# Vortex merging and splitting: A route to elastoinertial turbulence in Taylor-Couette flow

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We report experimental evidence of a new merge-split transition (MST) to elastoinertial turbulence (EIT) in Taylor-Couette flows of viscoelastic polymer solutions, caused by merging and splitting of base Taylor vortices when crossed by elastic axial waves (rotating standing waves, RSW). These vortex merging and splitting events are not due to transient behavior, finite aspect ratio, or shear-thinning behavior. They are random in nature and increase in frequency with Re; when superimposed on a RSW flow state they cause abrupt changes in the axial spatial wavelength, leading to the transition from a RSW to the EIT state. We thus identify MST as an inertial feature solely triggered by elasticity and independent of any shear-thinning behavior.

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# I. INTRODUCTION

Taylor-Couette flow (TCF) is the flow in the gap between two concentric cylinders with one or both rotating. Such flows have many practical applications in rheology or mixing [1,2]. Over the past century [3], they have also served as a great tool for the fluid mechanics community to study various flow instabilities induced by complex fluids. Indeed, with the inner cylinder rotated and the outer cylinder fixed, the purely azimuthal Couette flow (CF) is known to destabilize when a critical rotation speed is reached, leading to the flow transitioning to the so-called Taylor vortex flow (TVF). In Newtonian fluids a variety of steady and unsteady flow states already exists [4], depending on the Reynolds number (Re) defined as

$$\operatorname{Re} = \rho \Omega r_i d/\mu, \tag{1}$$

where  $\rho$  is the fluid density,  $\Omega$  the rotation speed,  $r_i$  the inner cylinder radius, and d the gap width. Alternatively, the Taylor number  $\text{Ta} = \rho \Omega \sqrt{r_i d^3} / \mu$  can also be used to describe the CF to TVF transition.

When the fluid in the gap is non Newtonian, more complex flow transitions can emerge, in particular when the fluid displays elastic properties. In the absence of inertia (vanishing Re), elastic fluids exhibit a CF-TVF transition induced by a purely elastic instability [5]. As elasticity increases, the flow exhibits a chaotic behavior, which is referred to as elastic turbulence [6,7]. A hysteretic

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FIG. 1. Schematic of the experimental setup showing the Taylor-Couette cell and the visualization arrangement.

behavior can also be observed in which diwhirls appear when the inner cylinder decelerates under conditions that would produce a purely azimuthal flow during acceleration [8-10].

In the presence of inertia (higher Re), elastic fluids are subject to elastoinertial instabilities, leading to the existence of nonaxisymmetric flow states such as ribbons (RIBs) [11] or rotating standing waves (RSWs) [10,12,13]. Gradual transitions from such flows to elastoinertial turbulence (EIT), through a series of increasingly chaotic flow states, have been reported in the literature [13,14].

Notably, in shear-thinning and elastic polyethylene oxide solutions, an interesting *defect* behavior of the RIB spirals has been observed [11]. It has been shown that the multiplications of such defects when increasing the rotation speed of the inner cylinder lead to the flow transitioning to EIT through a process called *defect mediated turbulence* (DMT) [11].

In the present work we report experimental evidence of a new merge-split transition (MST) to EIT, caused by merging and splitting of base Taylor vortices (abrupt changes in the axial spatial wavelength) when crossed by axial RSW waves. We identify MST as an inertial feature solely triggered by elasticity, independent of any shear-thinning behavior. It should be noted that the diwhirls previously observed [9,10] also correspond to a hysteresis in the number of vortices but occur only during deceleration of the inner cylinder.

#### **II. EXPERIMENTS**

Here we perform ramp-up (slow acceleration of the inner cylinder) and steady-state experiments (constant rotation speed of the inner cylinder) in a purely elastic Boger fluid made of 200 ppm PAAM (polyacrylamide, Sigma-Aldrich,  $M_w = 5.5 \times 10^6 \text{ g mol}^{-1}$ ) dissolved in a 28% water 72% glycerol mixture. The flow cell (Fig. 1) comprised a transparent acrylic outer cylinder and nylon inner cylinder spray painted with black nonreflective paint to avoid spurious light reflections and ensure smoothness of the rotating surface. Alignment between the inner and outer cylinder was ensured by a ball bearing and a notch complementing the inner cylinder's conical end, at the top and



FIG. 2. Oscillatory shear rheological characterization of the working fluid (1% strain). The elastic timescale is obtained by removing the contribution of the solvent viscosity  $\mu_s$  to G'' curves as  $\tilde{G}'' = G'' - \mu_s \times \omega$  and finding the crossover between G' and  $\tilde{G}''$  (vertical dashed line).

bottom lid, respectively. The cylinder was driven from the top using a stepper motor (SmartDrive Ltd., Cambridge, U.K.), the rotation of which could be controlled to a high degree of precision by a 52 000 microstep-revolution controller (SmartDrive Ltd., Cambridge, U.K.).

The top and bottom lids were stationary, with an  $\sim 3$  mm gap between the lid and cylinder at both ends. The inner chamber, which was completely filled with working fluid (no free surface), had an axial length of H = 155 mm, and the inner and outer radii were 21.66 and 27.92 mm, respectively. This corresponds to a gap width of d = 6.26 mm, a radius ratio of  $\eta = r_i/r_o = 0.77$ , and an aspect ratio AR = H/d = 21.56 (Fig. 1). The cell was enclosed in a rectangular chamber in which water was recirculated via a temperature bath to ensure that the temperature of the working fluid remained constant at 20 °C throughout the experiments.

The shear rheology was measured using a rotational rheometer (ARES, TA Instruments) equipped with a Couette geometry (inner diameter 32 mm, outer diameter 34 mm) in steady shear mode. A constant viscosity of  $\mu = 0.0481$  Pa s was found [Fig. 2(a)]. The elastic properties of the working fluid were assessed through oscillatory shear experiments on the same rheometer and geometry. The evolution of elastic and viscous moduli G' and G'', respectively, with oscillation frequency is measured in the linear deformation region (1% strain). G'' values were corrected by removing the contribution of the solvent viscosity,  $\mu_s = 0.0419$  Pa s, such that  $\tilde{G}'' = G'' - \mu_s \omega$ , and the elastic timescale is defined as  $t_e = 2\pi/\omega_c$ , where  $\omega_c$  is the crossover point between  $\tilde{G}''$  and G' curves [15] [see Fig. 2(b)]. The measured elastic timescale is  $t_e = 0.2110$  s, and the elastic number is  $El = t_e \mu/\rho d^2 = 0.2263$ , with  $\rho = 1198$  kg m<sup>-3</sup>. Rheological characterization of the working fluid before and after the experiments gave similar results, indicating negligible polymer degradation.

The flow was visualized by adding a small amount of reflective mica flakes at a volume fraction of the order of  $10^{-4}$  (0.01%), sufficiently low so as not to disturb the flow [16], and illuminating them using two LED stripes (PHLOX white LED linear light 260) arranged as shown in Fig. 1. The flakes' response time is defined as  $t_f = (l^2 \rho)/\mu$ , where *l* is the flakes' equivalent diameter ranging from about 10 to 100  $\mu$ m.  $t_f$  was found to be at least two orders of magnitude smaller than the fastest timescales of the flow. Images of the flow were acquired by a Phantom Miro 340 camera, along a narrow strip in the axial dimension (vertical), at 90 and 900 fps for ramp-up and steady-state experiments, respectively. For ramp-up experiments, this corresponds to a Reynolds number increment of  $\Delta Re = 0.007$  between two successive frames. The 2176 × 16 pixel images



FIG. 3. Reynolds-space and frequency-space diagrams of the ramp-up experiment. (a) *z* root mean square *i*<sup>\*</sup> of the (b) Reynolds-space flow map intensity, such that  $i^*(\text{Re}) = \langle I(z, \text{Re}) \rangle_{\text{rms},z}$  with *I* the gray-scale intensity of flow map 3 (b). (c) Frequency map where the frequency axis is scaled by the maximum inner cylinder frequency reached at the end of the experiment,  $f_{\text{max}} = 2\pi / \Omega_{\text{max}} = 9.45$  Hz. Vertical black dotted lines denote transitions from CF to TVF and to RSW states. The more gradual transition from RSW to EIT is also illustrated by a vertical gray dotted line. The cylinder frequency increase with Re is illustrated with the black dashed line. Horizontal dashed lines matching RSW state frequency ridges are plotted at  $f = k \times f_e$ ,  $k = [\frac{1}{3}, \frac{2}{3}, 1]$ .

 $(135 \times 0.994 \text{ mm})$  are averaged in the azimuthal direction to form an axial intensity profile for each instant or Reynolds number. All profiles are compiled into a matrix or flow map showing the evolution of the flow structures with time or Reynolds number [e.g., Figs. 3(b) and 4].

Flow maps are divided into shorter time sequences (256 successive times, 50% overlap) in order to calculate the average fast Fourier transform (FFT) for each row in each sequence. All the averaged spectra are then compiled to form a frequency map. This map shows the evolution of the characteristic frequencies of the flow as a function of time or Reynolds number [17] [e.g., Fig. 3(c)].

For the ramp-up experiments, the inner cylinder rotation speed  $\Omega$  is slowly increased at a constant rate,  $d\Omega/dt$ , up to a maximum value  $\Omega_{max}$ . For steady-state experiments, the rotation speed (and hence Reynolds number) is held constant during the recording time following a slow ramp-up phase. In both cases the acceleration rate, defined as  $\Gamma_0 = \frac{dRe}{dt^*} = \frac{\rho^2 r_i d^3}{\mu^2} \frac{d\Omega}{dt}$ , is kept below unity ( $\Gamma_0 = 0.3312$ ). This is commonly used as a criterion to ensure that transient, acceleration-related effects can be neglected [18]. The values of  $d\Omega/dt$  and the corresponding  $\Gamma_0$  were chosen as a best compromise to achieve quasisteady ramp up while avoiding polymer chain destruction. Experiments at higher acceleration rate ( $\Gamma_0 \sim 10$ ) have also been conducted, and the flow map remained unaffected.

#### **III. RESULTS**

#### A. Ramp up

Figure 3 shows the results of the ramp-up experiment, that allows the flow transitions to be monitored over a continuous range of Re. The flow state succession is the following: CF-TVF-RSW-EIT. This set of transitions is expected in purely elastic Boger fluids [12]. In Fig. 3(a) the rms of the flow map intensity along z is shown as a function of Re. This allows the critical Re for transition from CF to TVF to be identified at  $Re_{c1} = 80$ . This gives a  $Re_{c1}^* = Re_{c1}/Re_{c1}^0 = 0.88$ ,



FIG. 4. Steady-state recordings at constant Re of successive RSW and EIT states. (a)–(d) Time-space diagrams over 50-s time spans. (e)–(h) Detailed section of the same flow maps on the first 5 s and in the central region (dashed rectangles). Merging and splitting of Taylor vortices in the RSW flow state are indicated by full and dotted line ellipses, respectively. Note that the EIT flow state is essentially composed of a high number of indistinguishable merging and splitting along with axial oscillations. (i) and (j) are detailed closeups on splitting [(i) S2, t = 18 s] and merging [(j) S3, t = 38 s] events (RSW), where dashed lines are a guide to the eye showing the base Taylor vortices.

where  $\text{Re}_{c1}^0 = 92.3$  is the critical Reynolds number in an inelastic Newtonian fluid (same solvent without PAAM), measured in the same experimental setup. The TVF to RSW transition is clearly evidenced from the sudden appearance of a number of ridges in the frequency map [Fig. 3(c)] corresponding to the typical frequencies of the RSW state. This second transition occurs at  $\text{Re}_{c2} = 88$ ,  $\text{Re}_{c2}^* = \text{Re}_{c2}/\text{Re}_{c1}^0 = 0.95$ . We note that the frequencies of these ridges stay constant with increasing Re throughout the RSW state during ramp up [Fig. 3(c)].

Even more remarkably, the *k* harmonic frequencies of the RSW ridges can be written as  $f^k = k \times f_e$ , where  $f_e = 2c_e/\lambda$  is the elastic wave frequency based on the elastic wave celerity  $c_e = \sqrt{\mu/(\rho t_e)}$  [7,19] (assuming that the spatial wavelength is  $\lambda \simeq d$ , see Fig. 8). The first three dominant  $f^k$  frequencies, found at  $k = [\frac{1}{3}, \frac{2}{3}, 1]$ , are evidenced by the horizontal dashed lines of Fig. 3(c). Finally, the RSW state gradually transitions to EIT from  $\text{Re}_{c3} \simeq 122$  ( $\text{Re}_{c3}^* = \text{Re}_{c3}/\text{Re}_{c1}^0 = 1.3$ ) onwards. The previous flow state succession is consistent with the experiments of Groisman and Steinberg [12], even though TVF would have been expected to transition directly to EIT at the present El value. The discrepancy may be attributed to differences in the radius ratio ( $\eta = 0.71$  in [12]). Some merging and splitting events, highlighted in Fig. 3(b) by full and dotted circles, respectively, can be observed in the RSW state, confirming that such events can be observed in quasisteady ramp-up experiments.

#### **B.** Steady-state experiments

In Fig. 4, steady-state experiments performed at four different Reynolds numbers are reported. Note that while the RSW state can be seen in the ramp-up experiment at Re = 94, it corresponds to a clear TVF state in the steady-state experiments. This is not surprising, given the general sensitivity of non-Newtonian Taylor-Couette flows to experimental conditions.

In the TVF regime [S1, Figs. 4(a) and 4(e)], no merging or splitting occurs over a 50-s time span, and the Taylor vortices are steady. The RSW state [S2, S3, Figs. 4(b), 4(c), 4(f), and 4(g)] is characterized by a base Taylor vortex flow with axial oscillations corresponding to axial waves, namely, the "rotating spiral waves" [12]. Merging and splitting events (highlighted by full and dotted line ellipses, respectively) are clearly evidenced there. In S3, merging and splitting events involving



FIG. 5. Role of RSW waves in the merging and splitting of Taylor vortices, illustrated in the unwrapped  $(\theta, z)$  plane. Only a central vertical line of this plane is sampled to produce flow maps shown in Figs. 3 and 4, as explained in Fig. 1.

more than two vortex pairs are also observed. Note that some vortices appear to drift in or out of the map at the top or bottom, where they merge with or separate from the Ekman vortices, respectively. Details on two selected examples of splitting and merging in the RSW state are shown in Figs. 4(i) and 4(j), respectively. The EIT state [S4, Figs. 4(d) and 4(h)] appears as an extremely unsteady RSW state, where tracks of the base Taylor vortices are still visible but submerged in strong axial flow oscillations and frequent merging and splitting of multiple vortices simultaneously.

Figure 4 proves that MST does not require shear thinning as in DMT [11] and is not an effect of a transient behavior due to the finite  $\Gamma_0$  value. They occur in a purely elastic fluid and during steady-state experiments. A schematic representation of the MST mechanism is provided in Fig. 5 [in the  $(\theta, z)$  plane], illustrating the role of asymmetric RSW waves in merging and splitting vortices and vortex pairs.

## C. Space and time spectra

To provide further quantitative description of the observed flow states, frequency spectra of steady-state experiments (FFT of intensity time series at a given Re) are shown in Fig. 6(a), where the frequency axis is scaled by the elastic wave frequency  $f_e$ . Frequency spectra of various flow states are also extracted along vertical lines of Fig. 3(c) and plotted in Fig. 6(b), with the frequency axis normalized as  $2\pi f/\Omega$ . The spectra confirm the behavior observed also in the flow and frequency maps (Fig. 3), namely, that the RSW state is a superposition of waves of various frequencies, several of which have comparable amplitudes, and that this combination of waves transitions to EIT upon increasing Re [11]. One of the RSW spectral peaks corresponds to  $f = f_e$ , where  $f_e$  is the elastic wave frequency [7,12,19], as also seen in Fig. 3(c). The most energetic peaks are found for k subharmonics of  $f_e$  such that  $f^k = k \times f_e$ , with k = 1/3 and k = 2/3. When Re is increased, the peaks become less discernible, and the frequencies appear slightly shifted towards lower values on Fig. 6(b), as  $\Omega$  increases with Re while the elastic relaxation frequency  $f_e$  stays constant.

The spectra clearly illustrate the progressive transition from the RSW state to EIT as the discrete coherent oscillations of the RSW state, the frequencies of which do not depend on Re but rather correspond to the elastic frequency, merge into a continuous broadband [12,13] spectrum, consistent with the flow maps of Figs. 3 and 4. This latter spectrum [upper panel in Fig. 6(b)] is similar to



FIG. 6. Evolution with Re of the frequency spectra of flow states obtained from steady-state experiments (a) and extracted from the frequency map in Fig. 3(c) (b). Frequencies (x axis) are scaled by the elastic frequency  $f_e$  on (a) and by the cylinder's rotation frequency  $\Omega/2\pi$  on (b). In (b), vertical black and gray dotted lines denote this latter frequency and its first harmonic, respectively. Vertical mixed blue lines are plotted at  $f = \frac{1}{3}f_e$ . In (a) vertical dotted and mixed lines denote the  $f = f_e$  and  $f = \frac{1}{3}f_e$  peaks, respectively.

that of turbulent Taylor-Couette flows in Newtonian fluids [2,20,21], thus justifying the name of "elastoinertial turbulence" or "elasticity-dominated turbulence" [13,14].

To further investigate the role of merging and splitting events in this RSW to EIT transition, the axial spatial wavelength is computed for each vertical slice (Re) of the time-space or Re-space diagrams in Figs. 3(b) or 4. This is achieved by taking the FFT of the intensity signal along the axial dimension *z*, and finding the dominant peak frequency, which is simply the inverse of the spatial wavelength, as illustrated in Fig. 7(a). In doing so, one allows the wavelength to vary without being constrained to rational numbers (e.g., the height divided by the number of vortex pairs), thus accounting for the gradual merging, splitting, or drift of vortices (see Figs. 4, 8, and 7).



FIG. 7. (a) Instantaneous and (b) time-averaged spatial spectra (Fourier transform on intensity profiles in the axial direction) of steady-state experiments as a function of the normalized wavelength  $\lambda/d$  (a) and normalized wave number  $\tilde{k} = d/\lambda$  (b).



FIG. 8. Axial spatial wavelength  $\lambda/d$ , expressed as a function of time for steady-state experiments (a), and as a function of Re for the ramp-up experiment (d). (b) Shows the evolution of normalized standard deviation *S* of  $\lambda/d$  on the full duration of each steady-state experiment as a function of Re. (c) Evidences the  $S \sim \text{Re}^2 \sim N_1$  scaling by plotting  $S/\text{Re}^2$  as a function of Re.

Figure 7 shows examples of spatial Fourier transform of the intensity profile along the axial direction z for steady-state experiments. Note that bandpass filtering is applied to suppress frequencies lower than 10/H and higher than 100/H (with H the height of the flow cell). This is equivalent to assuming that the number of vortices in the test section is between 10 and 100, which can be checked visually on Figs. 2 and 3.

In subfigures (a) [(a1)–(a4)], instantaneous spectra are plotted as a function of the normalized wavelength  $\lambda/d$ . Two instantaneous spectra [(a2), (a3)] are shown for the RSW state cases to illustrate the wavelength drift due to merging and splitting. In subfigures (b) [(b1)–(b4)], time-averaged spectra are plotted as a function of the normalized wave number  $\tilde{k} = d/\lambda$ . The vertical dashed lines illustrate the time-averaged wavelength  $\langle \lambda/d \rangle$  or time-averaged wave number  $\langle d/\lambda \rangle$  on (a) and (b), respectively (vertical dashed lines). In Fig. 7(a) merging and splitting of Taylor vortices lead to a drift of the instantaneous wavelength in RSW and EIT states. In Fig. 7(b) the time-averaged spectra show a wave-number peak consistent with the time-averaged wave number  $\langle d/\lambda \rangle$  (see also Fig. 8).

In the absence of vortex merging and splitting, the wavelength stays constant in the TVF case. Variations of  $\lambda$  of the two RSW cases (S2, S3, see Fig. 4) are of similar amplitude but even more gradual and random for the higher Re of the two. They are a consequence of a more complex combination of merging, splitting, and drift. This effect is further enhanced in the EIT case [Fig. 8(a), dark curve]. The wavelength fluctuates around its time-averaged value  $\langle \lambda/d \rangle$ , reported in Fig. 8(a). This nominal wavelength varies between 0.88 and 1.02 among all steady-state experiments.

The amplitude of fluctuations *S* is related to vortex merging and splitting events, and is plotted in Fig. 8(b). It is quantified for all experiments as the normalized standard deviation of any  $\lambda/d$  time series, denoted std( $\lambda/d$ ), divided by the standard deviation of the  $\lambda/d$  times series in TVF, denoted std( $\lambda/d$ )<sub>*TVF*</sub>, such that

$$S = \frac{\operatorname{std}(\lambda/d)}{\operatorname{std}(\lambda/d)_{TVF}}.$$
(2)



FIG. 9. Spatiotemporal spectra obtained by two-dimensional FFT in RSW (a) and EIT (b) steady-state experiments. Spatially averaged spectra are projected in planes a3 and b3. Temporally averaged spectra are projected in planes a2 and b2. Projections are indicated by dashed arrows.

S values increase with increasing Re, i.e., with increasing the probability of merging and splitting events, as shown in Fig. 8(b). The dependency on Re appears to be quadratic, as illustrated by Fig. 8(c). The reason for this scaling is discussed in Sec. IV. Finally,  $\lambda/d$  is shown as a function of Re for the ramp-up experiment in Fig. 8(d). The gradual transition from RSW to EIT corresponds to increased noise in the main spatial wavelength.

Figure 9 finally displays plots of spatiotemporal spectra (two-dimensional FFT) for steady-state experiments S2 (a) and S4 (b). Temporally averaged spectra (as previously reported in Fig. 6) are projected on the a2 and b2 planes. Spatially averaged spectra (as previously reported in Fig. 7) are projected on the a3 and b3 planes. The spectra intensities are rescaled in arbitrary units. Figure 9 allows the correlation between spatial and temporal frequencies in the RSW state to be evidenced, and how this behavior turns to a broadband chaos in the EIT state, both in time and space.

Despite the broadband spectral behavior, EIT is here found at relatively low Re values for which no turbulence would exist in a Newtonian fluid. The structure of EIT is thus likely to be different from that of so-called viscoelastic turbulence, in which inertial turbulent scaling laws are modified by the presence of polymers [22]. Further investigation using time-resolved quantitative flow velocity measurements in the gap, such as particle image velocimetry [17], could allow characterization of the structure of transitional EIT.

### IV. DISCUSSION AND CONCLUSION

The fact that the RSW oscillation frequencies are Re independent and related to the elastic timescale of the polymer solution shows that the RSW state originates from the elastic features of the fluid. RSW is thus an inertial mode modified by elastic effects [12], and such effects induce a transition to elastoinertial turbulence. It is generally known that multiple periodic elastic waves may superimpose to generate randomness and transition to elastic [6] or elastoinertial turbulence [13,19,23]. The latter phenomenon is also observed here, with RSW transitioning to EIT.

In an elastic Taylor-Couette flow, polymer molecules are stretched by the strong base azimuthal flow and release energy into the transverse secondary flow. Such a polymer relaxation energy transfer is believed to be the origin of axial elastic waves in the RSW state [12]. This argument is also consistent with the early (elastic) onset of the TVF primary instability, attributed to the normal

stress difference of elastic polymeric solutions [5], and to direct numerical simulation findings on elastoinertial Taylor-Couette turbulence by [14].

The same physical mechanisms are likely to be responsible for the existence and increased occurrence with Re of merging and splitting events. The first normal stress difference  $N_1$  scales with the square of the shear rate  $\dot{\gamma}$  [12,24]. Defining  $\dot{\gamma} = \Omega r_i/d$  in a Taylor-Couette flow of constant viscosity fluids [17], we obtain

$$N_1 = 2\mu t_e \left(\Omega \frac{r_i}{d}\right)^2. \tag{3}$$

Combining Eqs. (1) and (3), and for a given constant viscosity  $\mu$ , one gets  $N_1 \sim \text{Re}^2$ . Here in Fig. 8(c), it appears that a  $S \sim \text{Re}^2 \sim N_1$  scaling satisfactorily describes the increase of merging and splitting probability upon Re or  $N_1$  increase.

As a final note, the fact that vortex merging and splitting occur in a Boger fluid (constant viscosity) during a steady-state experiment (no transient ramp-up effects) broadly suggests that this behavior is not due to the transient nature of the ramp-up process or to shear thinning. Experimental evidence herein supports the view that it is triggered by axial waves, as exist in RSW states. Interpretation of the results in terms of normal stress thus suggests that it is associated with fluid elasticity. Such abrupt wavelength changes prove to be one of the features leading to the observation of EIT when occurring repeatedly on top of a RSW flow state. This can be described as a merge-split elastoinertial transition to turbulence (MST).

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- M. A. Fardin, C. Perge, and N. Taberlet, The hydrogen atom of fluid dynamics Introduction to the Taylor-Couette flow for soft matter scientists, Soft Matter 10, 3523 (2014).
- [2] S. Grossmann, D. Lohse, and C. Sun, High-Reynolds number Taylor-Couette turbulence, Annu. Rev. Fluid Mech. 48, 53 (2016).
- [3] G. I. Taylor, Stability of a viscous liquid contained between two rotating cylinders, Philos. Trans. R. Soc. London, Ser. A 223, 289 (1923).
- [4] C. Andereck, S. Liu, and H. Swinney, Flow regimes in a circular Couette system with independently rotating cylinders, J. Fluid Mech. 164, 155 (1986).
- [5] R. G. Larson, E. S. G. Shaqfeh, and S. J. Muller, A purely elastic instability in Taylor-Couette flow, J. Fluid Mech. 218, 573 (1990).
- [6] S. Berti and G. Boffetta, Elastic waves and transition to elastic turbulence in a two-dimensional viscoelastic Kolmogorov flow, Phys. Rev. E 82, 036314 (2010).
- [7] A. Varshney and V. Steinberg, Elastic Alfven waves in elastic turbulence, Nat. Commun. 10, 652 (2019).
- [8] A. Groisman and V. Steinberg, Solitary Vortex Pairs in Viscoelastic Couette Flow, Phys. Rev. Lett. 78, 1460 (1997).
- [9] M. Lange and B. Eckhardt, Vortex pairs in viscoelastic Couette-Taylor flow, Phys. Rev. E 64, 027301 (2001).
- [10] D. G. Thomas, R. Sureshkumar, and B. Khomami, Pattern Formation in Taylor-Couette Flow of Dilute Polymer Solutions: Dynamical Simulations and Mechanism, Phys. Rev. Lett. 97, 054501 (2006).
- [11] N. Latrache, N. Abcha, O. Crumeyrolle, and I. Mutabazi, Defect-mediated turbulence in ribbons of viscoelastic Taylor-Couette flow, Phys. Rev. E 93, 043126 (2016).
- [12] A. Groisman and V. Steinberg, Couette-Taylor Flow in a Dilute Polymer Solution, Phys. Rev. Lett. 77, 1480 (1996).

- [13] C. S. Dutcher and S. J. Muller, Effects of moderate elasticity on the stability of co- and counter-rotating Taylor-Couette flows, J. Rheol. 57, 791 (2013).
- [14] N. Liu and B. Khomami, Elastically induced turbulence in Taylor-Couette flow: Direct numerical simulation and mechanistic insight, J. Fluid Mech. 737, R4 (2013).
- [15] J. D. Ferry, Viscoelastic Properties of Polymers (John Wiley & Sons, New York, 1980).
- [16] J. J. J. Gillissen, N. Cagney, T. Lacassagne, A. Papadopoulou, S. Balabani, and H. J. Wilson, Taylor-Couette instability in disk suspensions: Experimental observation and theory, Phys. Rev. Fluids 5, 083302 (2020).
- [17] N. Cagney and S. Balabani, Taylor-Couette flow of shear-thinning fluids, Phys. Fluids 31, 053102 (2019).
- [18] C. S. Dutcher and S. J. Muller, Spatio-temporal mode dynamics and higher order transitions in high aspect ratio Newtonian Taylor-Couette flows, J. Fluid Mech. 641, 85 (2009).
- [19] J. J. J. Gillissen, Two-Dimensional Decaying Elastoinertial Turbulence, Phys. Rev. Lett. 123, 144502 (2019).
- [20] P. R. Fenstermacher, H. L. Swinney, and J. P. Gollub, Dynamical instabilities and the transition to chaotic Taylor vortex flow, J. Fluid Mech. 94, 103 (1979).
- [21] G. S. Lewis and H. L. Swinney, Velocity structure functions, scaling, and transitions in high-Reynoldsnumber Couette-Taylor flow, Phys. Rev. E 59, 5457 (1999).
- [22] M. Q. Nguyen, A. Delache, S. Simoëns, W. J. T. Bos, and M. EL Hajem, Small scale dynamics of isotropic viscoelastic turbulence, Phys. Rev. Fluids 1, 083301 (2016).
- [23] S. Sid, V. E. Terrapon, and Y. Dubief, Two-dimensional dynamics of elasto-inertial turbulence and its role in polymer drag reduction, Phys. Rev. Fluids 3, 011301 (2018).
- [24] R. B. Bird, R. C. Armstrong, and O. Hassager, *Dynamics of Polymeric Liquids, Fluid Mechanics*, 2nd ed. (John Wiley & Sons, New York, 1987), Vol. 1.