40] and two profiles are nearly coincident. For high *T* (bottom panel) just below  $T_m^{Al}$ , the two profiles are separated by nearly 10 Å, indicating the presence of a premelting layer of liquid Al sandwiched between solid Al and liquid Pb. In the central panel at 850 K, only the first complete layer of Al at the interface is structurally disordered.

Results.-Contour plots of the fine-scale density profiles,  $\rho(z, T)$ , are shown in Fig. 2 for the (100), (110), and (111) Al-Pb solid-liquid interfaces as functions of temperature and distance (z) normal to the interface. Also plotted in Fig. 2 are the temperature-dependent interfacial positions defined by the midpoints of the structural and compositional order parameters. The distance between these two interfacial positions diverges as the Al melting point [46] is approached, due to the formation of the premelting layer. The peaks of the density profiles are seen as vertical striations in the plot, which are stronger and more highly localized in the solid phase, to the left of the structural order parameter curve. To the right of the structural order parameter curve, the density peaks are smaller in magnitude and more diffuse, consistent with the usual structural ordering of a liquid near a surface. The much smaller magnitude of the liquid structural



FIG. 2 (color online). Equilibrium total number density contour maps of (100), (110), and (111) Al-Pb solid-liquid interface. Interface positions determined from structural OP profiles (circles) and chemical OP profiles (squares) as a function of Tare plotted on top of the correspondingly contour map. The error bars represent 95% confidence levels. For symbols without error bars, the error is smaller than the size of the symbol.

ordering in (110), relative to (100) and (111), was previously noted and discussed in Ref. [40]. Note that the position of the interface as defined by the composition OP is roughly independent of temperature, due to the mutual immiscibility of liquid Pb in both solid and premelted Al. The slight shift of this position towards higher z near  $T_m$  for Al is due to the lower density (relative to the solid) of the growing premelted Al layer.

Figure 2 shows that solid-liquid premelting occurs in this system for all orientations studied, with nearly identical behavior. This is in contrast to surface premelting in many fcc metal surfaces, in which (110) surfaces are prone to premelting, while premelting is not seen in the other orientations [7,14]. Note that we have examined the local structure of the Al liquid within the premelting layer and found it to be consistent with that of bulk liquid, showing little influence of either confinement or the nearby presence of the liquid Pb phase (Supplemental Material [44]).

Our previous simulations at 625 K [40] suggested that the (100) and (110) interfaces are rough at that temperature, whereas the (111) interface is faceted. However, visual inspection (together with orientational order parameter analysis) indicates that the (111) interface undergoes a roughening transition at higher temperatures (for example, see the middle panel of Fig. 1). To probe this behavior in further detail, we examine the transport of Al atoms within the first layer of Al, which is characterized through the calculation of diffusion-constant profiles D(z) determined from the mean-squared displacement of Al atoms versus time; see Refs. [40,47] for details. The full diffusion



FIG. 3 (color online). Log-linear plot of the diffusion constant for Al atoms in the first Al layer as a function of  $1/k_BT$  for (100), (110), and (111), diamonds, squares, and circles, respectively. The Al melting point and estimated roughening temperature  $T_r$ are indicated by vertical lines. The scale at the top of the figure shows the temperatures corresponding to the inverse temperatures shown on the independent axis.

constant analysis is presented in the Supplemental Material [44], but here we focus on the diffusion constant measured within the first Al layer (that is, the particles making up the density peak closest to z = 0 on the negative side in Fig. 2). Figure 3 shows a log-linear plot of diffusion constant versus  $1/k_BT$  for the particles in the first Al layer for the three interfacial orientations studied. The magnitude of the slope of this Arrhenius plot of D can be interpreted as an activation energy for diffusion. Except very close to  $T_m^{\rm Al}$ , the slope for the rough (100) and (110) interfaces is constant. For (111), however, the slope undergoes a discontinuous change at a temperature of about 826(4) K, indicating a sudden decrease in the activation energy for diffusion in this layer to a value that is comparable to that of the rough (100)and (110) interfaces. This temperature at which the activation energy changes coincides roughly with the temperature at which the interfacial width begins to show a logarithmic dependence on undercooling (see below). The temperature is also very near the roughening temperature of 823 K previously reported for the (111) interface based on *in situ* TEM experiments of Pb inclusions in an Al matrix [41]. The close correspondence between these temperatures suggests that roughening and the onset of premelting approximately coincide for this interface.

As discussed earlier, theoretical considerations [36,39] predict a logarithmic dependence of the premelting width on undercooling [Eq. (2)]. To examine the validity of Eq. (2) for the solid-liquid premelting transition in Al-Pb, we plot the calculated width of the premelting layer w as a function of the undercooling,  $\Delta T = T_M - T$  on a linear-log plot in Fig. 4. The data are well described by Eq. (2) for all



FIG. 4 (color online). Linear-log plot of the premelting width versus undercooling  $T_m^{\text{Al}} - T$  for each of the three interfacial orientations studied. The lines are the results of weighted least-squares fits to Eq. (2).

three interfacial orientations for undercoolings up to 100 K—deviations are seen at lower temperatures when the width approaches atomic dimensions, as expected. Using a weighted least-squares linear regression over the temperature range 875 to 921 K, we obtain estimates for  $w_0$  and  $T_0$ . Central to the derivation of Eq. (2) is the assumption that the interaction between the two interfaces bounding the premelted layer (the so-called "disjoining potential") is exponential and repulsive [48]

$$\phi_d(w) = \Delta \gamma e^{-w/w_0},\tag{3}$$

where  $w_0$  is the length scale of the interaction and  $\Delta \gamma$  is given in Eq. (1). The quantity  $T_0$  in Eq. (2) is given by  $T_0 = \Delta \gamma T_m / w_0 \rho L$ , where  $\rho$  is the number density and L is the latent heat. The fitted values of  $w_0$ ,  $T_0$ , and  $\Delta \gamma$  are given in Table I. This fitting gives an estimate of about 1.4–1.5 Å for the range of the disjoining potential, which is relatively independent of orientation.

*Discussion and summary.*—Using MD simulation we predict the existence of a solid-liquid interface premelting transition at the interface between solid Al and liquid Pb. That is, as the melting point of Al is approached from below, the surface of the crystalline Al melts to form a

TABLE I. Values of  $w_0$ ,  $T_0$ , and  $\Delta \gamma$  [defined in Eqs. (1) and (2)] from a weighted linear least-squares regression of the data for w versus  $\ln(T_m - T)$ . Values in parentheses represent 95% confidence level error estimates in the last digits shown.

	(100)	(110)	(111)
w <sub>0</sub> (Å)	1.47(3)	1.46(3)	1.36(4)
$T_0$ (K)	$1.28(12) \times 10^3$	$1.09(9) \times 10^3$	$1.45(14) \times 10^3$
$\Delta \gamma \ (\text{mJ}\text{m}^{-2})$	174(16)	148(13)	183(18)

premelting layer of liquid Al separating the solid Al and liquid Pb bulk phases. This transition was seen in the simulations for all interfacial orientations studied: (100), (110), and (111). Although solid-vapor and grain-boundary premelting transitions are well established in the literature, premelting of a solid-liquid interface has not, to our knowledge, been previously reported at ambient pressures. Such a transition requires that the melt phase of the solid and the bulk liquid be mutually immiscible, which is true for the Al-Pb system studied here. The width of the premelting layer is shown to depend logarithmically on the undercooling  $\Delta T$ , as predicted by theoretical considerations [36,39,48].

At lower temperatures, near the melting point of Pb, we have previously shown that the (100) and (110) interfaces are rough, whereas the (111) interface is faceted—in agreement with experimental observations on liquid Pb inclusions in a solid Al matrix [41]. In the current simulations, we observe a change in the activation energy of Al surface diffusion at the (111) interface at 826(4) K, which correlates well with both the experimental observations of a roughening transition at 825 K for this orientation [41] and the observed onset of premelting in the present simulations (as evidenced by the logarithmic dependence of the premelting width on T). There are a number of other solidliquid interfacial systems in which the melt phase of the solid is immiscible in the bulk liquid, such as, for example, the interface between ice and liquid hydrocarbons, so further study of possible premelting in such systems is warranted.

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