Electrical autonomous Brownian gyrator

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We study experimentally and theoretically the steady-state dynamics of a simple stochastic electronic system featuring two resistor-capacitor circuits coupled by a third capacitor. The resistors are subject to thermal noises at real temperatures. The voltage fluctuation across each resistor can be compared to a one-dimensional Brownian motion. However, the collective dynamical behavior, when the resistors are subject to distinct thermal baths, is identical to that of a Brownian gyrator, as first proposed by Filliger and Reimann [Phys. Rev. Lett. **99**, 230602 (2007)]. The average gyrating dynamics is originated from the absence of detailed balance due to unequal thermal baths. We look into the details of this stochastic gyrating dynamics, its dependences on the temperature difference and coupling strength, and the mechanism of heat transfer through this simple electronic circuit. Our work affirms the general principle and the possibility of a Brownian ratchet working near room temperature scale.

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I. INTRODUCTION

Richard Feynman explored whether one can extract work simply from the stochastic motions agitated by a surrounding heat reservoir in his famous discussion of the Brownian ratchet [1]. He pointed out that in order to extract work autonomously, it is necessary to have the system in contact with an additional cooling reservoir. Therefore the second law of thermodynamics is demonstrated even under the consideration of microscopic stochastic dynamics.

Inspired by Feynman's discussion, and thanks to the recent advances in the manipulations on small-scale systems [2], enormous interest is emerging in the development of miniature thermal engines [3-10]. In these systems with few degrees of freedom, one expects to extract work from the microscopic Brownian movements, and in contrast to bulk systems, their dynamics exhibits a prominent stochastic nature. Among these studies, autonomous gyrators are more reminiscent of Feynman's original work. For example, Filliger and Reimann [11] introduced a Brownian gyrator, in which a structureless particle is simultaneously exposed to two heat reservoirs, each imposing on one of its motional degrees of freedom. An average gyrating motion can be observed in the nonequilibrium steady state (NESS) [12,13] if the two reservoirs are of distinct temperatures, and hence this two-dimensional (2D) Brownian gyrator can serve as a "minimal" version of autonomous heat engines. In Ref. [11], the authors listed two more criterions for the generation of a Brownian gyrator: (1) the landscape for the confining potential is not rotationally symmetric, and (2) the directions along which the two random forces are imposed do not coincide with the principal axes of the potential landscape.

Despite the simple requirements in the Brownian gyrator or similar autonomous heat engines, it is technically challenging to expose a minuscule to two heat baths simultaneously, each upon an independent direction [14]. Experimentally, mechanical and electrical realizations of these autonomous engines are crafted with artificial thermal noises and are often featured by nonlinear interactions [15–18]. Meanwhile,

mesoscopic conductors with asymmetric and nonlinear couplings to multiple charge heat baths were proposed to generate unidirectional charge current [19–21]. Net electrical currents have been observed experimentally in those mesoscopic ratchets [22,23], demonstrating their capability of rectifying heat to work.

In the current work, we report our studies on the stochastic dynamics of a capacitively coupled resistor-capacitor (RC) circuit [13,24] as illustrated in Fig. 1(a), where the resistors are agitated by real thermal noises of two real heat baths. We demonstrate that this simple linear system can be compared exactly to the Brownian gyrator as depicted in Ref. [11]. In contrast to the existing studies on this circuit system concerning its entropy fluctuation and the applicability of fluctuation theorems [24,25], we turn our attention to its analogous gyrating behavior, which is concealed in its fluctuating dynamics over the configuration space. While the voltage for each of the electrical element fluctuates due to thermal noises, an average heat is conducted from the hot to the cold reservoir via the circuit. Along with the average unidirectional gyrating motion, they both are representations of the second law of thermodynamics.

The rest of the paper is organized as follows. The experimental setup and its corresponding stochastic dynamical equation are given in Sec. II. The main results concerning the gyrating dynamics over the configuration space, featuring its steady-state probability and flux distributions, are reported in Sec. III A. In Sec. III B we provide more theoretical details for gyrating dynamics of the NESS, and we also demonstrate the dependence between the gyrating direction and the temperature gradient. In Sec. IV the dependence of energy flow and closed-cycle gyration is discussed with the aid of semiadiabatic processes. The dependencies of the rotating speed on the coupling strength and the temperature gradient are studied in Sec. V.

II. EXPERIMENTAL SYSTEM

Figure 1(a) shows the schematic of our study system. Two RC circuits (R_1, C_1) and (R_2, C_2) are connected through a coupling capacitor C_c [24]. The two resistors R_1 and R_2 are individually thermalized by the heat baths of temperature T_1

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FIG. 1. Electrical autonomous Brownian gyrator. (a) Schematics of the experimental system, featuring a capacitively coupled RC circuit agitated by two heat baths. (b) A snapshot of concurrent $V_1(t)$ and $V_2(t)$ over 30 ms with $C_c = 1.0$ nF and $T_1 = 120$ K. (c) A virtual particle evolving in the 2D phase space formed by V_1 and V_2 . A small segment of its trajectory [corresponding to the data in (b)] is shown by the orange line. The dashed lines indicate the q_1 and q_2 axes; see text. The virtual particle is influenced by two heat baths and experiences two random noises ξ_1 and ξ_2 from directions parallel to q_1 and q_2 axes, respectively, as noises are depicted by two sets of wavy arrows. The tilt ellipses designate potential contours with a minimum in the origin.

and T_2 , respectively. In our system of interest, the effects of electromagnetic induction are negligible, and the dynamics of the voltages across the resistors, $V_1(t)$ and $V_2(t)$, is governed by the coupled Langevin equation [24]

$$\hat{\mathbf{R}}\hat{\mathbf{C}}\vec{V} = -\vec{V} + \vec{\xi} \,, \tag{1}$$

where $\vec{V} \equiv \begin{pmatrix} V_1 \\ V_2 \end{pmatrix}$, $\vec{\xi} \equiv \begin{pmatrix} \xi_1 \\ \xi_2 \end{pmatrix}$, $\hat{\mathbf{R}} \equiv \begin{pmatrix} R_1 & 0 \\ 0 & R_2 \end{pmatrix}$, and $\hat{\mathbf{C}} \equiv \begin{pmatrix} C_1 + C_c & -C_c \\ -C_c & C_2 + C_c \end{pmatrix}$. The thermal (Johnson-Nyquist) noises ξ_1 and ξ_2 are Gaussian white and uncorrelated, namely, $\langle \xi_i(t)\xi_j(t') \rangle = 2k_B T_i R_i \delta_{ij} \delta(t-t')$, where k_B is the Boltzmann constant. Owing to a nonzero C_c , the dynamics of each voltage signal V_i is influenced explicitly by both thermal noises.

The measured RC circuits in metal shielding boxes are placed in a Faraday cage on an optical table. The resistor R_1 in a metal shielding box is cooled in a semiclosed liquid nitrogen dewar by liquid nitrogen vapor to create the NESS. We use voltage amplifiers with gain of 10⁴ to magnify the thermal voltages of V_1 and V_2 before sampling. The amplified signals are filtered by a 160 kHz antialiasing filter, digitized at 262.1 kHz, and averaged over 128 digitized points for a sample to achieve a sampling rate of 2048 Hz. Typically 10⁶ pairs of (V_1, V_2) are recorded during each run. The circuit parameters $C_1 = 488$ pF, $R_1 = 9.01M\Omega$, $C_2 = 420$ pF, and $R_2 = 9.51 \,\mathrm{M}\Omega$ are determined from the measured noise power spectrums of V_1 and V_2 at $C_c = 0$ when both circuits are at room temperature (see Ref. [25] for more experimental details and characterization). The coupling capacitance C_c varies from 100 pF to 10 nF. Its value is independently obtained by a LCR meter. The second reservoir is kept at room temperature ($T_2 =$ 296 K), and T_1 varies from 120 to 296 K. The value of T_1 below room temperature is measured by a K-type thermocouple and can be reaffirmed by the variance of statistics in V_1 with the knowledge of other circuit parameters. Figure 1(b) shows a snapshot of the concurrent voltage time traces $V_1(t)$ and $V_2(t)$ with $C_c = 1.0 \text{ nF}$ and $T_1 = 120 \text{ K}$. $V_1(t)$ and $V_2(t)$ resemble each other owing to the large C_c .

One can compare the electric circuit system to a Brownian particle in two dimensions, as depicted in Fig. 1(c). The vector $\vec{V}(t)$ can serve as the position of this virtual Brownian particle at time t. A small segment of its trajectory corresponding to the voltage time traces in Fig. 1(b) is shown by the orange line. In the thermally equilibriated case, $T_1 = T_2$, the virtual particle does not exhibit any net movement besides thermal fluctuations; when $T_1 \neq T_2$, the particle is unequally agitated by the two heat baths, causing a persistent, unidirectional movement on average. In the latter case, we set T_1 to be the colder heat bath throughout our study.

To compare our system to the Brownian gyrator described in Ref. [11], we introduce the linear transformation

$$\vec{q} \equiv \begin{pmatrix} q_1 \\ q_2 \end{pmatrix} = \hat{\mathbf{C}} \vec{V} ,$$
 (2)

where q_1 and q_2 represent the total capacitor charges in the neighbors of nodes 1 and 2, respectively. The potential energy of the system [depicted by equipotential elliptical contours in Fig. 1(c)], as stored in the capacitors, is $U = \frac{1}{2}C_1V_1^2 + \frac{1}{2}C_2V_2^2 + \frac{1}{2}C_c(V_1 - V_2)^2 = \frac{1}{2}\vec{V}^T\hat{\mathbf{C}}\vec{V} = \frac{1}{2}\vec{q}^T\hat{\mathbf{C}}^{-1}\vec{q}$. With this transformation of variables, the coupled Langevin equation (1) now reads

$$\hat{\mathbf{R}}\dot{\vec{q}} = -\hat{\mathbf{C}}^{-1}\vec{q} + \vec{\xi} = -\nabla_{q}U + \vec{\xi}$$
, (3)

which is identical to the overdamped Langevin equation (2) in Ref. [11]. Therefore, one can apply the framework of a Brownian particle confined in a 2D potential in Ref. [11] to the coupled RC circuit discussed in this work. Note that the virtual particle simultaneously experiences two thermal noises ξ_1 and ξ_2 from directions parallel to the q_1 and q_2 axes, respectively, as noises are depicted by the wavy arrows in Fig. 1(c). In this work, however, most results are presented on the V_1 - V_2 plane (the physically observed variables), and the dynamics of each V_i is influenced explicitly by both thermal noises.

III. BEHAVIOR IN NONEQUILIBRIUM STEADY STATE: PROBABILITY FLUX CIRCULATION

A. Experimental results

The main results of this work are visualized in Fig. 2. First, we present the equipotential lines of U as white concentric elliptical contours in Fig. 2. Due to the presence of a nonzero



FIG. 2. Behavior of Brownian gyrator. The figures present the main results of this work. The value of $C_c = 1.0 \text{ nF}$ is used here. White contour: the equipotential contours of the coupled RC circuit. Color map: the steady-state distribution $P_{ss}(\vec{V})$. Vector field: the probability flux, $\vec{J}_{ss}(\vec{V})$. The inset color map shows the curl of the probability flux, $\nabla \times \vec{J}_{ss}$. The experimental results are listed in (a) and (b). (a) Equilibrium case ($T_1 = T_2 = 296 \text{ K}$). The contour lines in P_{ss} and U mutually agree, and \vec{J}_{ss} hardly exhibits any flowing trend as the detailed balance is valid. (b) NESS case ($T_1 = 120 \text{ K}$). Contour lines of P_{ss} are tilted with respect to those in U, and \vec{J}_{ss} reveals a circulating trend about the origin. (c) Theoretical counterparts of (b).

 C_c , the potential possesses no rotational symmetry, and the principal axes of the contours are tilted in the V_1 - V_2 frame and do not coincide with q_1 - q_2 axes, where ξ_1 and ξ_2 act on. Therefore, this setup meets the two aforementioned requirements and can serve as an electrical version of a Brownian gyrator [11].

Our measured steady-state distribution $P_{ss}(\vec{V})$ is presented as a color-map plot in Figs. 2(a) and 2(b). At thermal equilibrium $(T_1 = T_2 \equiv T)$, P_{ss} follows the Boltzmann distribution. Thus P_{ss} is constant on equipotential contours, as shown in Fig. 2(a). The system falls into a NESS when $T_1 < T_2$ with a nonzero heat flow on average going from the T_2 heat bath to the T_1 heat bath through the circuit [24]. A NESS case of $T_1 = 120$ K is demonstrated in Fig. 2(b). While P_{ss} in Fig. 2(b) still has an elliptic shape, it does not stay in accordance with the potential landscape. Its principal axes rotate counterclockwise slightly when compared with those in Fig. 2(a). This behavior is attributed to the narrower distribution in V_1 in the NESS case due to the lower T_1 .

A major difference between thermal equilibrium and NESS lies in time reversibility. Theoretically, the former is achieved through the detailed balance condition, which is itself a signature of time reversibility. On the other hand, the detailed balance condition can fail in a nonequilibrium process, leading to persistent probability flows even in its steady state. Here we evaluate the probability flux $\vec{J}_{ss}(\vec{V}) \equiv P_{ss}(\vec{V})\vec{v}_{flow}(\vec{V})$ from the experimental trajectory of the virtual particle, where $\vec{v}_{\text{flow}}(\vec{V})$ represents the steadystate flow velocity at \vec{V} [14]. We use the operational definition $\vec{v}_{\text{flow}}(\vec{V}) \equiv [\langle \vec{V}(t+\Delta t) - \vec{V}(t) | \vec{V}(t) = \vec{V} \rangle - \langle \vec{V}(t) - \vec{V}(t) \rangle]$ $\vec{V}(t - \Delta t) | \vec{V}(t) = \vec{V} \rangle]/2\Delta t$, where $\Delta t = 0.488 \,\mathrm{ms}$ is the sampling interval (corresponding to the sampling rate of 2048 Hz), and the phase space is divided into grids with resolution $\Delta V = 0.67 \mu V$ in order to accumulate decent statistics. The experimental results of \vec{J}_{ss} are presented as vector fields in Figs. 2(a) and 2(b). There is clearly a circulating probability flux field in the NESS case [Fig. 2(b)], while no significant flow occurs in the thermal equilibrium case [Fig. 2(a)]. Therefore, in a NESS, the motion of the virtual particle can be depicted

by Brownian dynamics with an average counterclockwise circulation, i.e., it manifests as a Brownian gyrator in an electrical system. See also the supplemental videos [26] for the real-time evolutions of the virtual particle in the phase space.

The circulation of probability flux in the NESS results from the unbalanced competition between the conservative and diffusive driving forces. Naïvely speaking, on the V_1 - V_2 plane, the conservative force pulls the virtual particle inward. Meanwhile, the diffusive force from the gradient of P_{ss} tends to push the virtual particle outward. At thermal equilibrium [see Fig. 2(a)], the two sets of contour lines have identical shape, and their representative drives cancel out exactly. Thus the net flux is zero everywhere, a signature of the detailed balance. In the NESS case, however, due to the temperature difference, the principal axes for the contours of P_{ss} and U are different, and the two driving forces are mostly not balanced. As a result, the net force contributes to a nonvanishing flux. Circulating motion therefore emerges naturally since the flux at the steady state must be divergence-free (the curl of a nonzero field must exist somewhere for the divergence-free case).

Moreover, owing to the conservation of probability,

$$\frac{dP_{\rm ss}}{dt} = \nabla P_{\rm ss} \cdot \vec{v}_{\rm flow} + \frac{\partial P_{\rm ss}}{\partial t} = 0 \tag{4}$$

holds along the steady-state circulation trajectories. Since $\frac{\partial P_{ss}}{\partial t} = 0$, \vec{v}_{flow} and thus \vec{J}_{ss} must be perpendicular to ∇P_{ss} [27].

The results for the curl of the steady-state flux, $\nabla \times \vec{J}_{ss}$, are shown in the insets of Fig. 2, where $\nabla \times \vec{J}_{ss}$ points out of the V_1 - V_2 plane. In the NESS case, the large positive curling trend near the origin causes the virtual particle to gyrate counterclockwise on average. Note that away from the origin, small regions with a negative curling direction (shown as dark blue) can be observed from both our experimental and theoretical analysis. Negative curl exists in regions of approximately parallel field lines whose magnitude decreases as the virtual particle marches outward. Note that even in

the negative curl regions, the flux field lines still follow the counterclockwise gyrating trend with respect to the origin.

B. Theoretical analysis

We first consider the corresponding Fokker-Planck equation of this stochastic system:

$$\frac{\partial P(\vec{V},t)}{\partial t} = \boldsymbol{\nabla} \cdot [\hat{\mathbf{M}}^{-1} \vec{V} P(\vec{V},t)] + \frac{1}{2} \boldsymbol{\nabla} \cdot [\hat{\mathbf{M}}^{-1} \hat{\mathbf{\Gamma}} (\hat{\mathbf{M}}^{-1})^T \boldsymbol{\nabla} P(\vec{V},t)], \quad (5)$$

where $\hat{\mathbf{M}} \equiv \hat{\mathbf{R}}\hat{\mathbf{C}}, \hat{\mathbf{\Gamma}} \equiv \begin{pmatrix} \Gamma_1 & 0\\ 0 & \Gamma_2 \end{pmatrix} = \hat{\mathbf{R}}\hat{\mathbf{T}}$ and $\hat{\mathbf{T}} \equiv \begin{pmatrix} 2k_BT_1 & 0\\ 0 & 2k_BT_2 \end{pmatrix}$. It has a Gaussian steady-state distribution in

$$P_{\rm ss}(\vec{V}) = \sqrt{\frac{\det(\hat{\mathbf{M}}^T \hat{\mathbf{X}} \hat{\mathbf{M}})}{\pi^2}} \exp(-\vec{V}^T \hat{\mathbf{M}}^T \hat{\mathbf{X}} \hat{\mathbf{M}} \vec{V}), \quad (6)$$

where

$$\hat{\mathbf{X}} \equiv \frac{(\hat{\mathbf{M}}^{-1})^T \hat{\mathbf{\Gamma}}^{-1} \hat{\mathbf{M}}^{-1} + \frac{\hat{\mathbf{\Gamma}}^{-1}}{\det(\hat{\mathbf{M}})}}{\frac{\mathrm{Tr}(\hat{\mathbf{M}})}{\det(\hat{\mathbf{M}})} \left\{ 1 + \frac{1}{\det(\hat{\mathbf{\Gamma}})} \left[\frac{\Gamma_1 M_{21} - \Gamma_2 M_{12}}{\mathrm{Tr}(\hat{\mathbf{M}})} \right]^2 \right\}}$$
(7)

is a 2×2 symmetric matrix, and $\{M_{ij}\}$ represent the elements of the matrix $\hat{\mathbf{M}}$. With a little algebra one can show that

$$\hat{\mathbf{X}}\hat{\mathbf{M}} = \frac{\operatorname{Tr}(\hat{\mathbf{M}})}{B} (A\hat{\boldsymbol{\Gamma}}^{-1} - \epsilon \hat{\mathbf{Y}}), \qquad (8)$$

where $A \equiv \text{Tr}(\hat{\mathbf{M}}) \det(\hat{\mathbf{\Gamma}}), \hat{\mathbf{Y}} \equiv \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}, B \equiv \det(A\hat{\mathbf{\Gamma}}^{-1} - \epsilon\hat{\mathbf{Y}}) = A^2/\det(\hat{\mathbf{\Gamma}}) + \epsilon^2$, and $\epsilon \equiv \Gamma_1 M_{21} - \Gamma_2 M_{12} = 2k_B R_1 R_2 C_c$ $(T_2 - T_1).$

Equation (8) can be rewritten as

$$\hat{\mathbf{X}}\hat{\mathbf{M}} = \frac{A'\hat{\mathbf{\Gamma}}^{-1} - \epsilon'\hat{\mathbf{Y}}}{A'(1 + \epsilon'^2)},$$
(9)

where $A' \equiv \sqrt{\det \hat{\Gamma}}$, and $\epsilon' \equiv \epsilon/[A' \cdot \text{Tr}(\hat{\mathbf{M}})]$ gives a dimensionless measure for the deviation from thermal equilibrium. Thus one has

$$\hat{\mathbf{M}}^{T}\hat{\mathbf{X}}\hat{\mathbf{M}} = \left(\frac{\hat{\mathbf{C}}}{1+\epsilon^{\prime 2}}\right) \left(\hat{\mathbf{T}}^{-1} - \frac{\epsilon^{\prime}}{A^{\prime}}\hat{\mathbf{R}}\hat{\mathbf{Y}}\right).$$
 (10)

Note that $\epsilon' = 0$ when thermal equilibrium between the two resistors is reached $(T_1 = T_2)$. In this case, the matrix $\hat{\mathbf{M}}^T \hat{\mathbf{X}} \hat{\mathbf{M}} = \hat{\mathbf{C}} \hat{\mathbf{T}}^{-1}$, while the matrix $\hat{\mathbf{T}}$ reduces to a multiple of the identity matrix. Therefore, P_{ss} exhibits a Boltzmann distribution and follows the shape of the equipotential contour.

The probability flux of the system is

$$\vec{J} = -\hat{\mathbf{M}}^{-1}\vec{V}P - \frac{1}{2}\hat{\mathbf{M}}^{-1}\hat{\mathbf{\Gamma}}(\hat{\mathbf{M}}^{-1})^T \nabla P(\vec{V},t), \qquad (11)$$

in which the first term results from the restoring force towards the origin, while the second term can be attributed to the diffusive driving force. At the steady state, one has

$$\vec{J}_{\rm ss} = -\hat{\mathbf{M}}^{-1} [\vec{V} - \hat{\mathbf{\Gamma}} \hat{\mathbf{X}} \hat{\mathbf{M}} \vec{V}] P_{\rm ss} \equiv \hat{\mathbf{\Pi}} \vec{V} P_{\rm ss} \,. \tag{12}$$

In the case of thermal equilibrium, $T_1 = T_2$, Eq. (9) reduces to $\hat{\mathbf{X}}\hat{\mathbf{M}} = \hat{\mathbf{\Gamma}}^{-1}$. As a result, $\vec{J}_{ss} = \vec{0}$, which is a signature of the detailed balance. On the other hand, in a NESS case, the two representative forces in Eq. (11) do not cancel out, causing a persistent net flux in a NESS. The steady-state flux described by Eq. (12) is plotted as a vector field in Fig. 2(c).

The gyrating direction of the virtual particle can be identified by comparing the directions of \vec{J}_{ss} and $\nabla P_{ss} \times \vec{z}$, where \vec{z} is the unit vector point out of the V_1 - V_2 plane. The virtual particle is gyrating counterclockwise if both vectors are parallel and clockwise if they are antiparallel. Note that

$$\vec{J}_{ss} \cdot (\nabla P_{ss} \times \vec{z}) = -\nabla P_{ss} \cdot \hat{\mathbf{Y}} \vec{J}_{ss}$$

$$= -\frac{2\epsilon}{\mathrm{Tr}(\hat{\mathbf{M}})} (\hat{\mathbf{X}} \hat{\mathbf{M}} \vec{V})^T (\hat{\mathbf{M}} \hat{\mathbf{Y}} \hat{\mathbf{M}}^{-1} \hat{\mathbf{Y}}) (\hat{\mathbf{X}} \hat{\mathbf{M}} \vec{V}) P_{ss}^2 .$$
(13)

One can show that the matrix $\hat{\mathbf{M}}\hat{\mathbf{Y}}\hat{\mathbf{M}}^{-1}\hat{\mathbf{Y}}$ is symmetric, while Tr($\hat{\mathbf{M}}\hat{\mathbf{Y}}\hat{\mathbf{M}}^{-1}\hat{\mathbf{Y}}$) < 0 and det($\hat{\mathbf{M}}\hat{\mathbf{Y}}\hat{\mathbf{M}}^{-1}\hat{\mathbf{Y}}$) = 1. As a result, $\hat{\mathbf{M}}\hat{\mathbf{Y}}\hat{\mathbf{M}}^{-1}\hat{\mathbf{Y}}$ is negative-definite, and on average, the virtual particle is gyrating counterclockwise if $\epsilon > 0$, i.e., $T_2 > T_1$, and vice versa. As the direction of gyration coincides with that of heat transport from the hot towards the cold heat bath (see next section), we have therefore shown that for this coupled RC circuit, on average, heat is transferred from the highto low-temperature thermal baths. Hence the second law of thermodynamics is recapitulated here through the discussion of gyrating dynamics.

IV. ENERGY FLOW IN A CLOSED TRAJECTORY

The above observation reveals that on average, the virtual particle rotates about the origin in the V_1 - V_2 phase space, while its Brownian-motion signature is revealed within short-time intervals. The average circulating behavior shows periodic oscillations in V_1 and V_2 with an identical frequency and a constant phase difference. The system therefore acts like a mini electricity generator powered solely by the temperature difference and thus can be compared to a Brownian ratchet or a mini heat engine. The ac voltage could be conceivably used to power up devices or rectified to store electric energy.

How does energy transfer from the hot heat reservoir to the cold one in a directed cycle? First, we note that if the virtual particle circulates along some closed loop on the V_1 - V_2 diagram, the amount of energy flowing into the circuit through resistor R_i (the same as the amount of heat flowing out of the heat bath coupled to R_i) during one cycle is $Q_i = \oint V_i i_{R,i} dt = \oint V_i dq_i$, where $i_{R,i}$ is the current through R_i . One can find $Q_1 = -C_c \oint V_1 dV_2$ and $Q_2 = -C_c \oint V_2 dV_1 =$ $C_c \oint V_1 dV_2 = -Q_1$, and their magnitude is proportional to the loop area $|\oint V_2 dV_1|$ on the V_1 - V_2 diagram. Thus over each counterclockwise cycle $Q_2 = -Q_1 > 0$, and a net energy is flowing from the hot reservoir towards the cold one.

The energy transfer can be better understood using Fig. 3(a) as a schematic example. The cyclic diagram is constituted by



FIG. 3. Energy flow in a semiadiabatic cycle. (a) A closed cycle in the phase space formed by four chosen semiadiabatic paths (I, II, III, IV) about the origin. The red (blue) arrows indicate the processes adiabatic to T_1 (T_2), while the system is subject to energy exchanges with the T_2 (T_1) heat bath only. (b) Major current flows (black solid arrows) and energy flows (gray dashed arrows) in the circuit for the four processes. (c) An illustrated example of paving a closed cycle by semiadiabatic processes.

four simple paths (I, II, III, IV), which form a parallelogram with endpoints A, B, C, and D. The four paths are chosen such that q_1 stays fixed during I and III while q_2 stays fixed during II and IV. As a consequence, for processes I and III, no currents are flowing through R_1 , and the system can be considered adiabatic to the cold reservoir T_1 , while it can exchange energy with the hot reservoir T_2 . Similarly, for processes II and IV, $i_{R,2} = 0$, and the system can be considered adiabatic to the reservoir T_2 bath, while it can exchange energy with the T_1 reservoir.

One can show that during processes I and III, the resistor R_2 is exerting positive work on capacitors C_1 and C_2 , while the bridging capacitor C_c is discharging and also releasing energy into the other capacitors. And during processes II and IV, the capacitors C_1 and C_2 are discharging and releasing energy into R_1 and C_c . The directions of net energy flows and electric currents are shown in Fig. 3(b). Other than the reversed polarity in charges and currents, the processes III and IV simply repeat I and II, respectively. After a full cycle, the system resumes its original state, and a net energy is transferred from the T_2 to the T_1 heat bath through the circuit elements. The amount of transferred energy can be characterized via the enclosed area of the cycle, as larger cycles and faster gyrating rates signify higher heat conduction rates.

Note that for a parallelogram of the aforementioned semiadiabatic processes without centering at the origin, the magnitude and even the sign of transported energy to and from the capacitors for each individual process may vary. Yet the total amount of energy transported in the two processes I and III remains unchanged (and so on for II and IV). As a result, the energy transfer can be characterized in terms of area on the V_1 - V_2 plot, i.e., $|\oint V_2 dV_1|$. Furthermore, one can dissect any closed cycle (e.g., the elliptical contour in our experimental observation in a NESS) into infinite pavements of parallelograms [see Fig. 3(c) for an illustrated example]. Thus any closed cycle can be treated as a composite of semiadiabatic processes.

The linear coupled circuit described here does not convert any heat into work. Therefore, although the gyrating behavior is observed in our system, currently it remains meaningless to discuss its efficiency and output power. Nonetheless, we can briefly remark on the possibility of extracting work from the system. For all our discussed cases, the average entropy of this stochastic system (up to addition by some constant owing to $P_{\rm ss}$ is not a dimensionless quantity) is

$$\langle S \rangle / k_{B} = -\int P_{\rm ss}(\vec{V}) \ln P_{\rm ss}(\vec{V}) d\vec{V} = \langle \vec{V}^{T}(\hat{\mathbf{M}}^{T} \hat{\mathbf{X}} \hat{\mathbf{M}}) \vec{V} \rangle + \frac{1}{2} \ln \frac{\pi^{2}}{\det(\hat{\mathbf{M}}^{T} \hat{\mathbf{X}} \hat{\mathbf{M}})} = 1 + \ln(2k_{B}\pi) - \frac{1}{2} \ln \det(\hat{\mathbf{C}}) + \frac{1}{2} \ln \left\{ T_{1}T_{2} + \frac{C_{c}^{2}R_{1}R_{2}(T_{2} - T_{1})^{2}}{[\operatorname{Tr}(\hat{\mathbf{R}}\hat{\mathbf{C}})]^{2}} \right\}.$$
(14)

Furthermore, the average internal energy is $\langle U \rangle = \frac{1}{2}k_B(T_1 + T_2)$. Therefore, for the NESS case we consider, where the circuit is thermalized by two different heat baths at T_1 and T_2 , its average energy is identical with that in thermal equilibrium with the mean temperature $T = (T_1 + T_2)/2$. On the other hand, one can easily show that the NESS average entropy is less than the equilibrium result at the average temperature, suggesting that the circuit in a NESS is more ordered. Since in thermal equilibrium, entropy is a monotonic function of energy, thus in principle, the circuit in a NESS should be capable of providing work via some relaxation process towards the equilibrium where the system entropy is preserved. Note that with proper external driving, this linear system can function as a heat engine or a refrigerator [28].

V. ROTATION SPEED OF THE GYRATOR

The gyrating motion of the virtual Brownian particle can also be well visualized through the dynamics of $\phi(t) \equiv$ $\tan^{-1}\left[\frac{V_2(t)}{V_1(t)}\right]$ [29], the angle of the particle position vector $\vec{V}(t)$ relative to the V_1 axis in the configuration space. Figure 4(a) presents the gross behavior of $\phi(t)$ for various T_1 , while the stochastic behavior is magnified in the inset. In the NESS cases $(T_1 < T_2)$, the overall trend exhibits a linear growth in time, while such a feature is absent in the thermal-equilibrium case $(T_1 = T_2 = 296 \text{ K})$.

The dependence of average gyrating rate, $\langle \dot{\phi} \rangle$, on the temperature difference, $\Delta T \equiv T_2 - T_1$, is shown in Fig. 4(b). Note that experimentally we obtain $\langle \dot{\phi} \rangle$ via two methods: The first method is finding the slopes of the fitted straight lines in Fig. 4(a) (solid square), while the second is evaluating the average rotating speed from the probability flux: $\langle \dot{\phi} \rangle = \int \frac{\vec{V} \times \vec{v}_{\text{flow}}}{V^2} P_{\text{ss}} d\vec{V}$ (open circle). Both experimental evaluations



FIG. 4. Rotation speed of gyrator. (a) The measured time evolution in the angle of the virtual Brownian particle position $\phi(t)$ for various T_1 ($C_c = 1.0 \text{ nF}$ being used). The inset provides a zoom-in detail for fluctuating motions. (b) $\langle \dot{\phi} \rangle$ vs ΔT evaluated from the average slope of $\phi(t)$ (solid square) and the average rotating speed derived from \vec{v}_{flow} (open circle) ($C_c = 1.0 \text{ nF}$ being used). Theoretical result is provided as the dashed curve. (c) $\langle \dot{\phi} \rangle$ vs C_c for $T_1 = 120 \text{ K}$. Symbols show the results from measurement while the dashed curve gives the theoretical prediction. (d) The averaged leading angle $\langle \alpha \rangle$, defined by the advanced phase of oscillation in V_1 over that in V_2 , for a virtual particle circulating along the flux field [$T_1 = 120 \text{ K}$; the same symbols as in (c)].

agree well and indicate an approximately proportional relation between $\langle \dot{\phi} \rangle$ and ΔT .

The temperature dependence on the gyrating flux is also studied analytically. By defining $\hat{\Delta}\hat{\mathbf{M}} \equiv \hat{\mathbf{\Gamma}}\hat{\mathbf{X}}\hat{\mathbf{M}} - \hat{\mathbf{I}}$, where $\hat{\mathbf{I}}$ is the 2×2 identity matrix, one can show that

$$\hat{\Delta}\hat{\mathbf{M}} = \frac{-\epsilon^2 \hat{\mathbf{I}} - \epsilon \operatorname{Tr}(\hat{\mathbf{M}})\hat{\mathbf{\Gamma}}\hat{\mathbf{Y}}}{B} = -\frac{\epsilon \hat{\mathbf{Y}}\hat{\mathbf{X}}\hat{\mathbf{M}}}{\operatorname{Tr}(\hat{\mathbf{M}})}.$$
 (15)

Therefore, $\hat{\mathbf{\Pi}} = \hat{\mathbf{M}}^{-1} \hat{\Delta} \hat{\mathbf{M}}$ [refer to Eq. (12)], and $\hat{\mathbf{\Pi}}$, \vec{J}_{ss} and thus $\langle \dot{\phi} \rangle$ are approximately proportional to ϵ and hence ΔT when the temperature difference is small. The theoretical prediction of this linear behavior is shown by the dashed line in Fig. 4(b), as observed experimentally.

We further study the dependence of rotating speed on the coupling, C_c , as is shown in Fig. 4(c). Remarkably, $\langle \dot{\phi} \rangle$ does not increase monotonically with C_c . Our theoretical result [dashed curve in Fig. 4(c)] predicts a broad peak near $C_c \approx 700$ pF, while the peak circulating speed is about 5 rev/s. And the evaluation of $\langle \dot{\phi} \rangle$ from the experimental data (open circles) follow well with the theoretical curve, proving the existence of an optimal coupling for gyrating.

To investigate how the rotational speed of the virtual particle relates to the coupling, we first find from the average heat transfer rate [24]

$$\langle \dot{Q} \rangle = \frac{C_c^2 k_B (T_2 - T_1)}{\det(\hat{\mathbf{C}}) \cdot \operatorname{Tr}(\hat{\mathbf{R}}\hat{\mathbf{C}})}$$
(16)

that $\langle \dot{Q} \rangle$ increases monotonically over C_c , as $\langle \dot{Q} \rangle \sim O(C_c^2)$ in the weak-coupling regime (when C_c is small) and $\langle \dot{Q} \rangle \sim O(1)$

in the strong coupling regime (large C_c). Furthermore, the average heat transferred from T_2 to T_1 reservoir during one gyrating cycle, Q_{cycle} , is equal to the product of C_c and the average area of gyration on the V_1 - V_2 diagram. Therefore, Q_{cycle} is proportional to $C_c \pi / \sqrt{\det(\hat{\mathbf{M}}^T \hat{\mathbf{X}} \hat{\mathbf{M}})}$. One can show that Q_{cycle} is also increasing monotonically over C_c , as $Q_{cycle} \sim O(\sqrt{C_c})$ for large C_c and $Q_{cycle} \sim O(C_c)$ for small C_c . As a result, $\langle \dot{\phi} \rangle \approx 2\pi \cdot \langle \dot{Q} \rangle / Q_{cycle}$ leads to $\langle \dot{\phi} \rangle \sim O(C_c)$ for small C_c and $\langle \dot{\phi} \rangle \sim O(C_c^{-1/2})$ for large C_c . Hence $\langle \dot{\phi} \rangle$ is not increasing monotonically; instead it reaches a peak, as evidenced in Fig. 4(c). The decreasing trend of $\langle \dot{\phi} \rangle$ can also be understood by recognizing that at large C_c it takes a long time for the system to charge and discharge.

In Fig. 4(d) we present the average phase difference $\langle \alpha \rangle$ between V_1 and V_2 along the elliptical contours of constant $P_{\rm ss}(\vec{V})$ (positive if V_1 leads V_2). The leading angle $\langle \alpha \rangle$ is experimentally evaluated by the average of the instantaneous angle difference $\alpha = \tan^{-1}\left(\frac{-\dot{V}_1}{\omega V_1}\right) - \tan^{-1}\left(\frac{-\dot{V}_2}{\omega V_2}\right)$, where $\omega = \left|\frac{\vec{V} \times \vec{V}}{V^2}\right|$ is the instantaneous angular velocity of the virtual particle in the V_1 - V_2 phase space. For the special case that C_c vanishes, the elliptical contours are nontilted, and thus $\langle \alpha \rangle$ is equal to 90°. As C_c increases, the ellipses start to tilt due to the coupling between the signals V_1 and V_2 , and as a result $\langle \alpha \rangle$ decreases. Again the experimental results are well confirmed by theoretical analysis.

VI. CONCLUSION

We demonstrate in this work that the linear, coupled RC circuit system, under the agitation of two different thermal baths near room temperature scale, can serve as a nonmechanical realization of the autonomous Brownian gyrator. The incomplete cancellation between the diffusive drive and the potential-gradient dragging accounts for the net circulating flux in the steady state. For such an arrangement, the system acts like a mini electricity generator, while the possibility for the usage of this generated power is still being explored.

The observation that heat is conducted from the hot to the cold reservoir is simply consistent with the second law of thermodynamics. Yet the heat-transfer mechanism through the gyration in the configuration space is plausible, noting that the conducting element possesses two thermal degrees of freedom only. The direction of heat flow, the gyrating dynamics, and the total entropy production, are all representations of the second law, which speaks of time irreversibility in a nonequilibrium steady state. Our study helps reaffirm the general principle and the possible realization of a Brownian ratchet under real thermal baths.

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- [26] See Supplemental Material at http://link.aps.org/supplemental/ 10.1103/PhysRevE.96.032123, we provide real-time movies of the virtual-particle movement in the phase space for three experimental cases ($C_c = 1 \text{ nF}$, $T_1 = 120 \text{ K}$; $C_c = 1 \text{ nF}$, $T_1 =$ 296 K and $C_c = 0$, $T_1 = 120 \text{ K}$, respectively).
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