Diffusion enhancement of Brownian motors revealed by a solvable model

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A solvable model is proposed and analyzed to reveal the mechanism underlying the diffusion enhancement recently reported for a model of molecular motors and predicted to be observed in the biological rotary motor F_1 -ATPase. It turns out that the diffusion enhancement for the present model can approximately be described by a random walk in which the waiting time for a step to occur is exponentially distributed and it takes nonzero time to proceed forward by the step. It is shown that the diffusion coefficient of such a random walk can significantly be increased when the average waiting time is comparable to the average stepping time.

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I. INTRODUCTION

There can be various ways to produce an effective diffusion coefficient larger than what is expected from the Einstein relation. A classical example of such diffusion enhancement is the swimming of bacteria [1]. A bacterium swims with a constant speed and occasionally changes its swimming direction. The resulting motion is a random walk with an effective diffusion coefficient much larger than that of the Brownian motion it would undergo if it stopped swimming. This diffusive motion helps bacteria find their food or move away from harmful environments, for example. Recently, it was found that a Brownian particle moving in a one-dimensional periodic potential exhibits diffusion enhancement under a constant external force of magnitude close to the maximum slope of the potential [2-4]. This phenomenon was observed experimentally in a colloidal system [5], a biomolecule having a rotating subunit [6], and DNA diffusing in an array of entropic barriers [7]. The diffusion enhancement also occurs in on-off ratchets [8] in which an asymmetric, periodic potential for colloidal particles is switched on and off periodically, if the duration of potential-off interval is such that the root-meansquare displacement of the particle by free diffusion in this interval is comparable to the periodicity of the potential.

In our previous work [9], it is demonstrated theoretically that the diffusion enhancement can occur in molecular motors that move autonomously by consuming free energy available from the chemical reaction catalyzed by themselves if a constant external force of appropriate magnitude is applied. In particular, it is suggested that diffusion enhancement can be observed in the F_1 -ATPase, a biological rotary motor, which catalyzes the hydrolysis of adenosine triphosphate (ATP). It has turned out that the mechanism of enhancement in the case of high ATP concentration is essentially the same as the one for the particle in a tilted periodic potential [2–4]. However, the mechanism in the case of low ATP concentration has not been clarified yet. The purpose of the present work is to study the diffusion of a simplified model of molecular motors to elucidate the mechanism of diffusion enhancement characteristic of chemically driven systems. In what follows effective diffusion coefficients will simply be called the diffusion coefficients.

The models considered here and in the previous work [9] are of ratchet type [10-12], in which a moving part of the motor (e.g., the rotor in a rotary motor) is represented by a Brownian particle subject to a potential, which is switched to another upon a chemical transition associated with the reaction catalyzed by the motor. In the model used in the previous paper [9], an external force, as well as rate constants, can control the transition rates because the transition rates are assumed to depend on the particle position, which is affected by the force; the dependence of the diffusion coefficient on the force for given rate constants exhibits enhancement in a certain range of the force. By contrast, an external force is not included in the model of the present paper, and a rate constant is varied to study the diffusion enhancement. Another simplification is that chemical transitions are supposed to take place only when the particle is located at particular points, which enable us to obtain a closed-form expression for the diffusion coefficient.

The paper is organized as follows. The model is introduced in Sec. II, and the closed-form expressions for the velocity and diffusion coefficient are given in Sec. III. Explicit calculations of the diffusion coefficient are carried out for a model with piecewise linear potentials in Sec. IV, where the diffusion enhancement is demonstrated. In Sec. V, we discuss the mechanism of the diffusion enhancement observed in Sec. IV on the basis of a simple random walk, which we call an *extended Poisson walk*. Concluding remarks will be given in

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FIG. 1. Generic (a) and specific (b) models of molecular motors considered in this work. The motor is represented by a Brownian particle subject to one of the potentials $V_n(x)$ at a time. The potential is switched from V_n to V_{n+1} or V_{n-1} stochastically with rates proportional to ω_+ and ω_- , respectively, if the particle is located at $x = a_+ + nl$ or $a_- + nl$; we set $a_+ = 0$ and $a_- = -l$ for (b).

Sec. VI. Some of the details of calculations and expressions are given in the Appendices.

II. POTENTIAL-SWITCHING RATCHET

We consider a variant of pulsating ratchets as a model of a biological molecular motor [10–12]. The motor is modeled as a Brownian particle moving in one dimension, along the x axis, subject to potentials $V_n(x)$ ($n = 0, \pm 1, \pm 2, ...$) of identical shapes arranged periodically with period l as shown in Fig. 1(a), i.e., they satisfy

$$V_{n+1}(x) = V_n(x-l) \quad (n = 0, \pm 1, \pm 2, \dots).$$
(1)

The potentials are assumed to be unbounded above. Only one of the potentials acts on the particle at a time, say V_n , and it is stochastically switched to V_{n+1} or V_{n-1} . The motor will be said to be in *state* n if potential V_n is acting. The dynamics of the particle is assumed to be over-damped. The diffusion coefficient of the particle in the absence of the potentials is given by the Einstein relation $D_0 = k_{\rm B}T/\gamma$, where γ is the coefficient of the drag force on the particle from the surrounding fluid, T is the temperature, and $k_{\rm B}$ is the Boltzmann constant.

Let $P_n(x, t) dx$ be the probability to find the motor in state n and the particle in the interval (x, x + dx) on the x axis at time t, and $w_n^{\pm}(x)$ be the rate of transition from state n to state $n \pm 1$ when the particle is located at x. Then the time evolution of $P_n(x, t)$ is described by the Fokker-Planck equations,

$$\frac{\partial P_n}{\partial t} + \frac{\partial J_n}{\partial x} = -(w_n^+ + w_n^-)P_n + w_{n-1}^+ P_{n-1} + w_{n+1}^- P_{n+1}, \qquad (2)$$

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where J_n is the probability current in state *n* defined by

$$J_n \equiv -D_0 \left(\frac{\partial}{\partial x} + \frac{dU_n}{dx}\right) P_n,\tag{3}$$

with

$$U_n(x) \equiv V_n(x)/k_{\rm B}T \tag{4}$$

being the dimensionless potential. We remark that the arguments given in this section apply also to the case in which a constant external force F is applied to the particle if the right-hand side of Eq. (4) is replaced by $[V_n(x) - Fx]/k_BT$.

We assume that the transition from one state to another takes place when the particle is located at a particular position (this corresponds to the idea that the change in chemical state of a motor protein occurs when it is in a particular conformation [10]), and we adopt the following expressions for $w_n^{\pm}(x)$:

$$w_n^{\pm}(x) = \omega_{\pm}\delta(x - a_{\pm} - nl), \tag{5}$$

where $\delta(x)$ is the δ function, ω_{\pm} are positive constants, and a_+ and a_- are constants satisfying $a_- = a_+ - l$; see Fig. 1(a). The transition $n \rightarrow n + 1$ and its reversal occur at $x = a_+ + nl = a_- + (n + 1)l$. Supposing that the "forward" transition $n \rightarrow n + 1$ is triggered by a chemical reaction by which the free energy of the environment is decreased by $\Delta \mu$, we have the relation

$$\omega_{+}/\omega_{-} = \exp[U_{0}(a_{+}) - U_{0}(a_{-}) + \Delta\mu/k_{\rm B}T] \qquad (6)$$

from the condition of local detailed balance.

The velocity v and the diffusion coefficient D of the motor are defined by

$$v \equiv \lim_{t \to \infty} \frac{\langle x(t) - x(0) \rangle}{t}, \ D \equiv \lim_{t \to \infty} \frac{\langle [x(t) - x(0) - vt]^2 \rangle}{2t},$$
(7)

where x(t) is the location of the particle (motor) at time tand the angular brackets indicate the statistical average. The velocity can be obtained from the steady-state solutions $P_n(x)$ of the Fokker-Planck Eqs. (2), which satisfy the "periodicity condition" $P_n(x) = P_0(x - nl)$. Let P(x) be the rescaled $P_0(x)$, so that it satisfies

$$\int_{-\infty}^{\infty} P(x) dx = 1.$$
 (8)

Then we have [10,11]

$$v = \int_{-\infty}^{\infty} f(x)P(x) \, dx, \quad f(x) \equiv -D_0 \, dU_0(x)/dx.$$
(9)

To calculate the diffusion coefficient, we need to obtain the auxiliary function Q(x) that satisfies

$$\frac{d}{dx} \left[D_0 \frac{d}{dx} - f(x) \right] Q(x) - [w_0^+(x) + w_0^-(x)] Q(x) + w_0^+(x+l)Q(x+l) + w_0^-(x-l)Q(x-l) = \left[v - f(x) + 2D_0 \frac{d}{dx} \right] P(x)$$
(10)

and the boundary condition that $Q(x) \rightarrow 0$ as $|x| \rightarrow \infty$. The diffusion coefficient is calculated as [9,13,14]

$$D = D_0 + \int_{-\infty}^{\infty} [f(x) - v] Q(x) dx.$$
(11)

III. CLOSED-FORM EXPRESSIONS

The specific functional forms of $w_n^{\pm}(x)$ given in Eq. (5) enable us to derive closed form expressions for v and D, as explained in Appendix A. To express the result for v concisely, we introduce constants ζ , ϕ_0 , ϕ_1 , and u_{\pm} defined by

$$\zeta \equiv \int_{-\infty}^{\infty} e^{-U(x)} dx, \qquad (12)$$

$$\phi_0 \equiv \int_{a_-}^{a_+} e^{U(x)} \, dx, \tag{13}$$

$$\phi_1 \equiv \int_{a_-}^{a_+} e^{U(y)} \, dy \int_{-\infty}^{y} e^{-U(x)} \, dx, \qquad (14)$$

$$u_{\pm} \equiv \omega_{\pm} \exp[-U(a_{\pm})], \qquad (15)$$

where

$$U(x) \equiv U_0(x). \tag{16}$$

Then, the velocity is expressed as

$$v = \frac{(u_+ - u_-)D_0l}{\zeta(D_0 + \phi_0 u_-) + \phi_1(u_+ - u_-)}.$$
 (17)

Note that we have $u_+ > u_-$ for $\Delta \mu > 0$ according to the detailed-balance condition in Eq. (6) and that the denominator in Eq. (17) is positive since $\zeta \phi_0 - \phi_1 > 0$, which can be verified from Eqs. (12)–(14). Therefore, Eq. (17) indicates that v > 0 for $\Delta \mu > 0$, as expected.

The result for *D* can be expressed as

$$D = \lambda l + v \int_{-\infty}^{\infty} W(x) \, dx, \qquad (18)$$

with the constant λ and function W(x) given below. The function W(x) is defined by

$$W(x) \equiv h(x) - \int_{-\infty}^{x} P(y) \, dy, \qquad (19)$$

where the function h(x) is defined by

$$h(x) \equiv \begin{cases} 0 & (x < a_{-}), \\ (x - a_{-})/l & (a_{-} \leq x \leq a_{+}), \\ 1 & (x > a_{+}), \end{cases}$$
(20)

and the rescaled steady-state distribution P(x) is given by

$$P(x) = g(x) \exp[-U(x)], \qquad (21)$$

with

$$g(x) = \begin{cases} C_{-} & (x < a_{-}), \\ C_{-} - \frac{v}{D_{0}l} \int_{a_{-}}^{x} e^{U(y)} dy & (a_{-} \leq x \leq a_{+}), \\ C_{+} & (x > a_{+}). \end{cases}$$
(22)

Here, the constants C_{\pm} are defined by

$$C_{\pm} \equiv \frac{(1 + \phi_0 u_{\mp} / D_0) v}{(u_+ - u_-) l}.$$
(23)

The constant λ in Eq. (18) is given by

$$\lambda \equiv -\frac{\zeta \psi_0 u_- + \psi_1 (u_+ - u_-)}{\zeta (D_0 + \phi_0 u_-) + \phi_1 (u_+ - u_-)},$$
(24)

where ψ_0 and ψ_1 are integrals

$$\psi_0 \equiv \int_{a_-}^{a_+} R(x) e^{U(x)} \, dx, \qquad (25)$$

$$\psi_1 \equiv \int_{-\infty}^{\infty} e^{-U(x)} dx \int_{x}^{a_+} R(y) e^{U(y)} dy, \qquad (26)$$

involving a new function R(x) defined by

$$R(x) \equiv vW(x) - D_0P(x).$$
⁽²⁷⁾

IV. MODEL WITH PIECEWISE-LINEAR POTENTIALS

As a specific example, we consider a model with piecewise linear potentials for which $V_0(x)$ is given by

$$V_0(x) = K|x|,$$
 (28)

with a positive parameter K; see Fig. 1(b). The parameter for the locations of transitions is set as $a_+ = 0$ (which implies $a_- = -l$). For this model the integrals needed to calculate the velocity and diffusion coefficient can be carried out analytically, as explained below. This particular model will be referred to as *the ratchet model* (or the ratchet) for convenience, though it is merely an example of ratchet-type models, to distinguish it from other models to be discussed in Sec. V.

A. Results

It is straightforward to obtain the constants involved in Eq. (17) for *v*; the results are as follows:

$$\zeta = 2/\kappa, \quad \phi_0 = (e^{\kappa l} - 1)/\kappa, \quad \phi_1 = l/\kappa,$$
 (29)

$$u_{+} = \omega_{+}, \quad u_{-} = \omega_{-} e^{-\kappa l},$$
 (30)

where

$$\kappa \equiv K/k_{\rm B}T.$$
 (31)

Substituting expressions in Eqs. (29) and (30) into Eq. (17), we obtain the average velocity v of the motor for this model:

$$v = \frac{\kappa D_0(\omega_+ - \omega_- e^{-\kappa l})}{\omega_+ + (2/\kappa l)(\omega_- + \kappa D_0) - (1 + 2/\kappa l)\omega_- e^{-\kappa l}}.$$
 (32)

Note that *v* monotonically increases with ω_+ , which is proportional to the forward transition rate $w_n^+(x)$, Eq. (5), and tends to the limiting value $\kappa D_0 = K/\gamma$. This is identical to the average velocity of a particle subject to a constant external force *K*. This is because, in the limit of large ω_+ , the particle stays only on the left-side slopes of potentials V_n of Fig. 1(b), since the potential is switched from V_n to V_{n+1} right after the particle on the left-side slope of V_n reaches the potential minimum at x = nl, and this switching brings the particle to the left-side slope of V_{n+1} , and so on.

The expressions for the steady-state probability density P(x) and the auxiliary function W(x), both needed for calculating the diffusion coefficient, are presented in Appendix B.



FIG. 2. Dependence of the diffusion coefficient \tilde{D} on the forward transition rate $\tilde{\omega}_+$ for the ratchet model. (a) The results for several choices of \tilde{K} are shown in the case of $\tilde{\omega}_- = 0.1$. (b) The results for several choices of the rate $\tilde{\omega}_-$ of backward transition, in the cases of $\tilde{K} = 40$ and 20.

From the expressions for W(x) given in Eqs. (B3) and (B4), we have

$$\int_{-\infty}^{\infty} W(x) dx = \frac{l}{2} - \frac{vl}{2\kappa D_0} \left(1 + \frac{2}{\kappa l}\right), \qquad (33)$$

which contributes to the second term in Eq. (18) for *D*. The integrals ψ_0 and ψ_1 defined by Eqs. (25) and (26), respectively, can be carried out by substituting Eq. (27) with W(x) and P(x) given in Eqs. (B1)–(B4) into these definitions to obtain

$$\psi_0 = \frac{2v^2}{\kappa^2 D_0} \left(1 + \frac{\kappa l}{4} - \frac{e^{\kappa l} - 1}{\kappa l} \right) - \frac{D_0 \kappa l}{2}, \qquad (34)$$

$$\psi_1 = \frac{vl}{2\kappa} \left(1 - \frac{4}{\kappa l} \right) - \frac{v^2 l}{2\kappa^2 D_0}.$$
(35)

From these results and Eqs. (29) and (30), we find λ defined by Eq. (24), which contributes to the first term in Eq. (18). Substituting this result for λ together with Eq. (33) into Eq. (18) provides us with the analytic expression for *D*.

The dependence of the diffusion coefficient on ω_+ is shown in Fig. 2(a) for several choices of K and a fixed value of ω_- . The result is represented in terms of dimensionless parameters defined by

$$\tilde{D} \equiv D/D_0, \quad \tilde{\omega}_{\pm} \equiv l\omega_{\pm}/D_0, \quad \tilde{K} \equiv lK/k_{\rm B}T.$$
 (36)

We observe that \tilde{D} increases monotonically with $\tilde{\omega}_+$ for $\tilde{K} = 5$, whereas it has a peak around at $\tilde{\omega}_+ \sim 1$ for large values of \tilde{K} . The peak height increases with \tilde{K} . In either case, \tilde{D} tends to 1 (D tends to D_0) from below as $\tilde{\omega}_+ \rightarrow \infty$ (therefore, the curve $\tilde{D}(\tilde{\omega}_+)$ exhibits a shallow dip when it has a peak). The reason why D converges to D_0 is that, in this limiting case, the particle always experiences a constant external force as explained above, and hence its diffusion coefficient is the same as that of a free particle. The increase in the diffusion coefficient controlled by the transition rate shown in Fig. 2(a) is the *diffusion enhancement* in our model for molecular motors.

Figure 2(b) shows how the diffusion enhancement is affected by the rate parameter $\tilde{\omega}_{-}$ of the backward transition for the cases of $\tilde{K} = 20$ and 40. In the both cases, the peak height does not depend very much on $\tilde{\omega}_{-}$, while the peak position moves to the right (the direction of increasing $\tilde{\omega}_{+}$) as $\tilde{\omega}_{-}$ increases.

B. Limit of small ω_{-}

We see from Fig. 2(b) that, as $\tilde{\omega}_{-}$ decreases, \tilde{D} as a function of $\tilde{\omega}_{+}$ for a given \tilde{K} converges to a certain function [indicated by the solid line in Fig. 2(b)]. This limiting function is obtained by setting $\omega_{-} = 0$ in the expression for D obtained above; we have

$$D = \frac{v^3}{\kappa^3 D_0^2} \left[1 + \frac{2D_0}{l\omega_+} + 2\kappa l \left(\frac{D_0}{l\omega_+}\right)^2 \right],$$
 (37)

with the limiting velocity

$$v = \frac{\kappa D_0 \omega_+}{\omega_+ + 2D_0/l},\tag{38}$$

which has the "Michaelis-Menten–type" dependence [15] on ω_+ . We are interested in this limiting case because this case corresponds to the limit of low ATP concentration of the previous model [9] for molecular motors, and the mechanism of the diffusion enhancement observed in this situation has not been clarified, as mentioned in the Introduction.

Equation (37) tells that if $\tilde{K} > 4 + 2\sqrt{3} \approx 7.46$ then the function $\tilde{D}(\tilde{\omega}_+)$ has a peak at

$$\tilde{\omega}_{+}^{\max} = \tilde{K}/2 - 1 - \sqrt{\tilde{K}^2/4 - 2\tilde{K} + 1}$$
(39)

and a local minimum at $\tilde{\omega}_{+}^{\min}$ given by Eq. (39) with the sign of the last term being changed. The dependence of $\tilde{\omega}_{+}^{\max}$ and $\tilde{\omega}_{+}^{\min}$ on \tilde{K} are shown in Fig. 3(a); and the peak height \tilde{D}_{\max} and the value of \tilde{D} at the local minimum \tilde{D}_{\min} are plotted against \tilde{K} in Fig. 3(b). It is seen that the peak position $\tilde{\omega}_{+}^{\max}$ tends to unity as

$$\tilde{\omega}_{+}^{\max} \approx 1 + 3/\tilde{K} \tag{40}$$

in the large \tilde{K} limit, whereas the peak height \tilde{D}_{max} increases almost linearly in \tilde{K} . In fact, we have

$$D_{\rm max} \approx 2K/27 + 1/9 \tag{41}$$



FIG. 3. Dependencies of (a) $\tilde{\omega}_{+}^{\text{max}}$ and $\tilde{\omega}_{+}^{\text{min}}$ and (b) \tilde{D}_{max} and \tilde{D}_{min} on \tilde{K} . Here, $\tilde{\omega}_{+}^{\text{max}}$ and $\tilde{\omega}_{+}^{\text{min}}$ are the positions of the peak and the local minimum of function $\tilde{D}(\tilde{\omega}_{+})$, respectively, and \tilde{D}_{max} and \tilde{D}_{min} are the values of \tilde{D} at these locations. The solid lines are the results for the ratchet model given in Eq. (37) in the limit of $\tilde{\omega}_{-} = 0$, and the dashed lines are those for the extended Poisson walk, Eq. (53).

for large \tilde{K} . A diffusion coefficient of more than twice that of free diffusion ($\tilde{D} > 2$) can be achieved for $\tilde{K} \gtrsim 25$. The mechanism of the diffusion enhancement in this limiting case is discussed in the next section.

V. EXTENDED POISSON WALK

A. Diffusion of a random walker

For qualitative understanding of the diffusion enhancement we have observed in the preceding section, let us take a look at the motion of the particle for the case in which the backward transition can be neglected (Sec. IV B). The particle moves on the left-side slope of one of the V-shaped potentials shown in Fig. 1 toward its bottom point right after a forward transition occurs. After reaching the bottom, it moves around the potential minimum until another forward transition occurs. Suppose that we plot the particle positions x against time t at the occasions a forward transition occurs and the particle reaches the bottom of a potential for the first time. If we connect these points with line segments, we will have a trajectory like the one shown in Fig. 4.

Such a trajectory may be viewed as a trajectory of a random walker on a one-dimensional lattice of lattice spacing *l*. The walker stays on a lattice site until it takes a forward step. The time t_w for the walker to wait at the site (see the upper part of Fig. 4) is a random variable. It also takes a nonzero time t_s for the walker to move to the next lattice site; the stepping time t_s is also a random variable. Let t_c be the period of a cycle from the start of a waiting to the end of the stepping that follows it (Fig. 4), i.e., $t_c = t_w + t_s$. The walker moves forward by the distance *l* every time it completes a cycle. Hence, the average velocity *v* of the walker can be expressed as

$$v = l/\tau_{\rm c} \tag{42}$$

in terms of the average τ_c of t_c .

The diffusion coefficient of the walker may be obtained as follows. Consider a collection of trajectories x(t) of the walker starting from x = 0 at t = 0. The average of these trajectories is a straight line x = vt. Let $\Delta x(t)$ be the standard deviation of x(t) at time t; the shaded area in Fig. 4 represents the region satisfying $|x - vt| < \Delta x(t)$. Then, the diffusion



FIG. 4. Trajectory of a random walker on a one-dimensional lattice of lattice constant l, which mimics the trajectory of the particle in the ratchet model. It stays on a lattice site waiting to step forward for a period of time t_w , and it takes nonzero time t_s to make a forward step.

coefficient can be estimated as

$$D = [\Delta x(t_0)]^2 / 2t_0 = (v \Delta t_0)^2 / 2t_0, \tag{43}$$

for a sufficiently large t_0 , where Δt_0 is the half-width of the shaded region in Fig. 4 measured along the horizontal line $x = vt_0$. Now, Δt_0 can be calculated from the variance σ_c^2 of the cycle time t_c of the walker as follows. The walker completes $N = vt_0/l$ cycles while it travels distance vt_0 . The variance of the time needed to complete N cycles is $N\sigma_c^2$, and this variance is identified as Δt_0^2 . Hence, we have

$$\Delta t_0^2 = N\sigma_c^2 = v t_0 \sigma_c^2 / l. \tag{44}$$

Substitution of this expression and Eq. (42) into Eq. (43) results in

$$D = \sigma_{\rm c}^2 l^2 / 2\tau_{\rm c}^3.$$
 (45)

It should be noted that this expression for D obtained by the qualitative arguments agrees exactly with the one derived by mathematically rigorous calculations [16,17]; see also Refs. [3,4].

The waiting time of the walker corresponds to the time the Brownian particle in the ratchet model spends around the minimum of the potential before the transition, and the transition in the latter can be approximated as a Poisson process if the thermal equilibrium is achieved before the transition. For simplicity, we assume that the waiting of the walker is a Poisson process, and hence the waiting time t_w is distributed exponentially as

$$f(t_{\rm w}) = k \exp(-kt_{\rm w}),\tag{46}$$

with a rate constant k, which is supposed to be related with the forward transition rate of the ratchet model. Then the average τ and the variance σ^2 of t_w are given by $\tau = 1/k$ and $\sigma^2 = 1/k^2 = \tau^2$, respectively. If the stepping time t_s is zero, the walker undergoes a Poisson random walk [18]. A walk with nonzero t_s may be called an *extended Poisson* walk. The average and the variance of the stepping time t_s will be denoted by τ_s and σ_s^2 , respectively. Since the waiting and stepping are statistically independent, the average of $t_c =$ $t_w + t_s$ are given as the sum of the averages of t_w and t_s : $\tau_c = \tau + \tau_s$. Similarly, we have $\sigma_c^2 = \tau^2 + \sigma_s^2$. Hence, the expressions in Eqs. (42) and (45) are rewritten as

$$v = \frac{l}{\tau + \tau_s}, \quad D = \frac{l^2(\tau^2 + \sigma_s^2)}{2(\tau + \tau_s)^3}.$$
 (47)

Now, we examine the dependence of D given in Eq. (47) on the average waiting time τ . If the waiting time is vanishingly small, the diffusion coefficient is determined by the stepping process, which yields

$$D_s = \sigma_s^2 l^2 / 2\tau_s^3. \tag{48}$$

As τ increases from zero, both the denominator and the numerator in the expression for *D* in Eq. (47) increase. It is easy to see that the increase in the denominator exceeds that in the numerator if τ is small enough or large enough, implying that *D* decreases with increasing τ in these regions. However, if σ_s is much smaller than τ_s , then there is a region of τ where inequalities $\sigma_s \ll \tau \ll \tau_s$ hold. In this situation, we have significantly enhanced diffusion coefficient $D \sim D_s(\tau/\sigma_s)^2$ compared with D_s .

Precise calculations show that there is a region of τ where D given in Eq. (47) increases with τ if $\sigma_s/\tau_s < 1/\sqrt{3} \approx 0.577$, which indicates that function $D(\tau)$ has a peak, since D decreases for large τ as explained above. The height of this peak exceeds D_s (indicating diffusion enhancement) if $\sigma_s/\tau_s < (2/\sqrt{3}-1)^{1/2} \approx 0.393$. These results are demonstrated in Fig. 5, where the dimensionless diffusion coefficient D/D_s is plotted against the dimensionless waiting time τ/τ_s for several choices of σ_s/τ_s . As expected from the qualitative argument given in the preceding paragraph, we see that the diffusion coefficient is significantly enhanced for small enough σ_s/τ_s (see the graph of $\sigma_s/\tau_s = 0.2$). In the limit of small σ_s/τ_s , the location τ_{max} and the height D_{max} of the peak in $D(\tau)$ due to the diffusion enhancement can be estimated to be

$$\tau_{\max} \approx 2\tau_s, \quad D_{\max} \approx 2l^2/27\tau_s = (2\tau_s/3\sigma_s)^2 D_s/3, \quad (49)$$

respectively, from Eq. (47) by setting $\sigma_s \approx 0$. To summarize, the diffusion is enhanced when the waiting time is comparable to the stepping time for the extended Poisson walk if the fluctuations of the stepping time are small enough.



FIG. 5. Dependence of the diffusion coefficient *D* given in Eq. (47) on the average waiting time τ for the extended Poisson walk. The result is presented in dimensionless form for $\sigma_s/\tau_s = 1/5$, $(2/\sqrt{3}-1)^{1/2}$, $1/\sqrt{3}$, and 1.

B. Ratchet as a random walker

Now, we discuss the correspondence between the extended Poisson walker and the ratchet model studied in Sec. IV. Let t be the time needed for a particle moving in potential $V_0(x)$ given by Eq. (28) to arrive at x = 0 for the first time provided that it has started at x = -l. The probability density function p(t) of t (the first-passage time) is given [19] by

$$p(t) = \frac{l}{\sqrt{4\pi D_0 t^3}} \exp\left[-\frac{(l - \kappa D_0 t)^2}{4D_0 t}\right].$$
 (50)

The average τ_r and variance σ_r^2 of *t* are calculated from this distribution as

$$\tau_r = l/\kappa D_0, \quad \sigma_r^2 = 2l/\kappa^3 D_0^2.$$
 (51)

Note that the same results can be obtained from the closedform formulas for the moments of the first-passage time; see Ref. [4] and Sec. 7 in Ref. [20]. It seems reasonable to identify the first-passage time with the stepping time t_s of the walker. Therefore, τ_s and σ_s of the walker should correspond to τ_r and σ_r of the ratchet. The rate k associated with the waiting time of the walker should correspond to the rate of the transition in the ratchet. If the thermal equilibrium of x is achieved before the transition, then this rate is estimated as

$$w = \int_{-\infty}^{\infty} w_0^+(x) P_{\text{eq}}(x) \, dx = \kappa \omega_+/2, \qquad (52)$$

where $P_{eq}(x) \equiv (\kappa/2) \exp(-\kappa |x|)$ is the equilibrium distribution for the position of a particle in potential $V_0(x)$. Identifying τ_r , σ_r , and w of the ratchet with τ_s , σ_s , and $k = 1/\tau$ of the walker, respectively, we obtain the same expression for v as Eq. (38) and

$$D = \frac{v^3}{\kappa^3 D_0^2} \left[1 + 2\kappa l \left(\frac{D_0}{l\omega_+} \right)^2 \right]$$
(53)

from the results for v and D in Eq. (47) for the walker. Equation (53) agrees with Eq. (37) except the second term in the brackets in the latter, which is absent in the former.



FIG. 6. Dependence of the diffusion coefficient \tilde{D} on the rate parameter $\tilde{\omega}_+$. The result for the ratchet model in the absence of the backward transition, Eq. (37), is shown by the solid line, and that for the extended Poisson walk, Eq. (53), by the dashed line. The cases of $\tilde{K} = 20$ and 40 are presented. The solid lines here are identical to those in Fig. 2(b).

The diffusion coefficient in Eq. (53) obtained for the extended Poisson walk is plotted, in the dimensionless form, against $\tilde{\omega}_+ = l\omega_+/D_0$ in Fig. 6, together with the result of Eq. (37) for the ratchet model. We see that the position and the height of the peak of function $\tilde{D}(\tilde{\omega}_+)$ for the ratchet model agree reasonably well with those of the extended Poisson walk. The peak for the latter model is located at $\tilde{\omega}_+ = \tilde{\omega}_+^{max} \equiv [\tilde{K} - (\tilde{K}^2 - 6\tilde{K})^{1/2}]/3$ for $\tilde{K} > 6$; the peak position approaches unity as $\tilde{\omega}_+^{max} \approx 1 + 3/2\tilde{K}$ in the limit of large \tilde{K} , whereas the peak height increases linearly in \tilde{K} as $\tilde{D}_{max} \approx 2\tilde{K}/27 + 1/27$ in the same limit. These expressions are to be compared with Eqs. (40) and (41), respectively. The dependencies of $\tilde{\omega}_+^{max}$ and \tilde{D}_{max} , as well as $\tilde{\omega}_+^{min}$ and \tilde{D}_{min} [which are the values of $\tilde{\omega}_+$ and \tilde{D} at the local minimum of $\tilde{D}(\tilde{\omega}_+)$], on \tilde{K} are shown in Figs. 3(a) and 3(b), respectively.

In Fig. 6, we observe small discrepancies between the results for the ratchet model and its approximation as an extended Poisson walker for large values of $\tilde{\omega}_+$. This can be explained as follows. As noted above, the transition in the ratchet model can be approximated as a Poisson process if the thermal equilibrium is achieved before the transition. This condition is satisfied if the transition rate, which is proportional to $\tilde{\omega}_+$, is sufficiently small. Since the relaxation time for the thermal equilibrium in the potential given by Eq. (28) is on the same order as τ_r in Eq. (51), the approximation by the Poisson process is not adequate for the transition rate w in Eq. (52) as large as or larger than $1/\tau_r$ (i.e., $\tilde{\omega}_+ \gtrsim 1$). Hence, the difference between the ratchet model and its approximation as a random walker is appreciable for $\tilde{\omega}_+ \gtrsim 1$.

These results demonstrate that the pronounced enhancement of diffusion observed in the ratchet model for large \tilde{K} is well described by the extended Poisson walk. Hence, we suggest that the mechanism for the diffusion enhancement observed in the ratchet model is essentially the same as that for the extended Poisson walk; the diffusion is enhanced when the time needed for the particle to reach around the potential minimum after a transition is comparable to the time it spends around this minimum before the next transition. Remember that the condition for the diffusion enhancement to occur in the extended Poisson walk is that the fluctuation (the standard deviation) of the stepping time t_s should be somewhat smaller than its average. This condition is satisfied for large \tilde{K} in the ratchet model, since we have $(\sigma_r/\tau_r)^2 = 2/\kappa l = 2/\tilde{K}$, as can be seen from Eq. (51). This explains why the larger \tilde{K} is, the more salient the diffusion enhancement is.

C. A previous model of molecular motors

Let us see if the analogy between a ratchet model and the extended Poisson walk will work for the diffusion enhancement in our previous model of molecular motors [9], which has some relevance to the F_1 -ATPase [12], which is a biological rotary motor. This model will be referred to as the F_1 model. The F_1 model is also a potential-switching ratchet described by the Fokker-Planck Eq. (2) but with different functions for the potential and the transition rates: the potential for and the forward transition rate from state 0 are given by

$$V_0(x) = Kx^2/2, \qquad w_0^+(x) = k \exp(ax),$$
 (54)

respectively, and a constant external force *F* is applied, where *K*, *k*, and *a* are positive constants (*k* is proportional to the ATP concentration). The backward transition rate $w_1^-(x)$ from state 1 is obtained from Eq. (6) with the left-hand side ω_+/ω_- replaced by $w_0^+(x)/w_1^-(x)$. The particle position *x* represents the rotation angle of the rotor in the F₁-ATPase.

It turns out [9] that the dimensionless diffusion coefficient $\tilde{D} = D/D_0$ for the F₁ model depends on model parameters only though the four dimensionless quantities

$$\tilde{K} \equiv K l^2 / k_{\rm B} T, \quad \tilde{a} \equiv a l, \tag{55}$$

$$\tilde{k} \equiv \frac{kl^2}{D_0} \exp\left(-\frac{a\Delta\mu}{Kl}\right), \quad \tilde{F} \equiv \frac{Fl + \Delta\mu}{k_{\rm B}T}.$$
 (56)

Note that the meanings of K and \tilde{K} here are different from those used for the ratchet model. The solid lines in Fig. 7(a) show the dependence of \tilde{D} on \tilde{F} for several values of \tilde{k} with $\tilde{K} = 40$ and $\tilde{a} = 5$; the function $\tilde{D}(\tilde{F})$ has a peak at a certain value of \tilde{F} . We observe that, as \tilde{k} decreases (the ATP concentration decreases), the peak position \tilde{F}_{max} moves to the right, and the peak height increases and converges to a value of about 1.9. The dependence of \tilde{F}_{max} on \tilde{k} is presented by the solid line in Fig. 7(b), which indicates that \tilde{F}_{max} varies logarithmically with \tilde{k} for small \tilde{k} .

We have found that the backward transition has little contribution to the diffusion enhancement shown in Fig. 7 for $\tilde{k} < 0.1$; results for \tilde{D} obtained by setting $w_n^-(x) = 0$ (data not shown) are almost the same as those shown in this figure in the range $\tilde{F} > 20$ for $\tilde{k} < 0.1$. For small \tilde{k} , the transition rarely occurs, and we expect that the particle in state *n* stays for a while around the minimum of $V_n(x) - Fx$, and the thermal equilibrium is established before the transition to state n + 1 takes place. Therefore, the diffusion enhancement of the F₁ model for small \tilde{k} may be understood on the basis of an



FIG. 7. Diffusion enhancement for the F_1 model for $\tilde{K} = 40$ and $\tilde{a} = 5$. (a) The dependence of the diffusion coefficient \tilde{D} on the external force \tilde{F} for $\tilde{k} = 1$, 0.1, and 0.01. The dashed line indicates \tilde{D} for the Poisson walker given in Eq. (59) for $\tilde{k} = 0.01$. (b) The dependence of the peak position \tilde{F}_{max} of the function $\tilde{D}(\tilde{F})$ on \tilde{k} . The solid and dashed lines are for the F_1 model and the Poisson walker, respectively; the latter is given by Eq. (60). The results for $\tilde{k} = 1$ and 0.1 in (a) and the solid line in (b) are the same as those in Figs. 2 and 3(a) of Ref. [9], respectively.

extended Poisson walk, for which the average waiting time τ and stepping time τ_s are estimated as explained below.

The probability density function for x in state 0 in thermal equilibrium is given by $P_{eq}(x) \propto \exp[-K(x - F/K)^2/2k_BT]$. Then, the average transition rate w is calculated from the integral in Eq. (52) by substituting the second equation in Eq. (54) and the above expression for $P_{eq}(x)$. The average waiting time is obtained as the inverse of w, and we have

$$\tau = (1/k) \exp(-Fa/K - a^2 k_{\rm B} T/2K) = (l^2/D_0 \tilde{k}) \exp(-\tilde{F} \tilde{a}/\tilde{K} - \tilde{a}^2/2\tilde{K}).$$
(57)

After a transition, the particle moves downward on the potential $V_1(x) - F/K$ from the vicinity of x = F/K to the region around x = F/K + l, and the equilibrium distribution for x in this potential is realized in time of about $\gamma/K = k_B T/D_0 K$ [21], which can be identified as the stepping time τ_s of the extended Poisson walk:

$$\tau_s = k_{\rm B} T / D_0 K = l^2 / D_0 \tilde{K}.$$
 (58)

We have no idea of how to estimate the variance σ_s of the stepping time, and tentatively assume that it is small compared with t_s . Then the diffusion coefficient *D* of the walker is given by Eq. (47) with $\sigma_s = 0$, i.e.,

$$D = (l\tau)^2 / 2(\tau + \tau_s)^3,$$
(59)

and *D* as a function of τ has a peak at $\tau = \tau_{max}$, where τ_{max} and the peak height D_{max} are given in Eq. (49). According to Eq. (57), the value of τ can be varied by changing \tilde{F} with other parameters unaltered; The dimensionless diffusion coefficient $\tilde{D} = D/D_0$ calculated from Eq. (59) as a function of \tilde{F} for $\tilde{K} = 40$, $\tilde{a} = 5$, and $\tilde{k} = 0.01$ is shown by the dashed line in Fig. 7(a). Comparing this result for the walker with that for the F₁ model, we find that the peak position for the walker agrees relatively well with that for the F₁ model, whereas the



FIG. 8. Dependencies of (a) the position \tilde{F}_{max} and (b) height \tilde{D}_{max} of the function $\tilde{D}(\tilde{F})$ on \tilde{K} for $\tilde{a} = 5$ and $\tilde{k} = 0.01$. The solid and dashed lines are for the F₁ model and walker, respectively.

peak height for the former is somewhat larger than that for the latter.

The position \tilde{F}_{max} and height \tilde{D}_{max} of the peak in $\tilde{D}(\tilde{F})$ for the walker are obtained from Eq. (49) as

$$\tilde{F}_{\max} = \frac{\tilde{K}}{\tilde{a}} \ln \frac{\tilde{K}}{2\tilde{k}} - \frac{\tilde{a}}{2}, \quad \tilde{D}_{\max} = \frac{2\tilde{K}}{27}.$$
 (60)

The dependence of \tilde{F}_{max} on \tilde{k} for $\tilde{K} = 40$ and $\tilde{a} = 5$ is shown in Fig. 7(b) by the dashed line, which qualitatively agrees with that for the F₁ model shown by the solid line. In particular, the slope $-\tilde{K}/\tilde{a}$ of the line of the former perfectly agrees with that of the latter for small \tilde{k} . Another result of Eq. (60) that \tilde{D}_{max} for the walker depends only on \tilde{K} is consistent with the fact that \tilde{D}_{max} of the F₁ model is independent of \tilde{k} for small \tilde{k} mentioned above; see the solid lines for $\tilde{k} = 0.1$ and 0.01 in Fig. 7(a).

Finally, let us see if the dependencies of \tilde{F}_{max} and \tilde{D}_{max} on \tilde{K} in Eq. (60) for the walker agree with those for the F₁ model. Figure 8 presents such a comparison for $\tilde{a} = 5$ and $\tilde{k} = 0.01$. We see that the results for the walker qualitatively reproduce the results for the F₁ model. Note that the linear dependence of \tilde{D}_{max} on \tilde{K} for large \tilde{K} observed for the F₁ model is correctly described by the walker, although the proportionality constant of the walker is a few time larger than that of the F₁ model.

From all the results presented above, we think that the mechanism of the diffusion enhancement in the F_1 model for large K and small k (low ATP concentration) reported in our previous work [9] is essentially the same as that in the extended Poisson walk. One possible reason why the agreement between the results for the walker and for the F₁ model is not so good compared with that between those for the walker and for the ratchet model considered in the present work is likely that a forward transition can take place at any value of x for the F_1 model [Eq. (54)] while that for the ratchet model is allowed only at a particular value of x [Eq. (5)]. The chance that the transition occurs before the particle reaches the bottom of the potential in the former model increases with \tilde{F} since the waiting time estimated by Eq. (57) becomes short; hence, both Eqs. (57) and (58) become less reliable. Therefore, the picture of extended Poisson walk fails quantitative description of the dynamics of the F₁ model for large \tilde{F} , although it qualitatively explains the occurrence of the diffusion enhancement for this model.

VI. CONCLUDING REMARKS

We have proposed a solvable model of ratchet type for the Brownian motor to elucidate the mechanism underlying the diffusion enhancement reported for a model of molecular motors in our previous work [9]. We have suggested that the diffusion enhancement of the present model observed in a certain range of the transition rate (Sec. IV) and of the previous model [9] for a certain range of external force at low ATP concentrations is essentially the same as the one for a simpler system which we call the extended Poisson walk (Sec. V). In this random walk on a one-dimensional lattice, each step of the walk consists of two processes. One is the Poisson process for the walker to wait on a lattice site, and the other is the stepping to the next site that takes a nonzero time. The enhancement of diffusion occurs when the average waiting time is comparable to the stepping time. In the ratchet-type models, the waiting time corresponds to the time the Brownian particle spends in (quasi) thermal equilibrium around the minimum of the potential, and the stepping time corresponds to the duration between a transition and when it reaches this thermal equilibrium, approximated by the firstpassage time.

The analogy between the extended Poisson walk and the ratchet model studied in Sec. IV works only in the limit of small ω_{-} (the rate of backward transition). Therefore, this analogy cannot explain the result presented in Fig. 2(b) that the peak position of the diffusion coefficient as a function of the forward transition rate moves to the right as ω_{-} increases. Whether this behavior can be understood on the basis of a simple physical picture will be investigated in a future work.

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APPENDIX A: DERIVATION OF EQS. (17) AND (18)

To calculate the velocity from Eq. (9), we need to obtain the steady-state solutions $P_n(x)$ to the Fokker-Planck Eqs. (2). Let J(x) be the function defined by

$$J(x) \equiv \left[f(x) - D_0 \frac{d}{dx} \right] P(x), \tag{A1}$$

where P(x) is the rescaled $P_0(x)$ introduced in Sec. II. Making use of the relation $P_n(x) = P_0(x - nl)$ and Eq. (5), we obtain

$$\frac{dJ}{dx} = \mathcal{J}[\delta(x - a_-) - \delta(x - a_+)], \qquad (A2)$$

with

$$\mathcal{J} \equiv \omega_+ P(a_+) - \omega_- P(a_-) \tag{A3}$$

from Eq. (2). Equation (A2) implies that J(x) is piecewise constant, and the boundary condition $P(x) \rightarrow 0$ as $x \rightarrow \pm \infty$ and Eq. (A1) suggest that $J(x) \rightarrow 0$ as $x \rightarrow \pm \infty$. Therefore,

Eq. (A2) is integrated to yield

$$J(x) = \mathcal{J}\theta(x - a_{-})\theta(a_{+} - x), \tag{A4}$$

where $\theta(x)$ is the step function: $\theta(x) = 0$ for x < 0 and $\theta(x) = 1$ for $x \ge 0$. By making use of Eqs. (A1) and (A4), we can rewrite Eq. (9) as

$$v = \int_{-\infty}^{\infty} J(x) \, dx = \mathcal{J}l. \tag{A5}$$

Substituting Eq. (A4) into Eq. (A1) and integrating the resulting equation with the boundary condition $P \rightarrow 0$ as $|x| \rightarrow \infty$, we obtain

$$P(x) = \begin{cases} C_{-} \exp[-U(x)] & (x < a_{-}), \\ \varphi(x) \exp[-U(x)] & (a_{-} \leq x \leq a_{+}), \\ C_{+} \exp[-U(x)] & (x > a_{+}), \end{cases}$$
(A6)

where U(x) is defined in Eq. (16), function $\varphi(x)$ is defined by

$$\varphi(x) = C_{-} - \frac{\mathcal{J}}{D_0} \int_{a_{-}}^{x} e^{U(y)} \, dy, \tag{A7}$$

and constants C_{\mp} are defined by

$$C_{\mp} = \frac{1 + \phi_0 u_{\pm} / D_0}{u_{\pm} - u_{-}} \mathcal{J}, \tag{A8}$$

with ϕ_0 and u_{\pm} defined in Eqs. (13) and (15). We have also used Eq. (A3) to get Eq. (A8). From Eqs. (A5)–(A8) we obtain Eqs. (21)–(23).

Equation (A6) for P(x) together with Eqs. (A7) and (A8) contain the unknown constant \mathcal{J} . This constant can be determined from the normalization condition Eq. (8), which yields

$$\mathcal{J} = \frac{(u_+ - u_-)D_0}{\zeta(D_0 + \phi_0 u_-) + \phi_1(u_+ - u_-)},$$
 (A9)

where ϕ_1 is defined in Eq. (14). From Eqs. (A9) and (A5) we obtain Eq. (17).

To calculate the diffusion coefficient from Eq. (11), we need to solve Eq. (10) to obtain Q(x). Let L(x) be the function defined by

$$L(x) \equiv \left[f(x) - D_0 \frac{d}{dx} \right] Q(x).$$
 (A10)

Then, Eq. (10) is rewritten as

$$\frac{dL}{dx} = \lambda [\delta(x - a_{-}) - \delta(x - a_{+})] + \left[f(x) - v - 2D_0 \frac{d}{dx} \right] P(x), \quad (A11)$$

with

$$\lambda \equiv \omega_+ Q(a_+) - \omega_- Q(a_-). \tag{A12}$$

Taking account of the boundary condition $L(x) \rightarrow 0$ as $|x| \rightarrow \infty$, which comes from the similar condition for Q(x) and Eq. (A10), we integrate Eq. (A11) to get

$$L(x) = R(x) + \lambda \theta(x - a_{-})\theta(a_{+} - x), \qquad (A13)$$

where R(x) is defined by

$$R(x) \equiv \int_{-\infty}^{x} [f(y) - v] P(y) \, dy - 2D_0 P(x).$$
 (A14)

It is convenient to rewrite this expression as follows. From the definition of f(x) in Eq. (9) and the expression for P(x) in Eq. (21), we have

$$\int_{-\infty}^{x} f(y)P(y) \, dy = D_0 P(x) - D_0 \int_{-\infty}^{x} \frac{dg(y)}{dy} e^{-U(y)} \, dy$$
(A15)

by making use of integration by parts. Now, Eq. (22) for g(x) is used to rewrite the last term in Eq. (A15) as

$$D_0 \int_{-\infty}^x \frac{dg(y)}{dy} e^{-U(y)} \, dy = -vh(x), \qquad (A16)$$

where h(x) is defined in Eq. (20). Substitution of Eq. (A15) with Eq. (A16) into Eq. (A14) leads to Eq. (27), i.e.,

$$R(x) = vW(x) - D_0P(x),$$
 (A17)

with W(x) defined in Eq. (19).

Having the function L(x) thus obtained, we substitute Eq. (A13) with Eq. (A17) into Eq. (A10) and integrate the resulting equation to get

$$Q(x) = e^{-U(x)} \left[C - \frac{1}{D_0} \int_{a_-}^x L(y) e^{U(y)} \, dy \right], \qquad (A18)$$

where constant *C* is given by

$$C = \frac{(D_0 + \phi_0 u_+)\lambda + \psi_0 u_+}{(u_+ - u_-)D_0},$$
 (A19)

with ϕ_0 , u_{\pm} , and ψ_0 defined by Eqs. (13), (15), and (25), respectively. We have also used Eq. (A12) to get Eq. (A19).

Equation (A18) contains the unknown constant λ through *C* given in Eq. (A19). This constant cannot be determined uniquely, because Q(x) defined as the solution of Eq. (10) has ambiguity: if Q(x) is a solution of this equation, then Q(x) + cP(x), with *c* an arbitrary constant, is also a solution. However, this ambiguity does not affect the right-hand side of Eq. (11), since we have

$$\int_{-\infty}^{\infty} [f(x) - v] P(x) dx = 0$$

because of the first equation in Eq. (9). Therefore, we can assign any value to λ . We find it convenient to determine λ

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from the condition

$$\int_{-\infty}^{\infty} Q(x) \, dx = 0, \tag{A20}$$

from which we obtain Eq. (24).

Now, we have everything we need to calculate the diffusion coefficient by using Eq. (11), which reads

$$D = D_0 + \int_{-\infty}^{\infty} f(x)Q(x) dx$$
 (A21)

due to Eq. (A20). We will rewrite the second term of Eq. (A21), because the expression for Q(x) given in Eq. (A18) is quite complicated and hence Eq. (A21) is not convenient for practical use. First, we use Eqs. (A10) and (A13) to proceed as

$$\int_{-\infty}^{\infty} f(x)Q(x)\,dx = \int_{-\infty}^{\infty} L(x)\,dx = \lambda l + \int_{-\infty}^{\infty} R(x)\,dx.$$

Next, we use Eq. (A17) to obtain Eq. (18).

APPENDIX B: EXPRESSIONS FOR P(x) AND W(x)

Here, we present the explicit expressions for P(x) and W(x) obtained for the model considered in Sec. IV. The steady-state probability density P(x) in state 0 is found to be

$$P(x) = g(x)e^{-\kappa|x|},$$
(B1)

where $g(x) = C_{-}$ for x < -l,

$$g(x) = C_{-} - \frac{v}{\kappa l D_0} (e^{\kappa l} - e^{-\kappa x})$$
(B2)

for $-l \leq x \leq 0$, and $g(x) = C_+$ for x > 0 with C_{\pm} obtained by substituting Eqs. (29) and (30) into Eq. (23).

The function W(x) defined by Eq. (19) is given by

$$W(x) = \begin{cases} -(C_{-}/\kappa)e^{\kappa x} & (x < -l) \\ (C_{+}/\kappa)e^{-\kappa x} & (x > 0) \end{cases}$$
(B3)

and

$$W(x) = C_{+}\zeta \left(1 + \frac{x}{l}\right) - \frac{C_{-}}{\kappa} e^{\kappa x} + \frac{v}{\kappa^{2} l D_{0}} (e^{\kappa (x+l)} - 1)$$
(B4)

for $-l \leq x \leq 0$.

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