Inhomogeneous quasistationary state of dense fluids of inelastic hard spheres

Itzhak Fouxon

Department of Complex Systems, Weizmann Institute of Science, Rehovot 76100, Israel (Received 12 February 2014; published 19 May 2014)

We study closed *dense* collections of freely cooling hard spheres that collide inelastically with constant coefficient of normal restitution. We find inhomogeneous states (ISs) where the density profile is spatially nonuniform but constant in time. The states are exact solutions of nonlinear partial differential equations that describe the coupled distributions of density and temperature valid when inelastic losses of energy per collision are small. The derivation is performed without modeling the equations' coefficients that are unknown in the dense limit (such as the equation of state) using only their scaling form specific for hard spheres. Thus the IS is the exact state of this dense many-body system. It captures a fundamental property of inelastic collections of particles: the possibility of preserving nonuniform temperature via the interplay of inelastic cooling and heat conduction that generalizes previous results. We perform numerical simulations to demonstrate that arbitrary initial state evolves to the IS in the limit of long times where the container has the geometry of the channel. The evolution is like a gas-liquid transition. The liquid condenses in a vanishing part of the total volume but takes most of the mass of the system. However, the gaseous phase, which mass grows only logarithmically with the system size, is relevant because its fast particles carry most of the energy of the system. Remarkably, the system self-organizes to dissipate no energy: The inelastic decay of energy is a power law $[1 + t/t_c]^{-2}$, where t_c diverges in the thermodynamic limit. This is reinforced by observing that for supercritical systems the IS coincide in most of the space with the *steady* states of granular systems heated at one of the walls. We discuss the relation of our results to the recently proposed finite-time singularity in other container's geometries.

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I. INTRODUCTION

In the past decades a lot of attention was devoted to the study of formation of structures in closed systems with dissipative interactions (ordering). This formation is often associated with decrease of entropy due to the system's interaction with the environment. The latter is described effectively by the dissipative part of the interactions. In this work we consider the dissipative system of hard spheres with inelastic collisions that cools freely. This serves as basic model of the granular material, which is the dissipative system of macroscopic particles which interaction involves friction, like sand. We demonstrate the formation of stable spatial structure in this system.

The inelasticity of the collisions of the spheres, which model the sand grains, mimics the friction, describing effectively the transfer of energy to the inner degrees of freedom of the particles that play the role of the environment for the translational degrees of freedom [\[1,2\]](#page-20-0). We use the popular model where the normal component of the relative velocity of the particles is depleted after the collision by a positive constant $r < 1$ (which is called coefficient of normal restitution; $r = 1$ for the elastic collisions).

We consider the case where the inelasticity is small, 1 $r \ll 1$, so the energy is "almost" conserved in each collision. In this case, the inelasticity effect becomes significant only after a long time of evolution. Over the mean free time (or the liquid relaxation time in the dense regions), however, the inelasticity is negligible so the collection reaches the state of the local thermal equilibrium $[3,4]$. This is characterized by the local values of the density, temperature, and velocity that vary throughout the system and evolve according to the equations of the fluid mechanics.

The fluid-mechanical equations of the collection of inelastically colliding hard spheres contain a correction due to inelasticity. This brings finite effect over the time scale of the order of $(1 - r)^{-1}$ times the mean free time. During this time scale the energy depletion due to the inelasticity is of order 1, so the system's state completely differs from that of the elastic hard spheres.

In this paper we use the fluid-mechanical equations of granular materials to demonstrate new states of *dense* collections of inelastically colliding hard spheres where the liquid phase is present in the system. These states are states of mechanical equilibrium where the pressure is spatially uniform (this uniform pressure decays in time though due to inelasticity). The forces on each fluid element are balanced so the fluid is macroscopically at rest and the density profile is time independent. Thus these states can be said to be closest to the equilibrium states of collections of elastically colliding hard spheres (the thermal equilibrium is impossible due to the dissipation). The density, however, is inhomogeneous: The inelastic cooling opens the possibility of having stable inhomogeneous spatial profiles of density, which is absent in elastic systems.

This possibility of having states of free granular systems with inhomogeneous stationary profile of density [called *inhomogeneous states* (ISs)] was first discussed in Refs. [\[5,6\]](#page-20-0). Previously similar states were observed to hold in thermally agitated systems where one of the walls is kept at a constant temperature [\[7\]](#page-20-0). In both kinds of ISs the heat flux caused by the inhomogeneity of temperature is balanced by the inelastic cooling, which is also inhomogeneous. The states differ in that the states of forced systems are steady while the states of the free granular systems dissipate energy. It is remarkable that the ISs of free systems coincide with the steady states of forced systems in the major part of the volume in the regime of the supercritical systems; see the discussion in Sec. [XIII.](#page-19-0)

For free systems the spatial profile of the temperature is preserved up to the depletion of the overall amplitude. This spatial structure stably exists when the entropy monotonously decreases to $-\infty$ (the decrease stops eventually when the inner degrees of freedom start to return energy to the translational ones at the collisions), cf. Refs. [\[8–10\]](#page-20-0). However, the consideration of the thermodynamic limit of the IS, presenting the highest interest, is not possible within the dilute limit: it was found that the maximal density of the IS grows exponentially with the system size, so the density becomes comparable with the density of dense packing for large sizes of the system (thermodynamic limit). Thus the study of the thermodynamic limit necessitates considering dense regions. There, usually, the study can be performed only phenomenologically due to the strong coupling between the particles (for example, even the precise equation of state is unknown for liquids).

We succeed in deriving the dense ISs that hold in the thermodynamic limit without approximations. That is, the ISs are derived for granular liquids, taking into account the finite size of the particles and the corresponding excluded volume effects. The derivation uses a description that works uniformly both for gas and liquid phases, including the possibility of coexistence of the phases. This is despite the fact that the constitutive relations that appear in the fluid-mechanical equations (such as the equation of state) are not known explicitly in the liquid phase.We note that the particular scaling form of those functions, which holds due to the absence of the intrinsic energy scale for hard spheres, admits the IS solutions. Due to the robustness of this observation, one can expect that the existence of the IS is a fundamental property of granular materials.

The ISs have unusual properties. These are states of coexistence of liquid and gas phases. The phases are described by the time-independent density profile that varies continuously in space from large values in the liquid phase to low values in the gaseous phase.

Probably the most striking property of the IS is its particular organization of particles in space due to which the system does not dissipate energy in the thermodynamic limit. This is not because the particles freeze: The temperature is finite. However, the flow of energy in space due to the inhomogeneity of temperature compensates the local energy losses due to inelastic collisions so the energy obeys $[1 + t/t_c]^{-2}$, where t_c diverges in the thermodynamic limit. In particular, since the local energy dissipation rate is determined completely by the local density and temperature, this signifies that these fields "know" of the system size in the IS.

This is in sharp contrast to the well-known homogeneous cooling states (HSs) $[11]$, where the decay obeys the same law $[1 + t/t_c]^{-2}$, but t_c is a local property independent of the size of the system. Furthermore, the total entropy decreases due to the dissipation logarithmically in time. This decrease is proportional to the number of collisions that occurred in the system. Thus, roughly, the entropy decreases in each collision by the same, time-independent, amount.

Our derivation of the ISs holds for systems where on average the system is dilute, so the fraction of space occupied by the gas phase is close to unity. (This is, in particular, the case of the clustering instability of the HSs of granular gases, see below). However, the small fraction of space occupied by

the liquid contains the fraction of the total mass that is close to unity. In contrast, the energy of the system is predominantly contained in the gaseous state, where the particles' speed is higher. Thus in the IS both phases are present significantly, one carrying the mass and the other the energy of the total system.

Further insight into the physics of the IS is reached by considering the development of the solution in the intrinsic time variable which is the number of collisions of the particles that occurred by time *t*. In this variable rescaling of the fields by a time-dependent factor turns the IS into time-independent solution. To demonstrate this, we provide a time-dependent transformation that transforms the original equations, which do not have explicit time dependence, into the equations that also do not have explicit time dependence. The IS is the stationary solution in rescaled variables. We use this transformation to demonstrate that the evolution of small perturbations of the IS obeys the power-law behavior in time.

Once the IS solutions are derived, the question is if they are stable. The study of this question in the dilute case has a long history. It started from the study of the stability of the HS [\[11\]](#page-20-0). This state plays the role of the equilibrium state for systems with size smaller than an intrinsic instability length l_{cr} times π , which relax to the HS universally at large times. The scale l_{cr} is of order of the mean free path over $\sqrt{1-r}$. However, the HS is unstable for larger systems due to the famous clustering instability [\[11–15\]](#page-20-0). That instability, obtained by linearizing the equations around the HS, demonstrated the formation of clusters in the system that spontaneously break the translational symmetry. It was shown in Refs. [\[5,6\]](#page-20-0) that when the system size passes the instability length (supercritical systems), simultaneously with uniform solutions getting unstable, the ISs appear (that do not exist at the smaller length). Based on the analogy with instability in the Newtonian fluids, one can expect that the IS plays the role of the HS for supercritical systems and constitutes the result of evolution at large times. This was shown to be the case for systems that are not too large for the channel geometry of the particles' container [\[5\]](#page-20-0).

In the latter case, the fluid-mechanical fields depend only on the coordinate along the channel $[16–20]$. The limit of fast sound was considered in Ref. [\[5\]](#page-20-0), where the sound propagation time t_s across the system is much smaller than the characteristic time of the decay of energy due to inelasticity. Then, since *ts* is the characteristic time of relaxation of the pressure to the equilibrium uniform value, the inelastic evolution happens on the background of the pressure that is constant in space (but not in time). As a result, one can reduce the compete system of fluid-mechanical equations to one integrodifferential scalar equation. The numerical study of that equation demonstrated that the ISs are stable. Furthermore, the ISs provide universal result of the long-time evolution of the granular gas. In particular, they determine the ultimate result of the clustering instability of the HS [\[11–15\]](#page-20-0).

Thus the IS provided the first consistent prediction on the long-time result of the nonlinear development of the instability in a certain limit. This limit, though, demands that the length of the channel is not too large, so it cannot be used to study the thermodynamic limit. The consideration of the latter limit demands considering the full system of the fluid-mechanical equations, and it was not performed previously.

In this work we perform the numerical simulation of the complete system of the fluid-mechanical equations of the dilute granular gas in the channel (so the integral equation simulated in Ref. [\[5\]](#page-20-0) is a reduction of this system in the limit of moderate system size). We demonstrate that the IS is the result of the long-time evolution of the system for arbitrary lengths of the channel. Since for arbitrarily large but fixed sizes of the system, the dilute gas holds in the limit of small sizes of the particles, our result signifies that the IS is the result of the long-time evolution of the system in the thermodynamic limit taken *after* the limit of zero particle size.

To complete the proof that the IS is the universal result of the long-time evolution of the collection of inelastic hard spheres in the channel, one has to deal with the finite particles' size. The maximal density on the IS of the dilute gas grows exponentially with the size of the system, so the consideration of the thermodynamic limit of the collection of (real) finitesize particles necessitates the study of the fluid-mechanical equations not constrained by the diluteness assumption. We perform this study using the following consideration.

Our derivation of the IS does not assume that the fluid is dilute. Though the form of the coefficients of the fluidmechanical equations is not known in the dense case, we demonstrate that the structure of the solution can be determined independently of that form if the system is dilute on average (that is, if the spheres were distributed uniformly they would form the dilute gas). The IS in this case consists of the gas phase that occupies the volume's fraction close to unity and the liquid phase that occupies the remaining volume. The liquid phase produces effectively a wall boundary condition for the gas where the wall is located at the boundary between the phases.

This structure of the IS in the dense case is indicating strongly that it is stable. Indeed, the gas phase is locally stable in view of the stability of the dilute IS that was proved numerically. The liquid phase is locally stable too because the excluded volume effects do not allow significant growth of the density in the liquid state. Thus the IS is stable locally. If to discard the unlikely possibility of nonlocal mechanism of instability (note that the mechanism of instability of the HS is local $[11–15]$, then this completes the demonstration that the IS is the universal result of the long-time evolution in the channel.

The IS solutions considered in this work depend on one spatial coordinate only (we stress that microscopically the system is fully three or two dimensional), describing the physics of granular materials in channels. The IS solutions that depend on two or three variables exist too, so it is natural to pose the question of their role in situations where the fluid-mechanical flows depend on two or three coordinates, which is the situation of box geometry. Since the physics of the IS solutions consists of the balance of the Laplacian term describing heat conduction and local nonlinearity corresponding to the inelastic cooling, then the role of dimension should be important because it is important for the Laplacian. Recent numerical results indicate that in higher dimensions the ISs are unstable. The work of Ref. [\[21\]](#page-20-0) reports that two-dimensional fluid mechanics of granular gases produces finite-time singularities of density. This increases the importance of considering the dense ISs introduced in this work. Indeed, finite particles' size effects

will necessarily regularize the singularity of the density, cf. Ref. [\[20\]](#page-20-0). The corresponding study concerning whether the dense IS is the result of the long-time evolution of supercritical systems in the higher-dimensional case is a topic for future work.

It is assumed in our study that the initial conditions do not contain the solid-state phase and that the solid phase does not form in the system as a result of the evolution. This is reasonable due to the growth of the pressure in the liquid state. This guarantees the applicability of the fluid-mechanical description. It is to be stressed that the fluid-mechanical equations that we use are valid both in the dilute (gaseous) and in the dense (liquid) phases of the matter. Though the form of the coefficients (e.g., viscosity, heat conductivity, and equation of state) is not known precisely in the dense region, we succeed in dealing with the equations based on the separability of the dependence of the coefficients on the temperature and density that holds for hard-core particles. The result applies to the two-dimensional fluid of hard disks, too.

The following text is structured as follows. In the next section we derive the general form of the fluid-mechanical equations of the hard spheres that collide inelastically. We show that these equations have a particular scaling form that holds due to the absence of energy scale in the the hard spheres' interaction. In Sec. [III](#page-4-0) we derive the IS solutions of the fluid-mechanical equations and demonstrate their basic properties (that do not depend on the dimension). The following section introduces the time-dependent transformation of the fluid-mechanical equations that transform the IS to the time-independent solution of a system with no explicit time dependence, implying power-law behavior of the perturbations of the IS. In Sec. [V](#page-6-0) we provide the implicit form of the IS that depends on one spatial coordinate in terms of coefficients of the dense fluid. The next section provides the qualitative structure of the solution, which is relevant for the later consideration of the dense case. The following section describes the low-density limit of the IS not confined to the case of the dependence on one coordinate. The study of the IS of the dilute gas that depend on one coordinate only is performed in Sec. [VIII.](#page-8-0) Though this case was solved previously $[5,6]$, we provide the solution to stress its thermodynamic limit and to make the paper self-contained. The IS in the dilute case serves as the basis for the study of the IS in the dense case in Sec. [XI.](#page-15-0) Section [IX](#page-12-0) deals with introducing the Lagrangian form of the fluid-mechanical equations that is considerably more suitable for the numerical simulation. The latter is reported in Sec. [X.](#page-14-0) It is shown that the IS provide the result of the long-time evolution of initial conditions that are arbitrary. Section [XII](#page-18-0) discusses the recent conjecture on the finite-time singularity of the density of the dilute gas in the light of the dense IS obtained here. Finally, in the Conclusion, we discuss the implications of our results on the general study of the granular materials. Further questions risen by our results are considered.

II. FLUID MECHANICS OF DENSE COLLECTIONS OF INELASTICALLY COLLIDING HARD SPHERES

The fluid of elastic hard spheres has an exceptional feature that in the equilibrium the only energy scale is the temperature *T* (in usual fluids there is an energy scale that characterizes the

interactions). Thus, the intensive quantities, like the pressure *p* or the thermal conductivity κ (determined by the equilibrium properties via the Kubo formula), are determined completely by the density $ρ$, the particles' diameter $σ$, and T (we set the particles' mass equal to 1 with no loss). The only one of those quantities that contains the units of time is T . This allows us to use the dimensional analysis to determine uniquely the dependence of the intensive quantities on *T* . In this way, one fixes the temperature dependence in the constitutive equations for the functions that appear in the fluid-mechanical equations.

The inelasticity described by the dimensionless constant coefficient of the normal restitution r does not introduce a new energy scale. This is a unique property of the considered model of the inelasticity, while other models typically contain an energy scale characterizing the inelastic part of the interactions. Thus, the equations of hydrodynamics of the granular fluid of hard spheres also have coefficients whereby the dependence on *T* is fixed for any density.

We now discuss the description of the fluid mechanics of inelastic hard-sphere fluids. This form holds both for the dilute gases and for the dense fluids. We assume that inelasticity is small, i.e., $1 - r \ll 1$. Only under this assumption can one use the fluid mechanics, at least in its traditional form, that assumes the local thermal equilibrium. When $1 - r \ll 1$ the local relaxation to equilibrium that happens within a local relaxation time *τ*rel is weakly influenced by the inelasticity. In particular, the inelastic energy depletion that happens within *τ*rel is small. Further evolution of the system consists of the evolution of the fields that describe the variation of the parameters of the local thermal equilibrium in space, i.e., the density $\rho(\mathbf{x},t)$, the velocity $v(\mathbf{x},t)$, and the temperature $T(\mathbf{x},t)$. The evolution of these fields is derived from the local balance of mass, momentum, and energy. The equations are obtained by expressing the latter and their currents via $\rho(x,t)$, $v(x,t)$, and $T(x,t)$. The inelasticity produces a local term in the energy equation that describes inelastic energy losses.

We now describe the equations. The inelasticity does not change the local laws of conservation of mass and momentum. Using isotropy and Galilean invariance, one finds the following general form of the fluid-mechanical equations [\[3,4\]](#page-20-0):

$$
\frac{\partial \rho}{\partial t} + \nabla \cdot [\rho \mathbf{v}] = 0, \quad \rho \left[\frac{\partial v_i}{\partial t} + (\mathbf{v} \cdot \nabla) v_i \right] = -\nabla_i p + \frac{\partial \sigma_{ik}}{\partial x_k},
$$

$$
\sigma_{ik} = \eta \left(\frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} - \frac{2}{d} \delta_{ik} \nabla \cdot \mathbf{v} \right) + \zeta \delta_{ik} \nabla \cdot \mathbf{v},
$$
(1)

where σ_{ik} is the viscous momentum flux (cf. Ref. [\[3\]](#page-20-0)), $d = 2$ corresponds to the case of hard disks, and $d = 3$ corresponds to the case of hard balls. Using the dimensional analysis we have the following general form of the intensive quantities *p*, *η*, and *ζ* :

$$
p = TF_1(\rho, r), \quad \eta = \sqrt{T}F_2(\rho, r), \quad \zeta = \sqrt{T}F_3(\rho, r), \quad (2)
$$

where $F_i(\rho, r)$ are certain functions. Though this is not necessary to demonstrate the IS, we use $1 - r \ll 1$ to set $r = 1$ in the equations above. It will be clear below that to the leading order in $1 - r$ the difference of r from 1 needs to be accounted for only in the energy-loss term. The reason is that this is the only term for which there is a degeneracy at $r = 1$, where it vanishes identically. Its smallness is compensated by the large time of evolution (however small, the inelasticity will produce the final state which completely differs from the $r = 1$ case). The rest of the terms in the equations have a finite limit at $r \to 1$, so their effect is perturbative. Below we define $F_i(\rho) \equiv F_i(\rho, r = 1)$.

The function $F_1(\rho)$ gives the pressure of the fluid of elastic hard spheres and can be expressed with the help of the free energy F_{free} of that fluid. For *N* particles,

$$
F_{\text{free}} = F_{\text{id}} + NTF(\rho),\tag{3}
$$

where F_{id} is the free energy of the ideal gas. The function $F(\rho)$ is determined by the configuration integral and its meaning is that it gives the deviation of the entropy per particle *s* from the one of the ideal gas,

$$
s = -\frac{1}{N} \left(\frac{\partial F_{\text{free}}}{\partial T} \right) = s_{\text{id}} - F(\rho), \tag{4}
$$

where *N* is the number of spheres and $s_{id} = \ln[T^{1/(\gamma-1)}/\rho] +$ const is the entropy per particle for the ideal gas. The function *F*(ρ) vanishes in the limit $\rho \rightarrow 0$ and its Taylor expansion starts from the linear term. For the equation of state one obtains

$$
p = \frac{\rho^2}{N} \left(\frac{\partial F_{\text{free}}}{\partial \rho} \right) = \rho T + \rho^2 F'(\rho) T, \tag{5}
$$

and thus we have

$$
F_1(\rho) = \rho + \rho^2 F'(\rho). \tag{6}
$$

To write down the remaining fifth equation of the fluid mechanics, we first write the equation for the usual fluid of elastic hard spheres and then introduce the energy-loss term due to inelasticity. The energy balance equation can be written in the form [\[3\]](#page-20-0)

$$
\rho T\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla\right) s = \sigma_{ik}\frac{\partial v_i}{\partial x_k} + \nabla \cdot [\kappa \nabla T],\tag{7}
$$

 $\sqrt{T} F_4(\rho)$ similarly to Eqs. [\(10\)](#page-4-0). where κ is the thermal conductivity. One can write $\kappa =$

For the fluid of inelastic hard spheres the pressure has a particular role. The fluid tends to make the pressure uniform, which makes it a convenient variable to work with. To pass from *s* to *p* we insert $\rho T = p/[1 + \rho F'(\rho)]$ into the expression for the entropy of the ideal gas s_{id} , which gives

$$
s = \frac{\ln p}{\gamma - 1} - \frac{\ln[1 + \rho F'(\rho)]}{\gamma - 1} - \frac{\gamma \ln \rho}{\gamma - 1} - F(\rho). \tag{8}
$$

Putting this into Eq. (7), with $\gamma = 5/3$ for the threedimensional fluid of hard balls and $\gamma = 2$ for the twodimensional fluid of hard disks and using the continuity equation, one finds

$$
\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla\right) p = -F_5(\rho) p \nabla \cdot \mathbf{v} + \frac{(\gamma - 1) F_1(\rho)}{\rho}
$$

$$
\times \left(\sigma_{ik} \frac{\partial v_i}{\partial x_k} + \nabla \cdot \left[\sqrt{T} F_4(\rho) \nabla T\right]\right), \quad (9)
$$

where $F_5(\rho)$ is defined by

$$
F_5(\rho) = \frac{\gamma + 2\gamma \rho F'(\rho) + \rho^2 F''(\rho) + (\gamma - 1)\rho^2 F'^2(\rho)}{[1 + \rho F'(\rho)]}.
$$
\n(10)

To include inelasticity one should introduce into the equation the energy-loss term where the form can be fixed by dimensional analysis. We obtain the following:

$$
\begin{aligned}\n&\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla\right) p \\
&= -F_5(\rho) p \nabla \cdot \mathbf{v} - \Lambda(\rho) \rho^{1/2} p^{3/2} \\
&+ \frac{(\gamma - 1) F_1(\rho)}{\rho} \nabla \cdot \left[\sqrt{\frac{p}{F_1(\rho)}} F_4(\rho) \nabla \left(\frac{p}{F_1(\rho)}\right) \right] \\
&+ \frac{(\gamma - 1) F_1(\rho)}{\rho} \sigma_{ik} \frac{\partial v_i}{\partial x_k},\n\end{aligned} \tag{11}
$$

where $\Lambda(\rho)$ tends to a positive constant Λ in the dilute limit [\[1\]](#page-20-0). The system of Eqs. (1) and (11) is the complete system of equations of the granular fluid of hard balls. This has a special dependence on the fields of *p* and *ρ*, where both the cooling and the thermal conductivity terms depend on *p* as $p^{3/2}$. It turns out that, based on this form only, one can find a new type of solution, compared to the usual fluid of elastic hard spheres, that holds due to the inelasticity.

III. INHOMOGENEOUS SOLUTIONS

We look for the solution to Eqs. [\(1\)](#page-3-0) and (11) that obeys $v \equiv$ 0. The continuity equation implies that these solutions describe a stationary distribution of particles in space, $\rho = \rho(\mathbf{x})$. The momentum equation gives that the pressure must be spatially uniform and it can depend only on time, $p = p(t)$. Finally, Eq. (11) under the assumption $\rho = \rho(\mathbf{x})$ and $p = p(t)$ can be written as follows:

$$
\frac{1}{p^{3/2}}\frac{dp}{dt} = -\Lambda(\rho)\rho^{1/2} + \frac{(\gamma - 1)F_1(\rho)}{\rho}\nabla \cdot \left[\frac{\tilde{F}_4(\rho)}{\sqrt{\rho}}\nabla \frac{1}{\rho}\right],\tag{12}
$$

where we defined $\tilde{F}_4(\rho) \equiv F_4(\rho) F'_1(\rho) \rho^{5/2} / F_1^{5/2}(\rho)$. Since the left-hand side of Eq. (12) by assumption is a function of time, while the right-hand side is the function of coordinate, then the solutions exist if both sides are equal to a constant −*c*, where minus is written for further convenience,

$$
\frac{1}{p^{3/2}}\frac{dp}{dt} = -c, \quad \frac{(\gamma - 1)F_1(\rho)}{\rho}\nabla \cdot \left[\frac{\tilde{F}_4(\rho)}{\sqrt{\rho}}\nabla\left(\frac{1}{\rho}\right)\right] -\Lambda(\rho)\rho^{1/2} = -c.
$$
\n(13)

Dividing the above equation by $F_1(\rho)/\rho$ and integrating over space we find

$$
c = \frac{\langle \Lambda(\rho)\rho^{3/2}F_1^{-1}(\rho)\rangle}{\langle \rho F_1^{-1}(\rho)\rangle}, \ \ \langle f\rangle \equiv \frac{1}{\Omega} \int_{\Omega} f(\mathbf{x}) d\mathbf{x},
$$

where Ω is the system volume, the angular brackets stand for spatial averages, and we assumed that either the heat flux vanishes at the boundary or that the periodic boundary

conditions hold, so the boundary terms vanish. We obtain that the pressure obeys the power-law

$$
p(t) = \frac{p(0)}{[1 + t/t_c]^2}, \quad t_c \equiv \frac{2\langle \rho F_1^{-1}(\rho) \rangle}{\langle \Lambda(\rho)\rho^{3/2} F_1^{-1}(\rho) \rangle p^{1/2}(0)}, \quad (14)
$$

where the density field obeys the nonlinear partial differential equation (PDE)

$$
\frac{(\gamma - 1)F_1(\rho)}{\rho} \nabla \cdot \left[\frac{\tilde{F}_4(\rho)}{\sqrt{\rho}} \nabla \left(\frac{1}{\rho} \right) \right] - \Lambda(\rho)\rho^{1/2}
$$

$$
= -\frac{\langle \Lambda(\rho)\rho^{3/2}F_1^{-1}(\rho) \rangle}{\langle \rho F_1^{-1}(\rho) \rangle}.
$$
(15)

Introducing

$$
K(\rho) \equiv -\int \frac{\tilde{F}_4(\rho)d\rho}{\rho^{5/2}}, \quad \nabla K = \frac{\tilde{F}_4(\rho)}{\sqrt{\rho}} \nabla \left(\frac{1}{\rho}\right), \quad (16)
$$

one can rewrite Eq. (15) in the form

$$
\nabla^2 K = f[\rho(K)],\tag{17}
$$

where $\rho(K)$ is the inverse function of $K(\rho)$ and

$$
f(\rho) \equiv \tilde{F}(\rho) - \frac{\langle \tilde{F}(\rho) \rangle}{[1 + \rho F'(\rho)] \langle [1 + \rho F'(\rho)]^{-1} \rangle}
$$

$$
\tilde{F}(\rho) \equiv \frac{\Lambda(\rho)\rho^{3/2}}{F_1(\rho)(\gamma - 1)}.
$$
(18)

The previous work $[5,6]$ characterized the solutions in the limit of the dilute gas where one can neglect the term with *F* and $\tilde{F}(\rho) \approx \Lambda \rho^{1/2} / (\gamma - 1)$ [where $\Lambda = \Lambda (\rho = 0)$]. One finds $f(\rho) \approx \Lambda[\langle \rho^{1/2} \rangle - \rho^{1/2}]/(\gamma - 1)$. Solutions in the dilute case that depend on one coordinate were worked out in detail in Ref. [\[5\]](#page-20-0), while the higher-dimensional case for the spherically symmetric situation in was considered in Ref. [\[6\]](#page-20-0). It is clear that there are nonspherically symmetric solutions that depend on two or three coordinates; however, the discussion of these solutions is beyond the scope of this work.

Studying the solutions in the dense case, one can consider the model equation of state $F'(\rho) = \pi g(\rho)/\sqrt{3}$ of Carnahan and Starling [\[22\]](#page-20-0) where

$$
g(\rho) = \frac{1 - 7\pi\rho/[32\sqrt{3}]}{(1 - \pi\rho/[2\sqrt{3}])^2}
$$
(19)

is the equilibrium pair correlation function of hard disks at contact (we use here units with $\sigma = 1$ and consider $d = 2$, the study of $d = 3$ is similar). The corresponding expression for the cooling coefficient $\Lambda(\rho)$ derived in Ref. [\[23\]](#page-20-0) in the spirit of Enskog theory is $\Lambda(\rho) = \Lambda g(\rho)$; thus

$$
\tilde{F}(\rho) = \frac{\Lambda g(\rho)\rho^{1/2}}{(\gamma - 1)[1 + \pi \rho g(\rho)/\sqrt{3}]}.
$$
 (20)

The simplest solution is the uniform solution $\rho = \rho_0$ where ρ_0 is a constant,

$$
p(t) = \frac{p(0)}{[1 + t/t_c]^2}, \quad t_c^{\text{unif}} = \frac{2}{\Lambda(\rho_0)\rho_0^{1/2}p^{1/2}(0)}.
$$
 (21)

This solution is the well-known HS in the dilute gas limit $\rho_0 \sigma^3 \ll 1$, where $\Lambda(\rho_0)$ tends to a constant $\Lambda \neq 0$, see

Ref. [\[11\]](#page-20-0). However, we could not find in the literature these solutions in the dense case, where $\rho_0 \sigma^3 \sim 1$ and $\Lambda(\rho_0)$ differs from appreciably. This solution is quite notable because $\Lambda(\rho) = \Lambda g(\rho)$ diverges when the density approaches the density of the dense packing, see Eq. [\(19\)](#page-4-0), so the cooling becomes infinitely fast. Further, while the instability of the uniform solutions for the gases is well known, see Refs. [\[12–](#page-20-0) [15\]](#page-20-0), there is no corresponding study for the dense fluid. It is clear, though, that the instability of perturbations with a large-enough wavelength (whereby its existence demands the system size to be sufficiently large), which was proved for the gases, holds for dense fluids, too, because the instability mechanism does not depend on the diluteness [\[12–15,24\]](#page-20-0). The study of the dependence of the critical length on ρ_0 in the dense case is left for future work. Here we confine the consideration to the dilute case where the total number of particles is such that $N\sigma^3/\Omega \ll 1$, which guarantees that the uniform state is unstable.

Thus for large system size the unstable uniform solutions have little practical value. However, there are also inhomogeneous solutions to Eq. (17) , see Ref. [\[6\]](#page-20-0). These can provide the final state of the fluid at large system size, see below and Ref. [\[5\]](#page-20-0), giving importance to their consideration. Before we discuss those solutions we consider the behavior of the energy and the entropy on the IS that can be found independently of the form of the density.

The thermal energy density is equal ρT (the one of ideal gas), so the total system's energy $E(t)$ obeys

$$
E(t) = p(t) \int \frac{d\mathbf{x}}{1 + \rho F'(\rho)} = \frac{E(0)}{[1 + t/t_c]^2},\qquad(22)
$$

where we used that the integral is a constant that can be fixed using the initial value of $E(t)$. We used that the system has no macroscopic kinetic energy. While the energy decay is necessary, whether the entropy decays or grows is less obvious. The energy losses cause the entropy to decrease, but the spatial inhomogeneity leads to the increase of entropy. We use that $s =$ $\ln[p^{1/(\gamma-1)}]$ plus a function of the density. Since the density in the IS is time independent, the entropy is then

$$
S(t) = \int \frac{\rho \ln p}{\gamma - 1} dx + B = \frac{N \ln p(t)}{\gamma - 1} + B
$$

= $S(0) - \frac{2N \ln[1 + t/t_c]}{\gamma - 1}$, (23)

where B is a constant determined by $S(0)$. Thus the IS are the states for which the entropy decreases logarithmically to minus infinity as *t* grows. The system continuously organizes with chaotic disorder decreasing due to the energy decrease. Of course, as the fluid cools down, eventually the effective description breaks down as a physically realistic description so the physical entropy stays finite (when the inner degrees of freedom have energy comparable with the one of the translational degrees of freedom they will stop to be the energy sink described by inelasticity but will exchange energy with the translational degrees of freedom).

Finally, we consider the total number of particles' collisions $N_c(t)$ that occurred by the time *t*. By dimensional analysis, the local rate of collisions $\Gamma(t)$ obeys $\Gamma(t) = L(\rho)p^{1/2}$, where

L($ρ$) is a function of $ρ$. We find

$$
\frac{dN_c}{dt} = \int L(\rho)p^{1/2}dx = \frac{\text{const}}{1 + t/t_c},\tag{24}
$$

which simply says that the local rate of collisions is proportional to the typical relative velocity of the particle $T^{1/2}$. Integration yields

$$
N_c(t) = \text{const} \times t_c \ln[1 + t/t_c]. \tag{25}
$$

The number of collisions grows only logarithmically in time. The particles collide more and more rarely with time due to the decrease of their velocity.

It is observed that the decrease of the entropy is proportional to the number of collisions that occurred in the system,

$$
S(t) - S(0) = -\frac{2NN_c(t)}{\text{const} \times t_c(\gamma - 1)}.
$$
 (26)

Thus on the IS the entropy decreases by roughly the same quantity in each collision.

We showed in this section that the fluid-mechanical equations of dense granular fluids of hard spheres have exact solutions for which the pressure is spatially uniform and the generally inhomogeneous profile of the density exists in space. The solutions hold due to the special combination of scalings where the pressure is proportional to T , while both the cooling and the heat conduction scale as $T^{3/2}$. The density profile is preserved via the balance of inhomogeneous cooling and heat conduction which sum to a spatially independent value. Due to the robustness of this balance we expect that the IS are general and present also when $1 - r$ is not small and the fluid mechanics does not hold.

The decay of the pressure and of the energy in the IS obeys a universal power law with exponent 2 independently of the details of the density profile. The entropy decreases logarithmically in time and proportionally to the number of particle collisions that occurred in the system. The number of collisions $N_c(t)$ turns out to be the natural time variable in which to consider the evolution, as we now show. Below we use the arbitrariness in the choice of the initial moment of time to set $p(0) = 1$ in the IS.

IV. BEHAVIOR OF SMALL PERTURBATIONS OF THE IS

The system of Eqs. (1) and (11) admits a time-dependent transformation of variables such that in the new variables the system is still time independent. The unique property of this transformation is that the IS become time independent in the new variables. In particular, the transformation allows us to conclude that the linearized perturbations around the IS have a power-law behavior in time.

For an arbitrary constant *C*, we pass to the new functions ρ' , p' , and v' defined by

$$
p = \frac{p'}{[1 + Ct]^2}, \quad \rho = C^2 \rho', \quad v = \frac{v'}{C[1 + Ct]}, \quad (27)
$$

and the new space and time variables

$$
\tau = \ln[1 + Ct], \quad \frac{\partial}{\partial t} = \frac{C}{1 + Ct} \frac{\partial}{\partial \tau}, \quad x' = C^2 x. \quad (28)
$$

We have

$$
\frac{\partial \mathbf{v}}{\partial t} = \frac{1}{[1 + Ct]^2} \frac{\partial \mathbf{v}'}{\partial \tau} - \frac{\mathbf{v}'}{[1 + Ct]^2},\tag{29}
$$

$$
\frac{\partial p}{\partial t} = \frac{C}{[1 + Ct]^3} \frac{\partial p'}{\partial \tau} - \frac{2Cp'}{[1 + Ct]^3}.
$$
\n(30)

In the new variables the system of (1) and (11) becomes

$$
\frac{\partial \rho'}{\partial \tau} + \nabla' \cdot [\rho' \mathbf{v}'] = 0, \quad \rho' \left[\frac{\partial v_i'}{\partial \tau} - \mathbf{v}' + (\mathbf{v}' \cdot \nabla') v_i' \right] = -\nabla_i' p' + \frac{\partial \sigma_{ik}'}{\partial x_k'}, \quad \frac{\partial p'}{\partial \tau} - 2p' + \mathbf{v}' \cdot \nabla' p' \n= -F_5 (C^2 \rho') p' \nabla' \cdot \mathbf{v}' - \Lambda (C^2 \rho') \rho'^{1/2} p'^{3/2} \n+ F_6 (C^2 \rho') \left(\sigma_{ik}' \frac{\partial v_i'}{\partial x_k'} + \nabla' \cdot \left[\sqrt{\frac{p'}{\rho' [1 + \rho' F'(\rho')]}} F_4 (C^2 \rho') \nabla' \left(\frac{p'}{\rho' [1 + \rho' F'(\rho')]}\right) \right] \right),
$$

where

$$
\sigma'_{ik} = \sqrt{\frac{p'}{\rho'[1 + \rho' F'(\rho')]}} F_2(C^2 \rho') \left(\frac{\partial v'_i}{\partial x'_k} + \frac{\partial v'_i}{\partial x'_k} - \frac{2}{3} \delta_{ik} \nabla' \cdot \mathbf{v'} \right) + \sqrt{\frac{p'}{\rho'[1 + \rho' F'(\rho')]}} F_3(C^2 \rho') \delta_{ik} \nabla' \cdot \mathbf{v'}.
$$

Importantly, the IS solution is time independent in the new variables and reads as follows:

$$
\rho'(\mathbf{x}') = \frac{1}{C^2} \rho_0 \left(\frac{\mathbf{x}'}{C^2}\right), \quad C = \frac{c}{2}, \quad \mathbf{v}' = 0,
$$

$$
p'^{-1/2} = \frac{\langle F_6^{-1} (C^2 \rho') \Lambda (C^2 \rho') \rho'^{1/2} \rangle}{2 \langle F_6^{-1} (C^2 \rho') \rangle} = \text{const}, \quad (31)
$$

as can be verified from Eq. [\(15\)](#page-4-0) on ρ_0 . It should be noted that though the transformation allows for any value of *C*, different values of*C* do not generate new solutions. Rather they describe the generation of the new solutions using the translational invariance in time: The IS remain the solutions if *t* is changed to *t* plus a constant. For example, for $C = 1$, one recovers the previous solution with $p^{1/2}(0)$ such that $t_c = 1$.

The described transformation is useful for studying the behavior of small perturbations of the IS. There one can choose $C = 1/t_c$, so $\tau(t) = (\gamma - 1) [S(0) - S(t)] / (2N)$ is proportional to the change of the entropy. In the new variables the eigenmodes of the linearized operator that describes the behavior of small perturbations near the IS behave exponentially in time. Thus the behavior of the modes is a power law in physical time.

Clearly, $\tau(t)$ can also be taken as the number of collisions $N_c(t)$. Thus the IS are time independent in the rescaled fields when considered as a function of the number of collisions that occurred since the initial moment of time.

V. IS DEPENDING ON ONE COORDINATE

The density field in the IS obeys the nonlinear PDE [\(17\)](#page-4-0) [or [\(15\)](#page-4-0)] that must be solved either with von Neumann boundary conditions (that describe the demand that the heat does not flow through the boundary) or with periodic boundary conditions. It is not possible to find the solution without specifying the form of $f(K)$ except for the case where the density depends on one spatial coordinate *x* only. In this case Eq. [\(17\)](#page-4-0) describes one-dimensional mechanical motion where $f(K)$ is the force

(cf. the radially symmetric solution provided in [\[6\]](#page-20-0)),

$$
\frac{d^2 K}{dx^2} = -\frac{\partial U[\rho(K)]}{\partial K} = -\frac{\rho^{5/2} \partial_{\rho} U}{\tilde{F}_4(\rho)}[\rho = \rho(K)];
$$

$$
\partial_{\rho} U = -\frac{\tilde{F}_4(\rho) f(\rho)}{\rho^{5/2}} = \frac{\tilde{F}_4(\rho) \tilde{F}(\rho)}{\rho^{5/2}} - \frac{\tilde{F}_4(\rho) \langle \tilde{F}(\rho) \rangle}{\rho^{3/2} F_1(\rho) \langle \rho / F_1(\rho) \rangle}.
$$
(32)

One has

$$
U = \int \frac{\tilde{F}_4(\rho)\tilde{F}(\rho)}{\rho^{5/2}} d\rho - \frac{\langle \tilde{F}(\rho) \rangle}{\langle \rho/F_1(\rho) \rangle} \int \frac{\tilde{F}_4(\rho)d\rho}{\rho^{3/2}F_1(\rho)}. \quad (33)
$$

It follows that the "energy"

$$
E \equiv \frac{1}{2} \left(\frac{dK}{dx} \right)^2 + U(\rho[K(x)]) = \frac{\tilde{F}_4^2}{2\rho^5} \left(\frac{d\rho}{dx} \right)^2 + U[\rho(x)]
$$

is conserved. This can be verified directly from the onedimensional version of Eq. [\(15\)](#page-4-0),

$$
\frac{d}{dx}\left[\frac{\tilde{F}_4(\rho)}{\rho^{5/2}}\frac{d\rho}{dx}\right] = f(\rho). \tag{34}
$$

The resulting solution for $\rho(x)$ is implicitly given by

$$
x = \int \frac{\tilde{F}_4(\rho)d\rho}{\rho^{5/2}\sqrt{2[E - U(\rho)]}},
$$
\n(35)

where the constant of integration and *E* should be determined using the boundary conditions. The physical significance of solutions depending on one coordinate only is obtained by considering the evolution of the fluid in a long channel. Provided the channel is sufficiently narrow in the transverse direction it will remain macroscopically uniform in those directions due to the stabilizing action of the heat conduction that is dominant at small scales (the same mechanism makes the uniform cooling state stable for small systems). Thus for long channels the fluid-mechanical fields depend on *t* and *x* only. The solutions to Eq. (15) are natural candidates for the steady state of the system.

To perform the study of the IS and their role in the evolution of the system, it is necessary to have explicit expressions for the coefficients of the fluid mechanics of the fluid. The coefficients are known in the dilute limit, while in the case $\rho \sigma^3 \sim 1$, one has to use certain approximations. Since the understanding is lacking in the case of the dilute gas already, then below we study if the IS provide the long-time state of the system in the case of the dilute granular gas in the long channel. Later we use this result to demonstrate the stability of the IS in the dense case, too.

In the case of the dilute gas one can write down the IS and the fluid-mechanical equations explicitly. While the ISs form is known in the case of the gas [\[5,6\]](#page-20-0), its stability is only known for channels of moderate length $L \ll l_{cr}/\sqrt{1-r}$ that correspond to the fast sound limit, see Ref. [\[5\]](#page-20-0) and below. Here πl_{cr} is the instability length that separates large systems where the uniform cooling state is unstable from the small ones where it is stable. In this work we settle positively the question whether the IS present the state of the gas at large times when *L* is large but not necessarily bounded by $l_{cr}/\sqrt{1-r}$.

In the limit of small density we have $\tilde{F}_4 \approx \kappa_0/(\gamma - 1)$, where κ_0 is the thermal conductivity of the dilute gas, $\tilde{F} \approx$ $\Lambda \rho^{1/2}/(\gamma - 1)$, where $\Lambda = \Lambda(\rho = 0)$. We find

$$
U = -\frac{\kappa_0 \Lambda}{(\gamma - 1)^2 \rho} + \frac{2\kappa_0 \Lambda \langle \rho^{1/2} \rangle}{3(\gamma - 1)^2 \rho^{3/2}},
$$

(ρ) = $\frac{2\kappa_0}{3(\gamma - 1)^2 \rho^{1/2}} = \left[\frac{2\kappa_0}{3\gamma} \right]^{1/3}$. (36)

$$
K(\rho) = \frac{2\kappa_0}{3(\gamma - 1)\rho^{3/2}}, \quad \rho^{1/2} = \left[\frac{2\kappa_0}{3K(\gamma - 1)}\right]^{1/3}
$$

We find that Eq. (32) becomes

$$
\frac{2\kappa_0}{3(\gamma-1)}\frac{d^2}{dx^2}\frac{1}{\rho^{3/2}}=\frac{\rho^{5/2}\partial_\rho U}{\tilde{F}_4(\rho)}=\frac{\Lambda[\rho^{1/2}-\langle\rho^{1/2}\rangle]}{(\gamma-1)}.
$$

The solution to this equation was found in Ref. [\[5\]](#page-20-0), where the consideration relied on the use of the mass coordinate frame. In the next section we describe the qualitative structure of the solution in the real space which will serve the basis for the study of the dense case. The quantitative description that reproduces the results of Ref. [\[5\]](#page-20-0) together with further details relevant to this work is performed in Sec. [VIII.](#page-8-0)

VI. QUALITATIVE STRUCTURE OF THE IS IN ONE-DIMENSIONAL CASE

In this section we describe qualitatively the IS in the dilute one-dimensional case. Note that the study is quite similar to the consideration of soliton solutions in nonlinear physics. We use that

$$
\frac{d^2K}{dx^2} = -\frac{\partial U}{\partial K},
$$

\n
$$
U = \left(\frac{2}{3}\right)^{1/3} \frac{\Lambda \kappa_0^{1/3}}{(\gamma - 1)^{4/3}} \left[K\left(K^{-1/3}\right) - \frac{3K^{2/3}}{2}\right]
$$

is identical in form to the Newton law of motion, where *x* is "time" and $K(x)$ is the "coordinate." We consider the behavior of $U(K)$ in the physically allowed domain of variation of K which is $K \geqslant 0$. The potential has a minimum at

$$
K_0 = \langle K^{-1/3} \rangle^{-3}
$$
 which is negative, $U(K_0) < 0$. We have

$$
U \approx -\left(\frac{2}{3}\right)^{1/3} \frac{\Lambda \kappa_0^{1/3}}{(\gamma - 1)^{4/3}} \frac{3K^{2/3}}{2}, \quad 0 < K \ll K_0;
$$
\n
$$
U \approx \left(\frac{2}{3}\right)^{1/3} \frac{\Lambda \kappa_0^{1/3}}{(\gamma - 1)^{4/3}} K \langle K^{-1/3} \rangle, \ K_0 \ll K.
$$

The uniformly cooling solution corresponds to the particle fixed in the minimum of the potential $K(x) \equiv K_0 = \langle K \rangle$. The IS result from considering the finite periodic motion of the particle between the smaller and larger solutions $K_1(E)$ and $K_2(E)$ of the equation $E = U[K]$, where $U(K_0) < E < 0$,

$$
x = \int_{K}^{K_2(E)} \frac{dK'}{\sqrt{2[E - U(K')]}},
$$

where the origin is chosen so the minimum of the density ρ , which corresponds to the maximum $K_2(E)$ of K, is at $x = 0$. When *E* is slightly larger than $U(K_0)$ the motion is harmonic, so its period is finite. When *E* increases, the period of the motion increases, becoming infinite when *E* tends to zero from below. The period becomes infinite because $K_0 \propto \langle \rho^{1/2} \rangle^{-3} \propto$ $L^{3/2}$ diverges in the thermodynamic limit; see the computation in the next sections. Since $K_2(E = 0) = 27K_0/8$, then the period's divergence occurs due to the square-root divergence of the integral in Eq. [\(59\)](#page-10-0) at large *K*.

The physical solution is determined from the condition that half the period of the periodic motion is equal to the size of the channel *L*,

$$
L = \int_{K_1(E)}^{K_2(E)} \frac{dK'}{\sqrt{2[E - U(K')]}}.
$$

Here we consider the no-heat-flux boundary conditions (b.c.) within which $\rho'(x)$ vanishes at the ends of the channel, implying that $K'(x)$ is also zero there (thus the ends of the channel correspond to the turning points in the solution). The solutions obtained by considering the full period of the motion (or any integer number of half-periods) obey the b.c., too, but they are not stable, see Ref. [\[5\]](#page-20-0) and below.

Thus the IS exists for the channel length in the interval $L_{\text{min}} < L < \infty$, where L_{min} corresponds to the finite period of the harmonic motion near the minimum of the oscillator $(L_{\text{min}} = \pi l_{\text{cr}}$, see Ref. [\[5\]](#page-20-0) and the next section). The density grows monotonously from its minimum at $x = 0$ to the maximum at $x = L$. In the thermodynamic limit the minimum tends to zero (corresponding to divergence of $K_2[E = 0]$), while the maximum tends to infinity (corresponding to $K_1[E = 0] = 0$). In particular, the dilute gas assumption breaks down in the thermodynamic limit. The resulting changes in the solution and omitted details are provided in the following sections.

VII. IS EQUATIONS IN THE DILUTE GAS LIMIT

In the limit of small density the fluid-mechanical equations take a simpler form, where the viscosity coefficients and the thermal conductivity become proportional to \sqrt{T} , while Λ

becomes a constant. Using Eq. (10) , we find

$$
\frac{\partial \rho}{\partial t} + \nabla \cdot [\rho \mathbf{v}] = 0,
$$
\n
$$
\rho \left[\frac{\partial v_i}{\partial t} + (\mathbf{v} \cdot \nabla) v_i \right] = -\nabla_i p + v \frac{\partial}{\partial x_k} \left[\sqrt{\frac{p}{\rho}} \left(\frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} - \frac{2}{d} \delta_{ik} \nabla \cdot \mathbf{v} \right) \right],
$$
\n
$$
\left(\frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right) p = -\gamma p \nabla \cdot \mathbf{v} - \Lambda \rho^{1/2} p^{3/2} + \frac{2\kappa_0}{3} \nabla^2 \left(\frac{p}{\rho} \right)^{3/2} + (\gamma - 1) v \sqrt{\frac{p}{\rho}} \left[\frac{\partial v_i}{\partial x_k} \frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} \frac{\partial v_i}{\partial x_k} - \frac{2}{d} (\nabla \cdot \mathbf{v})^2 \right],
$$
\n(37)

where $\Lambda = 2\pi^{(d-1)/2}(1 - r^2)\sigma^{d-1}/[d\Gamma(d/2)]$ (see, e.g., Ref. [\[24\]](#page-20-0)), $\Gamma(\dots)$ is the gamma function, $\nu = (2\sigma \sqrt{\pi})^{-1}$ and *κ*₀ = 4*ν* in *d* = 2, and *ν* = 5(4*σ*²√*π*)⁻¹ and *κ*₀ = 5*ν/*2 in $d = 3$ [\[1\]](#page-20-0).

Equations (37) differ from the fluid mechanics of a dilute gas of *elastically* colliding spheres only by the presence of the inelastic loss term $-\bar{\Lambda} \rho^{1/2} p^{3/2}$ which is proportional to the average energy loss per collision, $\sim (1 - r^2)p$, and to the collision rate, $\sim \rho^{1/2} p^{1/2}$ (note that *p* = ρT , where *T* is the temperature). As discussed above, the inequality $1 - r \ll 1$ guarantees that the characteristic cooling time $1/\Lambda \rho^{1/2} p^{1/2}$ inferred from the equation on pressure is much larger than the mean free time $1/(\sigma^{d-1} \rho^{1/2} p^{1/2}).$

As already mentioned, the system of Eqs. (37) has wellknown homogeneous cooling solutions [\[11\]](#page-20-0). These solutions are described by Eqs. (21) with the cooling time t_c provided by the reduced expression

$$
t_c \equiv \frac{2}{\Lambda \rho_0^{1/2} p^{1/2}(0)}.\tag{38}
$$

The solutions are known to be unstable with respect to the sinusoidal perturbations where wave vector *k* is smaller than $1/l_{cr}$ and the critical length l_{cr} is given by

$$
l_{\rm cr} = \sqrt{\frac{2\kappa_0}{\Lambda \rho_0^2}},\tag{39}
$$

see Refs. [\[12–15\]](#page-20-0). Such wave vectors exist when the system size exceeds πl_{cr} for no-flux b.c. and when the system size exceeds $2\pi l_{cr}$ for periodic boundary conditions (p.b.c.). Small perturbations with large wavelength get enhanced and particles start to form clusters (the rotational modes that behave differently are not relevant for the present work). Correspondingly this instability is often called the clustering instability.

The length *l*_{cr} also has a special physical meaning with respect to the IS, see the previous section. For system size below πl_{cr} all the IS are homogenous, so the uniformly cooling states are the only states of the macroscopic rest of the system. In contrast, for larger system sizes, while the uniformly cooling state continues to hold, inhomogeneous solutions appear as well [\[5\]](#page-20-0). For no-flux b.c. the inhomogeneous solutions appear at system sizes greater than πl_{cr} , while for the p.b.c. they appear at system sizes greater than 2*πl*cr. This "coincidence" makes it natural to suggest that at these system sizes the inhomogeneous solutions become the attractors for the system's evolution in time instead of the uniform cooling states holding for subcritical systems. This was proved in the limit of fast sound $[5]$.

Finally, we present the equation on the density in the IS in the dilute limit. Setting $F_4 = \kappa_0$ in Eq. [\(15\)](#page-4-0) one finds

$$
\rho_0^{1/2} - \langle \rho_0^{1/2} \rangle - \frac{2\kappa_0}{3\Lambda} \nabla^2 \rho_0^{-3/2} = 0, \tag{40}
$$

while the pressure is given by Eq. (14) with $1/t_c =$ $\Lambda \langle \rho_0^{1/2} \rangle p^{1/2}(0)/2$. This equation and the numerical inhomogeneous solution for the spherically symmetric case were presented in [\[6\]](#page-20-0). The Cauchy-Schwarz inequality implies $\langle \rho_0^{1/2} \rangle \leq \langle \rho_0 \rangle^{1/2}$, so the energy decay for the inhomogeneous solutions is always slower than the one of the uniformly cooling state, see Eq. [\(21\)](#page-4-0).

The complete description of the solutions to the nonlinear PDE (40) is likely to be available only numerically. Thus, even in the limit of the dilute gas of inelastic hard spheres, neither the complete description of the IS nor the understanding of their relevance to the evolution of the system are available. The case that allows progress is the case of fields depending on only one spatial coordinate, to which we now turn. Though the solutions that we describe below were obtained previously [\[5,6\]](#page-20-0), their consideration is necessary here. This is because the thermodynamic limit was never considered in detail and because these solutions are needed to consider the dense IS.

VIII. IS DEPENDING ON ONE COORDINATE FOR DILUTE GRANULAR GAS

We now concentrate on the study of the solutions to Eq. (40) that depend only on the coordinate *x* and obey

$$
\frac{2\kappa_0}{3\Lambda} \frac{d^2}{dx^2} \rho_0^{-3/2} = \rho_0^{1/2} - \langle \rho_0^{1/2} \rangle.
$$
 (41)

This equation is relevant for long channels with length *L*, so it is considered in the interval (0*,L*). We consider two kinds of boundary conditions, where the solutions are slightly different—the p.b.c. and the no-heat-flux boundary condition. For the considered solution with the spatially uniform pressure the condition of no heat flux gives the condition of vanishing derivative of ρ_0 at the boundary. It is convenient to measure the density in the units of average density ρ_0 and the distance in the units of l_{cr} . We find that the rescaled density ρ' obeys in the new coordinate x' the following equation:

$$
\rho'^{1/2} - \langle \rho'^{1/2} \rangle' - \frac{1}{3} \frac{d^2}{dx^2} \rho'^{-3/2} = 0,
$$

$$
\langle \rho' \rangle' \equiv \frac{1}{\mathcal{L}} \int_0^{\mathcal{L}} \rho'(x') dx' = 1,
$$
 (42)

where the last condition follows from $\langle \rho' \rangle = 1$ and uniformity of ρ' in the transversal directions. The rescaled length $\mathcal{L} =$ L/l_{cr} of the channel is

$$
\mathcal{L} = \frac{L}{l_{\text{cr}}} = \begin{cases} (\sqrt{\pi}/2)(1 - r^2)^{1/2} \rho_0 \sigma L & \text{in 2D,} \\ \sqrt{16\pi/75} \left(1 - r^2\right)^{1/2} \rho_0 \sigma^2 L & \text{in 3D.} \end{cases}
$$
(43)

Equation [\(42\)](#page-8-0) and the solution to it were obtained in Ref. [\[5\]](#page-20-0). Here we reproduce the solution with the purpose of discussing its thermodynamic limit. It is convenient to pass to the mass coordinate

$$
m(x') \equiv \int_0^{x'} \rho(x'') dx'', \quad x'(m) = \int_0^m \frac{dm'}{\rho'(m')} , \quad (44)
$$

where the solution's interval of definition is the same interval $(0, \mathcal{L})$ since in the rescaled variables, the rescaled length of the channel $\mathcal L$ coincides with the rescaled total mass of the gas, $\int_0^L \rho'(x') dx'$, cf. Eq. [\(42\)](#page-8-0). In the mass coordinate frame the condition that the average density is 1, given by equation [\(42\)](#page-8-0), becomes the condition that the "average length" equals 1,

$$
\frac{1}{\mathcal{L}} \int_0^{\mathcal{L}} \frac{dm}{\rho'(m)} = \int_0^{\mathcal{L}} \frac{dx}{\mathcal{L}} = 1.
$$
 (45)

We obtain the following equation for $w \equiv \rho^{-1/2}$:

$$
\frac{d^2w}{dm^2} = w - w^2 \langle w \rangle_m, \tag{46}
$$

where the angular brackets with the subscript designate the "spatial" average over *m*. Equation (46) is defined on the interval $0 < m < L$, at the ends of which we demand a zero first derivative of *w*, which corresponds to the no-flux boundary conditions. To get rid of the (*a priori* unknown) factor $\langle w \rangle_m$, we introduce a new variable,

$$
f(m) = \langle w \rangle_m w(m), \tag{47}
$$

and obtain

$$
\frac{d^2f}{dm^2} = f - f^2.
$$
\n(48)

Integrating the above equation from 0 to \mathcal{L} , we find that, for both p.b.c. and no-flux b.c., the averages of f and f^2 coincide. Since $\langle f \rangle_m = \langle w \rangle_m^2$ and $\langle f^2 \rangle_m = \langle w \rangle_m^2 \langle w^2 \rangle_m$ we conclude that the condition of conservation of "average length" $\langle w^2 \rangle_m =$ 1 is obeyed automatically once the b.c. are imposed on *f* . After *f* is found, one can restore *w* via

$$
w = \frac{f}{\sqrt{\langle f \rangle_m}}.\tag{49}
$$

Equation (48) has appeared in numerous applications, and its solutions are well known. We consider *f* as a coordinate of a Newtonian particle of unit mass, moving in the potential $U(f) = f^3/3 - f^2/2$. The "total energy"

$$
E = \frac{1}{2} \left(\frac{df}{dm} \right)^2 + \frac{f^3}{3} - \frac{f^2}{2}.
$$
 (50)

is conserved. The boundary conditions can be obeyed only by bounded solutions with $-1/6 \le E \le 0$, where we can write

$$
\frac{f^3}{3} - \frac{f^2}{2} - E = \frac{(f - a[E])(f - b[E])(f - c[E])}{3}, \quad (51)
$$

where $a[E] > b[E] > c[E]$ are the real roots of the cubic polynomial that give the turning points of the trajectory where the velocity vanishes. Here we stressed that these roots are functions of the "energy" *E*. The no-flux b.c. condition demands that the "initial coordinate" *f* (0) and the "final coordinate" $f(\mathcal{L})$ are either *a* or *b* (since $c < 0$ these are the only physically meaningful turning points). The solutions obeying the p.b.c. can be obtained by gluing together the solutions with no-flux b.c., so $f(0) = f(\mathcal{L})$ is either *a* or *b*. Thus we first consider the solutions obeying the no-flux b.c. A bounded solution of Eq. (48) can be written as

$$
m(f) = \int_{f}^{a(E)} \frac{df'}{\sqrt{2E - 2f'^{3}/3 + f'^{2}}}.
$$
 (52)

This solution obeys $m[a(E)] = 0$ and $m'[a(E)] = \infty$ so the above solution satisfies the correct boundary condition at $m = 0$,

$$
\frac{df}{dm}|_{m=0} = 0.\tag{53}
$$

This solution is constructed so *f* (*m*) reaches its maximal value $a(E)$ at $m = 0$. The first positive zero m_1 of $f'(m)$ determined by (52) is given by

$$
m_1 = \int_{b(E)}^{a(E)} \frac{df'}{\sqrt{2E - 2f'^3/3 + f'^2}}.\tag{54}
$$

In particular, if we consider the "fundamental" solution with no zeros of $f'(m)$ at $0 < m < L$, then the "energy" $E(L)$ of the solution corresponding to length $\mathcal L$ is determined from

$$
\mathcal{L} = \int_{b[E(\mathcal{L})]}^{a[E(\mathcal{L})]} \frac{df}{\sqrt{2E(\mathcal{L}) - 2f^3/3 + f^2}},
$$
(55)

$$
= \sqrt{\frac{6}{a[E(\mathcal{L})] - c[E(\mathcal{L})]}} \mathbf{K} \left(\sqrt{\frac{a[E(\mathcal{L})] - b[E(\mathcal{L})]}{a[E(\mathcal{L})] - c[E(\mathcal{L})]}} \right),
$$
(56)

where the value of the integral and the definition of the complete elliptic integral $K(x)$ can be found in Ref. [\[25\]](#page-20-0). The choice of the initial condition above corresponds to $f(m)$ that monotonously decreases from $f(0) = a[E(\mathcal{L})]$ to $f(\mathcal{L}) =$ $b[E(\mathcal{L})]$. The solution $f(m)$ for which $f(m)$ monotonously grows from $f(0) = b[E(\mathcal{L})]$ to $f(\mathcal{L}) = a[E(\mathcal{L})]$ can be obtained as f ($\mathcal{L} - m$), which gives

$$
\mathcal{L} - m(\tilde{f}) = \int_{\tilde{f}}^{a[E(\mathcal{L})]} \frac{df'}{\sqrt{2E(\mathcal{L}) - 2f'^3/3 + f'^2}}.
$$
 (57)

Using Eq. (55) we may also write

$$
m(\tilde{f}) = \mathcal{L} - \int_{\tilde{f}}^{a[E(\mathcal{L})]} \frac{df'}{\sqrt{2E(\mathcal{L}) - 2f'^3/3 + f'^2}}
$$

$$
= \int_{b[E(\mathcal{L})]}^{\tilde{f}} \frac{df'}{\sqrt{2E(\mathcal{L}) - 2f'^3/3 + f'^2}}.
$$
(58)

The above solution, of course, could also be obtained directly. The usefulness of this solution is that it being glued with the previous solution it gives the fundamental solution for the p.b.c. This solution is also as relevant for the evolution toward the IS as the previous solution.

Returning to Eq. [\(52\)](#page-9-0), using the formula from p. 234 of Ref. [\[25\]](#page-20-0) and the definition of the elliptic integral, we find

$$
\sqrt{\frac{a-c}{6}}m = \int_0^{\arcsin\sqrt{(a-f)/(a-b)}} \frac{d\alpha}{\sqrt{1 - \frac{(a-b)\sin^2\alpha}{a-c}}}
$$

Next, using the definitions from p. 924 of Ref. [\[25\]](#page-20-0), we find

$$
f(m) = c + (a - c) dn^2 \left(\sqrt{\frac{a - c}{6}} m, \sqrt{\frac{a - b}{a - c}} \right), \quad (59)
$$

.

where *dn* is one of the Jacobi elliptic functions. To write the solution for $w(m)$ we use the value of the integral from p. 644 of Ref. [\[25\]](#page-20-0),

$$
\langle f \rangle_m = c[E(\mathcal{L})] + (a[E(\mathcal{L})] - c[E(\mathcal{L})]) \frac{E(\sqrt{s[E(\mathcal{L})]})}{K(\sqrt{s[E(\mathcal{L})]})}
$$

$$
\equiv C^2(\mathcal{L}), \quad s[E(\mathcal{L})] \equiv \frac{a[E(\mathcal{L})] - b[E(\mathcal{L})]}{a[E(\mathcal{L})] - c[E(\mathcal{L})]}, \quad (60)
$$

where $E(x)$ is the complete elliptic integral of the second kind. The function $C(\mathcal{L})$ has a very important role for the IS because it determines the decay rate of the pressure for these solutions. We have

$$
\langle \rho_0^{1/2} \rangle = \bar{\rho}^{1/2} \frac{1}{\mathcal{L}} \int_0^{\mathcal{L}} \rho'^{1/2}(x') dx' = \rho_0^{1/2} \langle w \rangle_m
$$

= $\rho_0^{1/2} \langle f \rangle_m^{1/2} = \rho_0^{1/2} C(\mathcal{L}).$ (61)

It follows that the pressure for the IS is given by

$$
p(t) = \frac{p(0)}{[1 + t/t_c]^2}, \quad t_c \equiv \frac{2}{C(\mathcal{L})\Lambda \rho_0^{1/2} p^{1/2}(0)}.
$$

Thus $C(\mathcal{L})$ determines the deviations of the decay time from the decay time of the uniformly cooling state, and as we saw one must have $C(\mathcal{L}) \leq 1$ with equality holding only for uniformly cooling state. Finally, using Eqs. (49) and (52) , we write the solution for $\rho'(m)$ as follows:

$$
\frac{1}{\rho'(m)^{1/2}} = \frac{c + (a - c) \, \mathrm{d} n^2 \left(\sqrt{\frac{a - c}{6}} \, m, \sqrt{\frac{a - b}{a - c}} \right)}{C(\mathcal{L})}.\tag{62}
$$

We now consider solutions derivable from the fundamental solution above and the solutions' limits for different system sizes.

A. Periodic boundary conditions and solutions with multiple reflections

We constructed above the solution that is monotonic in $(0, \mathcal{L})$. We called this solution "fundamental" as the rest of the solutions can be obtained from it by gluing it to the reflected solution. If we reflect the above solution and glue it with $w(2\mathcal{L} - m)$ we get the fundamental periodic solution for the system with length $2\mathcal{L}$. Further application of reflections and gluing produce solutions with multiple reflections at the turning points. Numerical simulations indicate the the solution with the minimal possible number of the turning points is the one which is stable, cf. Ref. [\[5\]](#page-20-0). Thus for no-flux boundary conditions the solution that is stable is the fundamental solution described above, while for the p.b.c. the stable solution is the fundamental periodic solution described above.

B. The critical lower length for the existence of the IS

Clearly for any system size $\mathcal L$ there are solutions with $f = 1$ where the particle stands indefinitely at the potential minimum at $f = 1$. This is the uniformly cooling state described above. The inhomogeneous solutions correspond to the deviation of the particle from the minimum of the potential and these solutions have a minimal period corresponding to the harmonic expansion of the potential near the minimum. The existence of this minimal period signifies that inhomogeneous solutions exist only for $\mathcal L$ larger than a certain critical length. This length is fixed by considering $E = -1/6 + \delta E$, $0 < \delta E \ll 1$. In this limit, the effective "Newtonian" particle is a harmonic oscillator with $U(f) \approx -1/6 + (f-1)^2/2$. It follows that for no-flux b.c. the fundamental solution is $f(m) = 1 + \frac{f(m)}{m}$ $\sqrt{2\delta E}$ cos *m* and $w(m) = 1 + \sqrt{2\delta E}$ cos *m*, where we noticed $\langle f \rangle_m = 1$. These solutions exist only above the critical length $\mathcal{L} = \pi$ and are a small-amplitude sinusoidal modulation of the uniformly cooling state $w(m) = 1$. For the p.b.c. the solution has the same form and it exists above the critical length $\mathcal{L} = 2\pi$. The expressions for $E(\mathcal{L})$ can be obtained by considering the usual corrections to the independence of the period of the amplitude.

The sinusoidal solutions for slightly supercritical systems described above were checked numerically to provide the universal state of the gas after a long time of evolution. The description of the numerical results is provided later.

C. The IS in the thermodynamic limit

Our main interest here is the solution for large \mathcal{L} . At $\mathcal{L} \gg 1$ the correspondence between the energy E and length $\mathcal L$ is $|E| \approx 72 \exp[-2\mathcal{L}]$. This can be found by noting that at small $|E|$ we have $a \approx 3/2$, $b \approx \sqrt{2|E|}$, and $c \approx -\sqrt{2|E|}$. Using that at *z* close to unity

$$
K(z) = -\frac{1}{2}\ln(1-z^2) + \ln 4 + \dots,
$$
 (63)

where \dots vanish at $z = 1$, we find

$$
K\left(\sqrt{\frac{a-b}{a-c}}\right) \approx -\frac{1}{2}\ln\left(\frac{b-c}{a-c}\right) + \ln 4
$$

$$
\approx -\frac{1}{4}\ln|E| + \frac{1}{4}\ln 72. \tag{64}
$$

It follows from Eq. [\(56\)](#page-9-0) that the relation between E and $\mathcal L$ at large system size is $|E| = 72 \exp[-2\mathcal{L}]$. Note the difference of the factor of 2 from Ref. [\[5\]](#page-20-0): It arises due to the use of no-flux, rather than periodic, boundary conditions; see above.

Thus the thermodynamic limit of $\mathcal{L} \to \infty$ corresponds to $|E| \rightarrow 0$. To study this limit we consider the solution

$$
m(f) = \int_{f}^{a(E)} \frac{df'}{\sqrt{2E(\mathcal{L}) - 2f'^3/3 + f'^2}}.\tag{65}
$$

at $|E| \rightarrow 0$. In the lowest-order approximation we can set $E = 0$. We have

$$
m(f) = \int_{f}^{3/2} \frac{df'}{f'\sqrt{1 - 2f'/3}} = \ln\left(\frac{1 + \sqrt{1 - 2f/3}}{1 - \sqrt{1 - 2f/3}}\right).
$$
\n(66)

Inverting the above relation we obtain

$$
f = \frac{3}{2\cosh^2(m/2)}, \quad \mathcal{L} - m \gg 1,
$$
 (67)

where the condition follows from negligibility of the term *E* in the denominator of Eq. [\(65\)](#page-10-0). Due to $\mathcal{L} \gg 1$ the above asymptotic form covers almost all the interval $(0, \mathcal{L})$; however, there is a vicinity of $m = \mathcal{L}$ that is not described by Eq. (67). This approximation used to derive Eq. (67) becomes invalid as *f* approaches zero (*f* reaches *b* which is small), which is signalled by the divergence of $m(f)$ in Eq. [\(66\)](#page-10-0) at $f = 0$. To study the vicinity of $f = 0$ we write

$$
m(f) = \mathcal{L} - \int_{b(E)}^{f} \frac{df'}{\sqrt{2E(\mathcal{L}) - 2f'^3/3 + f'^2}}.
$$
 (68)

At $|E| \to 0$ we have $b(E) \approx \sqrt{2|E|} \to 0$, so considering $b(E) \leqslant f \ll 1$ we have

$$
\mathcal{L} - m(f) \approx \int_{\sqrt{2|E|}}^{f} \frac{df'}{\sqrt{f'^2 - 2|E(\mathcal{L})|}}
$$

$$
= \cosh^{-1} \frac{f}{\sqrt{2|E|}}.
$$
(69)

Using $\sqrt{2|E|} \approx 12 \exp[-\mathcal{L}]$ we find

$$
f \approx 12e^{-\mathcal{L}}\cosh(\mathcal{L}-m), \quad m \gg 1. \tag{70}
$$

where the condition $m \gg 1$ corresponds to $f \ll 1$. It is immediate from the expressions above that $\langle f \rangle$ is determined by $m \ll \mathcal{L}$ where one can use Eq. (67),

$$
C^2(\mathcal{L}) = \langle f \rangle \approx \frac{3}{\mathcal{L}},\tag{71}
$$

which can also be obtained directly by expanding Eq. [\(60\)](#page-10-0) at small $|E|$. We find that in the limit $\mathcal{L} \gg 1$, the pressure obeys

$$
p(t) = \frac{p(0)}{[1 + t/t_c]^2}, \quad t_c \equiv \frac{2\sqrt{L}}{\sqrt{3l_{cr}}\Lambda \rho_0^{1/2} p^{1/2}(0)}.
$$

We observe that the decay time grows with the system size in contrast to the uniformly cooling state having decay time which is local. This behavior can be traced to the power law $\rho(x) \propto (L - x)^{-1}$ that holds in a wide region of scales. This law would diverge in a nonintegrable way at $x = L$. Thus the integral for the mass $\int \rho(x) dx$ is determined by the right cutoff of $(L - x)^{-1}$ near $x = L$. In contrast $\int \rho^{1/2} dx$, which determines the decay time, converges at $x = L$, so it is determined by the left cutoff of the $(L - x)^{-1}$ law producing $\int \rho^{1/2} dx \sim L^{1/2}$, which corresponds to $\langle \rho^{1/2} \rangle \propto L^{-1/2}$.

Thus the IS are solutions where the system acts as a single whole so local measurements would be affected by the global structure of the solution. For *w* we find

$$
w \approx \frac{\sqrt{3\mathcal{L}}}{2} \frac{1}{\cosh^2(m/2)}, \quad \mathcal{L} - m \gg 1,
$$

$$
w \approx \sqrt{48\mathcal{L}} e^{-\mathcal{L}} \cosh(\mathcal{L} - m), \quad m \gg 1.
$$
 (72)

The two of the above asymptotic expressions overlap in the wide interval and together they cover $(0, \mathcal{L})$ completely. For the density $\rho' = w^{-2}$ we have

$$
\rho' \approx \frac{4}{3\mathcal{L}} \cosh^4(m/2), \quad \mathcal{L} - m \gg 1,\tag{73}
$$

$$
\rho' \approx \frac{e^{2\mathcal{L}}}{48\mathcal{L}\cosh^2(\mathcal{L} - m)}, \quad m \gg 1. \tag{74}
$$

In the joint asymptotic region the density grows exponentially according to $\rho' \approx \exp[2m]/12\mathcal{L}$.

In the thermodynamic limit $\mathcal{L} \gg 1$ the solution for ρ' is determined by Eq. (73) . Indeed, the mass coordinate gives directly the mass of the gas described by the corresponding asymptotic expression. The condition $\mathcal{L} - m \gg 1$ signifies that, in the thermodynamic limit, a fixed, arbitrarily close to unity, fraction *y* of the mass of the gas that obeys $\mathcal{L}(1 - y) \gg 1$ is described by the asymptotic expression (73) . To write the corresponding expressions in real space we use the inverse transformation $x'(m)$ from Eq. [\(44\)](#page-9-0). We find

$$
x' = \frac{3\mathcal{L}}{2} \int_0^{m/2} \frac{dm'}{\cosh^4 m'} = \frac{3\mathcal{L}}{2} \left[\tanh\left(\frac{m}{2}\right) - \frac{\tanh^3\left(\frac{m}{2}\right)}{3} \right].
$$

Thus $w(x')$ is determined implicitly by

$$
\frac{2x'}{3\mathcal{L}} = \tanh\left(\frac{m}{2}\right) - \frac{\tanh^3\left(\frac{m}{2}\right)}{3},\tag{75}
$$

$$
\frac{2w}{\sqrt{3L}} \approx 1 - \tanh^2\left(\frac{m}{2}\right). \tag{76}
$$

This formula can be made explicit using the substitution $tanh(m/2) = 2 \sin \phi$. This solves explicitly the cubic polynomial in the first line, changing it into $x'/\mathcal{L} = \sin 3\phi$, so the distribution of mass in space obeys

$$
\tanh\left[\frac{m(x')}{2}\right] = 2\sin\left(\frac{\arcsin(x/\mathcal{L})}{3}\right),\tag{77}
$$

provided $\mathcal{L} - m(x') \gg 1$. We obtain

$$
m(x') \approx \frac{4x'}{3\mathcal{L}}, \quad x \ll \mathcal{L},
$$

$$
m(x') \approx \frac{1}{2} \ln \left(\frac{6\mathcal{L}}{\mathcal{L} - x'} \right), \quad \exp[-2\mathcal{L}] \ll 1 - \frac{x'}{\mathcal{L}} \ll 1, \tag{78}
$$

where we noted that the condition $\mathcal{L} - m(x') \gg 1$ gives $\mathcal{L} +$ ln[1 − *x'* / \mathcal{L}]/2 \gg 1 or 1 − *x'* / \mathcal{L} \gg exp[−2 \mathcal{L}]. It follows that the mass of the system concentrates in the neighborhood of \mathcal{L} , defined by $1 - x'/\mathcal{L} \ll 1$ (the mass in the region $(0, \mathcal{L}[1 - \epsilon])$ is proportional to $\ln 1/\epsilon$, which is negligible in comparison with the total mass $\mathcal L$ if $\mathcal L \gg \ln 1/\epsilon$, cf. below). Noting that $w/\sqrt{3\mathcal{L}+1/2} = \cos 2\phi$, we obtain in physical variables

$$
\rho(x) = \frac{4\rho_0 l_{\rm cr}}{3L} \left[2\cos\left[\frac{2}{3}\arcsin\left(\frac{x}{L}\right)\right] - 1 \right]^{-2},
$$

$$
1 - \frac{x}{L} \gg \exp\left[-\frac{2L}{l_{\rm cr}}\right],
$$
 (79)

where the condition is equivalent to $\mathcal{L} - m(x') \gg 1$. This formula is equivalent to the formula provided in Ref. [\[5\]](#page-20-0). Note that, as explained above, for large-enough $\mathcal L$ one can extend

the above expression to such *x'* that the mass fraction $m(x')/\mathcal{L}$ is close to unity and the expression describes the distribution of the major part of the mass of the gas. In fact, Eq. [\(79\)](#page-11-0) covers almost all gas length $(0, \mathcal{L})$, excluding the exponentially small vicinity of $x = \mathcal{L}$. Performing the expansion at $x/L \ll 1$ or $x/L \approx 1$ or directly differentiating $m(x')$, one obtains

$$
\rho(x) \approx \frac{4\rho_0 l_{\rm cr}}{3L}, \quad x \ll L/l_{\rm cr},
$$

$$
\rho(x) \approx \frac{\rho_0 l_{\rm cr}}{2(L - x)}, \quad \exp\left[-\frac{2L}{l_{\rm cr}}\right] \ll 1 - \frac{x}{L} \ll 1.
$$

It is illuminating to write the results in the form

$$
\rho(x) = \frac{4\rho_0 l_{\rm cr}}{3L} \left[2\cos\left[\frac{2}{3}\arcsin\left(\frac{x}{L}\right)\right] - 1 \right]^{-2}, \quad \rho \ll \rho_{\rm max},
$$

$$
\rho(x) \approx \frac{\rho_0 l_{\rm cr}}{2(L - x)}, \quad \frac{\rho_0 l_{\rm cr}}{L} \ll \rho(x) \ll \rho_{\rm max}.
$$
 (80)

This form shows clearly the behavior of the density. The density field has large variation in space, changing from its value $4\rho_0 l_{cr}/3L$ in the dilute phase at $x \ll L$ to $\rho \sim \rho_{max}$ in the vicinity of $x = L$. The interpolation between the two regions follows a power law $[L - x]^{-1}$.

The first of the equations above shows that the density has self-similar scaling in *L*: One has $\rho(x) = \tilde{F}(x/L)/L$. It is nonobvious how this form can describe mass that grows linearly with *L* (we keep ρ_0 constant) since $\int_0^{\mathcal{L}} \tilde{F}(x/L) dx/L$ would give an \mathcal{L} -independent quantity. The resolution to this apparent paradox is that Eq. (79) applies roughly up to $x =$ $L - L \exp[-2L]$ and the integral would diverge at $x = L$,

$$
\int_0^{\mathcal{L}-\mathcal{L}\exp[-2\mathcal{L}]} \frac{4dx'}{3\mathcal{L}} \left[2\cos\left[\frac{2}{3}\arcsin\left(\frac{x'}{\mathcal{L}}\right)\right]-1\right]^{-2}
$$

$$
\sim \int_0^{\mathcal{L}-\mathcal{L}\exp[-2\mathcal{L}]} \frac{dx'}{2\mathcal{L}-2x'} \sim \frac{1}{2}\ln\frac{2\mathcal{L}}{2\mathcal{L}\exp[-2\mathcal{L}]}\sim \mathcal{L}.
$$

We now show that in fact the domain $\rho \ll \rho_{\text{max}}$ contains the larger part of the system's mass, while the neighborhood of the maximum defined by $\rho \sim \rho_{\text{max}}$ contains mass of order one. This can be seen from Eq. (74) , which shows that the density decays away from the maximum exponentially. Thus $\rho'(m) \ll \rho'_{\text{max}}$ when $\mathcal{L} - m \gg 1$, say, $\rho' [m = \mathcal{L} - 3] \approx$ 4 exp[−6]*ρ*max - *ρ*max. Since the difference of the mass coordinates measures the mass in physical space, then we conclude that the mass contained in the region $\rho \sim \rho_{\text{max}}$ is of order 1. This mass is much smaller than the total "mass" $\mathcal L$ in the considered limit.

Finally, to describe the whole interval $(0, \mathcal{L})$, we use Eq. (74) , employing the relation between x' and m in the following form:

$$
\mathcal{L} - x' = \int_{m}^{\mathcal{L}} \frac{dm'}{\rho(m')}.
$$
 (81)

Confining the above expression to $m \gg 1$ we may use Eq. [\(74\)](#page-11-0) to find

$$
\mathcal{L} - x' = 48\mathcal{L}e^{-2\mathcal{L}} \left[\frac{\mathcal{L} - m}{2} + \frac{\sinh[2(\mathcal{L} - m)]}{4} \right].
$$
 (82)

The above expression together with Eq. [\(74\)](#page-11-0) determine implicitly the profile of the density in the region not covered by the previous asymptotic expressions. In the regions $m \gg 1$ and $\mathcal{L} - m \gg 1$ the above equation reproduces the power-law behavior of the density. In the region $\mathcal{L} - m \ll 1$, not captured by the previous results, we find

$$
\mathcal{L} - x = 48\mathcal{L}e^{-2\mathcal{L}}(\mathcal{L} - m). \tag{83}
$$

Using the above equation and Eq. (74) we find

$$
\rho \approx \frac{\rho_{\text{max}}}{\cosh^2[\rho_{\text{max}}(\mathcal{L} - x)]}, \quad \rho_{\text{max}} \equiv \frac{e^{2\mathcal{L}}}{48\mathcal{L}},
$$

$$
\rho_{\text{max}}(\mathcal{L} - x) \ll 1.
$$

Keeping above the cosh($\mathcal{L} - m$) term and not expanding it at $\mathcal{L} - m \ll 1$ is a matter of convenience. The above form makes it obvious that the density has a maximum whose width is inverse to the maximum.

To summarize, in the thermodynamic limit one can use Eq. [\(79\)](#page-11-0) in the major part of the system. This expression, however, would diverge at $x = \mathcal{L}$ in a nonintegrable way, and it needs to be cut off at the maximal density ρ_{max} . The latter grows exponentially with the system size, though the mass contained in the region $\rho \sim \rho_{\text{max}}$ is of order 1.

The indefinite growth of ρ_{max} with the system size shows that the consistent consideration of the thermodynamic limit cannot be made within the frame of the dilute gas approximation, even if the condition $\rho_0 \sigma^3 \ll 1$ is satisfied. The consideration demands studying the IS of the dense fluids introduced in the previous sections and their stability. Nevertheless, the first step to understanding the stability of the IS is to study that in the dilute gas approximation. Then, as described in the Introduction, this can be used to derive the stability of the dense IS. Thus we now discuss the analysis of the question whether the IS constitute the final state of the fluid in the dilute gas approximation.

IX. THE IS AS THE UNIVERSAL LONG-TIME LIMIT OF EVOLUTION

It was shown in Ref. [\[5\]](#page-20-0) that the IS is the attractor for the long-time evolution of the gas in the limit of fast sound. Within this limit the sound travel time through the system $t_s \sim L/\sqrt{T}$ is assumed to be much smaller than the characteristic time scale of the cooling $t_c \sim 1/\Lambda \rho_0 \sqrt{T}$, so $L \ll 1/\Lambda \rho_0$. Since $1/\Lambda \rho_0 \sim l_{cr}/\sqrt{1-r^2}$, then the fast sound limit is the case $L \ll l_{cr}/\sqrt{1-r^2}$. Thus the limit of the <u>fast sound</u> allows nontrivial values of $L \geq \pi l_{cr}$ only for $1/\sqrt{1-r^2} \ll 1$, which is a more restrictive inequality than the $1 - r^2 \ll 1$ needed for the validity of the hydrodynamic approach as such. Due to the assumption $t_s \ll t_c$, the pressure becomes uniform throughout the gas faster than any effects due to inelasticity take place. Thus the latter effects can be analyzed assuming they develop on the background of a uniform pressure. Clearly this limit does not allow us to address the thermodynamic limit $L \to \infty$.

Thus we study the system behavior in the thermodynamic limit, which is probably the most important physical question about the considered system. As we argued, for long channels the macroscopic fields depend on only one spatial coordinate *x*. The evolution of these fields is then described by the corresponding reduction of the system [\(37\)](#page-8-0) that reads

$$
\frac{\partial \rho}{\partial t} + \frac{\partial (\rho v)}{\partial x} = 0, \tag{84}
$$

$$
\rho \left(\frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} \right) = -\frac{\partial p}{\partial x} + v_0 \frac{\partial}{\partial x} \left(\sqrt{\frac{p}{\rho}} \frac{\partial v}{\partial x} \right), \quad (85)
$$

$$
\frac{\partial p}{\partial t} + v \frac{\partial p}{\partial x} = -\gamma p \frac{\partial v}{\partial x} - \Lambda \rho^{1/2} p^{3/2} + \kappa_0 \frac{\partial}{\partial x} \left[\sqrt{\frac{p}{\rho}} \frac{\partial}{\partial x} \left(\frac{p}{\rho} \right) \right]
$$

$$
+ v_0 (\gamma - 1) \sqrt{\frac{p}{\rho}} \left(\frac{\partial v}{\partial x} \right)^2.
$$
(86)

where $v_0 = 4v/3$ in $d = 3$ and $v_0 = v$ in $d = 2$. The system is considered for $0 < x < \mathcal{L}$ where $\mathcal{L} \equiv L/l_{cr}$ is the channel length L measured in the units of l_{cr} . The system should be supplied with the appropriate boundary condition. We will assume rigid, insulating walls when both particles and heat flux vanish, $v(x = 0) = v(x = L) = 0$ and $\partial_x T(x = 0) =$ $\partial_x T(x = L) = 0$, where the ideal gas relation $T = p/\rho$ should be used.

The above system needs to be solved at the average value of the three-dimensional density equal to 1. Since the density is uniform in transversal directions, then the average one-dimensional density is also 1,

$$
\frac{1}{\mathcal{L}} \int_0^{\mathcal{L}} \rho(x) dx = 1.
$$
 (87)

This equation is a constraint on the solutions. The thermodynamic limit corresponds to considering the limit $\mathcal{L} \to \infty$ at average one-dimensional density fixed at 1. We study if at large times the solutions to the above system tend to the IS,

$$
\rho = \rho_0 \left(\frac{x}{l_{\rm cr}}\right), \quad v = 0, \quad p(t) = \frac{p(0)}{\left[1 + C(\mathcal{L})t/t_c^0\right]^2}, \quad (88)
$$

where t_c^0 is the decay time of the uniformly cooling states and $\rho_0(x)$ is the IS's density profile. The convergence to the IS would signify that for the supercritical systems the density profile saturates at large times at an inhomogeneous profile,

$$
\lim_{t \to \infty} \rho(x, t) = \rho_0(x). \tag{89}
$$

For the pressure we would like to check the existence of the following limit:

$$
\lim_{t \to \infty} p(x,t) \left[1 + C(\mathcal{L})t/t_c^0 \right]^2 = p_0,
$$
\n(90)

with some effective constant p_0 . There is no need to check separately the corresponding convergence of the velocity as it is implied by the relations above.

Below we measure distances in the units of l_{cr} and times in the units of t_c^0 where instead of $p(0)$ one uses p_0 . Thus we assume that the IS is the attractor for the system evolution, so there is a certain value of p_0 , and we check the self-consistency of this assumption. We also consider dimensionless fields and measure density in the units of ρ_0 , velocity in the units of l_{cr}/t_c^0 , and pressure in the units of p_0 . Keeping with no ambiguity the original notation for the fields and the coordinates we find that the following dimensionless form of the system (84) – (86)

holds in $d = 3$,

*ε*1*ρ*

$$
\frac{\partial \rho}{\partial t} + \frac{\partial (\rho v)}{\partial x} = 0,
$$

\n
$$
e_{1}\rho \left[\frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} \right] = -\frac{\partial p}{\partial x} + \varepsilon_{2} \frac{\partial}{\partial x} \left[\sqrt{\frac{p}{\rho}} \left(\frac{\partial v}{\partial x} \right) \right],
$$

\n
$$
\frac{\partial p}{\partial t} + v \frac{\partial p}{\partial x} = -\gamma p \frac{\partial v}{\partial x} - 2\rho^{1/2} p^{3/2} + \frac{2}{3} \frac{\partial^{2}}{\partial x^{2}} \left(\frac{p}{\rho} \right)^{3/2}
$$

\n
$$
+ \varepsilon_{2} (\gamma - 1) \sqrt{\frac{p}{\rho}} \left(\frac{\partial v}{\partial x} \right)^{2}.
$$
 (91)

where $\varepsilon_1 = \kappa_0 \Lambda / 2$ and $\varepsilon_2 = 2 \nu \Lambda / 3$. Note that $\varepsilon_1 \sim \varepsilon_2 \sim 1$ $r^2 \ll 1$.

It is more convenient to study the solution ρ_0 and its attracting properties by using the mass coordinate frame. This is defined by the passage from coordinates $[x,t]$ to $[m(x,t),t]$ where

$$
m(x,t) = \int_0^x \rho(x',t)dx', \ \partial_t m + v \partial_x m = 0, \quad (92)
$$

where we used in the last equation that the gas velocity vanishes at the boundary $v(x = 0,t) \equiv 0$ [of course, also $v(x = \mathcal{L}, t) \equiv 0$. It follows from the above that the inverse transformation $x(m,t)$ is a Lagrangian coordinate,

$$
\frac{\partial x(m,t)}{\partial t} = v[x(m,t),t],\tag{93}
$$

which means simply that the end point of the interval $[0, x(m, t)]$ containing a given mass *m* moves with the fluid. The equations take a somewhat simpler form in [*m,t*] coordinates,

$$
\frac{\partial}{\partial t} \frac{1}{\rho} = \frac{\partial v}{\partial m},\tag{94}
$$

$$
\varepsilon_1 \frac{\partial v}{\partial t} = -\frac{\partial p}{\partial m} + \varepsilon_2 \frac{\partial}{\partial m} \left(\sqrt{p\rho} \frac{\partial v}{\partial m} \right),\tag{95}
$$

$$
\frac{\partial p}{\partial t} = -\gamma p \rho \frac{\partial v}{\partial m} - 2\rho^{1/2} p^{3/2} + \rho \frac{\partial}{\partial m} \left[\sqrt{p \rho} \frac{\partial}{\partial m} \left(\frac{p}{\rho} \right) \right].
$$

$$
+ \varepsilon_2 (\gamma - 1) \rho^{3/2} p^{1/2} \left(\frac{\partial v}{\partial m} \right)^2.
$$
(96)

By a transformation similar to the one described in Sec. [IV](#page-5-0) we now discuss the variables in which the IS solution is time independent. We introduce fields p' and v' by

$$
p = \frac{p'}{[1 + C(\mathcal{L})t]^2}, \quad v = \frac{v'}{1 + C(\mathcal{L})t}, \tag{97}
$$

and the new time variable

$$
\tau = \frac{1}{C(\mathcal{L})} \ln[1 + C(\mathcal{L})t], \quad \frac{d\tau}{dt} = \frac{1}{1 + C(\mathcal{L})t}.
$$
 (98)

In the new field and variables the system takes the form

$$
\frac{\partial}{\partial \tau} \frac{1}{\rho} = \frac{\partial v'}{\partial m},
$$

$$
\frac{\partial v'}{\partial \tau} - \varepsilon_1 C(\mathcal{L}) v' = -\frac{\partial p'}{\partial m} + \varepsilon_2 \frac{\partial}{\partial m} \left(\sqrt{p' \rho} \frac{\partial v'}{\partial m} \right),
$$

*ε*1

$$
\frac{\partial p'}{\partial \tau} - 2C(\mathcal{L})p' = -\gamma p' \rho \frac{\partial v'}{\partial m} - 2\rho^{1/2} p'^{3/2} + \rho \frac{\partial}{\partial m} \left[\sqrt{p' \rho} \frac{\partial}{\partial m} \left(\frac{p'}{\rho} \right) \right].
$$
 (99)

The IS solution in these variables has a very simple form as follows:

$$
\rho = \rho_0(m), \quad p' = 1, \ v' = 0. \tag{100}
$$

These variables are significantly more convenient for numerical studies than the original variables for which the IS is time dependent. We have performed the numerical studies of the system of Eqs. (99). The studies of the thermodynamic limit $\mathcal{L} \rightarrow \infty$ appear impossible due to the exponential growth of the maximal density with the system size. We have succeeded in performing simulations up to the system size $\mathcal{L} = 8$. For this size the maximal density is about 23 100. We have observed that the IS is the global attractor of the system dynamics at large times. Further increase in the system size appears impractical within the frame of the direct numerical simulations. Say, for system size $\mathcal{L} = 9$, that the maximal density is already about 152 000. Clearly, a special device is needed to study the system's relaxation to the IS for the decade of $\mathcal{L} \gg 1$.

The simulations were performed for the no-flux boundary conditions. We used the value of $\gamma = 2$ of the two-dimensional gas and the values of $\varepsilon_1 = 1 - r^2$ and $\varepsilon_2 = (1 - r^2)/4$ for $r = 0.98$. This value of *r* does not give a large value of $1/\sqrt{1-r^2}$ and, consequently, there is no nontrivial region of applicability of the fast sound regime in this case. Thus no theoretical prediction on the relevance of the IS exists in this case. The simulations showed that for the supercritical systems with $\mathcal{L} > \pi$, the IS are stable attractors for $\mathcal{L} \le 8$. While the uniformly cooling state is the steady state of the system at $\mathcal{L} < \pi$, at $\pi < \mathcal{L} \le 8$, the place of the uniformly cooling state is taken by the IS. These states are both linearly and nonlinearly stable, that is, they are the universal attractors of the system evolution in time for arbitrary initial conditions. We now discuss the description of the results of the numerical simulations.

FIG. 1. The evolution of the density to ρ_0 for $\mathcal{L} = 4$. The plot of ρ_0 is marked by circles.

FIG. 2. The evolution of the density to ρ_0 for $\mathcal{L} = 6$. The plot of ρ_0 is marked by circles.

X. RESULTS OF THE NUMERICAL SIMULATIONS

The results of the simulations for the system's size $\mathcal{L} =$ 4, $\mathcal{L} = 6$, $\mathcal{L} = 7$, and $\mathcal{L} = 8$ are shown in Figs. 1[–4.](#page-15-0) The evolution clearly brings the initial conditions to the IS. The relaxation is exponential. In this section we use *t* instead of τ , so in physical time the relaxation is a power law.

The numerical simulations allow us to discuss the basic fact of the relaxation of the initial conditions to the IS (which, if it exists, is exponential by the equations), as well as the dependence of the relaxation exponent on \mathcal{L} . We studied the exponents of relaxation of the density and the pressure. The two exponents must correspond to the same eigenmode of the linearized operator described in the previous section and, hence, must be equal. This is confirmed by the results of the numerical experiments where the exponents coincide with the numerical accuracy.

The dependence of the exponent *λ* that describes the exponential relaxation to the IS at large times exhibits remarkably strong dependence on \mathcal{L} . The exponent does not change much from $\mathcal{L} = 4$ (where $\lambda \sim 0.42$) to $\mathcal{L} = 6$ (where

FIG. 3. The evolution of the pressure to unity for $\mathcal{L} = 4$.

FIG. 4. The evolution of the pressure to unity for $\mathcal{L} = 6$.

 $\lambda \sim 0.42$). However, at $\mathcal{L} = 7$ the exponent jumps to $\lambda \sim 40$ and at $\mathcal{L} = 8$ one has $\lambda \sim 60$. These numbers are given within an accuracy of 10 to 20% and they are not an artifact of a numerical problem: The decay fit to the exponential relaxation is extremely good as is clear from the figures (Figs. 5[–11\)](#page-16-0). Thus the decay exponent *λ* experiences a significant jump by about a factor of 10 as one passes from $\mathcal{L} = 6$ to $\mathcal{L} = 7$. This jump apparently signifies that between those values of $\mathcal L$ the system enters the asymptotic region of large sizes $\mathcal{L} \gg 1$ with the corresponding change of the functional dependence of *λ* on $\mathcal L$. The study of $\lambda(\mathcal L)$ at large $\mathcal L$ is beyond the current abilities of the numerical experiment and the explanation of the jump is postponed for future work. Here we would only like to establish the fundamental fact that the IS is the attractor of the system's evolution at large times.

XI. THE IS IN THE DENSE CASE

In this section we consider the IS in the dense case without presuming that $\rho \sigma^3 \ll 1$ holds everywhere. This is always the

FIG. 5. The evolution of the maximal density to the steady-state value for $\mathcal{L} = 4$. The best fit is $\rho_{\text{max}} = 12.3$ – 3 925 814 exp(−*t/*2*.*39).

FIG. 6. The evolution of the maximal density to the steady-state value for $\mathcal{L} = 6$. The best fit is $\rho_{\text{max}} = 551$ – 27 000 000 exp(−*t/*2*.*02).

case in the thermodynamic limit where the maximal density grows exponentially with the system size. The properties of the IS of the dilute gas that were derived in the previous sections show that the dilute gas assumption breaks down when the system size *L* obeys $\rho_{\text{max}} = \rho_0 l_{\text{cr}} \exp[2L/l_{\text{cr}}]/48L \sim \rho_p$, where $\rho_p \equiv \sigma^{-3}$ is of the order of the density of close packing. In this case in the region of maximal density the diluteness breaks down. We describe the resulting changes in the distributions of mass and energy throughout the system.

It is assumed that the total number of particles *N* obeys $N\sigma^3/\Omega = \rho_0 \sigma^3 \ll 1$ so, on average the fluid is still dilute (which is, in particular, the case of the clustering instability). Then the conservation of mass implies that the dense, liquid regions that form in the system occupy the volume's fraction that is much less than unity. It can be expected then that the ISs that hold in the dilute case will be changed so the dilute gas solution holds approximately in the interval $0 \le x \le l_g$ while

FIG. 7. The evolution of the maximal pressure to unity for $\mathcal{L} = 6$. The best fit is $p_{\text{max}} = 0.99953 - 2298 \exp(-t/2.44)$.

FIG. 8. The long-time exponential relaxation of the maximal pressure to unity for $\mathcal{L} = 7$. The best fit is $p_{\text{max}} = 1 + \frac{1}{2}$ 0*.*000 05 exp(−*t/*0*.*0227).

at $x \ge l_g$ the IS differs due to the density comparable with ρ_p . This is proved below. Note that $1 - l_g/L \ll 1$.

We use that the solution can be described by $K(x)$ that obeys

$$
\frac{d^2K}{dx^2} = -\frac{\partial U(K)}{\partial K},\tag{101}
$$

where $U(K) = U[\rho(K)]$ with

$$
U(\rho) = \int \frac{\tilde{F}_4(\rho)\tilde{F}(\rho)}{\rho^{5/2}} d\rho - \frac{\langle \tilde{F}(\rho) \rangle}{\langle \rho/F_1(\rho) \rangle} \int \frac{\tilde{F}_4(\rho)d\rho}{\rho^{3/2}F_1(\rho)},\tag{102}
$$

where $\rho(K)$ is a monotonically decreasing function of K. The corrections due to the finite size of the particles change the dilute gas relation [\(36\)](#page-7-0) for $U(K)$ at small $K \sim K(\rho_p)$. Further change in $U(K)$ is caused by the changes in the averages $\langle \hat{F}(\rho) \rangle$ and $\langle \rho / F_1(\rho) \rangle$ due to the deviation of the IS from the dilute gas solution. We demonstrate that the change in the

FIG. 9. The long-time exponential relaxation of the maximal density to the steady-state value for $\mathcal{L} = 7$. The best fit is $\rho_{\text{max}} =$ 3546 + 2*.*8565 exp(−*t/*0*.*0276).

FIG. 10. The long-time exponential relaxation of the maximal pressure to unity for $\mathcal{L} = 8$. The best fit is $p_{\text{max}} = 1 + \frac{1}{2}$ 0*.*000 03 exp(−*t/*0*.*0183).

latter is negligible. We observe that the ratio of the pressure to the pressure of the dilute gas $p/\rho T$ is a growing function of *ρ*. Thus $\rho/F_1(\rho) = \rho T/p \leq 1$. It follows that the integral of $\rho/F_1(\rho)$ over the yet-to-be-found solution is the integral over a positive function that equals 1 in almost all the volume except the dense region of the liquid where this function is bounded between zero and 1. We conclude that the contribution of the dense region in the integral can be neglected producing $\langle \rho / F_1(\rho) \rangle \approx 1$. Similarly, one can demonstrate that $\langle \tilde{F}(\rho) \rangle$ taken on the IS with dense regions is close to the one that would hold for the dilute gas. The reason is that in the case of the dilute gas where $\tilde{F}(\rho) \propto \rho^{1/2}$ the integral $\int \rho^{1/2}$ is determined by the dilute region far from the maximum (in which the liquid forms). This will be shown below using self-consistency.

Thus we can confine the consideration of changes in $U(K)$ due to the formation of the liquid to the consideration of the role of the changes in the functional form of $U(K)$ at small $K \sim K(\rho_p)$. First, we note that the functions that

FIG. 11. The long-time exponential relaxation of the maximal density to the steady-state value for $\mathcal{L} = 8$. The best fit is $\rho_{\text{max}} =$ $23\,040 + 14.3 \exp(-t/0.0156)$.

appear in the definition [\(102\)](#page-16-0) of $U(\rho)$ remain bounded and smooth when ρ approaches ρ_p . Consider first the function $\tilde{F}_4(\rho) \equiv F_4(\rho) F'_1(\rho) \rho^{5/2} / F_1^{5/2}(\rho)$ that appears both in $U(\rho)$ and the definition of $K(\rho)$. The heat conductivity of the fluid of hard spheres F_4 diverges in the limit of dense packed fluid like pressure F_1T ; see Ref. [\[26\]](#page-20-0) and also Refs. [\[27,28\]](#page-20-0). In contrast, the pressure described by $F_1 = p/T$ grows indefinitely when the fluid gets denser. To see the impact of this divergence we consider the most divergent term in the Carnahan-Starling equation of state,

$$
F_1(\rho)/\rho = 1 + \rho F'(\rho) = \frac{1}{[1 - \rho/\rho_p]^2},
$$

where the notation ρ_p is taken for clarity; see the definitions [\(19\)](#page-4-0) and [\(20\)](#page-4-0). We observe that though F_1 diverges at $\rho = \rho_p$, \tilde{F}_4 is still finite due to the division by $F_1^{5/2}$. We assume that the conclusion that $\tilde{F}_4(\rho)$ is finite holds for the true constitutive relation. Finally, \ddot{F} described by Eq. [\(20\)](#page-4-0) remains finite in the dense limit, too.

We conclude that the change in $U(K)$ caused by the finite density is finite. This change is such that $K = 0$ becomes a forbidden value of $K(x)$, so $K(x)$ cannot go to unphysical values smaller than $K(\rho_p)$. Further, we note that in the thermodynamic limit the energy *E* will still approach $E = 0$ since the divergence of the period of the particle's motion occurs in the region of large *K* or small density, see Sec. [VI](#page-7-0) (this follows from the fact that the major part of the volume is occupied by the dilute gas so the time that the particle spends at large *K* is infinite in the thermodynamic limit). Thus $U(K)$ has to increase at $K \sim K(\rho_p)$ so the smaller turning point at zero energy, defined by $U(K) = 0$, is given by a finite *K* of order $K(\rho_p)$. Correspondingly we assume that the change in $U(K)$ is such that it increases smoothly at $K \sim K(\rho_p)$ in comparison with the dilute gas value but remains monotonously decreasing. Note that the minimum of the potential is realized at K_0 that diverges in the thermodynamic limit and thus occurs at the density of the dilute gas, so the finite-density changes only the behavior of $U(K)$ at $K \ll K_0$, far from the potential's minimum. We assume that there is no new extremum of $U(K)$ at small *K* which seems physically necessary. Thus $U(K)$ decreases monotonously from $U[K(\rho_p)]$ to its minimum at $K = K_0$ where K_0 belongs to the dilute gas region.

It follows that the qualitative structure of the solution described in Sec. [VI](#page-7-0) is not changed by the finite particles' size. These changes become relevant when the energy *E* of the solution is such that the smallest positive solution to $E = U(K)$ is comparable with $K(\rho_p)$. They change the correspondence between *L* and *E*: the "particle" with coordinate $K(x)$ spends different times at small K. Thus we introduce $E_{\text{dense}}(L)$ as the dependence of *E* on *L* determined by the condition that the half the period of the periodic motion with energy $E_{\text{dense}}(L)$ equals *L*. The solution is given by

$$
x = \int_{K}^{K_2[E_{\text{dense}}(L)]} \frac{dK'}{\sqrt{2[E_{\text{dense}}(L) - U(K')]}}.
$$

It follows that in the region of the dilute gas where $U(K)$ is the same as in the dilute case, the solution is the same as in the dilute case. The only change is that instead of $E(L)$ that would correspond to the considered *L* in the dilute gas limit $\sigma \to 0$, one has to use $E_{dense}(L)$. Introducing $L_{eff}(L)$ by $E[L_{\text{eff}}(L)] = E_{\text{dense}}(L)$ [this is possible because both $E(L)$ and $E_{\text{dense}}(L)$ are monotonic] we can say that the solution in the dilute region is like that for the dilute gas with the effective length of the channel $L_{\text{eff}}(L)$.

Thus the solution in the dense case has the following structure. The density profile starts from its minimum at $x = 0$ where the dilute gas holds. The density increases monotonously like it would for the dilute gas in the channel with the length $L_{\text{eff}}(L)$ [note that $L_{\text{eff}}(L)$ tends to infinity in the thermodynamic limit]. Then, at a certain scale l_g , the dilute gas assumption breaks down, so in the region (l_g, L) the density obeys $\rho \sigma^{-3} \sim 1$. Since there is no sharp boundary between the phases, then *lg* is defined up to a factor of order 1, which will be seen inessential for the final result. The total mass m_g of the dilute gas in the region $(0, l_g)$ can be described by the formula [\(78\)](#page-11-0) with $L_{\text{eff}}(L)$ instead of L. The condition $m_g + m_l = \mathcal{L}$ that the total mass equals \mathcal{L} gives $(x_g = l_g/l_{cr})$

$$
\frac{1}{2}\ln\left(\frac{6\mathcal{L}_{\text{eff}}}{\mathcal{L}_{\text{eff}}-x_g}\right)+(\mathcal{L}-x_g)[c_l\rho_0\sigma^3]^{-1}=\mathcal{L},
$$

where $m_l = (\mathcal{L} - x_g)[c_l \rho_0 \sigma^3]^{-1}$ is the mass of the liquid contained in the region (l_g, L) with c_l a constant of order 1. Since m_g depends on L only logarithmically and $\rho_0 \sigma^3 \ll 1$, then we find that at large $\mathcal L$ (one divides the equation by $\mathcal L$ and takes the limit $\mathcal{L} \to \infty$)

$$
1 - \frac{l_g}{L} \approx c_l \rho_0 \sigma^3, \quad l_g \approx L(1 - c_l \rho_0 \sigma^3), \tag{103}
$$

that is, almost all the mass of the system is contained in the liquid phase. To determine m_g we note that since $\rho(l_g) \sim \sigma^{-3}$, then we can use for $\rho(l_g)$ the asymptotic form in Eq. [\(80\)](#page-12-0). This gives the self-consistency condition

$$
\rho_0(l_g) \approx \frac{\rho_0 l_{\rm cr}}{2(L_{\rm eff} - l_g)} \sim \sigma^{-3},
$$

which gives

$$
L_{\rm eff}-l_g \sim \rho_0 \sigma^3 l_{\rm cr}.
$$

Since $l_{cr} \ll l_g$, then $L_{eff} \approx l_g$, that is, the effective length of the channel is where the liquid phase starts. In other words, the beginning of the liquid phase is like a wall boundary condition for the gas. It follows that the mass of the gas phase is

$$
m_g \approx \frac{1}{2} \ln \left(\frac{6L}{\rho_0 \sigma^3 l_{\rm cr}} \right),
$$

where the approximate equality holds with logarithmic accuracy. Thus the mass of the gas is infinite in the thermodynamic limit; however, it is only logarithmically large in the system size, demonstrating that the gas represents a vanishing fraction of the total mass of the system.

The energy of the fluid is, however, determined by the gas phase and not by the liquid phase. Indeed, the energy density is given by $\rho T/(\gamma - 1)$. Throughout the region of the dilute gas, which occupies most of the volume, this coincides with $p(t)$ /(γ − 1). It follows that the energy density is uniform through most of the volume, deviating from the constant only in the liquid region. In the latter region the energy density can be written as $p(t) \rho/(\gamma - 1) F_1(\rho)$, so it is bounded from above by $p(t)/(\gamma - 1)$. We find that the total energy $E(t)$ obeys

$$
E(t) = \frac{p(t)\Omega}{\gamma - 1} \langle \rho / F_1(\rho) \rangle \approx \frac{p(t)\Omega}{\gamma - 1},
$$
 (104)

where we used $\langle \rho / F_1(\rho) \rangle \approx 1$ derived previously. It follows that in the considered case where the gas is dilute on average, $\rho_0 \sigma^3 \ll 1$, so the gas phase volume is close to Ω , we have that almost all the energy of the system is contained in the gaseous phase.

The conclusion that, though the liquid phase contains the fraction of the total mass that is close to unity, its energy is negligible, can be understood by noting that the temperature of the gas particles is much higher than that of the liquid ones. Consider, for example, $x \ll L$, where $\rho(x) \approx 4\rho l_{cr}/3L$, so the temperature there $T(x) \approx 3Lp(t)/4\rho l_{cr}$ grows linearly with the size of the system. Thus, though the gas particles are few in number, their velocity is so high that they provide a dominant contribution to the system's energy.

Finally, we consider the decay time of the solution t_c ,

$$
t_c \equiv \frac{2\langle \rho F_1^{-1}(\rho) \rangle}{\langle \Lambda(\rho)\rho^{3/2} F_1^{-1}(\rho) \rangle p^{1/2}(0)},
$$
(105)

see Eq. [\(14\)](#page-4-0). We observed previously that $\langle \rho F_1^{-1}(\rho) \rangle \approx 1$, so it remains to consider $\langle \Lambda(\rho)\rho^{3/2}F_1^{-1}(\rho)\rangle = (\gamma - 1)(\tilde{F})$. We saw previously that \tilde{F} remains finite in the dense region, and, hence, we can write

$$
\int_0^L \tilde{F} dx \sim \int_0^{l_g} \tilde{F} dx + c_l \rho_0 \sigma^3 L \tilde{F}(l_g), \qquad (106)
$$

where we used Eq. (103) and noted that continuity and finiteness of \tilde{F} imply $\tilde{F}(l_g) \sim \tilde{F}(L)$ (the latter is because the density throughout the liquid phase preserves its order of magnitude ρ_p). The first integral can be found using $\tilde{F}(x)$ in the dilute phase,

$$
\int_0^{l_g} \tilde{F} dx \approx \frac{\Lambda}{\gamma - 1} \int_1^{l_g} \frac{\rho_0^{1/2} l_{\rm cr}^{1/2} dx}{2^{1/2} (l_g - x)^{1/2}},
$$

where one can write approximate equality because the integral is determined by $x \ll l_g$, that is, $\langle \Lambda(\rho)\rho^{3/2}F_1^{-1}(\rho)\rangle$ is determined by *x* inside the dilute phase far from the boundary of the liquid. In particular, this implies that $\langle \Lambda(\rho)\rho^{3/2}F_1^{-1}(\rho)\rangle$ is approximately the same as for the dilute IS with *L*eff instead of *L*. Using that $L_{\text{eff}} \approx L$, we conclude that t_c coincides with the one of the dilute IS,

$$
t_c \approx \frac{2}{C(\mathcal{L})\Lambda \rho_0^{1/2} p^{1/2}(0)},
$$

$$
t_c \approx \frac{2\sqrt{L}}{\sqrt{3l_{cr}}\Lambda \rho_0^{1/2} p^{1/2}(0)}, \quad L \gg l_{cr}.
$$

Thus the result that t_c diverges in the thermodynamic limit is not changed by the finite particles' size effects. The liquid phase influences the solution in the dilute region only by a minor correction to the effective length of the channel (the wall becomes located not at the end of the channel but at the beginning of the liquid phase); hence, the uniform decay rate of the pressure which value can be found considering the dilute phase is approximately the same as in the dilute case.

The study assumes that the solid phase does not form in the system, so the fluid mechanics holds. Though this seems reasonable due to the growth of the pressure when the density becomes comparable with σ^{-3} , cf. Refs. [\[18–20\]](#page-20-0), this question has to be studied. It is left for the future work.

We conclude that for large system sizes the evolution is similar to the gas-liquid transition. If one starts with the uniform initial state of the dilute gas, the formation of dense regions starts due to the clustering instability. The system develops the IS where the liquid condenses in a small part of the total container that takes almost all the mass of the system. The larger fraction of the system's volume is occupied by the dilute gas. At the boundary between the two phases the no-heat flux b.c. holds approximately so the gas state is the same as would hold if the liquid would be the wall. Though the mass of the dilute gas is only logarithmic in the system size, the gas phase carries most of the energy of the system via the high velocity of its particles.

XII. FINITE-TIME SINGULARITY REGULARIZED BY THE IS

In recent work $[21]$ the numerical simulations of the fluid-mechanical equations (37) of the dilute granular gas was performed in two dimensions. The results indicate the possibility of the finite-time singularity. This is quite plausible physically since the heat conduction coefficient that counterbalances the nonlinear growth of the density due to cooling would tend to zero at such a presumed singularity. Indeed, if the pressure remains finite at the singularity, which seems to be the case, then the temperature tends to zero inversely proportionally to the growth of the density. Although in the one-dimensional case the heat conduction does stop the growth of the density, in the higher-dimensional case, where there are wider geometric possibilities for the formation of regions of growing density, this might be not the case. In fact, this is indicated by the analogy between the IS solutions and the soliton solutions of nonlinear physics. Within the latter there are cases where in dimensions higher than 1, the nonlinearity produces finite-time singularities that cannot be stopped by the Laplacian terms in the equations.

Thus the conjecture that the density of the dilute granular gas becomes singular in finite time when the container's geometry is a box (which is described by fluid mechanics of dimensions higher than 1) is reasonable. This increases further the relevance of our derivation of the IS in the dense case. The finite-time singularity signifies that the frame of the dilute granular gas is inconsistent in dimensions higher than 1, so physical factors not included into that frame have to be taken into account. The immediate factor is the finite size of the particles and the related excluded volume effects. It is clear that the fluid mechanics of (possibly) dense fluid of hard spheres, described by Eqs. (1) and (11) , does not have finite-time singularities, becoming then *the* only consistent framework of consideration in the higher-dimensional case. The IS solutions (including the uniform dense solution) become then highly important as the reference solutions on which further theoretical and experimental study can rely.

XIII. COMPARISON WITH THE STEADY STATES OF FORCED GRANULAR SYSTEMS

The formation of spatial profile of density via the interplay of heat flux and inelastic cooling displayed in the freely cooling granular system [\[5,6\]](#page-20-0) was discussed first for forced systems. In Ref. [\[7\]](#page-20-0) the steady state of the granular system heated at one of the walls was considered. In this case, due to the constant input of energy, the steady state is formed. The pressure is uniform, too, and the resulting equations on the density profile are quite similar to those considered in this work: These are Eqs. [\(13\)](#page-4-0) with $c = 0$. Since c^2 behaves inversely proportionally to the size *L* of the system, then one could think that in the thermodynamic limit $L \to \infty$ the states of the freely cooling and forced granular systems would coincide. This is further reinforced by quasistationarity of the freely cooling system holding in this limit.

In fact, the IS coincide with the steady states of forced system in the supercritical regime $L \gg l_{cr}$. It is readily seen that $\langle \rho_0^{1/2} \rangle^2 \sim \rho_0 l_{cr}/L$ so the last term in Eq. [\(41\)](#page-8-0) describing $c \neq 0$ can be dropped when $\rho \gg \rho_0 l_{cr}/L$. The resulting equation is solved by Eq. (80) . It coincides with the steady-state solution of Ref. [\[7\]](#page-20-0).

XIV. CONCLUSION

We described the IS states of the dense fluids of inelastically colliding hard-core particles. Though we used the fluid mechanics, the IS are not really fluid mechanical: They involve no flow. The inhomogeneity of the temperature is preserved by the balance of heat conduction and inhomogeneous inelastic cooling, cf. Refs. $[5-7]$.

The IS are exact solutions: They solve the complete system of the coupled PDE of the fluid mechanics of the system. Though the precise form of the coefficients of those equations is unknown in the dense region, we succeeded to demonstrate the IS using only the special separable form of those coefficients that holds for hard spheres with constant coefficient of normal restitution.

The fluid mechanics of fluid of hard balls in the dense region was used to describe the states of granular systems previously, see e.g., Refs. [\[7,28–30\]](#page-20-0). The studies involved the use of phenomenological relations in the dense region. We introduced in this work the way of dealing with the dense region exactly. Within this approach one relies only on the possibility to determine the temperature dependence of fluid-mechanical properties using the dimensional analysis. We demonstrated that the resulting scaling form of the fluid mechanics of hard balls admits the IS solutions. Our approach can be used then to refine the previous results.

The IS have universal properties that hold independently of the constitutive relations of the coefficients of the fluidmechanical equations. The pressure and the energy decay as $[1 + t/t_c]^{-2}$ while the number of collisions that occurred in the system and minus the entropy increase as $ln(1 + t/t_c)$. The only unknown characteristic of the IS is the form of the density field that does depend on the form of the coefficients. Thus the IS exhibit many universal properties that make one suggest that the displayed physical mechanisms can be important in other situations.

The characteristic decay time t_c in the power law $[1 +$ t/t_c ⁻² of inelastic cooling becomes infinite in the thermodynamic limit. The growth of the cooling time (that by itself is determined by the local density and temperature) with the system's size signifies that the whole system is strongly correlated. The existence of the nontrivial steady state in the dissipative system (the trivial one being the frozen particles) is unusual. It poses for study the question regarding whether self-organization and the minimization of the dissipation can be related in the considered case. Furthermore, we demonstrate that for supercritical systems, besides near the hot end of the system, the IS coincides with the true steady state of the system heated at that wall [\[7\]](#page-20-0). Thus the evolution of the free system tries to build the steady state of the forced one.

The IS solutions depend on the absence of the characteristic energy scale in the problem: The interaction of the hard spheres involves no energy scale. The IS would not exist as exact solutions for the finite interaction potential (instead of the infinite step potential of the hard spheres) that possesses a certain scale of energy or for inelasticity where its law changes at a certain scale of the energy. In the former case the coefficients of the fluid mechanics would have unknown dependence on the temperature, while in the latter case the coefficient of the inelastic energy-loss term would have unknown dependence on the temperature. Nevertheless, it seems that the considered model can describe realistically certain regimes of evolution of the granular media, arising as intermediate asymptotic regime.

We introduced a transformation that transforms the IS into the time-independent solutions of a system of PDE that does not depend on time explicitly. Thus there is natural "frame of the IS" where the solutions are stationary. This is done by using the time variable which is the number of collisions that occurred in the system and rescaling the fields with time to compensate for the decays due to inelasticity. In particular, the transformation shows that the linear perturbations near the IS obey the power-law behavior in time.

To consider the IS further we studied the dilute granular gas in the channel, where the fluid-mechanical fields depend only on the spatial coordinate along the channel (the microscopic motion is still three dimensional for balls and two-dimensional for disks). While the ISs in this case are known from previous works [\[5,6\]](#page-20-0), their stability was known only in the case of channelsthat are not too long. In the limit of large sizes the density field of the IS has large variation where it changes from a small value (that vanishes in the thermodynamic limit of infinite length of the channel) to a value ρ_{max} that is exponentially large in the channel's length. The interpolation between the two regions follows the inverse linear law. In the region of the power law the equations solve those of forced systems and the solution coincides with the one of the system heated at the higher temperature wall [\[7\]](#page-20-0). The mass contained in the neighborhood $\rho \sim \rho_{\text{max}}$ is of order 1. These solutions hold if the diluteness condition $\rho_{\text{max}}\sigma^3 \ll 1$ holds. When the length of the channel is fixed, this condition holds if the particles' diameter σ is small.

We showed numerically that the ISs provide the universal long-time limit of the evolution of the gas when the length of the channel exceeds the critical length l_{cr} . To consider the thermodynamic limit for finite-size particles, where dense liquid regions appear in the fluid, we demonstrated the phase separation in IS. In the limit of large system sizes, the fluid separates into the liquid phase, which contains most of the mass of system, and the gaseous phase, which contains most of the energy of the system and occupies the volume's fraction close to unity. Since there is local stability in both phases, then it follows that the IS is globally stable and constitutes the result of the long-time evolution of the system. Thus the question of the long-time limit of the granular gas is settled completely, though for a special geometry of the container.

An additional question posed by the parallel between the IS and the steady states of forced systems is the question regarding the marginal stability of the IS. The steady states of the forced systems can be unstable with respect to fluctuations of macroscopic fields depending on the transversal coordinate [30,31]. This question is left for further work.

Our study shows that the IS plays crucial role in the behavior of the granular fluid of hard spheres in the channel. However, there are higher-dimensional ISs that exist in any geometry of the container [6], posing the question regarding the IS relevance to the case where the fluid-mechanical fields depend on two or three spatial variables. The numerical works reported in Ref. [21] indicate that the dilute granular gas develops infinite density in finite time if the density depends on two coordinates. The ISs that take into account the excluded volume effects do not have such singularities and become important objects for the study of the evolution in the box geometry of the container. This study is left for future work.

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