Scaling laws and bounds for the turbulent G.O. Roberts dynamo

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Numerical simulations of the G.O. Roberts dynamo are presented. Dynamos both with and without a significant mean field are obtained. Exact bounds are derived for the total energy which conform with the Kolmogorov phenomenology of turbulence. Best fits to numerical data show the same functional dependences as the inequalities obtained from optimum theory.

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I. INTRODUCTION

Purely hydrodynamic or magnetohydrodynamic (MHD) flows driven by a volume force in threedimensional periodic boxes have a long history in the study of fundamental properties of turbulence and magnetic field generation. Under the assumption that there are universal features in turbulence independent of the shape of distant boundaries, spatially periodic models should allow us to study those features conveniently. Body forces are frequently used to model the effect of actual boundaries, such as moving propellers, which are too cumbersome to simulate in full. While this problem is mostly rooted in engineering, it has also become of interest in MHD research because of laboratory dynamo experiments in which liquid metal is forced by a moving boundary more easily represented by a volume force in numerical simulations intended to design or reproduce the experiments (as, for example, in Refs. [\[1,2\]](#page-10-0)). Finally, some mechanisms to drive flows in geo- or astrophysics involve a volume forcing if observed in the appropriate frame of reference, such as precession or tides [\[3\]](#page-10-0).

Even the numerically convenient setting of a flow in a periodic box overstrains computational possibilities if Reynolds numbers get too large. Exact analytical solutions for turbulent flows are unknown, but techniques are known to determine at least upper bounds for certain quantities. This approach is frequently called optimum theory. These techniques have been applied to several idealized flows, notably, Couette flows and convection in plane layers, and also to MHD problems ([\[4–6\]](#page-10-0) and references therein). These bounds were obtained by using either a background field technique going back to Hopf [\[7\]](#page-10-0) and Doering and Constantin [\[8\]](#page-11-0), or by using an optimization procedure introduced by Howard [\[9\]](#page-11-0) and later on championed by Busse [\[10\]](#page-11-0), mostly in the context of convection. Both of these methods rely on the presence of boundaries where boundary conditions restrict admissible fields and are not useful in a periodic domain. The results presented here for dynamos draw on the work for nonmagnetic flows in periodic boxes by Doering and Foias [\[11\]](#page-11-0) (see also [\[12,13\]](#page-11-0)), who formulate bounds in as general terms as possible. The present paper proceeds by way of example and studies a periodic flow introduced by G.O. Roberts [\[14\]](#page-11-0), but the procedure is applicable to general forcing. The G.O. Roberts flow has served as a paradigm for numerous problems [\[15–19\]](#page-11-0) and resembles qualitatively the helical flows generated by convection in rotating systems.

The model which will be considered here is a three-dimensional periodic box driven by a force density such that the flow assumed in the G.O. Roberts dynamo is a solution of the Navier-Stokes equation with that forcing. In general, this flow is unstable. If magnetic field growth sets in, the most important question is at which amplitude the field will saturate. This issue was already tackled with the tools of weakly nonlinear analysis $[20,21]$. Far from onset, dimensional or heuristic arguments are necessary [\[22,23\]](#page-11-0). Heuristics are always uncertain, and dimensional arguments face the problem that more than one length scale (different periodicity lengths in different directions) or more than one velocity scale (the kinetic velocity and the Alfven velocity) may be available to form expressions ` with certain prescribed units. Optimum or bounding theory on the other hand is rigorous but has a

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mixed record regarding its performance in approximating or tightly bounding the quantity of interest. A bound is, of course, the more interesting the closer it is to the value it bounds. The present paper explores the possibilities of this tool when applied to the G.O. Roberts dynamo.

II. THE MODEL

Consider a fluid with density ρ , conductivity σ , kinematic viscosity ν , magnetic permeability μ_0 , and magnetic diffusivity $\lambda = \mu_0 \sigma$ moving at a velocity $v(r,t)$ as a function of position *r* and time *t*. The magnetic field is $B(r,t)$. The flow is driven by the time-independent force density $f(r)$. Periodic boundary conditions are imposed with a periodicity length *h* along the *z* axis and *a* along the *x* and *y* axes. It will later be of interest to apply additional restrictions and to allow mean fields (obtained by averaging over the periodicity volume or over planes) only for certain components. Dimensions are removed from the equations of evolution by using *a* and a^2/λ as units of length and time, and by introducing the rescaled variables $v a / \lambda$, $p a^2 / (\nu \lambda \rho)$ (*p* is the pressure), $B a / \sqrt{\rho \mu_0 \lambda \nu}$, and $fa^3/(\rho \lambda \nu)$. Using the same symbols for the rescaled and for the original variables, the equations of evolution read

$$
\frac{1}{\text{Pm}}(\partial_t \mathbf{v} + \mathbf{v} \cdot \nabla \mathbf{v}) = -\nabla p + \nabla^2 \mathbf{v} + (\nabla \times \mathbf{B}) \times \mathbf{B} + \mathbf{f}, \tag{1}
$$

$$
\partial_t \mathbf{B} + \nabla \times (\mathbf{B} \times \mathbf{v}) = \nabla^2 \mathbf{B}, \tag{2}
$$

$$
\nabla \cdot \mathbf{v} = \nabla \cdot \mathbf{B} = 0,\tag{3}
$$

with Pm = v/λ . The periodicity enforces $v(r,t) = v(r + \hat{x},t) = v(r + \hat{y},t) = v(r + l_z\hat{z},t)$, with $l_z = h/a$ and likewise for *B*. Hats denote unit vectors.

With *V* the volume of the periodicity cell, define the time-averaged densities of magnetic energy E_B and dissipation ϵ_B as

$$
E_B = \left\langle \frac{1}{V} \int \frac{1}{2} \mathbf{B}^2 dV \right\rangle, \ \epsilon_B = \left\langle \frac{1}{V} \int (\nabla \times \mathbf{B})^2 dV \right\rangle \tag{4}
$$

and time-averaged densities of kinetic energy and dissipation as

1

$$
E_{\rm kin} = \left\langle \frac{1}{V} \int \frac{1}{2} \mathbf{v}^2 dV \right\rangle, \ \epsilon_v = \left\langle \frac{1}{V} \int (\partial_j v_i)(\partial_j v_i) dV \right\rangle = \left\langle \frac{1}{V} \int (\nabla \times \mathbf{v})^2 dV \right\rangle, \tag{5}
$$

where $\langle \ldots \rangle$ denotes the time average and with the standard index notation in which summation over repeated indices is implied. It will be convenient to use the force amplitude *F* defined through $f(r) = F\Phi(r)$, with $F \ge 0$. The shape function Φ is normalized to $\frac{1}{V} \int |\Phi(r)|^2 dV = 1$ and obeys $\nabla \cdot \mathbf{\Phi} = 0$. (A contribution with nonzero divergence to f can always be balanced by the pressure gradient.)

A characteristic velocity can be defined from the kinetic energy. Because velocities are given in multiples of λ/a in the units chosen here, this characteristic velocity actually is the magnetic Reynolds number Rm defined as

$$
Rm = \sqrt{2E_{\rm kin}}.\tag{6}
$$

The hydrodynamic Reynolds number Re is given by

$$
Re = Rm/Pm.
$$
 (7)

The choice of units also leads to a factor Pm in the expression for the total energy E_{tot} :

$$
E_{\text{tot}} = \frac{1}{\text{Pm}} E_{\text{kin}} + E_B. \tag{8}
$$

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One obtains an energy balance by dotting Eq. [\(1\)](#page-1-0) with v , Eq. [\(2\)](#page-1-0) with B , integrating over V , adding the two equations, and using the fact that time derivatives of time averages are zero:

$$
\epsilon_v + \epsilon_B = F \bigg\langle \frac{1}{V} \int \Phi \cdot \boldsymbol{v} dV \bigg\rangle. \tag{9}
$$

Equations (1) – (3) were solved numerically for a volume force of the form

$$
\Phi = \begin{pmatrix} \sin(2\pi x)\cos(2\pi y) \\ -\cos(2\pi x)\sin(2\pi y) \\ \sqrt{2}\sin(2\pi x)\sin(2\pi y) \end{pmatrix}
$$
(10)

in the domain $0 \le x, y \le 1, 0 \le z \le l_z$. Velocity and magnetic fields were enforced to be periodic in all three directions. Zero wave number modes were allowed for v in the z direction (to conform with the structure of Φ) and for *B* in the *x* and *y* directions (to allow a mean field in the *x*, *y* plane).

The results of six suites of simulations will be presented below, three for $l_z = 1$ and three for $l_z = 2$. For both l_z , three series of runs simulated Pm = 3, 1, and 0.3 for different *F*. The numerical scheme was the same finite difference method implemented on graphics processing units as used in Ref. $[19]$. Spatial resolutions reached up to $512³$.

III. BOUNDS

All the bounds derived below follow from two theorems. The first is the Cauchy-Schwarz inequality stating that

$$
\left| \int gh dV \right|^2 \leqslant \int g^2 dV \cdot \int h^2 dV \tag{11}
$$

for any two square integrable functions *g* and *h*, and the second is Poincare's inequality in the form ´

$$
\int g^2 dV \le l^2 \int |\nabla g|^2 dV,\tag{12}
$$

where l^2 is the inverse of the smallest eigenvalue of $-\nabla^2$ whose eigenfunction is compatible with the boundary conditions and restrictions imposed on g [\[11\]](#page-11-0). We will apply Poincaré's inequality to components of both velocity and magnetic fields and use inverse eigenvalues l_v^2 and l_B^2 . Periodicity alone allows spatially constant fields, leading to infinite l_v and l_B . However, we will want to exclude uniform translation and a uniform magnetic field (which does not decay through Ohmic diffusion), and l_p and l_B are determined by the smallest wave vector of the admitted fields. It may be interesting to make different choices for v and B regarding the admissible fields with the largest length scale, as was done at the end of the previous section, so that we keep track of two different lengths l_v and l_B .

It is now trivial to obtain bounds in which F plays the role of the control parameter. Poincaré's inequality applied to the definitions of energies and dissipation rates yields

$$
\epsilon_v \geqslant \frac{1}{l_v^2} 2E_{\text{kin}}, \ \epsilon_B \geqslant \frac{1}{l_B^2} 2E_B. \tag{13}
$$

Combined with the Cauchy-Schwarz inequality applied to Eq. (9), this leads to

$$
\frac{Rm^2}{l_v^2} + \frac{2E_B}{l_B^2} \leqslant \epsilon_v + \epsilon_B \leqslant FRm.
$$
\n(14)

Since all variables in this inequality are positive, it immediately follows that

$$
\text{Rm} \leqslant Fl_v^2,\tag{15}
$$

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and from searching the extremum of E_B over Rm in Eq. [\(14\)](#page-2-0), that

$$
E_B \leqslant \frac{1}{8} (l_B l_v F)^2,\tag{16}
$$

so that the total energy is bounded from above by

$$
E_{\text{tot}} = \frac{1}{\text{Pm}} E_{\text{kin}} + E_B \leqslant \left(\frac{1}{\text{Pm}} \frac{1}{2} l_v^2 + \frac{1}{8} l_B^2\right) l_v^2 F^2. \tag{17}
$$

This upper bound is of very limited practical interest. The dependence of E_{tot} in F^2 suggests that this bound needs to be so large in order to accommodate laminar solutions which will become unstable in an actual time integration at sufficiently large F , so that the E_{tot} obtained in numerical simulations of turbulent flows will be far below this bound. Optimum theory as we currently know it is not able to discriminate between stable and unstable solutions, which is one of its major weaknesses.

For now, we will seek bounds independent of *F*, which relates energies and dissipation rates. One obtains the following from dotting Eq. [\(1\)](#page-1-0) with *f* and averaging

$$
\frac{1}{\text{Pm}} F\left\langle \frac{1}{V} \int \Phi \cdot \{ (\mathbf{v} \cdot \nabla) \mathbf{v} \} dV \right\rangle
$$
\n
$$
= F\left\langle \frac{1}{V} \int \Phi \cdot \nabla^2 \mathbf{v} dV \right\rangle + F\left\langle \frac{1}{V} \int \Phi \cdot \{ (\nabla \times \mathbf{B}) \times \mathbf{B} \} dV \right\rangle + F^2.
$$
\n(18)

Two of the integrals appearing in this equation can be manipulated into more convenient forms:

$$
\int \Phi \cdot \{ (\mathbf{v} \cdot \nabla) \mathbf{v} \} dV = -\int v_i v_j \frac{1}{2} (\partial_i \Phi_j + \partial_j \Phi_i) dV \tag{19}
$$

and

$$
\int \Phi \cdot \{ (\nabla \times \mathbf{B}) \times \mathbf{B} \} dV = -\int B_i B_j \frac{1}{2} (\partial_i \Phi_j + \partial_j \Phi_i) dV. \tag{20}
$$

The tensor $\frac{1}{2}(\partial_i \Phi_j + \partial_j \Phi_i)$ is real and symmetric and therefore has real eigenvalues. Denote by *e* the largest absolute value of these eigenvalues found anywhere in the volume. One then has

$$
\left| \left\langle \frac{1}{V} \int \Phi \cdot \{ (v \cdot \nabla) v \} dV \right\rangle \right| \leqslant 2e E_{\text{kin}} \tag{21}
$$

and

$$
\left| \left\langle \frac{1}{V} \int \Phi \cdot \{ (\nabla \times \mathbf{B}) \times \mathbf{B} \} dV \right\rangle \right| \leqslant 2eE_B.
$$
 (22)

These bounds could be sharpened. In order to improve the first inequality, one could determine the divergence-free, periodic field *v* which maximizes $\int \Phi \cdot \{ (v \cdot \nabla)v \} dV$ and obtain a better estimate from there. This procedure requires the solution of a multidimensional linear eigenvalue problem, which is a large numerical effort which does not seem appropriate for this paper. It should also be pointed out that in the context of the G.O. Roberts flow, the first of the above integrals will be grossly overestimated, anyway. It is known from numerical simulations that the velocity field resembles the laminar flow even if the forcing is chosen large enough to create turbulence [\[18\]](#page-11-0). If Φ is the force field of the Roberts flow of Eq. [\(10\)](#page-2-0) and *v* the laminar response, then the integral $\int \Phi \cdot \{(\mathbf{v} \cdot \nabla)\mathbf{v}\}dV$ is strictly zero.

The remaining integral in Eq. [\(18\)](#page-3-0) can be estimated using the Cauchy-Schwarz inequality:

$$
\left\langle \frac{1}{V} \int \Phi \cdot \nabla^2 v dV \right\rangle = \left\langle \frac{1}{V} \int v \cdot \nabla^2 \Phi dV \right\rangle = \frac{1}{V} \int \langle v \rangle \cdot \nabla^2 \Phi dV
$$

$$
\leqslant \sqrt{\frac{1}{V} \int \langle v \rangle^2 dV} \sqrt{\frac{1}{V} \int |\nabla^2 \Phi|^2 dV}
$$

$$
\leqslant \sqrt{\frac{1}{V} \left\langle \int v^2 dV \right\rangle} ||\nabla^2 \Phi|| = \text{Rm} ||\nabla^2 \Phi|| \tag{23}
$$

with the shorthand notation $\|\nabla^2 \Phi\| = \sqrt{\frac{1}{V} \int |\nabla^2 \Phi|^2 dV}$. Inserting these inequalities into Eq. [\(18\)](#page-3-0) leads to

$$
F \leqslant 2eE_{\text{tot}} + \|\nabla^2 \Phi\| \text{Rm}.
$$

This inequality is finally introduced into $\epsilon_v + \epsilon_B \leq F R m$ [see Eq. [\(14\)](#page-2-0)] to yield

$$
\epsilon_v + \epsilon_B \leqslant 2eE_{\text{tot}}\text{Rm} + \|\nabla^2\Phi\|\text{Rm}^2. \tag{25}
$$

It can be seen from the definitions of Rm and *E*tot, Eqs. [\(6\)](#page-1-0) and [\(8\)](#page-1-0), that *E*tot varies as a function of Rm as Rm² for $E_B = 0$ and possibly faster if $E_B \neq 0$. The first term on the right-hand sides of Eqs. (24) and (25) thus exceeds the second term by at least a factor Rm. If we now restrict attention to the limit Rm $\rightarrow \infty$ and retain only the dominating term in Rm on the right-hand sides in Eqs. (24) and (25), we find that asymptotically,

$$
E_{\text{tot}} \geqslant \frac{1}{2e}F\tag{26}
$$

and

$$
\epsilon_v + \epsilon_B \leqslant 2eE_{\text{tot}}\text{Rm}.\tag{27}
$$

The first inequality is a lower bound for the total energy in terms of *F*, which complements the upper bound derived above and expresses the scaling expected for turbulent flow.

The second inequality (27), if used as an equality, is familiar from the Kolmogorov picture of turbulence in that it states that a dissipation rate is given by an energy multiplied by a large-scale Reynolds number. Note that a relation of this type could only be derived for the total energy, not kinetic and magnetic energies separately.

It is always true that $\epsilon_v + \epsilon_B \geq \epsilon_B$, and at large Rm, one expects the dissipation rate to be dominated by Ohmic dissipation, so that $\epsilon_v + \epsilon_B \approx \epsilon_B$, and one can transform with little loss Eq. (27) into $\epsilon_B \leq 2eE_{\text{tot}}Rm$. For infinite Pm (more precisely, for $Rm^2/Pm \to 0$), one has the additional simplification

$$
\epsilon_B \leqslant 2eE_B \text{Rm},\tag{28}
$$

which suggests that in this case the Kolmogorov phenomenology applies to the magnetic field alone.

The next section will study among others the ratio ϵ_B/E_B . For infinite Pm, ϵ_B/E_B is evidently bounded from above by 2*e*Rm. The bound is more complicated in the general case. Inserting $\epsilon_v \ge Rm^2/l_v^2$ into Eq. (25) leads to

$$
\frac{\epsilon_B}{E_B} \leqslant 2e\text{Rm} + 2e\frac{E_{\text{kin}}}{E_B \text{Pm}}\text{Rm} + \left(\|\nabla^2\Phi\| - \frac{1}{l_v^2}\right)\frac{\text{Rm}^2}{E_B}.\tag{29}
$$

This expression frequently simplifies, as, for instance, for the G.O. Roberts flow, because $\|\nabla^2 \Phi\| =$ $1/l_v^2$ and the last term disappears.

FIG. 1. $\overline{E}_B/(E_B - \overline{E}_B)$ as a function of Rm for $l_z = 2$ (blue symbols with an enclosed surface) and $l_z = 1$ (red symbols built of crosses and stars). For $l_z = 2$, Pm is 0.3 (squares), 1 (circles), and 3 (diamonds). Results for the same Pm are shown for $l_z = 1$: Pm = 0.3 (+), 1 (x), and 3 (*). The solid line indicates the power law Rm^{-1} .

Up to here, this section was kept in general terms independent of a particular choice for Φ . The next section presents numerical simulations of the G.O. Roberts dynamo, which means that Φ is given by Eq. (10) , which implies

$$
\|\nabla^2 \Phi\| = 8\pi^2, \ e = 2\pi. \tag{30}
$$

The velocity is allowed to have a component independent of *z* but is required to be periodic with periodicity length 1 in the *x* and *y* directions, so that $1/l_v^2 = 8\pi^2$. The magnetic field on the other hand is allowed to have a mean field along the *x* and *y* directions but is required to be strictly periodic in the *z* direction with periodicity length l_z , so that $1/l_B^2 = (2\pi/l_z)^2$.

IV. RESULTS

We start with an overview of the solutions obtained numerically. The G.O. Roberts dynamo is the prototypical α^2 dynamo with a large mean field for control parameters near a dynamo onset at small Rm. We therefore compute both the total magnetic energy density E_B and the energy density of the mean field,

$$
\overline{E}_B = \left\langle \frac{1}{V} A \int dz \frac{1}{2} \left(\frac{1}{A} \int dy \int dx B \right)^2 \right\rangle, \tag{31}
$$

where *A* is the cross section of the computational volume *V* in the *x*, *y* plane, and $A = \int dx \int dy$. The ratio of mean to fluctuating energies, $\overline{E}_B/(E_B - \overline{E}_B)$, is shown as a function of Rm in Fig. 1. The computations with the better separation of scales $(l_z = 2)$ show a magnetic field dominated by the mean field at low Rm. The contribution of the mean field to the total field suddenly decreases at an Rm between a few hundred and 1000. Beyond that sudden drop, $E_B/(E_B - E_B)$ decreases approximately as $1/Rm$, whereas the runs with the worse separation of scales ($l_z = 1$) always have $\overline{E}_B/(E_B - \overline{E}_B)$ < 1 and show a decrease of this ratio roughly in 1/Rm. A similar abrupt drop as in the case $l_z = 2$ was observed in convection-driven dynamos [\[24\]](#page-11-0), where this drop signaled a transition from dynamos generating a mean magnetic field to dynamos which do not generate a mean field and in which all observed mean fields are merely statistical fluctuations. In the convection dynamos, the transition occurred at even smaller Rm than observed here for the G.O. Roberts dynamo. A dramatic

FIG. 2. $(1 - f_0)$ Pm^{-1/2} as a function of Re with the same symbols as in Fig. [1.](#page-5-0)

decrease of mean field generation at large Rm was already noticed in Ref. [\[18\]](#page-11-0) and could be linked to a transition from a large-scale to a small-scale dynamo. While the disappearance of the mean field is observed in the dynamos with the columnar flow structures mentioned above, it does not appear in less organized turbulent flows [\[25\]](#page-11-0). For the purpose of the present paper, it suffices to note that the simulations discussed here contain cases of fields dominated by a mean field as well as cases with a small mean field.

Another result relevant to the discussion below is the ratio of magnetic and total dissipation rate:

$$
f_{\Omega} = \frac{\epsilon_B}{\epsilon_B + \epsilon_v}.
$$
\n(32)

This ratio has received much attention in recent years, partly due to an attempt to theoretically predict saturation field strengths in convection dynamos $[26]$. f_{Ω} is zero for Rm below the onset of dynamo action and tends to 1 for Rm tending to infinity. Brandenburg [\[27\]](#page-11-0) found that $\epsilon_v/(\epsilon_B + \epsilon_v) = 1 - f_{\Omega}$ scales as Pm^{1/2}, and later [\[28\]](#page-11-0) that $\epsilon_v/\epsilon_B \propto Pm^{0.6}$. Finally, a dependence of the exponent on helicity was discovered in Ref. [\[29\]](#page-11-0). Figure 2 plots $(1 - f_{\Omega})$ Pm^{-1/2}. The factor Pm^{-1/2} obviously has not removed the Pm dependence from the graph. In fact, there is no recognizable scaling for f_{Ω} in the present data collection. The point of interest for the discussion below is that $0.07 < f_{\Omega} < 0.8$ for all points in Fig. 2.

The most natural global quantity to investigate regarding its scaling behavior is the total energy E_{tot} as a function of the driving force *F*, as shown in Fig. [3.](#page-7-0) The bounding theory of the previous section provides us with an upper and a lower bound on E_{tot} . According to [\(24\)](#page-4-0) and for Rm $\rightarrow \infty$, one has for the G.O. Roberts flow $E_{\text{tot}} \geqslant F/(4\pi)$, and Eq. [\(17\)](#page-3-0) yields $E_{\text{tot}} \leqslant F^2(\frac{1}{\text{Pm}} + \frac{1}{2}l_z^2)/(128\pi^4)$. As mentioned above, the second bound is required by laminar solutions and can only be of interest for small *F*. The scaling for large *F* suggested by the first bound can also be inferred from heuristic arguments: The energy injected into, and dissipated by, the flow is in order of magnitude *FU* with *U* a characteristic flow velocity, whereas the total energy dissipation is within the Kolmogorov phenomenology proportional to $E_{\text{tot}}U/L$, so that $E_{\text{tot}} \propto FL$, with *L* an integral length scale and the proportionality factor is of course left undetermined. This scaling matches the lower bound in Eq. [\(24\)](#page-4-0). The bounding theory provides us with prefactors. In the high Rm limit, this prefactor differs by a factor 2π from the prefactor obtained from the fit shown in Fig. [3.](#page-7-0) The exponent on the other hand is close to the one found in the actual simulations, in as far as one accepts exponents deduced from the limited set of data in Fig. [3.](#page-7-0) The upper and lower bounds represent the actual scalings in separate intervals of *F*, because one is based on laminar solutions and the other is not.

FIG. 3. Total energy as a function of the driving force *F* with the same symbols as in Fig. [1.](#page-5-0) The continuous line shows the function $F/2$, and the dashed line is given by $F^2/(3 \times 10^4)$.

The upper bounds for the energy dissipation are not infested by laminar unstable solutions. For large Rm [so that the term $8\pi^2$ Rm² is negligible in Eq. [\(25\)](#page-4-0)] one has

$$
\epsilon_v + \epsilon_B \leqslant 4\pi \, E_{\text{tot}} \text{Rm}.\tag{33}
$$

The factor 4π is again an order of magnitude larger than the factor found in the simulations at the highest Rm, as seen in Fig. 4. However, the important point about this bound is, in analogy with the nonmagnetic case [\[11\]](#page-11-0), that it provides a rigorous underpinning to the Kolmogorov phenomenology as long as it is applied to total energy and dissipation in the form $\epsilon_v + \epsilon_B \propto E_{tot} U/L$. The bounding theory does not in general provide support for any extensions of this phenomenology in which magnetic and kinetic energies are split and which provides us with a scaling for the magnetic field amplitude. Some simplification is achieved at large Rm, in which case $\epsilon_B \gg \epsilon_v$ and Eq. [\(25\)](#page-4-0) simplifies to

$$
\epsilon_B \leqslant 4\pi \, E_{\text{tot}} \text{Rm}.\tag{34}
$$

FIG. 4. $E_{\text{tot}}\text{Rm}/(\epsilon_B + \epsilon_v)$ as a function of Re with the same symbols as in Fig. [1.](#page-5-0)

FIG. 5. $E_{\text{tot}}\text{Rm}/\epsilon_B$ as a function of $\text{Rm}/\epsilon_P^{\text{m}^{-1/2}}$ with the same symbols as in Fig. [1.](#page-5-0) The factor $l_z\text{Pm}^{-1/2}$ is introduced on the *x* axis for a better collapse of the data points and a more compact graphical representation, but it has no known physical significance.

Figure 5 verifies relation [\(34\)](#page-7-0). A regime asymptotic in Rm of the form E_{tot} Rm/ $\epsilon_B \rightarrow$ const cannot be discernible yet because ϵ_B is not much larger than ϵ_v in any of these simulations. Note the appearance of E_{tot} instead of E_{kin}/Pm on the right-hand side of Eq. [\(34\)](#page-7-0). An equation containing only magnetic quantities, at least in the form of a bound, is only obtained in the limit Pm $\rightarrow \infty$ [see Eq. [\(28\)](#page-4-0)]. Equation [\(13\)](#page-2-0) always bounds E_B in terms of ϵ_B but reflects the scaling pertaining to laminar solutions, so that this bound will be of little practical interest in the turbulent regime.

The distinction between E_{tot} and E_{kin}/P m on the right-hand side of Eq. [\(34\)](#page-7-0) becomes mute if there is equipartition between magnetic and kinetic energies, because then, all energies are proportional to each other. We are therefore led to investigate the ratio $E_B P m / E_{kin}$ in Fig. 6. This ratio is not perfectly constant as F is varied, but except for the case $l_z = 2$, Pm = 3, it varies around its mean by less than 30% (and less than a factor of 2 over all). In the range of Rm in which Fig. 5 suggests the validity of a Kolmogorov phenomenology (typically the last three or four points of each series), the ratio of energies varies by at most 20% around its mean value, while the energies themselves vary by more than an order of magnitude. For the purpose of the scaling implied by Eq. [\(34\)](#page-7-0), $\epsilon_B \propto E_{\text{tot}}$ Rm,

FIG. 6. $E_B Pm/(E_{kin}l_z)$ as a function of *F* with the same symbols as in Fig. [1.](#page-5-0)

FIG. 7. $l_z \epsilon_B/E_B$ as a function of Rm with the same symbols as in Fig. [1.](#page-5-0) The solid line shows the function 4 Rm.

we have nearly $E_B \propto E_{\text{kin}}/Pm \propto E_{\text{tot}}$ and it cannot be tested whether E_{tot} on the right-hand side of this scaling relation is essential or whether it could be replaced by E_B .

However, it is clear from Fig. [6](#page-8-0) that $E_B Pm/E_{kin}$ depends on l_z and Pm, so that there is no strict equipartition between magnetic and kinetic energies but only a proportionality between the two. The same situation was already found in convection dynamos, in which $E_B \propto E_{kin}$ at high Rm, with a proportionality factor depending on additional control parameters [\[30\]](#page-11-0). Reference [\[18\]](#page-11-0) claims to have found equipartition between E_B and E_{kin} . However, this finding was fortuitous because it was obtained for $l_z = 2$ and Pm of order 1. For these parameters, one indeed obtains $E_B \approx E_{kin}/Pm$, but not at general l_z and Pm. From a balance between the Lorentz force term ($\nabla \times \mathbf{B}$) $\times \mathbf{B}$ and the advection term $v \cdot \nabla v$ /Pm and the assumption that *B* and $\nabla \times B$ are dominated by a mean field which varies on the length scale l_z while *v* varies on the length scale 1, one obtains $E_B \propto l_z E_{kin}/Pm$. The same result was derived by Brandenburg [\[22\]](#page-11-0) from an argument based on helicities and the assumption of a dynamo field dominated by its mean component. While these arguments do yield a nontrivial prefactor in $E_B \propto E_{\text{kin}}/Pm$, they require a strong mean field which does not exist in all simulations presented here (see Fig. [1\)](#page-5-0), so that it comes to no surprise that $E_B Pm/(E_{kin}l_z)$ does not yield a value independent of all other parameters in Fig. [6.](#page-8-0)

Let us neglect these additional dependences for the moment and assume E_{kin}/Pm to be proportional to E_B/l_z . Since E_{kin}/Pm is for most points in Fig. [6](#page-8-0) larger than E_B , let us approximate $E_B + E_{kin}/Pm \approx bE_B/l_z$ with some numerical constant *b*, so that Eq. [\(27\)](#page-4-0) becomes

$$
\epsilon_v + \epsilon_B \leqslant b2e \frac{E_B}{l_z} \text{Rm}.\tag{35}
$$

For large Rm, one expects $\epsilon_B \gg \epsilon_v$. The inequality

$$
\epsilon_B \leqslant b2e \frac{E_B}{l_z} \text{Rm} \tag{36}
$$

derived from relation (35) should therefore not be much more inaccurate than relation (35) itself.

Figure 7 tests Eq. (36). At the level of accuracy of double logarithmic plots, the scaling $\epsilon_B \propto$ $\frac{E_B}{l_z}$ Rm implied by (36) viewed as an equality adequately represents the data cloud at large Rm. It should be stressed that this scaling is not strictly supported by the bounds of the previous section, since some heuristic input was necessary concerning $E_B Pm/E_{kin}$.

It is of interest to characterize the magnetic field through a time or length scale extracted from its energy and dissipation rate, ϵ_B/E_B . An initial study on convection dynamos found $\epsilon_B/E_B \propto Rm$ [\[31\]](#page-11-0). Later investigations yielded smaller exponents [\[24\]](#page-11-0). The present computations do not reach to high enough Rm to accurately determine an exponent, but Fig. [7](#page-9-0) suggests $\epsilon_B/E_B \propto$ Rm. Equation [\(29\)](#page-4-0) applied to the G.O. Roberts flow reads

$$
\frac{\epsilon_B}{E_B} \leqslant 4\pi \text{Rm} \bigg(1 + \frac{E_{\text{kin}}}{E_B \text{Pm}} \bigg). \tag{37}
$$

If the bracket tends to a constant for $\text{Rm} \rightarrow \infty$, this inequality shows that the exponent *c* in $\epsilon_B/E_B \propto \text{Rm}^c$ must obey $c \leq 1$.

V. CONCLUSION

The G.O. Roberts dynamo is known as a dynamo generating a mean magnetic field, but this study has shown that as Rm is increased, there is a sudden drop in the contribution by the mean field to the total magnetic energy. The same phenomenon was already observed in convection-driven dynamos in plane layers, which perhaps is not surprising because both flows consist of helical vortices with parallel axes. However, if this is the essential feature common to both flows, one would expect an analogous behavior in convection-driven dynamos in spherical shells. If the analogy is valid, the energy of the axisymmetric modes should suddenly decrease at high Rm in favor of modes with a nonzero azimuthal wave number.

It is possible to derive several rigorous bounds for the G.O. Roberts dynamo. These concern the total energy, either as a function of the driving force or the total dissipation. The same functional dependences appear in these bounds as in heuristic arguments, but the prefactors in proportionalities are determined in the bounds and differ by about an order of magnitude from prefactors determined from best fits to the numerical data. The prefactors and numerical constants in the bounds presented above could be improved with some numerical effort. The Kolmogorov phenomenology relating total energy to total dissipation is compatible with the bounds. But the optimum theory as presented here does not give any bound of interest for the turbulent regime on magnetic energy alone, unless one is interested in the limit of infinite Pm, or unless one accepts an independent result, extracted from numerical simulations, which states that the ratio of magnetic and kinetic energy is nearly independent of Rm at large Rm. In these cases, one obtains a phenomenology of the Kolmogorov type for the magnetic field alone.

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