# Kinetic temperature and pressure of an active Tonks gas

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Using computer simulation and analytical theory, we study an active analog of the well-known Tonks gas, where active Brownian particles are confined to a periodic one-dimensional (1D) channel. By introducing the notion of a kinetic temperature, we derive an accurate analytical expression for the pressure and clarify the paradoxical behavior where active Brownian particles confined to 1D exhibit anomalous clustering but no motility-induced phase transition. More generally, this work provides a deeper understanding of pressure in active systems as we uncover a unique link between the kinetic temperature and swim pressure valid for active Brownian particles in higher dimensions.

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#### I. INTRODUCTION

A fundamental model for understanding the behavior of liquids is the one-dimensional (1D) hard rod fluid or Tonks gas [1], where purely repulsive particles are confined to move in a 1D channel. The statistical mechanics of this system can be solved exactly, and many of its equilibrium properties are derivable in a closed analytical form [1–8]. There is a rich history in statistical physics of studying the Tonks gas and its variations to validate theories and approximation [9–16]. More recently, 1D models have achieved elevated importance as meaningful representations of physical systems, including the single-file diffusion of colloids in microfluidic channels, ion transport across cellular membranes, and the clustering of red blood cells in microcapillary flows [17–25].

Here, we focus on an active variant of the Tonks gas where active Brownian particles are restricted to move in a narrow channel. Active Brownian particles (ABPs) are a popular minimal model for self-propelled particles as their collective behavior captures many of the features exhibited by active suspensions [26–33]. Understanding the active Tonks gas is paramount, as many of the proposed applications of microscopic active matter will operate in highly confined environments. Examples include targeted drug delivery to specific cellular targets [34–36] and the autonomous exploration of porous media [37,38]. Also, active particles tend to accumulate on surfaces, leading to the formation of 1D boundary layers [39–48].

Surprisingly, there is little work exploring the role of pressure in 1D active systems. Nevertheless, pressure is critical in characterizing the behavior of active systems [49–61], and has aided in explaining a variety of phenomena, including motility-induced phase separation [62–72], active particle motion within vesicles and droplets [73–80] and the dynamics of passive colloidal structures in an active bath [81–99]. In this work, we introduce the concept of a kinetic temperature to aid in deriving an accurate analytical expression for the pressure of an active Tonks gas. Inspiration is taken from the study of granular matter, where a granular temperature can be defined to account for the inelastic nature of collisions [16]. We find excellent agreement between our analytical result and numerical simulation. In addition, we derive an exact relation between the kinetic temperature and the so-called swim pressure [52,65] valid for ABPs in any dimension. To conclude, we explain the unusual clustering observed in 1D active systems and the absence of a motility-induced phase transition.

## **II. MODEL**

To model the active Tonks gas or 1D-ABP system, we consider N purely-repulsive active Brownian disks confined to a periodic 1D channel of length L as shown in Fig. 1. An active force  $F_a = \gamma U_a \cos \theta$  is applied to each particle where  $\theta$  is the angle between the positive x axis and the particle's orientation vector,  $\gamma$  the translation drag coefficient, and  $U_a$  the constant self-propelling speed. All particles undergo rotational Brownian motion with a characteristic reorientation time  $\tau_R$ , where the particle's orientation vector is restricted to the 2D plane parallel to the channel. Thus, the motion of each particle is governed by the overdamped set of equations

$$v = \dot{x} = \gamma^{-1}(F_a + F_c) = U_a \cos(\theta) + \gamma^{-1}F_c,$$
 (1a)

$$\theta = \xi(t), \tag{1b}$$

where  $F_c$  is the interparticle force and  $\xi(t)$  is Gaussian white noise characterized by  $\langle \xi(t) \rangle = 0$  and  $\langle \xi(t) \xi(t') \rangle = (2/\tau_R) \delta(t - t')$ . We consider the limit where the effects of translational Brownian motion are nominal. The interparticle force  $F_c$  arises from a Weeks-Chandler-Anderson potential characterized by a potential depth  $\varepsilon$  and Lennard-Jones diameter  $\sigma$  [100]. As our active force is bounded, a sufficiently steep potential mimics a hard-particle interaction. A choice of  $\varepsilon/(F_a\sigma) = 100$  results in hard particle statistics with a particle length of  $\sigma_p = 2^{1/6}\sigma$ . Using

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FIG. 1. Schematic of 1D-ABP system. Each purely repulsive particle moves at a speed  $U_a \cos \theta$  while undergoing rotational Brownian motion with reorientation time  $\tau_R$ .

the HOOMD-blue software package [101], all simulations were conducted with 1000 particles and run for a minimum duration of 5000  $\sigma/U_0$ .

#### **III. RESULTS AND DISCUSSION**

Two dimensionless parameters describe the state of the purely-repulsive 1D-ABP system: the packing fraction  $\phi =$  $\rho \sigma_p$  where  $\rho = N/L$  is the particle line density and the dimensionless run-length  $\ell_0 = (U_a \tau_R) / \sigma$ . In the limit of small run-lengths, the behavior of the 1D-ABP system recovers that of the equilibrium Tonks gas. The emergent behavior that arises as run-length increases is the formation of large dynamic clusters. Cluster formation appears to be a universal feature of 1D active matter systems and has been previously observed in several studies [102-111]. To quantify cluster formation, we define an empirical measure of the degree of clustering  $\Theta = 1 - 1/\langle N_c \rangle$ , where  $\langle N_c \rangle$  is the average number of particles in a cluster and  $\langle ... \rangle$  denotes a time average. Here, particles are considered clustered when in contact (i.e., the separation distance is less than  $\sigma_p$ ). If there are predominately unclustered particles in the system  $\Theta \approx 0$ , while if all particles belong to a single cluster  $\Theta = 1 - 1/N \approx 1$ .

In Fig. 2(a), we plot the degree of clustering  $\Theta$  for the 1D-ABP system as a function of packing fraction  $\phi$  for different values of  $\ell_0$ . The degree of clustering increases with the packing fraction and approaches  $\Theta = 1$  at close-packing (i.e.,  $\phi = 1$ ). In the opposite limit as  $\phi \to 0$ , there is little clustering and  $\Theta \to 0$ . Yet, it is notable that  $\Theta$  can increase dramatically even at low packing fractions when  $\ell_0$  becomes large. In the Supplemental Material [112], we include movies from simulations illustrating the cluster dynamics at different run-lengths.

A notable observation for the 1D-ABP system is that particles' velocities are significantly reduced when clustered. To



• 0.1 • 0.2 • 0.5 • 1.0 • 2.0 • 5.0 • 10.0 • 20.0 • 50.0 is the axis

FIG. 2. (a) Degree of clustering  $\Theta$  and (b) reduced kinetic temperature  $\mathcal{T}_k$  as a function of packing fraction  $\phi$  for different run-lengths  $\ell_0$ .

quantify this reduction in particle speed, we define a reduced average translational kinetic energy:  $\mathcal{K} = K/K_0 = 2\langle v^2 \rangle/U_a^2$ , where *K* and *K*<sub>0</sub> are the kinetic energies of the interacting and ideal 1D-ABP system, respectively. It is worth noting the reduced average translation kinetic energy  $\mathcal{K}$  is closely related to the dissipation or irreversible energy loss typically defined in stochastic thermodynamics [113,114]. Interestingly, recent work has linked dissipation to the structure and transport properties of active liquids [115–117].

For the 1D-ABP system, it is easy to show from Eq. (1) that  $\mathcal{K} = 1 - 2\langle F_c^2 \rangle / (\gamma U_a)^2$ . The second term represents the reduction in kinetic energy due to interparticle collisions. In deriving  $\mathcal{K}$ , we use a unique property of ABPs, which we prove in the Supplemental Material [112], where  $\langle vF_c \rangle = 0$ . A consequence of this property is  $\langle F_a F_c \rangle = -\langle F_c^2 \rangle$  for all packing fractions, run-lengths, and system sizes. Remarkably, this property is not a result of 1D confinement, but the analog  $\langle v \cdot F_c \rangle = 0$  is also true for ABPs in higher dimensions.

For a 1D system in thermal equilibrium, the temperature T can be obtained by application of the equipartition theorem to give the well-known result  $k_BT = 2K/N$ , where  $k_B$  is the Boltzmann constant. In a similar spirit, we define a kinetic temperature for ABPs as  $T_k = 2K/N$ , resulting in a reduced kinetic temperature:

$$\mathcal{T}_{k} = \frac{T_{k}}{T_{0}} = 1 - \frac{2\langle F_{c}^{2} \rangle}{(\gamma U_{a})^{2}},$$
(2)

where  $T_0$  is the kinetic temperature of the ideal active system, and the second term is the relative reduction of the kinetic temperature due to collisions.

In Fig. 2(b), we plot  $\mathcal{T}_k$  for the 1D-ABP system. The reduced kinetic temperature decreases monotonically as the packing fraction increases and, in agreement with our previous observation, scales inversely with the degree of clustering shown in Fig. 2(a). At low packing fraction,  $\mathcal{T}_k$  approaches the ideal result, and at close-packing,  $\mathcal{T}_k$  tends to zero for all run-lengths. This temperature reduction or kinetic energy loss is a peculiarity of active Brownian systems. The inelastic nature of collisions reduces a particle's velocity during a collision and, in turn, temporarily removes kinetic energy from the system.

The utility of  $\mathcal{T}_k$  is that it can be related directly to the mechanical pressure. The total pressure for the 1D-ABP system is computed via the virial theorem as  $P = \rho \langle xF_{net} \rangle$  where  $F_{net} = F_a + F_c$  is the net force acting on a particle. Here, P is the average force the ABPs exert on the boundary. The two contributions to the total pressure P are the collisional pressure  $P_c = \rho \langle xF_c \rangle$  and the swim pressure  $P_s = \rho \langle xF_a \rangle$ . For convenience, we use an alternative yet equivalent expression for the swim pressure valid for ABPs known as the "active impulse" form given by  $P_s = \rho \langle vF_a \rangle \tau_R$  [118–120]. The pressure of the ideal 1D-ABP system is  $P_0 = \rho \gamma U_a^2 \tau_R/2$ , and the reduced swim pressure of the interacting system is

$$\mathcal{P}_{s} = \frac{P_{s}}{P_{0}} = 1 - \frac{2\langle F_{c}^{2} \rangle}{(\gamma U_{a})^{2}},$$
(3)

where we again use the relation  $\langle F_a F_c \rangle = -\langle F_c^2 \rangle$ . Upon comparison of Eqs. (2) and (3), we find the two expressions are identical and arrive at one of the central results of this work,



FIG. 3. Brownian dynamics simulation results for the reduced (a) swim pressure, (b) collisional pressure, and (c) total pressure as a function of packing fraction for different run-lengths. The dotted lines correspond to the analytical expressions for the Tonks gas. The dashed curves are the analytical expression derived based on the scaling argument for the kinetic temperature.

which is the equivalence of the reduced swim pressure and reduced kinetic temperature:  $\mathcal{P}_s = \mathcal{T}_k$ . This equivalence can be easily extended to ABPs in higher dimensions, as shown in the Supplemental Material [112]. In Fig. 3(a), we plot  $\mathcal{P}_s$ computed from simulation and validate  $\mathcal{P}_s = \mathcal{T}_k$  by comparison with Fig. 2(b). A practical outcome of  $\mathcal{P}_s = \mathcal{T}_k$  is that the kinetic temperature offers a convenient method of computing the swim pressure of ABPs as particle velocities are readily available from simulation.

We derive an analytical expression for the reduced kinetic temperature using a simple scaling argument predicated on the dynamics of an individual particle. There are two relevant time scales for a given particle: the average duration of a collision  $\tau_C$  and the average time between collisions  $\tau_F$ . The reduced kinetic temperature can be estimated as  $T_k =$  $[(1)\tau_F + (0)\tau_C]/(\tau_F + \tau_C) = 1/(1 + \tau_C/\tau_F)$ , where between collisions  $T_k = 1$  as particle motion is unimpeded and during a collision  $\mathcal{T}_k = 0$ . We approximate the duration of a collision as being comparable to the reorientation time of a particle:  $\tau_C \sim \tau_R$ . While the time between collision scales as  $\tau_F \sim$  $\lambda/U_a$ , where  $\lambda$  is the mean free path and  $U_a$  is the intrinsic speed of a particle. The mean free path in the limit of small run-length is  $\lambda = (1 - \phi)/\rho$  as particles are nearly uniformly distributed. For the more general case,  $\lambda \sim (1 - \phi)/(\rho \sqrt{T_k})$ as clustering increases the distance a particle must travel between collisions (see Supplemental Material [112]). A full discussion of the dependence of  $\tau_C$  and  $\tau_F$  will be published separately.

This expression captures the asymptotic behavior of the reduced kinetic temperature in Fig. 2(b) (i.e.,  $\mathcal{T}_k \rightarrow 1$  as  $\tau_C/\tau_F \rightarrow 0$  and  $\mathcal{T}_k \rightarrow 0$  as  $\tau_C/\tau_F \rightarrow \infty$ ). We expect the exact value of the kinetic temperature will be sensitive to the assumption that particle velocities are exactly zero when clustered. We recognize this is not strictly true as we observe that clusters retain a small drift velocity. To account for this drift behavior and the approximation of  $\tau_C$  and  $\tau_F$ , we introduce a correction factor  $\alpha$ , to be determined *a posteriori*, and obtain an algebraic equation for the reduced kinetic temperature:

$$\mathcal{T}_{k} = \left(1 + \alpha \frac{\tau_{C}}{\tau_{F}}\right)^{-1} = \left(1 + \alpha \ell_{0} \frac{\phi}{1 - \phi} \sqrt{\mathcal{T}_{k}}\right)^{-1}.$$
 (4)

By solving Eq. (4) (see Supplemental Material [112]), we obtain the following analytical expression for  $T_k$ :

$$\mathcal{T}_{k} = \frac{1}{9b^{2}} \left[ 2\cos\left(\frac{1}{3}\arccos\left(\frac{27}{2}b^{2} - 1\right)\right) - 1 \right]^{2}, \quad (5)$$

where  $b = \alpha \ell_0 \phi / (1 - \phi)$ . In Fig. 3(a), we find excellent agreement between simulation results and our analytical solution for  $\mathcal{T}_k$  or equivalently  $\mathcal{P}_s$ . As expected,  $\alpha$  exhibits a weak dependence on  $\ell_0$  and can be approximated by  $\alpha = c/(1 + \ell_0)^d$  where c = 1.1 and d = 0.05.

We now derive an analytical expression for the collisional pressure of the 1D-ABP system. As the run-length decreases, the collisional pressure [Fig. 3(b)] approaches the known analytical result for the equilibrium system:  $\mathcal{P}_c = P_c/P_0 =$  $\phi/(1-\phi)$ . For particles interacting through an additive pairwise potential, the collisional pressure can be expressed as  $P_c = \rho \langle x_{ij} F_{ij} \rangle / 2$  where  $x_{ij} = x_j - x_i$  is the distance between the  $i^{th}$  and  $j^{th}$  particles and  $F_{ij}$  is the resulting force between the pair. As we consider nearly hard particle interactions, a suggestive scaling for the collisional pressure is  $P_c =$  $\rho \langle x_{ij} F_{ij} \rangle / 2 \sim \rho(\sigma_p \overline{F}_{ij}) / 2$ , where  $\overline{F}_{ij}$  is the average magnitude of the force experienced between a pair of particles. To recover the equilibrium result in the limit of small runlengths, it is required  $\overline{F}_{ij} = \gamma U_a^2 \tau_R [\rho/(1-\phi)] = \mathcal{F}_a \tau_C / \tau_F$ , where  $\mathcal{F}_a = \gamma U_a$ . This expression for  $\overline{F}_{ij}$  can be generalized to large run-lengths by replacing the force scale  $\mathcal{F}_a$  by a more appropriate force scale  $\mathcal{F}_a = \gamma U_a \sqrt{\mathcal{T}_k}$ , which captures the observed reduction in  $\mathcal{P}_c$  as  $\ell_0$  is increased [see trend in Fig. 3(b)]. Thus, an expression for  $P_c$  valid for all run-lengths is

$$P_{c} = \frac{\rho}{2} \left( \sigma_{p} \gamma U_{a} \sqrt{\overline{\tau_{k}}} \frac{\tau_{C}}{\tau_{F}} \right) = P_{s} \left[ \frac{\phi}{1 - \phi} \right]. \tag{6}$$

In Fig. 3(b), we see excellent agreement between simulation results and the analytical expression  $\mathcal{P}_c = \mathcal{T}_k[\phi/(1-\phi)]$ . Remarkably, the reduced collisional pressure is simply the product of  $\mathcal{T}_k$  and the equilibrium collisional pressure of the Tonks gas. A unique feature of the 1D-ABP system, highlighted in Fig. 4(a), is the ratio of the collisional and swim pressure collapses onto a universal curve given by  $P_c/P_s = \phi/(1-\phi)$ . This behavior is a direct result of the single-file



FIG. 4. The ratio of the collisional pressure  $P_c$  to the swim pressure  $P_s$  for the 1D-ABP system collapse onto a universal curve  $P_c/P_s = \phi/(1 - \phi)$ . (b) The compressibility as a function of packing fraction for various run-lengths. The dotted line corresponds to the reduced compressibility of the equilibrium Tonks gas  $\mathcal{X} = (1 - \phi)^2$ . The dashed line traces out the location of the maximum of the reduced compressibility  $\mathcal{X}_m$ .

confinement and not observed for ABPs in higher dimensions [121–125].

By combining our results for the swim and collisional pressure, we achieve our primary aim of an analytical expression for the total pressure of the 1D-ABP system:

$$\mathcal{P} = \mathcal{P}_s + \mathcal{P}_c = \mathcal{T}_k \left[ 1 + \frac{\phi}{1 - \phi} \right] = \mathcal{T}_k \left[ \frac{1}{1 - \phi} \right].$$
(7)

In Fig. 3(c), we find excellent agreement between our analytical expression for  $\mathcal{P}$  and simulation results. In the limit of small run-lengths, Eq. (7) reproduces the analytical result for the equilibrium Tonks gas:  $\mathcal{P} = 1/(1 - \phi)$ . We also identify an analog to the Boyle temperature of an equilibrium system, which we call the Boyle run-length, where the second virial coefficient is zero and  $\mathcal{P} \approx 1$ . The Boyle run-length occurs at  $\ell_0 \approx 1$  and indicates a crossover from a regime where the interaction between particles are predominantly repulsive to one where there is an effective attraction between particles. This crossover is consistent with the activity-induced clustering shown in Fig. 2(a). It is straightforward to show from Eq. (7) that the single homogeneous phase for the 1D-ABP system is always mechanically stable (i.e.,  $(\partial P/\partial \rho)_{\ell_0} > 0$ ). These findings provide a mechanical interpretation to prior studies on 1D active systems where there was found to be clustering but no motility-induced phase separation [102–111].

We can further quantify the clustering behavior by investigating the constant run-length compressibility – a thermodynamiclike response function that provides a measure of clustering and local density fluctuations [126,127]. In

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Fig. 4(b), the reduced constant run-length compressibility was calculated from Eq. (7) as

$$\mathcal{X} = \frac{\chi_a}{\chi_0} = \left[\frac{\mathcal{T}_k}{(1-\phi)^2} + \frac{\phi}{1-\phi} \left(\frac{\partial \mathcal{T}_k}{\partial \phi}\right)\right]^{-1},\qquad(8)$$

where  $\chi_a = (\partial \ln \rho / \partial P)_{\ell_0}$  and  $\chi_0 = 1/P_0$  are the compressibility for the interacting and ideal system, respectively. In the limit of small run-lengths, the 1D-ABP system approaches the result of the equilibrium Tonks gas  $\mathcal{X} = (1 - \phi)^2$  and in the ideal limit where  $\phi \to 0$ ,  $\mathcal{X} \to 1$ . Above the Boyle run-length,  $\mathcal{X}$  is no longer monotonic but exhibits a maximum  $\mathcal{X}_m$ . The existence of this maximum suggests a structural transition or weak thermodynamic singularity similar to the Frenkel or Widom line of supercritical fluids [128–131] and will be characterized in future work.

In the limit of large run-length, the location of  $\mathcal{X}_m$  becomes independent of  $\ell_0$  and analytically can be shown to asymptotically approach a packing fraction  $\phi = 1/3$  as shown by the dashed line in Fig. 4(b). For these large values of the run-length,  $\mathcal{X}_m$  exhibits a power law dependence given by  $\mathcal{X}_m \approx 0.9(\ell_0)^{\frac{10}{19}/30}$ . If we consider  $\mathcal{X}/\mathcal{X}_m$  for these large run-lengths (See Supplemental Material [112]), we observe a collapse onto a universal curve similar in shape to that of  $\ell_0 = 50$  in Fig. 4(b). The 1D-ABP system has the interesting property that the compressibility can be made arbitrarily large by increasing the run-length, but there is no emergent singularity consistent with a critical point as the shape of  $\mathcal{X}$  stops evolving in the limit of large run-lengths. A physical interpretation of this behavior is that density fluctuations and clusters can become arbitrarily large, but it is impossible to form a large stable cluster that would give rise to a new dense phase.

#### **IV. CONCLUSIONS**

This work derives an accurate analytical expression for the mechanical pressure of a purely-repulsive 1D-ABP system using the concept of kinetic temperature. By analyzing trends in the pressure, we obtain a mechanical interpretation for the phase behavior of the 1D-ABP system and the lack of a motility-induced phase transition. Further investigation is warranted to establish when the concept of a kinetic temperature can be extended to other active particle models, including those with hydrodynamic or electrostatic interactions.

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