Long ligands reinforce biological adhesion under shear flow

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In this work, computer modeling has been used to show that longer ligands allow biological cells (e.g., blood platelets) to withstand stronger flows after their adhesion to solid walls. A mechanistic model of polymer-mediated ligand-receptor adhesion between a microparticle (cell) and a flat wall has been developed. The theoretical threshold between adherent and non-adherent regimes has been derived analytically and confirmed by simulations. These results lead to a deeper understanding of numerous biophysical processes, e.g., arterial thrombosis, and to the design of new biomimetic colloid-polymer systems.

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I. INTRODUCTION

Adhesion is ubiquitous in different fields of physics, material science, physical chemistry, and biology. Adhesion mechanisms may be complex and involve various physical interactions, for example, electrostatics, lubrication forces, capillarity, roughness, friction, etc. [1-3] Unlike non-living matter, biological cells often rely on "key-lock" ligand-receptor binding involving special membrane-anchored proteins-cell adhesion molecules (CAMs)-and the adhesive substrate, e.g., extracellular matrix, collagen, or other another cell [4–7]. The importance of adhesion in biological systems is supported by numerous examples, such as the formation and growth of bacterial clusters and biofilms [8] on medical implants [9], adhesion of blood cells to endothelial lining of blood vessels during hemostatic [10–12] and immune response [13,14], tissue formation, etc. The adhesion should be reliable and adjustable, especially when the cells are supposed to function in strong hydrodynamic flows. One of the most intriguing examples is the adhesion of blood platelets to a damaged blood vessel during the hemostatic process [15-25]. It is provided by the reversible binding between the GPIb-IX-V receptor complex on the platelet membrane and protein ligand-the von Willebrand factor (vWf). Normally, the vWf exists in the form of long chains-"multimers"-that provide platelet aggregation in the case of severe bleeding [26-30]. In some cases, these aggregates can obstruct blood vessels, limiting blood circulation and causing thrombosis. Understanding the mechanics and regulation of this phenomenon may help in development of anti-thrombotic therapy and laboratory tests [31], hemocompatible materials for implants [32], and the design of biomimetic colloidal-polymer systems [33].

Earlier models [14,34–39] and experiments [40–42] underlined the role of reaction rates and loading forces on the dynamics of blood cells subjected to microvascular and arterial flow conditions. A number of leukocyte rolling models assumed that the ligand length was small in comparison to the cell diameter [43,44]. Apparently, this is not the case for vWf-mediated adhesion and aggregation of platelets. One of the essential features of the vWf is that these proteins can expand laterally up to several micrometers due to blood flow [27,45–47] and capture widely scattered platelets from the flowing blood. This protein is also responsible for preventing the bleeding by binding blood platelets to the extracellular matrix or damaged blood vessel walls [12,41,48]. It is known that vWf deficiency of concentration in blood causes bleeding disorders, as well as short length of such macromolecular ligands [49]. At the same time, ultra-long vWf chains may cause thrombotic conditions [50]. The role of ligand length in cell adhesion to walls has to be studied and quantified.

The questions are why long tethers are required for efficient blood cell adhesion within the blood flow and how long should these tethers be to accomplish their physiological role. In this work, we try to answer these questions by means of computer simulations.

II. METHODS

A. Theory

The adhesion of a microscopic colloid (cell) to a flat wall via binding to a polymer ligand in Couette flow has been studied. A basic mechanistic model has been used for the theoretical description. Consider a spherical particle retained against hydrodynamic forces by the polymer near a solid impenetrable wall (Fig. 1). Let us denote the cell radius as R and the tether length as L. In the case of a long ligand $(R/L \ll 1)$, the cell could be represented as a material point. The force balance requires that $F = T \cos \alpha$, where T is the tension force of the tether and $F = A R^2 \dot{\gamma}$ is the hydrodynamic drag force with $\dot{\gamma}$ being the near-wall shear rate. The coefficient A depends on the dynamic viscosity μ of the fluid, the shape of the particle, and the proximity of the walls. According to the Goldman-Cox-Brenner theory [51], $A \approx 1.7 \times 6\pi \mu$. The tethering polymer can detach from the sphere if T exceeds some threshold value T_{max} . The tethering angle α may be determined on the condition that the non-deformed sphere touches the wall, so that $\sin \alpha \approx R/L$. This results in the following expression for the critical shear rate:

$$\dot{\gamma}_{\rm cr} = \frac{T_{\rm max}}{AR^2} [1 - (R/L)^2],$$
 (1)

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FIG. 1. Illustration of polymer-mediated adhesion mechanics. (a) In the shear flow a spherical particle is rolling and translating along the wall within distance h. The tether can stick to the sphere (b), and if the tether is long enough, it develops a sufficient tension force $T \cos \alpha$ to hold the sphere against the drag force F. Yet if α is too big, then the maximum tension T_{max} is reached and the tether detaches (a).

which means the adhesion is firm if $\dot{\gamma} \leq \dot{\gamma}_{cr}$ and impossible otherwise. In the opposite case $(R/L \gg 1)$, the size of the particle becomes substantial, and the corrected formula reads [52]

$$\dot{\gamma}_{\rm cr} = \frac{T_{\rm max}}{AR^2} \left[1 - \left(\frac{R}{L+R}\right)^2 \right].$$
 (2)

From these expressions we see the advantages of longer ligands: they increase the projection $T_x = T \cos \alpha$ of the tension force **T** that counterbalances the hydrodynamic drag force **F** (Fig. 1). This hypothesis has been verified by computer simulations in this work.

B. Computer simulation

A three-dimensional computer model has been developed on the basis of the open-source package ESPResSo (version 3.4). A hybrid lattice Boltzmann (LB) particle dynamics (PD) model has been employed [53–55]. For the sake of convenience, dimensionless values were used so that $[L] = 1 \ \mu m$, [F] = 1nN, and $[t] = 1 \ \mu s$. A lattice Boltzmann Bhatnagar-Gross-Krook approximation has been used to simulate low Reynolds number hydrodynamics of a viscous fluid in the simulation box [56]. Each adhering object (sphere or platelet) immersed into the fluid was represented by a mesh of Lagrangian surface points connected by elastic bonds [54]. A molecular dynamics (MD) approach has been used to track cell motion over time. The coupling between fluid flow and cell membrane was introduced by a viscous drag force $\mathbf{F}_i = -\xi \Delta \mathbf{u}_i$ exerted on the cell membrane nodes. The hydrodynamic part of the model has been successfully used in prior works [54,57]. Before each simulation the ligand polymer (tether) was attached to the bottom wall of the simulation box by one end and stretched along the x axis. After that, a short equilibration run $(500 \ \mu s)$ was performed before each simulation. The polymer was modeled as a chain of N beads of radius $a = 0.05 \ \mu m$



FIG. 2. (a) Three types of particles used in this work. (b) The drag on a sphere held against the flow with constant velocity U. Numerical results (squares for the smaller sphere, circles for the bigger one) agree with Stokes's law (lines).

connected with elastic elements, for which a non-linear Finitely Extensible Nonlinear Elastic potential was used [58].

Spheres of two sizes were used: R = 0.64 and 1.28 μ m. The platelet volume was equal to the volume of the smaller sphere and had a realistic 2:1 aspect ratio [Fig. 2(a)]. In order to ensure that the model yields correct values of drag forces and torques, validation tests have been performed. A non-deformable sphere was placed into the simulation box in different flow setups. The total drag force F and torque M on the sphere were measured during simulations. The first test was based on a well-known Stokes drag formula: $F_{\text{Stokes}} = 6\pi \mu RU$. The sphere was placed into the center of the simulation box and immobilized; a constant velocity condition (U,0,0) was imposed on the boundaries of the box. The results of this test show a reasonable agreement with Stokes law [Fig. 2(b)]. Additionally, a set of validation runs has been performed for the sphere near a flat wall in shear flow (Fig. 3) and then compared to known theoretical expressions [51, 59]. According to these results, the hydrodynamic accuracy of the model is quite high.



FIG. 3. Drag force (left) and torque (right) on the immobile sphere $(R = 0.64 \,\mu\text{m})$ near a wall in shear flow. Symbols correspond to simulation results for different distances *h* between the sphere and the wall; lines correspond to the analytical formulas from [51,59].



FIG. 4. Adhesion regimes diagram: red crosses correspond to cases where the tether was unable to hold the sphere, green circles to where the sphere remained attached until the end of the simulation, orange triangles to rolling with stops, and light green diamonds to adhesion when the tethering occurred on the second (or third, etc.) approach. The dashed line corresponds to Eq. (1) and the dash-dotted line to Eq. (2). The solid red line is a visual guide for the boundary between adhesive and non-adhesive regimes.

III. RESULTS

The first set of results corresponds to the spheres. In the beginning of each simulation the sphere was placed within distance $h_0 = 2a$ from a wall. A big set of simulations allowed a map of adhesion regimes to be plotted (Fig. 4). Here, as the theory suggests, the increase of cell size R relative to the contour length of the tether polymer $(L = Nr_0)$ causes the adhesive bond to break at lower shear rates. The simulations support this idea, as seen in Fig. 4 (see also Supplemental Material, Movies 1 and 2 [58]). When the ratio is small $(R/L \ll 1)$, the threshold of stable adhesion is the highest, as predicted by Eq. (1), and it only slightly depends on R/L. For a sphere with $R = 0.64 \ \mu m$, the threshold shear rate between the firmly adherent state and the free-flowing regime is approximately 1200 s⁻¹. If $R/L \gg 1$, the maximum force that a bond can sustain falls rapidly to zero [in simulations it decreases even faster than predicted by Eq. (2)]. For ultra-long chains ($N \ge 100$, R/L < 0.06), an intermediate regime was observed: slow rolling with halts and re-initiation of motion. Apparently, when the force balance is reached, the cell stops. But due to rotation of the sphere around the x axis, the equilibrium crashes, and the cell starts to roll again (see Supplemental Material, Movie 3 [58]).

The mean velocity of the cell was measured during the time span of 100 ms after the start of each simulation. Simulation snapshots, Fig. 5(a), show the initial stages of adhesion. In the beginning, the tension force T_x component (parallel to the wall) is minimal. As the cell moves along the flow, the tethering angle α sharpens. Ideally, $\alpha \rightarrow 0$ for $R/L \rightarrow 0$. Yet, if T_{max} is not sufficient to hold the cell attached to the wall for a given $L = Nr_0$, the tether breaks and the cell starts flowing with the fluid. It was found that longer ligands indeed help to withstand



FIG. 5. (a) Series of simulation shots for $R = 0.64 \ \mu \text{m}$, N = 20, and $\dot{\gamma} = 10^3 s^{-1}$. (b) Mean velocity of the sphere (R = 0.64) plotted against shear rate for different N. Dashed line corresponds to the theoretical velocity $V = \dot{\gamma}(R + h)$ of a free-flowing sphere at distance $h = 0.15 \ \mu \text{m}$ from the wall. (c) Distance traveled by the sphere ($R = 0.64 \ \mu \text{m}$) before stopping in cases of durable adhesion for different N.

more intensive flows [Fig. 5(b)]. Negligible mean velocity corresponds to lasting adhesion. The transition between adhesion regimes shifts to greater shear rates for longer polymers, in accordance with the theory. Longer linkers (>10 monomers) also decelerate the cell even in the no-adhesion regime, as there is a period of slow rolling over the polymer chain with consequent detachment. The longer the chain, the longer this period. In cases of stable adhesion the distance traveled by the cell before it stops increases non-linearly with the shear rate [Fig. 5(c)].

The value of the bond-rupturing shear rate $\dot{\gamma}_{cr}$ depends strongly on the cell size: if we double the sphere radius, then the drag increases fourfold (as $F_{drag} \propto \dot{\gamma} R^2$). Therefore, for the same detachment force T_{max} and the same R/L (i.e., double the length of ligand and the radius) the critical shear rate for the big cell should be four times smaller than for the small one. This was observed in simulations (Fig. 6): for the



FIG. 6. Mean velocity of a sphere plotted against the shear rate for different N and R. Lines correspond to theoretical velocity of a free-flowing sphere.



FIG. 7. (a) Simulation of the platelet motion before adhering to a wall via binding with grafted von Willebrand factor chain. (b) Diagram comparing the maximum shear rate sustained by the platelet (yellow) and the equivolume sphere (blue). For the platelet, the error bars correspond to deviation due to its initial placement (different orientation of symmetry axes), and for the sphere, to a systematic uncertainty (50 s⁻¹) caused by the step change of shear rate between two consequent simulations.

small sphere and the five-monomer-long ligand $\dot{\gamma}_{\rm cr} \approx 850 \,{\rm s}^{-1}$, while for the big sphere and the ten-monomer-long ligand $\dot{\gamma}_{\rm cr} \approx 215 \,{\rm s}^{-1}$. It should be noted that if the ligand length is kept the same, then $\dot{\gamma}_{\rm cr}$ decreases even more: for $R = 1.28 \,\mu{\rm m}$ and N = 5 the maximum shear rate is 160 s⁻¹. This means that longer polymers are required to hold bigger cells against the stream (see Supplemental Material, Movie 4 [58]). The blood platelets have a typical size of $1-2 \mu m$ and the adhesive ligand (von Willebrand factor) could be 20–50 monomers long (on average), which, as simulations suggest, is sufficient to withstand drag at a wall shear rate of 1000–1200 s⁻¹.

Blood platelets are not spherical: normally they are oblate spheroids. In order to investigate the effect of the cell shape, simulations with a platelet-shaped particle have also been performed in a range of shear rates. Different ligand lengths and different initial placements of the platelet were used. It has been discovered that platelets demonstrate a more complicated motion than spheres [35,60]. Due to the shape and the non-penetration condition, the center of mass of the platelet jumps and falls as the cell rolls over the adhesive wall [Fig. 7(a)], unlike the sphere. The results of the simulations, presented in Fig. 7(b), suggest that platelets can sustain greater wall shear rates than spheres. This is due to their streamlined shape, lower profile, and, consequently, weaker drag force (see Supplemental Material, Movie 5 [58]).

IV. CONCLUSION

In conclusion, this study shows that longer tethers are preferable for binding of blood platelets to injury, thrombus, or extracellular matrix due to the more favorable direction of the tether tension force. The oblate shape and small size allow platelets to minimize the drag and promote aggregation. Hopefully, these findings will deepen the physical insight into physiological phenomena that rely on cell adhesion, e.g., thrombosis and hemostasis.

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