

**Turbulent burning velocity and thermodiffusive instability of premixed flames**Hsu Chew Lee,<sup>1,2</sup> B. Wu,<sup>1</sup> Peng Dai,<sup>1</sup> Minping Wan,<sup>1,2,3,\*</sup> and Andrei N. Lipatnikov<sup>4,†</sup><sup>1</sup>*Guangdong Provincial Key Laboratory of Turbulence Research and Applications, Department of Mechanics and Aerospace Engineering, Southern University of Science and Technology, Shenzhen 518055, People's Republic of China*<sup>2</sup>*Guangdong-Hong Kong-Macao Joint Laboratory for Data-Driven Fluid Mechanics and Engineering Applications, Southern University of Science and Technology, Shenzhen 518055, People's Republic of China*<sup>3</sup>*Jiaxing Research Institute, Southern University of Science and Technology, Jiaxing, 314031, Zhejiang, People's Republic of China*<sup>4</sup>*Department of Mechanics and Maritime Sciences, Chalmers University of Technology, Göteborg, 412 96, Sweden*

(Received 26 February 2023; accepted 2 August 2023; published 1 September 2023)

Reported in the paper are results of unsteady three-dimensional direct numerical simulations of laminar and turbulent, lean hydrogen-air, complex-chemistry flames propagating in forced turbulence in a box. To explore the eventual influence of thermodiffusive instability of laminar flames on turbulent burning velocity, (i) a critical length scale  $\Lambda_n$  that bounds regimes of unstable and stable laminar combustion is numerically determined by gradually decreasing the width  $\Lambda$  of computational domain until a stable laminar flame is obtained, and (ii) simulations of turbulent flames are performed by varying the width from  $\Lambda < \Lambda_n$  (in this case, the instability is suppressed) to  $\Lambda > \Lambda_n$  (in this case, the instability may grow). Moreover, simulations are performed either using mixture-averaged transport properties (low Lewis number flames) or setting diffusivities of all species equal to heat diffusivity of the mixture (equidiffusive flames), with all other things being equal. Obtained results show a significant increase in turbulent burning velocity  $U_T$  when the boundary  $\Lambda = \Lambda_n$  is crossed in weak turbulence, but almost equal values of  $U_T$  are computed at  $\Lambda < \Lambda_n$  and  $\Lambda > \Lambda_n$  in moderately turbulent flames characterized by a Karlovitz number equal to 3.4 or larger. These results imply that thermodiffusive instability of laminar premixed flames substantially affects burning velocity in weak turbulence only, in line with a simple criterion proposed by Chomiak and Lipatnikov (*Phys. Rev. E* **107**, 015102, (2023)).

DOI: [10.1103/PhysRevE.108.035101](https://doi.org/10.1103/PhysRevE.108.035101)**I. INTRODUCTION**

Since premixed turbulent combustion is a multiscale and highly nonlinear phenomenon [1], it involves a variety of local effects, reviewed elsewhere [2–6], with these effects significantly enriching the physics of turbulent reacting flows. In particular, the rate of premixed combustion is known to be increased not only by a wide spectrum of turbulent velocity fluctuations [7–10], but also by hydrodynamic (Darrieus-Landau, DL) and thermodiffusive (TD) instabilities of laminar flames<sup>1</sup> [11–16], with the interactions between turbulence and flame instabilities still challenging the combustion community. This fundamental challenge has also

been attracting rapidly growing interest in applied computational fluid dynamics (CFD) research aimed at developing zero-emission technologies for power generation by utilizing chemical energy bound in renewable carbon-free fuels such as hydrogen. The point is that (i) since pioneering experiments by Karpov *et al.* [17,18], significant differences between molecular diffusivities of  $H_2$ ,  $O_2$ , and heat were well known to result in strongly increasing turbulent burning velocities  $U_T$  in sufficiently lean hydrogen-air mixtures, as reviewed elsewhere [8,16,19], see also recent experimental studies [20–22]; (ii) a similar phenomenon was also documented in experiments with fuel blends that contain  $H_2$ , e.g., lean syngas/air mixtures [23–26] or lean ammonia/hydrogen/air mixtures [27–31]; (iii) a widely established predictive model of this important effect has yet to be developed, while (iv) the effect is often discussed [16,21,27,30,32–37] in terms of TD instability of laminar premixed flames.

Indeed, on the one hand, both the increase in  $U_T$  and TD instability result from variations in local burning rate, caused by differential diffusion effects, i.e., local variations in temperature and reactant concentrations due to imbalance of molecular fluxes of thermal and chemical energies from and to, respectively, reaction zones stretched by the local velocity field [3,8,11,38]. This similarity of the governing physical mechanisms encourages researchers to link the two phenomena. However, on the other hand, the present authors are not aware of convincing evidence that the increase in  $U_T$  stems from local instabilities of inherently laminar flames

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<sup>1</sup>While hydrodynamic instability can arise in any premixed flame characterized by a finite density drop from the unburned side to the burned side, thermodiffusive instability can only arise in mixtures characterized by a low Lewis number  $Le < 1$  [11], which is equal to a ratio of molecular mass diffusivity of deficient reactant to molecular heat diffusivity of the mixture. Accordingly, a premixed laminar flame characterized by a low  $Le$  is subject to both instabilities. Henceforth, the term “DL instability” refers to hydrodynamic instability of a laminar flame characterized by  $Le \geq 1$ , whereas the term “TD instability” refers to joint effects of both hydrodynamic and thermodiffusive instabilities on a laminar flame characterized by a low  $Le < 1$ , as the latter effect is stronger.

in a turbulent flow. Specifically, the present authors are not aware of a model that predicts the increase magnitude by invoking characteristics of TD instability, such as, e.g., its growth rate. On the contrary, a high magnitude of an increase in  $U_T$  in lean hydrogen flames was computed [19,39] adopting another approach, which disregarded TD instability, but, following the leading point concept of premixed turbulent combustion [8,11], highlighted local variations in temperature, reactant concentrations, and burning rate in highly stretched reaction zones localized to the leading edge of a premixed flame brush. A summary of recent developments in that research direction will be provided in the end of Sec. III.

Moreover, the following simple order-of-magnitude criterion

$$Ka = \frac{\tau_f}{\tau_K} < Ka_{TD}^{cr} = \sqrt{15}\tau_f \max\{\omega_{TD}(k)\} \quad (1)$$

of importance of TD instability in turbulent flows has recently been introduced [40] by highlighting mitigation of flame instabilities by normal flame strain rates [41–43], which are created by small-scale eddies in turbulent flows. Here,  $Ka$  is a Karlovitz number;  $\tau_f = \delta_L/S_L$ ,  $S_L$ , and  $\delta_L = (T_b - T_u)/\max\{|dT/dx|\}$  are the laminar flame time scale, speed, and thickness, respectively;  $T$  is the temperature; subscripts  $u$  and  $b$  designate unburned reactants and burned products;  $\max\{\omega_{TD}(k)\}$  is the maximum growth rate of TD instability (dependence of the instability growth rate  $\omega_{TD}$  on the instability wave number  $k$  has a bell-shape form [44–49], as discussed in the next section); and  $\tau_K$  is Kolmogorov time scale, which characterizes the order of magnitude of the highest velocity gradients generated by the smallest-scale turbulent eddies [12,50,51]. Similar criteria of importance of DL instability in turbulent flows were earlier introduced using the same reasoning [19], as well as other reasoning [52,53], and results of subsequent numerical [54–57] and experimental [58,59] studies qualitatively supported those criteria by indicating a minor role played by DL instability under conditions of sufficiently intense turbulence.

However, a role played by TD instability of laminar premixed flames in turbulent flows is still an intricate fundamental and practically important issue. The present paper aims at clarifying it by reporting results of a target-directed direct numerical simulation (DNS) study. In the next section, the adopted research method is presented and the DNS attributes are summarized. Obtained results are discussed in Sec. III, followed by conclusions.

## II. METHOD

### A. Key point

The present work is based on a seminal idea put forward and developed recently by Matalon *et al.* [54–57] who numerically studied interactions of DL instability with turbulence. This idea stems from the following considerations. Both theoretical [60–64] and experimental [65,66] studies of DL instability show that dependence of the instability growth rate  $\omega_{DL}$  on perturbation wave number  $k$  has a bell-shape form, see Fig. 1, i.e., a peak growth rate  $\omega_{DL} > 0$  is reached at certain wave number  $k_m$ , whereas molecular transport processes stabilize the flame with respect to small-scale

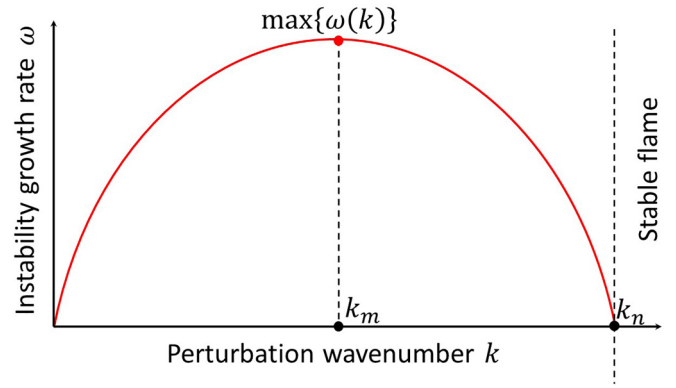


FIG. 1. A typical dispersion relation for unstable laminar premixed flame.

perturbations whose wave number is larger than the neutral wave number  $k_n$ , with  $k_n \approx 2k_m$  and  $\omega_{DL}(k > k_n) < 0$ . Accordingly, variations in a computational domain width  $\Lambda$  offer the opportunity to numerically explore a role played by DL instability in premixed turbulent combustion by comparing results simulated under conditions of  $\Lambda < \Lambda_n = 2\pi/k_n$  (the instability is suppressed) and  $\Lambda > \Lambda_n$  (the instability can grow), with all other things being equal. Results obtained in such simulations [54–57] showed that DL instability could substantially contribute to  $U_T$  under conditions of weak turbulence only, in line with simple phenomenological criteria proposed earlier [19,52,53].

Recent two-dimensional numerical simulations of laminar premixed flames subject to TD instability [44–49] have shown that  $\omega_{TD}(k)$  has a bell-shape form also, with  $\omega_{TD}(k = k_m) = \max\{\omega_{TD}(k)\} > 0$ ,  $\omega_{TD}(k > k_n) < 0$ , and  $k_n \approx 2k_m$ . Therefore, the influence of TD instability on turbulent burning velocity may be explored by comparing DNS results obtained in the cases of  $\Lambda < \Lambda_n = 2\pi/k_n$  (the instability is suppressed) and  $\Lambda > \Lambda_n$  (the instability can grow), with all other things being equal.

This approach is implemented in the present work by simulating lean (the equivalence ratio  $\phi = 0.5$ ) complex-chemistry hydrogen-air flames propagating under room conditions either in a laminar flow or in forced turbulence in a box. It is worth stressing, however, that the primary goal of the present study calls for specific conditions of the performed DNSs.

First, since (i) the study aims at comparing results computed in domains whose widths are comparable with (slightly smaller and slightly larger than)  $\Lambda_n$  and (ii)  $\Lambda_n$  is sufficiently small for the adopted mixture, see Sec. II.C, the DNSs should be run in narrow computational domains, significantly narrower than computational domains used in a typical DNS study of a complex-chemistry turbulent premixed flame. Accordingly, the present work does not aim at exploring evolution of TD instability in a laminar or turbulent flow, because much wider computational domains are known to be required to numerically predict major characteristics of a nonlinear stage of the growth of a laminar flame instability [67–69]. As the present work aims solely at investigating eventual suppression of TD instability by turbulence, the focus of the study is placed on the onset (if any) of the instability in various turbulent flows.

TABLE I. Characteristics of DNS cases.

Case	$S_L$ , m/s	$\delta_L$ , mm	$u'/S_L$	$L/\delta_L$	$Re_\lambda$	$Ka$	$Da$	$\Delta x/L$	$\Delta x/\eta_K$	$N$	$\Lambda$ mm	$\overline{U_T}/S_L$
LT/S	0.58	0.41	0.34	0.58	7.9	0.9	1.8	0.08	0.21	64	1.26	1.05
LT/U	0.58	0.41	0.34	0.61	7.5	0.9	1.8	0.08	0.22	64	1.32	1.64
WT/U	0.58	0.41	0.50	0.61	9.8	1.6	1.2	0.08	0.30	64	1.32	1.71
T/S	0.58	0.41	1.0	0.58	13.7	4.4	0.6	0.04	0.24	128	1.26	1.90
T/U	0.58	0.41	1.0	0.61	14.0	4.3	0.6	0.04	0.25	128	1.32	1.93
T/UM	0.58	0.41	1.0	1.1	18.0	3.4	1.1	0.04	0.40	128	2.4	3.29
T/U1	0.78	0.29	0.74	0.61	14.7	2.2	1.2	0.04	0.24	128	1.32	1.10
T/UM1	0.78	0.29	0.74	1.1	18.0	1.8	2.1	0.04	0.40	128	2.4	1.73

Second, as discussed in Sec. III, TD instability is suppressed by moderately intense turbulence characterized by  $Ka > Ka_{TD}^{cr}$ , where the critical value is  $1.6 < Ka_{TD}^{cr} < 3.4$  for the studied mixture. Since the restriction on the computational domain width, highlighted above, requires considering small-scale turbulence (its integral length scale  $L$  should be significantly less than the width  $\Lambda$ ) and  $Ka \propto (u'/S_L)^{3/2}(L/\delta_L)^{-1/2}$ , this critical value  $Ka_{TD}^{cr}$  can be reached at sufficiently low rms turbulent velocities  $u'$ . Such a weak and small-scale turbulence is characterized by a sufficiently low Reynolds number and even the use of the word ‘‘turbulence’’ may be disputed, e.g., due to the lack of the inertial range of turbulence spectrum. Nevertheless, such unusual conditions may still be appropriate for the major goal of the present study. Indeed, if such weak turbulence can suppress TD instability, as will be shown in Sec. III, there is no reason to expect that the instability could arise in more intense turbulence characterized by a higher  $Ka$ . If TD instability can play a role in weakly and moderately turbulent flames only, running DNS of highly turbulent flames to explore TD instability effects does not seem to be a worthy task.

Thus, when the present DNS study was started, its conditions were set using a constraint of  $\Lambda \approx \Lambda_n$  and Eq. (1). Since the computed results agreed with Eq. (1) to the leading order, there was no need for running DNS by increasing  $u'/S_L$ , especially as DNS results obtained recently from highly turbulent flames propagating in wider boxes were already reported by us [70–77].

### B. DNS attributes

Since the present DNSs are basically similar to our simulations discussed in detail earlier [70–77], only a summary of the DNS attributes is given below.

Unsteady three-dimensional simulations of statistically one-dimensional and planar flames propagating under room conditions in forced turbulence (or a laminar flow) in a box were performed using a detailed chemical mechanism (9 species and 22 reversible reactions) by K eromn es *et al.* [78], with mixture-averaged molecular transport and chemical reaction rates being modeled using open-source library Cantera-2.3 [79]. Navier-Stokes, energy, and species transport equations written in the low-Mach-number formulation were numerically integrated using solver DINO [80]. It adopts a sixth-order finite-difference central stencil and a

semi-implicit third-order Runge-Kutta method for time advancement.

A rectangular computational domain of  $16\Lambda \times \Lambda \times \Lambda$  was discretized using a uniform Cartesian grid of  $16N \times N \times N$  cells. The adopted numerical meshes ensured more than 20 grid points across the thickness  $\delta_L$  in the majority of the studied cases, while the number of grid points per  $\delta_L$  was less (15) in two equidiffusive flames discussed later. In all cases, half the Kolmogorov length scale  $\eta_K$  was larger than the grid size  $\Delta x$ , see Table I. Along the streamwise direction  $x$ , inflow and outflow boundary conditions were set. Other boundary conditions were periodic.

Within a rectangular domain of  $0.5\Lambda \leq x \leq 8\Lambda$ , turbulence was generated using the linear velocity forcing method [81–83] and the evolution of this turbulence was simulated for at least 50 integral time scales  $\tau_t = L/u'$  before embedding the steady planar laminar flame solution obtained using Cantera-2.3 [79] in the computational domain. Here,  $u' = \langle u'_i u'_i \rangle / 3$  is rms turbulent velocity; the integral length scale  $L = u_0^3 / \langle \overline{\varepsilon} \rangle_0$  yielded by the adopted forcing method is about  $0.19\Lambda$  [81–83];  $\varepsilon = 2\nu S_{ij} S_{ij}$  is the dissipation rate of turbulent kinetic energy;  $\nu$  is the kinematic viscosity of the mixture;  $S_{ij} = (\partial u_i / \partial x_j + \partial u_j / \partial x_i) / 2$  is rate-of-strain tensor;  $u_i$  is  $i$ th component of velocity vector; overline and angle brackets refer to time and transverse-averaged quantities, respectively; summation convention applies to repeated indexes ( $i$  or  $j$ ); and subscript 0 refers to the constant-density nonreacting turbulent flow simulated before embedding the flame into the computational domain. In turbulent flame brush,  $u'$  varies weakly, while  $\langle \overline{\varepsilon} \rangle$  increases gradually along the axial direction [72]. The combustion simulations were run for at least  $30\tau_t$ .

### C. DNS conditions

The simulation conditions are summarized in Table I, where  $Re_\lambda = u'\lambda/\nu$  is the turbulent Reynolds number based on the Taylor length scale  $\lambda = u'(15\nu/\langle \overline{\varepsilon} \rangle)^{1/2}$ ;  $Ka = \tau_f/\tau_K$  and  $Da = \tau_t/\tau_f$  are turbulent Karlovitz and Damk ohler numbers, respectively;  $\eta_K = (\nu^3/\langle \overline{\varepsilon} \rangle)^{1/4}$  and  $\tau_K = (\nu/\langle \overline{\varepsilon} \rangle)^{1/2}$  are Kolmogorov length and time scales, respectively, with the time and transverse-averaged dissipation rate  $\langle \overline{\varepsilon} \rangle$  being averaged over flame-brush leading edge characterized by  $\langle c_F \rangle(x, t) = 0.01$ ;  $c_F = 1 - Y_F/Y_{F,u}$  designates combustion progress variable evaluated using the fuel mass fraction  $Y_F$ ; and  $\Delta x = \Lambda/N$  is the grid size. Reported in the last column

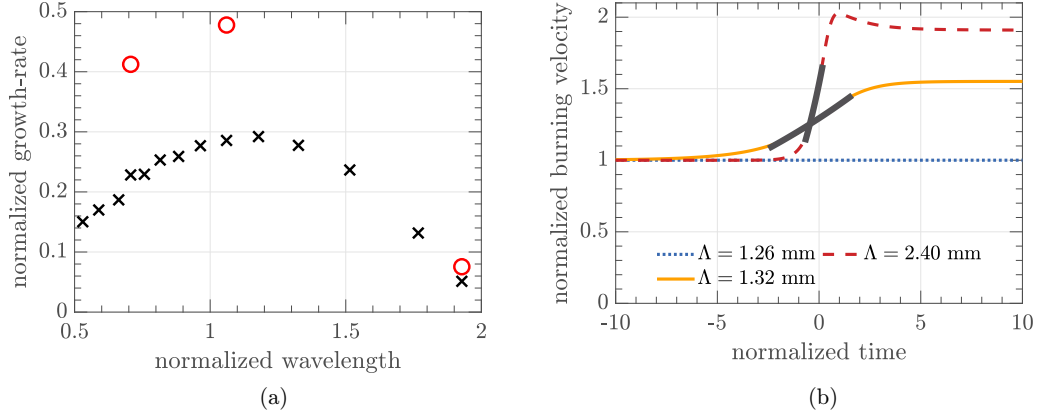


FIG. 2. (a) Normalized instability growth rates  $\tau_f \omega_{TD}(k)$  obtained from two-dimensional (black crosses) and three-dimensional (red circles) laminar flames by varying the width  $\Lambda$  of the computational domain and the perturbation wave length  $k = 2\pi/\Lambda$ , with all other things being equal. (b) Normalized laminar burning velocities computed by varying  $\Lambda$  and  $k = 2\pi/\Lambda$ . In two unstable cases, the normalized time  $t/\tau_f$  is shifted to get the maximum rate of an increase in the burning velocity at  $t' = 0$ . To evaluate the instability growth rate, the ordinate axis is scaled in the natural-logarithm units and thick black straight lines fit the computed curves.

are normalized time-averaged values of turbulent burning velocities, which have been evaluated by integrating the fuel consumption rate  $\dot{\omega}_{H_2}(\mathbf{x}, t)$  over the computational domain, i.e.,

$$U_T(t) = \frac{1}{(\rho Y_{H_2})_u \Lambda^2} \iiint |\dot{\omega}_{H_2}|(\mathbf{x}, t) d\mathbf{x}. \quad (2)$$

Here,  $\rho$  is the density.

When compared to our earlier simulations [70,72], three differences should be emphasized. First, the rms velocity  $u'$  was reduced, because TD instability was assumed to be suppressed in highly turbulent flames and this assumption was supported in subsequent simulations, as discussed in Sec. III. Accordingly, letters LT, WT, and T in case names in Table I refer to transition from laminar to turbulent flows, weak turbulence, and moderately turbulent flames, respectively.

Second, the domain width  $\Lambda$  was varied from  $\Lambda < \Lambda_n$  to  $\Lambda > \Lambda_n$ , with the neutral width  $\Lambda_n$  being found in pre-simulations of two-dimensional and three-dimensional laminar flames. In the two-dimensional case,  $\Lambda$  was changed with a small step, and weak periodic velocity perturbations with the wave number  $k = 2\pi/\Lambda$  were generated at the inlet. Those presimulations were run adopting the same chemical and molecular transport models, the same solver, and  $N = 128$ , with the independence of the numerical results on the spatial resolution being checked using  $N = 256$  or 512. Subsequently, these results were adopted to set conditions of a few three-dimensional presimulations, which were performed to find  $\Lambda_n$  in the three-dimensional case.

The results of these presimulations, reported in Fig. 2, see also Figs. 4(a) and 4(b) in the next section, show that the laminar flame is stable at  $\Lambda = 1.26$  mm, but unstable at  $\Lambda = 1.32$  mm, both in the two-dimensional and three-dimensional cases. For instance, instability growth rates computed in the two-dimensional and three-dimensional cases are plotted in black crosses and red circles, respectively, in Fig. 2(a). As illustrated in Fig. 2(b), these growth rates have been evaluated by (i) computing laminar burning velocities adapting Eq. (2) and (ii) fitting the linear parts of the obtained

dependencies of  $\ln(U_L/S_L)$  on time with straight lines. Dispersion relations  $\omega(k)$  similar to the curve plotted in black crosses in Fig. 2(a) are well known from theoretical [60–64] and experimental [65,66] studies of DL instability, as well as from recent two-dimensional numerical simulations of thermodynamically unstable laminar flames [44–49]. At large  $t/\tau_f$ , a nonlinear stage of instability development, characterized by a quasistationary value of  $\ln(U_L/S_L)$ , is reached, see Fig. 2(b). This quasistationary value of  $\ln(U_L/S_L)$  depends on the computational domain width  $\Lambda$ . Such a nonlinear stage was already investigated in recent two-dimensional numerical simulations [68,69] performed using significantly wider computational domains and, therefore, is beyond the scope of the present study, whose focus is solely placed on the onset of TD instability.

Based on the presented results of the laminar flame presimulations, letters S or U in case names in Table I refer to  $\Lambda = 1.26$  mm (TD instability cannot arise, stable case) and  $\Lambda = 1.32$  mm (the instability may occur, unstable case), respectively. The major goal of the present study is to compare turbulent burning velocities  $U_T$  computed in LT/S and LT/U or T/S and T/U cases.

Third, if  $\Lambda$  is slightly above  $\Lambda_n$ , the growth rate  $\omega_{TD}(k)$  of allowed unstable perturbations is low, see Fig. 2(a), or compare the maximum slopes of curves plotted in yellow solid and red dashed lines in Fig. 2(b). Therefore, even if TD instability with respect to such perturbations is of minor importance when compared to turbulence, perturbations with the maximum growth rate  $\omega_{TD}(k_m)$  might significantly affect turbulent burning velocity. To explore such a scenario, the width  $\Lambda$  was increased to 2.4 mm, i.e., by a factor of about two when compared to  $\Lambda_n$ . In this case, TUM, labeled with extra letter M in Table I, appearance of perturbations whose growth rates were close to  $\max\{\omega_{TD}(k)\}$  was enabled, see the highest circle in Fig. 2(a).

However, the aforementioned increase in  $\Lambda$  can increase  $U_T$  not only due to development of TD instability, but also due to an increase in the turbulence length scale  $L$  (recall that  $L = 0.19\Lambda$  under conditions of the present DNS), because



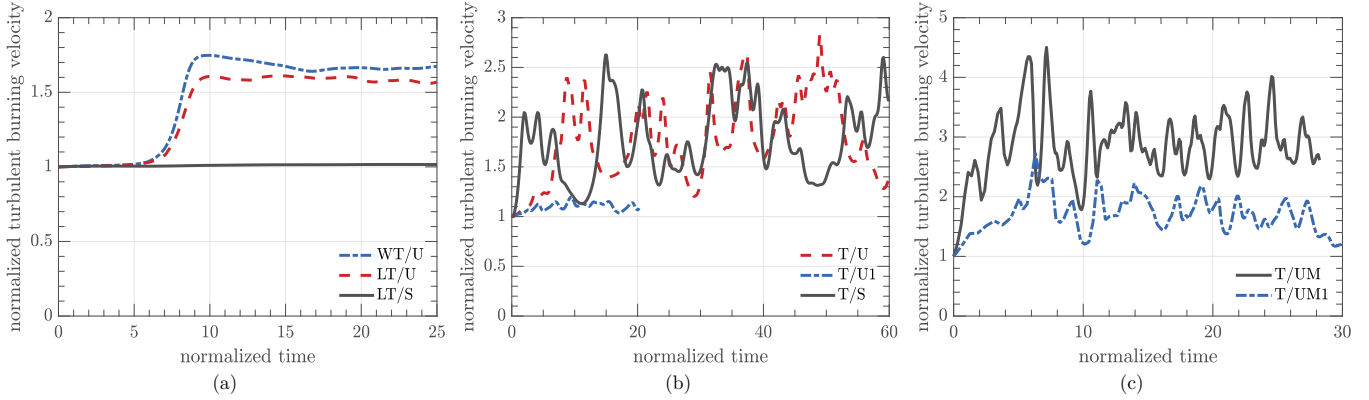


FIG. 3. Evolution of the normalized turbulent burning velocities  $U_T/S_L$  in flames (a) LT/S (black solid line), LT/U (red dashed line), and WT/U (blue dotted-dashed line), (b) T/S (black solid line), T/U (red dashed line), and T/U1 (blue dotted-dashed line). (c) T/UM (black solid line), and T/UM1 (blue dotted-dashed line). Time is normalized using the laminar flame time scale  $\tau_f$ .

burning velocity is increased by turbulence length scale, as reviewed elsewhere [84], see also a recent DNS study by Yu and Lipatnikov [85] or a recent experimental work by Kim *et al.* [86]. To compare magnitudes of these two effects, i.e., (i) an eventual increase in  $U_T$  due to TD instability and (ii) an increase in  $U_T$  with increasing the length scale  $L$ , two more cases T/U1 and T/UM1 (in addition to cases T/U and T/UM, respectively) were run by setting molecular diffusivities  $D$  of all species equal to molecular heat diffusivity  $\kappa$  of the mixture. Number one in the names of these two cases shows that the Lewis number  $Le = \kappa/D_{H_2} = 1$ . In other cases,  $Le = 0.32$ . Since TD instability does not appear if  $Le = 1$  [11], the difference between values of  $U_T$ , obtained in cases T/UM1 and T/U1, results from different  $L$  in these two cases, i.e., effect (ii). Consequently, a ratio  $R1$  of turbulent burning velocities computed in these two cases characterizes magnitude of this effect (an increase in  $U_T$  by  $L$ ). As far as difference between values of  $U_T$  obtained in cases T/UM and T/U is concerned, it could also result from TD instability, i.e., effect (i) in addition to effect (ii). Therefore, comparison of a ratio  $R$  of burning velocities obtained in cases T/UM and T/U with the ratio  $R1$  offers the opportunity to estimate importance of TD instability under conditions when not only perturbations with  $k \approx k_n$  (cases LT/S, LT/U, WT/U, T/S, and T/U), but also perturbations with  $k \approx k_m$  (case T/UM) and, hence, much higher growth rate  $\omega(k)$ , see Fig. 2(a), are enabled. Thus, cases T/UM1 and T/U1 were run to estimate contribution  $R1$  of effect (ii) to the ratio  $R$  computed in cases T/UM and T/U.

### III. RESULTS AND DISCUSSION

Computed dependencies of the normalized turbulent burning velocity  $U_T(t)/S_L$  on the normalized time  $t/\tau_f$  are reported in Fig. 3, with representative images of instantaneous turbulent flame surfaces being shown in Figs. 4(c)–4(f). The following trends are worth noting.

First, in case LT/S, the flame surface looks weakly perturbed, see Fig. 4(c), and  $U_T(t) \approx S_L$ , see curve plotted in black solid line in Fig. 3(a). At the same time, a small increase (less than 10%) in the computational domain width results in significantly increasing flame-surface perturbations, see Fig. 4(d), and turbulent burning velocity, see curve plotted

in red dashed line in Fig. 3(a), with the increase in  $U_T$  being as large as 60%. Moreover, subsequent increase in  $u'$  by about 50% results in weakly increasing (less than 5%)  $U_T/S_L$ , see curve plotted in blue dot dashed line in Fig. 3(a). Furthermore, normalized burning velocities obtained from turbulent flames LT/U and WT/U at large  $t/\tau_f$  are close to burning velocity associated with the nonlinear stage of development of TD instability of the three-dimensional laminar flame in the same computational domain, see curve plotted in yellow solid line in Fig. 2(b). These results indicate that an increase in turbulent burning velocity in cases LT/U and WT/U when compared to case LT/S is mainly controlled by TD instability.

Second, both flame-surface perturbations, cf. Figs. 4(e) and 4(f), and dependencies of  $U_T(t)/S_L$ , cf. curves plotted in black solid and red dashed lines in Fig. 3(b), look similar in cases T/S and T/U. Since development of TD instability is allowed in case T/U only, these results imply that TD instability weakly affects burning velocities in flames T/S and T/U. Nevertheless,  $U_T/S_L$  is significantly higher in low  $Le$  flame T/U when compared to counterpart equidiffusive flame T/U1, see curve plotted in blue dot dashed line in Fig. 3(b). This difference indicates that Lewis number substantially affects turbulent burning velocities in the discussed flames despite TD instability does not do so.

Third, comparison of curves plotted in black solid and blue dot dashed lines in Fig. 3(c) shows that differential diffusion results in significantly increasing  $U_T(t)/S_L$  in low  $Le$  flame T/UM when compared to counterpart equidiffusive flame T/UM1. However, the effect magnitudes are comparable (i) for these two flames (a ratio of mean values of  $\overline{U_T}/S_L$ , obtained from flames TU/M and TU/M1, is about 1.9, see the far right column in Table I) and (ii) for two flames T/U and T/U1 (the counterpart ratio is about 1.75) despite perturbations with the highest growth rate  $\omega_{TD} \approx 0.5\tau_f^{-1}$ , see the top red circle in Fig. 2(a), are allowed in the former pair of flames only.

This observation is supported by comparing the ratio  $R1 = 1.6$  of  $\overline{U_T}$ , obtained from equidiffusive flames T/UM1 and T/U1, with the counterpart ratio  $R = 1.7$  for low Lewis number flames T/UM and T/U. A weak difference in  $R1$  and  $R$  implies that the computed increase in  $U_T$  with increasing  $\Lambda$  may be attributed to an increase in  $U_T$  by the turbulence length

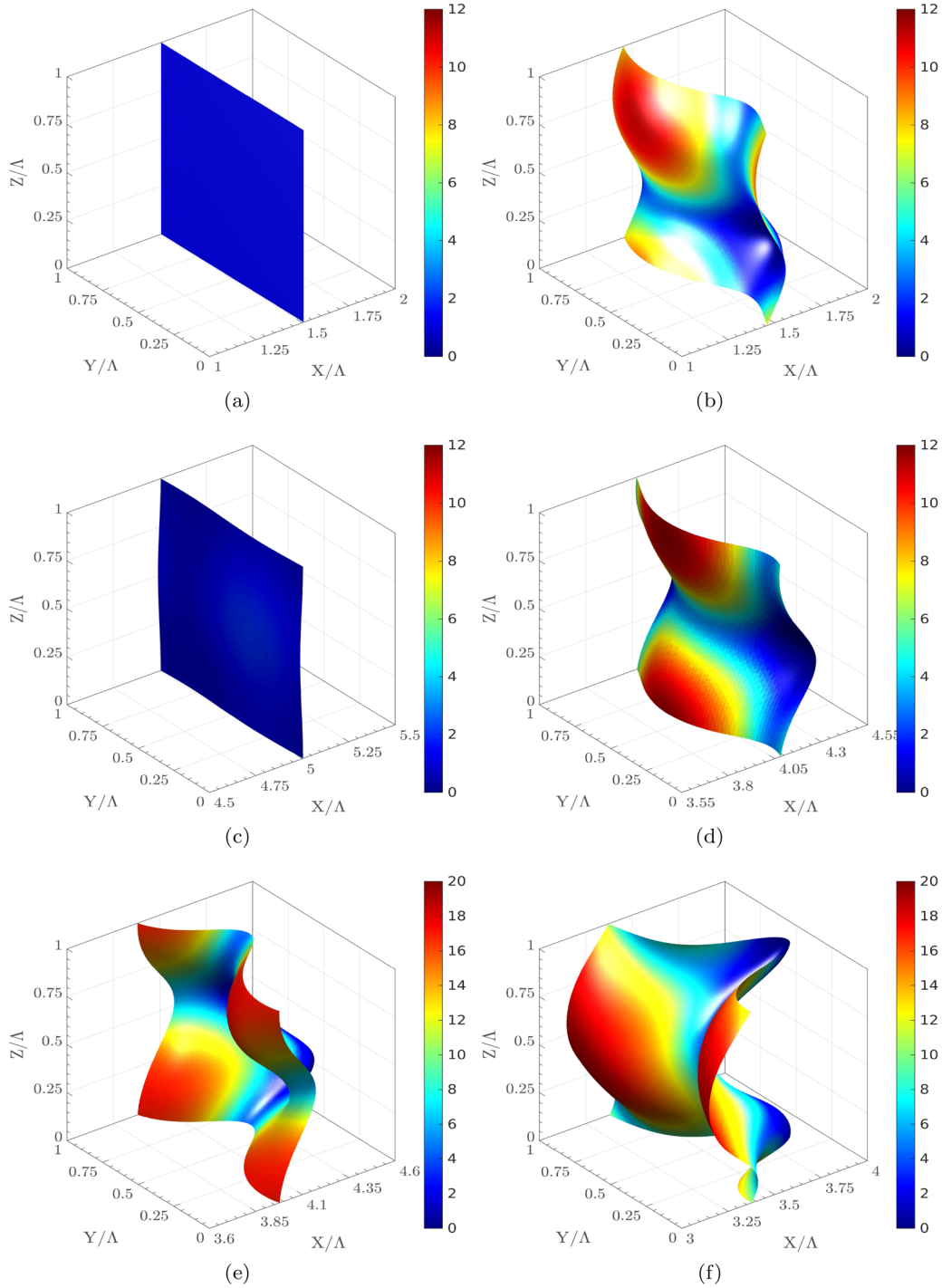


FIG. 4. Images of the instantaneous isosurfaces  $c_F(\mathbf{x}, t) = 0.5$ , with color bars showing the local fuel consumption rate  $\dot{\omega}_{H_2}(\mathbf{x}, t)$  normalized with the rate  $\dot{\omega}_{H_2, L}(c_F = 0.5)$  obtained from the unperturbed laminar flame. (a) stable laminar flame,  $\Lambda = 1.26$  mm; (b) unstable laminar flame,  $\Lambda = 1.32$  mm; (c) flame LT/S; (d) flame LT/U; (e) flame T/S; and (f) flame T/U.

scale  $L$  to the leading order, whereas eventual appearance of perturbations with a high growth rate  $\omega_{TD}$  plays a minor role in case T/UM.

The reported results indicate that, under the present DNS conditions, TD instability weakly affects turbulent burning velocity at  $Ka \geq 3.4$  (cases T/UM and T/U). However, the ratio  $U_T/S_L$  is controlled by the instability at  $Ka = 1.6$  (case WT/U). These numerical findings agree with Eq. (1), which yields  $Ka_{TD}^{cr} = 1.9$  if  $\tau_f \max\{\omega_{TD}(k)\} \approx 0.5$ , see the top red

circle in Fig. 2(a). Note that the critical Karlovitz number is substantially less for DL instability [19,53] because  $\max\{\omega_{DL}(k)\} < \max\{\omega_{TD}(k)\}$  [49, Fig. 2].

Since development of TD instability is commonly associated with growth of flame surface area, the present results indicating weak contributions of TD instability to  $U_T$  in flames T/U and T/UM are in line with earlier DNS [37,75,87] and experimental [29] data, which showed significant (weak) influence of differential diffusion on turbulent burning

velocity (flame surface area, respectively). Moreover, the present results are in line with (i) DNS data by Day *et al.* [88], which indicate that both magnitudes and length scales of fuel consumption rate perturbations differ significantly in unstable laminar and turbulent lean hydrogen-air flames, cf. Figs. 6(a) and 6(b) in the cited paper; (ii) DNS data by Berger *et al.* [37], which show significantly different mean local flame characteristics in unstable laminar and moderately turbulent lean H<sub>2</sub>-air flames, see Figs. 13, 17, 19-21, 23-25 in the cited paper; and (iii) DNS data by Howarth *et al.* [89], which demonstrate a significant increase in mean local consumption velocity with increasing  $Ka$  in lean hydrogen-air flames, see Fig. 20 in the cited paper [the same trend is observed when comparing color scales in Figs. 4(d)-4(f)]. Such DNS data imply that scales and local characteristics of unstable laminar flames are of minor value for predicting the counterpart scales and characteristics of turbulent flames. Furthermore, when discussing DNS data obtained from two V-shaped weakly turbulent ( $u'/S_L = 0.72$  and 2.8) flames, Day *et al.* [90, p. 1043] have written that “with increasing turbulence levels fluctuations, at even the lowest intensity levels, appear to suppress to some extent the growth and propagation of the spherical burning cells characteristic of the thermodiffusive instability.” Howarth *et al.* [89, p. 15] have also noted that “turbulence is beginning to dominate thermodiffusive effects” at moderate values of Karlovitz number.

Since higher values of  $U_T$  obtained from low  $Le$  flames T/U and T/UM when compared to their equidiffusive counterparts T/UI and T/UM1, respectively, do not result from TD instability, this difference in the computed burning velocities requires another explanation. In this regard, leading point concept [8,19], which is based on mathematically rigorous KPP theory [91] of convection-diffusion-reaction equations, see Refs. [92–96] also, appears to be the most promising approach to predicting the significant influence of differential diffusion on turbulent burning velocity, with such effects being documented both experimentally [18,20,29] and numerically [74,97] even in highly turbulent flames. Within the framework of the concept [8], (i) turbulent flame propagation is, in line with the KPP theory, hypothesized to be controlled by reaction zones that advance furthest into fresh reactants (so-called leading points) and (ii) these leading reaction zones are hypothesized to be critically stretched by turbulent eddies, with further stretching of the zones resulting in local combustion quenching (thus, limiting advancement of the zones deeper into the reactants). Accordingly, a critically stretched laminar flame is considered to be a simple model of local burning structures that control flame propagation. In highly stretched laminar flames characterized by a low  $Le$ , the local temperature and, hence, burning rate, are well known [3,11] to be significantly increased due to imbalance of molecular fluxes of chemical and thermal energies to and from, respectively, the flame reaction zones. For instance, such an effect is well pronounced in positively curved (curvature center in products) elements of flame surfaces shown in Figs. 4(e) and 4(f) (note that the normalized local fuel consumption rate is as large as 18). Accordingly, substitution of characteristics of unperturbed laminar flames with characteristics of highly stretched laminar flames, which control flame propagation within the framework of leading point

concept, offers the opportunity to predict a strong increase in  $U_T$  with decreasing  $Le$  [3,19] without invoking a hypothesis on TD instability. Further discussion of the concept is beyond the scope of this paper and the reader interested in recent advancements in the concept and its substantiation is referred to articles by Venkateswaran *et al.* [23,25], Kim [98], Zhang *et al.* [26], Dave *et al.* [99], Lipatnikov *et al.* [100], Verma *et al.* [101], Lee *et al.* [70,75,77], Somappa *et al.* [102], Howarth *et al.* [89], and references therein.

#### IV. CONCLUDING REMARKS

The presented DNS data indicate that the influence of thermodiffusive instability on burning velocity is of primary (secondary) importance in weakly (moderately, respectively) turbulent flames. Under conditions of the present simulations, the instability plays an important role at Karlovitz numbers lower than a critical value, which is of unity order. These DNS results agree with a simple criterion of importance of TD instability in turbulent flames, proposed recently [40].

It is worth bearing in mind that a method adapted to reach the above conclusions required using a narrow computational domain whose width was about  $3\delta_L$  in most cases. Accordingly, the reported results could be contaminated by a confinement effect. Such an effect is not expected to reverse the conclusions for the following two reasons. First, TD instability is caused by local variations in burning rate within thin reaction zones and such a small-scale phenomenon should be weakly sensitive to a confinement effect, especially as the domain was sufficiently wide to enable the instability growth. Second, the same major message was delivered when doubling computational domain width (cases T/UM and T/UM1). Nevertheless, more simulations run in wider domains are desirable to confirm the conclusions drawn in the present study. For instance, new simulations could be performed by setting a larger  $\Lambda$  and varying  $u'$  around a critical value guessed using  $Ka_{TD}^{cr}$ . Such a study is ongoing and results will be reported in a future paper. Another alternative consists in (i) setting sufficiently large  $\Lambda$  and  $u'$ , (ii) switching off turbulence forcing, and (iii) exploring transition from turbulence-dominated to instability-dominated regime of flame propagation as the turbulence decays. Preliminary results obtained in such simulations [103] are consistent with the conclusions drawn in the present paper.

#### ACKNOWLEDGMENTS

A.N.L. gratefully acknowledges the financial support by the Chalmers Area of Advance Transport. Other authors have been supported in part by NSFC (Grants No. 91752201, No. 51976088, and No. 92041001), the Shenzhen Science and Technology Program (Grants No. KQTD20180411143441009 and No. JCYJ20210324104802005), Department of Science and Technology of Guangdong Province (Grants No. 2019B21203001 and No. 2020B1212030001), National Science and Technology Major Project (Grants No. J2019-II-0006-0026 and No. J2019-II-0013-0033), and the Center for Computational Science and Engineering of Southern University of Science and Technology.

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