Effects of mirror aberrations on Laguerre-Gaussian beams in interferometric gravitational-wave detectors

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A fundamental limit to the sensitivity of optical interferometers is imposed by Brownian thermal fluctuations of the mirrors' surfaces. This thermal noise can be reduced by using larger beams which "average out" the random fluctuations of the surfaces. It has been proposed previously that wider, higher-order Laguerre-Gaussian modes can be used to exploit this effect. In this paper, we show that susceptibility to spatial imperfections of the mirrors' surfaces limits the effectiveness of this approach in interferometers used for gravitational-wave detection. Possible methods of reducing this susceptibility are also discussed.

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I. INTRODUCTION

Long-baseline laser-interferometer gravitational-wave detectors, such as those used in LIGO [1], VIRGO [2], GEO600 [3], and LCGT [4], use Michelson interferometry to measure tiny differential changes in arm length induced by gravitational waves. Spurious motions of a mirror's surface, such as those caused by seismic, thermal, and radiation-pressure fluctuations, can compromise the sensitivity to gravitational-wave signals. Brownian thermal noise in the dielectric mirror coatings, or *coating Brownian noise*, is known to be the dominant noise source in the intermediate frequency band of Advanced LIGO [5] and other similar interferometers.

As described by the fluctuation-dissipation theorem [6,7], dissipation via internal friction in the dielectric coatings must lead to fluctuations in the thickness of the coatings. When the beam spot size is much larger than the coating thickness, coating Brownian noise at different locations on the mirror's surface can be considered to be uncorrelated. This leads to the following scaling law [8,9]:

$$S_x \propto \frac{\int I^2(\vec{r}) d^2 \vec{r}}{\left[\int I(\vec{r}) d^2 \vec{r}\right]^2} \tag{1}$$

which describes how the power spectrum of observed coating Brownian noise S_x depends on the intensity profile $I(\vec{r})$ of the optical field which is used to read out the mirror motion; i.e. the coating Brownian noise power spectrum is inversely proportional to the effective area of the optical mode.

Three families of optical modes have so far been considered for mitigating coating thermal noise (see Table I). Among these modes, only the higher-order Laguerre-Gauss (LG) mode, LG_{3,3}, can be supported by optical cavities employing standard spherical mirrors. Because of the practical advantages associated with the use of spherical mirrors, experimental testing of LG_{3,3} modes has begun. It has thus far been demonstrated that these

modes can be generated with high efficiency and resonated in tabletop cavities with small mirrors [14,15].

An unpleasant property of higher-order LG modes is that each $LG_{p,l}$ mode is 2p + |l| + 1-fold degenerate, the $LG_{3,3}$ mode being tenfold degenerate. Mirror figure errors will inevitably split each formerly degenerate mode into 2p + |l| + 1 single modes with eigenfrequencies which depend on the particulars of the figure error. By contrast, a nondegenerate mode, under the same figure error, will usually remain as a single, weakly perturbed nondegenerate mode.

In this work we explore the effects of LG_{3,3} modal degeneracy quantitatively, via both numerical and analytical methods. Guided by experience with existing interferometers we have selected contrast defect as our metric of interferometer performance.

To ground our investigation in reality, we incorporate mirror figure errors derived from measurements of the first Advanced LIGO optics. The creation of these maps is described in Sec. II.

In Sec. III, we use perturbation theory to analyze the effect of such mirror perturbations on the degenerate subspace which includes the LG_{3,3} mode. We then use this newly perturbed set of modes to calculate the contrast degradation of a single Fabry-Perot arm cavity analytically in Sec. IVA.

TABLE I. Beam shapes that have been considered for use in gravitational-wave detectors, mirror shapes that support them, and their thermal-noise suppression factors (in power) for Advanced LIGO parameters (cavity length L=4 km, mirror radius of 17 cm).

Mode	Mirror shape	Suppression factor	Ref.
LG _{3,3}	Spherical	1.61	[10]
Mesa	Sombrero	1.53	[11,12]
Conical	Conical	2.30	[13]

In Sec. IV B, we utilize a sophisticated numerical field propagation code to confirm analytical results and examine a more complicated interferometer topology.

In Sec. V, we explore two methods of mitigating contrast degradation; neither of the methods was ultimately successful.

II. MIRROR FIGURE ERRORS

In this work we investigate the consequences of realistic mirror imperfections on the performance of the LG_{3,3} mode. The parameters of the particular imperfections applied are therefore significant.

Figure 1 illustrates measured surface roughness power spectral densities of selected Advanced LIGO mirror substrates, prior to the application of dielectric mirror coatings [the power spectral density (PSD) plots end up to a spatial wavelength of 2 mm]. Based on the measured Initial LIGO optics and small optics of Advanced LIGO, we construct an analytical model (solid black line) which falls roughly in the middle of Advanced LIGO test mass PSDs.

$$S(f) \propto (1 + (0.04f)^2)^{-1}.$$
 (2)

This one-dimensional function was used to generate random mirror maps which are statistically similar to those one might find in an advanced gravitational-wave interferometer. Such random mirror maps, used in all aspects of this investigation, were constructed by multiplying each point of the amplitude spectral density's magnitude by a random complex number a + ib before transforming back to coordinate space and appropriately scaling the result to yield the desired rms. Scalars a and b are drawn independently from a normal distribution with zero mean and a standard deviation of one [16].

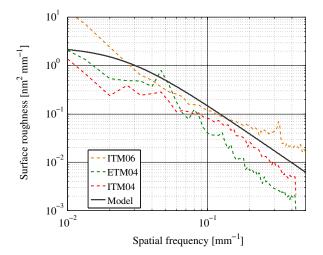


FIG. 1 (color online). Power spectral densities of uncoated mirror surface roughness. The dashed lines are the measured spectra of three Advanced LIGO arm cavity mirrors. A model approximating these spectra [black trace, see (2)] was created to generate the random maps used in our work.

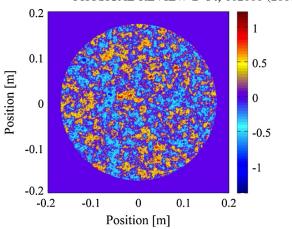


FIG. 2 (color online). Surface figure (in nm) of a typical generated phase map with piston, tilt, power, and astigmatism terms subtracted.

The entire surface is fit by Zernike polynomials and the terms corresponding to Piston, tilt and power (Zernike polynomials Z_0^0 , $Z_1^{\pm 1}$ Z_2^0) were removed from our maps (the Piston term is irrelevant because the lock process adjusts the microscopic length; the tilt term is removed to represent the alignment control; the ROC of the generated surface is corrected by hand). The rms values quoted are calculated after this subtraction.

Figure 2 shows the surface figure of one map generated using our algorithm. This map is typical of a larger population and was selected as a reference to be used in all analytical calculations.

III. DEGENERATE PERTURBATION-THEORY ANALYSIS

A. Laguerre-Gauss modes

The Laguerre-Gauss modes $(LG_{p,l})$ are a set of circularly symmetric modes which can be written in cylindrical coordinates as [17]

$$u_{p,l}(r,\phi,z) = \sqrt{\frac{2p!}{\pi(|l|+p)!}} \frac{1}{\omega(z)} \left[\frac{\sqrt{2}r}{\omega(z)} \right]^{|l|} L_p^{|l|} \left[\frac{2r^2}{\omega^2(z)} \right]$$

$$\times \exp[i(2p+|l|+1)\psi(z)]$$

$$\times \exp\left[-ik \frac{r^2}{2R(z)} + il\phi \right] \exp\left[\frac{-r^2}{\omega^2(z)} \right], \quad (3)$$

TABLE II. Suppression factors of thermal noise (in power spectral density) for LG modes with a fixed clipping loss of 1 ppm.

	LG _{0,0}	LG _{0,9}	LG _{1,7}	LG _{2,5}	LG _{3,3}	LG _{4,1}
Beam radius (mm)	9.96	16.5	17.3	17.9	18.2	18.4
Suppression factor	1	1.51	1.62	1.64	1.61	1.51

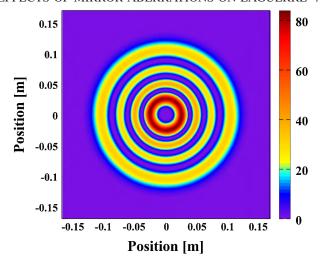


FIG. 3 (color online). Normalized intensity distribution of the LG_{3,3} mode at the mirror position ($\omega_0 = 0.021$ m, z = 1997.25 m).

where $\omega(z)$ is the beam radius, $\psi(z)$ is the Gouy phase, and R(z) is phase front curvature of the beam. $L_p^{|I|}(x)$ is the associated Laguerre polynomial where $p \ge 0$ and l are the radial and azimuthal indices, respectively.

The mode selectivity of the cavity is determined by the cavity finesse and the mode dependent phase shift $(2p + |l| + 1)\psi(z)$. From this we see that the $LG_{p,l}$ mode has 2p + |l| + 1 degenerate eigenmodes. For example, $LG_{3,3}$ belongs to a tenfold degenerate space, which can be spanned by $LG_{3,\pm 3}$, $LG_{0,\pm 9}$, $LG_{1,\pm 7}$, $LG_{2,\pm 5}$, and $LG_{4,\pm 1}$.

Coating Brownian noise power is proportional to the integral of beam intensity, as the scaling law [Eq. (1)] indicates. In Table II, we present theoretical thermal-noise suppression factors for selected LG modes. To permit a fair comparison, the widths of all modes considered here and henceforth were chosen to be 0.018 m, which yield a clipping loss [18], due to the finite size of the cavity mirrors, of around 1 ppm. We see that the LG_{3,3}, considered by many as the leading candidate for use in gravitational-wave interferometers, offers a theoretical thermal-noise reduction factor of \sim 1.6 compared to a standard Gaussian beam (LG_{0,0}). The transverse intensity distribution of the LG_{3,3} mode is presented in Fig. 3.

B. Application of degenerate perturbation theory to the perturbed Fabry-Perot cavity

The combination of eigenmodes excited in a cavity depends on the composition of the incident field and on the properties of the cavity itself. In this section we discuss how first-order perturbation theory can be applied to this problem. We first explore how mirror figure error breaks the degeneracy of LG cavity modes before describing the phase shift each mode experiences in an optical cavity and finally constructing the total field (prompt plus leakage) reflected from a perturbed Fabry-Perot resonator.

1. Mode splitting

Figure 4 illustrates light propagation in a simple Fabry-Perot cavity, introducing the notation employed in our formalism.

We use the following standard method for propagating cavity fields:

$$\Psi_r(\vec{r}) = \int K(\vec{r}, \vec{r}') \Psi_l(\vec{r}') d^2 \vec{r}', \tag{4}$$

or $|\Psi_r\rangle = \hat{K}|\Psi_l\rangle$, where Ψ_r and Ψ_l are the electric fields near the right and left mirror, respectively, and K is the field propagator from the left mirror to the right:

$$K(\vec{r}, \vec{r}') = \frac{ik}{2\pi L} e^{-(ik/2L)|\vec{r} - \vec{r}'|^2}.$$
 (5)

Therefore, if $|\psi\rangle$ is an eigenmode of the cavity,

$$|\psi\rangle = \hat{R}\,\hat{K}\,\hat{R}'\hat{K}|\psi\rangle,\tag{6}$$

where \hat{R} is the reflection operator of the left mirror and \hat{R}' is for the right. Hence, $|\psi\rangle$ is an eigenmode of the operator $(\hat{R} \hat{K} \hat{R}' \hat{K})$.

We assume that the mirror on the left is ideal and study the consequences of applying a surface figure perturbation δh to the right hand (end mirror) optic. The reflection operator \hat{R}' can then be written as

$$\hat{R}' = \hat{R}e^{2ik\delta h} \approx \hat{R}(1 + 2ik\delta h). \tag{7}$$

To obtain the real cavity eigenmodes, we need to solve for the eigenfunctions of $(\hat{R} \hat{K} \hat{R}' \hat{K})$. Note that the original LG₃₃ mode is an eigenfunction of an unperturbed cavity:

$$|33\rangle = (\hat{R}\,\hat{K}\,\hat{R}\,\hat{K})|33\rangle. \tag{8}$$

As introduced above, the LG₃₃ mode is degenerate with nine other modes, each having eigenfrequency ω_0 , thus $\hat{R} \hat{K} \hat{R} \hat{K}$ also has ten degenerate eigenmodes at ω_0 .

For reasonable parameters, modes outside of this degenerate subspace are far enough from resonance that we may ignore them in this first-order analysis. Therefore, to good approximation, we can assume the new eigenmodes of the perturbed cavity are still members of the Hilbert space of the original ten LG modes, which we represent by $|i\rangle$ (i = 1, 2, ..., 10). These new eigenmodes, denoted $|i'\rangle$, are the eigenvectors of the matrix with elements $\langle i|\hat{R} \hat{K} \delta h \hat{R} \hat{K} |j\rangle = \langle i|\delta h|j\rangle$ (i, j = 1, 2, ..., 10):

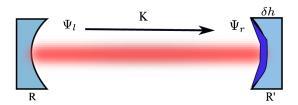


FIG. 4 (color online). Fabry-Perot cavity with a perturbation $\delta h(x, y)$ on the end mirror.

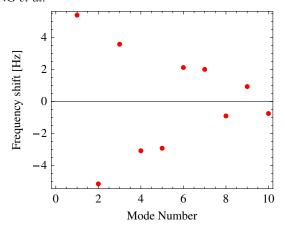


FIG. 5 (color online). Frequency shift of LG modes introduced as a result of realistic mirror perturbations.

$$\begin{pmatrix} \langle 1|\delta h|1\rangle & \dots & \langle 1|\delta h|10\rangle \\ \vdots & \ddots & \vdots \\ \langle 10|\delta h|1\rangle & \dots & \langle 10|\delta h|10\rangle \end{pmatrix}. \tag{9}$$

Denoting the electric field of $|i\rangle$ as ϕ_i , we write

$$\langle i|\delta h|j\rangle = \iint \phi_i^*(x,y)\delta h(x,y)\phi_j(x,y)dxdy.$$
 (10)

The frequency shift of the degenerate modes introduced by the perturbation is then proportional to the eigenvalues of the matrix,

$$\omega_i = \frac{kc}{L} \langle i' | \delta h | i' \rangle, \tag{11}$$

where $k = 2\pi/\lambda$ is the optical wave number, c is the speed of light, and L is the cavity length.

This quantity was evaluated using the reference map shown above (Fig. 2). The rms roughness of the reference was scaled to be similar to those of measured Advanced LIGO mirror surfaces (0.3 nm rms). Results are presented in Fig. 5. Here the frequency splits are given in hertz $(\omega/2\pi)$. The frequency shifts are 1 order of magnitude smaller than the advanced gravitational-wave interferometer's cavity linewidth. Thus, multiple perturbed eigenmodes will be partially resonant, radically distorting the shape of the output field.

2. The modal input-output equation

Above we have shown that mirror figure errors will lift the modal degeneracy and split the degenerate LG_{3,3} space into distinct states with unique eigenfrequencies. We now consider how each of these modes interacts with a cavity.

For any mode |in | injected into an ideal cavity, there exists a frequency dependent phase shift between the input and total reflected or *output* fields. This can be written as [19]

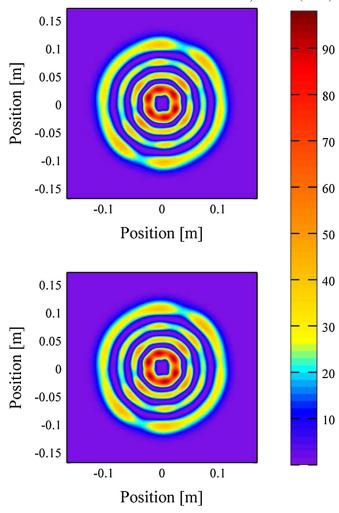


FIG. 6 (color online). Intensity distributions of the total field reflected from an arm cavity whose end mirror was perturbed by the reference map. These distributions were calculated independently via two different techniques. Top—analytic method described in Sec. III B. Bottom—fast-Fourier-transform(FFT)-based numerical simulation (see Sec. IV B).

$$|\text{out}\rangle = \frac{\gamma_c + i(\omega - \omega_0)}{\gamma_c - i(\omega - \omega_0)}|\text{in}\rangle,$$
 (12)

where ω is the frequency of the injected field, ω_0 is the resonant frequency of the cavity closest to ω , and $\gamma_c = c T_{\text{input}}/4L$ is the cavity pole frequency in hertz. Here, T_{input} denotes the power transmissivity of the cavity input mirror; the transmissivity of the end mirror is assumed to be zero.

Suppose that this ideal cavity hosts an N-fold degenerate space and that we inject an input mode $|\text{in}\rangle$ which belongs to this space. If the N-fold degeneracy is broken by some mirror figure error, the new eigenmodes can be approximated by $|n\rangle$, $n=1,2,\ldots,N$, where each mode still belongs to the original subspace, but has a new eigenfrequency ω_n . As we shall see in the Appendix, this

is justified as long as the cavity finesse is high enough and the eigenfrequencies of the nondegenerate modes are well separated from this subspace.

The output from the perturbed cavity can be obtained by projecting the input mode $|\text{in}\rangle$ onto the new basis $|n\rangle$ and calculating the phase shifts using the following relation:

$$|\text{out}\rangle = \sum_{n'=1}^{N} \frac{\gamma_c + i(\omega - \omega_{n'})}{\gamma_c - i(\omega - \omega_{n'})} |n'\rangle\langle n'| \text{in}\rangle.$$
 (13)

This procedure was applied to the LG_{3,3} degenerate space using the resonant frequencies of the previous section, ω_n . With the reference phase map scaled to 0.3 nm rms, the intensity profile of the resulting output mode is shown in Fig. 6.

IV. CONTRAST DEFECT

In gravitational-wave interferometers, contrast defect is defined as the ratio of the minimum possible optical power at the antisymmetric (dark) port to the power incident on the beam splitter. This quantity can be expressed as

$$C = \frac{P_{\rm AS}}{P_X + P_Y},\tag{14}$$

where X and Y are labels for the two arm cavities, $P_{\square} = \int \!\!\!\! \int_{\mathbb{R}^2} (\Psi^{\text{out}}_{\square})^* \Psi^{\text{out}}_{\square} dx dy$ and $\Psi^{\text{out}}_{AS} = \Psi^{\text{out}}_X - \Psi^{\text{out}}_Y$ represents the field at the antisymmetric port (AS) of the interferometer.

In principle, the dark port could be completely dark. However, the presence of intentional imbalances in the arms (finite beam splitter size, Schnupp asymmetry, etc.) and unintentional imperfections (mirror shape, scatter loss, mirror motion, etc.) result in imperfect destructive interference between the fields which recombine at the beam splitter. This imperfect interference leads to the leakage of some "junk" light to the dark port where the gravitational-wave signal is also detected. Excess light at the dark port can lead to a degradation of sensitivity via several mechanisms and compromise the robust operation of interferometer longitudinal and alignment control systems [20,21]. Contrast defect is thus a useful metric to employ when comparing interferometer configurations.

The above perturbation analysis shows that the fields resonating in the arm cavities of a real interferometer will no longer be pure $LG_{3,3}$ modes. Further, the relative amplitudes of the quasidegenerate modes are strongly dependent on mirror properties, which will, in general, be different for each arm. Hence, the perturbed arm cavity fields will interfere imperfectly at the beam splitter. We therefore expect an $LG_{3,3}$ interferometer to exhibit a larger contrast defect than, e.g., an $LG_{0,0}$ mode. We now test this hypothesis by analytical and numerical means.

A. Analytic calculation

According to the Appendix, the contrast defect in an interferometer with one perfect arm cavity and one perturbed arm cavity can be analytically written as

$$\epsilon = 1 - |\langle \text{in} | \text{out} \rangle|, \tag{15}$$

when the mirror perturbations are sufficiently small $(\epsilon \ll 1)$.

The Appendix also shows that, when a frequency shift is small compared with the line width of the cavity, i.e. $\omega - \omega_n \ll \gamma$, Eq. (17) can be approximated as

$$\epsilon = \left[\sum_{n'} \langle 33|\delta h|n'\rangle \langle n'|\delta h|33\rangle - \langle 33|\delta h|33\rangle^2 \right] \left(\frac{8\sqrt{2}\pi}{\lambda T} \right)^2, \tag{16}$$

where

$$\langle 33|\delta h|pl\rangle = \int \delta h(u_{33}^* u_{pl}) dx dy. \tag{17}$$

Alternatively, this can be written as

$$\epsilon = \left[\frac{(8\sqrt{2}\pi)}{\lambda T} \right]^2 \delta z^2, \tag{18}$$

where

$$\delta z^2 = \sum_{\substack{2p+|l|=10\\(p,l)\neq(33)}} |\langle 33|\delta h|pl\rangle|^2.$$
 (19)

This suggests that in order to minimize contrast defect, one must strive to suppress the projection of δh onto the nine complex basis functions, given by $u_{33}^*u_{pl}$. Since these

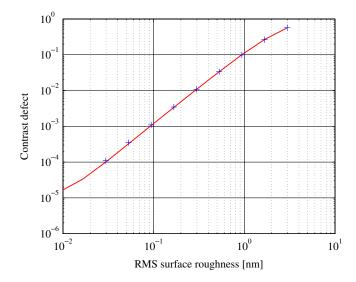


FIG. 7 (color online). Contrast defect with the ETM of one cavity perturbed by rescaling the reference phase map: solid red is from the analytical calculation, blue marker is from the FFT calculation.

functions are complex and δh is real, this actually corresponds to 18 basis functions.

Based on Eq. (13), the contrast defect has been evaluated analytically in the case that only the end mirror (ETM) of one cavity is perturbed with the reference phase map of Fig. 2. The perturbation for different rms values was obtained by rescaling the reference phase map. The results are shown in Fig. 7.

One can show that, for small perturbations, perturbing two cavity mirrors using phase maps derived from the same power spectral density function, will, on average, result in twice the contrast defect when compared to perturbations of a single mirror. However, depending on the spatial correlations between the mirrors, the contrast defect can be as much as twice the average in some cases.

B. Numerical calculation

To confirm the results obtained via perturbation theory and to extend our analysis to more complicated configurations, a parallel investigation was carried out using numerical methods. We utilized an FFT-based field propagation tool—the stationary interferometer simulation (SIS) [22].

SIS is predominantly used to inform the design of the Advanced LIGO interferometers and is under continuous development at Caltech's LIGO Laboratory. SIS employs an iterative procedure to find the stationary fields for a given optical configuration and input beam. Mirror surface maps can be generated from user-defined power spectral density functions, allowing one to study the effects of various hypothetical mirror aberrations. Cavity systems are "locked" using a Pound-Drever-Hall signal [23] to realize an operating condition similar to that which would be observed experimentally.

SIS was used to model Advanced LIGO Fabry-Perot arm cavities supporting $LG_{0,0}$, $LG_{3,3}$, and nearly concentric mesa modes [11,12]. The parameters of the $LG_{3,3}$ and mesa cavities (see Table III) were adjusted to yield systems with round-trip diffraction loss equivalent to that of the fiducial $LG_{0,0}$ resonator (≤ 1 ppm). In each case the input beam remained fixed as the beam which was ideally coupled to an unperturbed cavity. To suppress the aliasing effect, a larger FFT grid of 1024×1024 points on a $0.7 \text{ m} \times 0.7 \text{ m}$ square was used for all modes.

TABLE III. Cavity parameters used in the numerical simulations. All three resonators had a length of 3994.5 m. The mesa radii of curvature refer to the fiducial sphere from which the mesa correction profile is subtracted (cf. [11]). Cavity *g* factor is not well defined for mesa modes.

	LG _{0,0}	LG _{3,3}	Mesa
R_{itm}	1934 m	2857 m	1997.25 m
$R_{\rm etm}$	2245 m	2857 m	1997.25 m
Cavity g factor	0.83	0.16	

Initially SIS was used to simulate a configuration identical to that studied analytically. Under these conditions both sets of results are in good agreement (better than 10%) (see Figs. 6–8). The flexibility of SIS was then used to consider more complex simulations where both cavity mirrors are perturbed and to emulate a Fabry-Perot Michelson interferometer. SIS was also employed to study high-rms cases in which the analytic approximation breaks down.

For each simulation run, two random surfaces, with a specified rms roughness and a spatial spectrum approximating that of the first Advanced LIGO mirrors (see Fig. 1), were generated and added to the profiles of the cavity mirrors. SIS then evaluated the field Ψ^{out} reflected from the cavity at its operating point, which is chosen from the cavity which is locked by using the Pound-Drever-Hall error signal.

Results from two discrete, single-cavity simulations, representing the X and Y arms of an interferometer, were then combined according to Eq. (16) to estimate interferometer contrast defect. Multiple trials were conducted at each value of rms surface roughness with different random maps, allowing one to consider more than 100 unique arm cavity pairs. From these data, the mean and standard deviation of interferometer contrast defect were found as a function of mirror aberration rms. Results for all three beams are shown in Fig. 9. The simulated contrast defect for Gaussian beam (TEM00) is consistent with the measured value of LIGO, which is around 10^{-4} [24] and low enough for the effective detection.

Our numerical work confirms the result from perturbation theory; LG_{3,3} interferometers are more sensitive to mirror surface roughness than those supporting a fundamental Gaussian mode. We further show that LG_{3,3} beams are also outperformed in this respect by nearly concentric mesa beams, indicating that this sensitivity arises due to the properties of the Laguerre-Gauss mode itself and is not

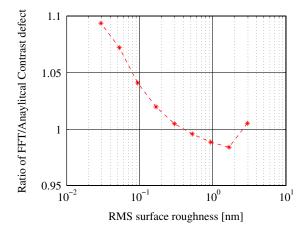


FIG. 8 (color online). Ratio, numerical/analytical, of single-cavity contrast defects calculated with the end mirror perturbed by a 0.3 nm rms figure error.

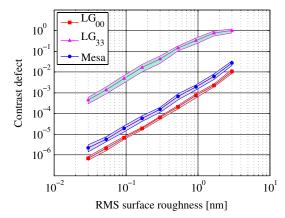


FIG. 9 (color online). Interferometer contrast defect as a function of test mass surface roughness (all four mirrors are perturbed with random phase map at the same level of rms). Solid markers report mean values of numerical results with the corresponding shaded regions illustrating 1 standard deviation (see IV B), which is roughly 4 times higher than the trace in Fig. 7.

an inevitable handicap for all beams capable of mitigating mirror thermal noise.

V. CONTRAST DEFECT IMPROVEMENT

Here we examine several methods of reducing the contrast defect.

A. Better polishing

The most direct approach is to reduce the mirror figure error. However, reaching appropriate levels of surface roughness is beyond the capabilities of current technology. We estimate that, in order to achieve reasonable performance, LG_{3,3} modes require mirrors with an rms roughness roughly 1 order of magnitude smaller than is currently

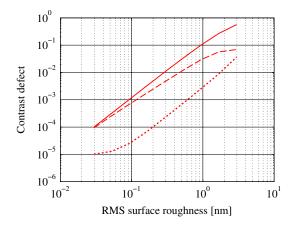


FIG. 10 (color online). Analytic calculation with different conditions for reducing the contrast defect: solid curve is the original contrast defect; dashed line has corrective rings added to the phase map; dotted curve is with detuned injecting laser frequency.

achievable (assuming the mirror coatings introduce no additional roughness, i.e. perfectly smooth, uniform coatings).

In the remainder of this section, we thus consider more unconventional means of reducing the contrast defect. Figure 10 shows the results of each investigation.

B. Arm cavity detuning

Equation (14) shows that the output field varies with the frequency of light injected into a cavity, or equivalently with cavity length. This motivated us to study the variation in contrast defect as a function of arm cavity detuning.

It was found that detuning was effective in modifying contrast defect. Unfortunately, the large detuning necessary to recover good contrast had the effect of simultaneously reducing the optical power circulating in the cavity.

With a detuning of 100 Hz (approximately two cavity linewidths), it was possible to recover acceptable contrast (dotted line, Fig. 10). However, the same detuning causes the circulating power to drop by $\sim 60\%$. We therefore do not consider this approach to be viable in gravitational-wave interferometers where the injected frequency is usually tuned to maximize the optical power circulating in the coupled-cavity system. This technique can, however, be considered for experiments where the thermal noise needs to be reduced, but the cavity's stored power is not of concern.

C. Mirror corrections

The increase in contrast defect observed when using LG_{3,3} modes in the presence of realistic surface roughness results from the presence of multiple pseudodegenerate higher-order modes. Here we attempt to see if this effect can be mitigated by depositing corrective structures on the mirror's surface.

By introducing material at the nodes of the desired $LG_{3,3}$ mode it was hoped that the unwanted modes from the same subspace could be suppressed.

As a concrete example, two Gaussian rings were added to the random phase map at nodes 1 and 3 of the $LG_{3,3}$ mode. Each ring was of the form:

$$f(x, y) = \frac{\lambda}{20} e^{-\{(r - r_p)^2 / [2(R/100)^2]\}},$$
 (20)

where r_p indicates the position of the different nodes. The frequency split is plotted in Fig. 11. Compared to Fig. 5, the frequency splits under this condition are much larger, therefore the other degenerate modes will be harder to excite.

The analytically computed contrast defect for this case is plotted as the dashed line in Fig. 10. Although the defect is improved for values of surface roughness similar to that which is currently achievable, we find that, in order to significantly break the modal degeneracy, the height of

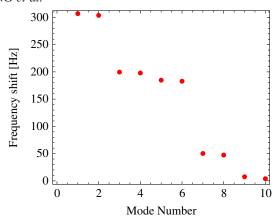


FIG. 11 (color online). Frequency shift in LG modes introduced by adding rings to the reference phase map.

the rings must be increased to such a degree that the induced scatter becomes unacceptably high ($\sim 500\,$ ppm), reducing the stored power and thus the interferometer's phase sensitivity. We hence conclude that this approach is not promising.

At Caltech, Yamamoto has studied a similar approach whereby the mirror reflectivity is set to zero at the nodes of the LG_{3,3} mode [25]. This technique was found to be similarly unsuitable for application to gravitational-wave interferometers.

D. Mode healing

Previous work [26] has shown that the presence of a signal recycling cavity can substantially reduce the contrast defect in the case where the resonant mode in the interferometer is TEM_{0.0}. The higher-order transverse modes are not resonant in the signal recycling cavity and are therefore suppressed. In the LG_{3,3} case, however, the signal cavity is resonant for the LG_{3,3} mode as well as all of the modes which are in the degenerate subspace. Therefore, our expectation is that there would not be a mode healing effect when using any higher-order mode which can be split in this way. In the case where the signal recycling cavity is detuned to amplify the gravitationalwave response at a particular frequency, the situation could be significantly more complicated due to the frequency splitting shown in Fig. 5. To quantitatively explore the effect of the compound cavity on degenerate modes, further analytic and numerical work is required.

VI. CONCLUSIONS

In this paper, we use numerical analysis as well as perturbation theory to analyze the modes of a Fabry-Perot cavity resonating a LG_{3,3} beam. We prove that with realistic mirror figure errors, the real output mode of the cavity will change significantly, resulting in an unacceptable increase of the contrast defect.

We also investigate unconventional corrective techniques to reduce the contrast defect. While they turn out to be unsuitable for quantum shot noise limited interferometers, they may have some utility for other classes of cavities. For LG_{3,3} modes to function effectively, we estimate that surface figure errors must be reduced to the order of 10^{-2} nm rms to achieve the required contrast defect of LIGO ($\sim 10^{-4}$). Such precise polishing and coating uniformity will likely not be available for several years. Using high-order Laguerre-Gauss modes in standard spherical mirror cavities appears to be a poor choice in light of current technologies.

Numerical simulations using mesa and normal Gaussian beams show these beams are not so sensitive to figure errors. Future effort will be directed toward the construction of a new family of optical modes which can reduce the thermal-noise impact while simultaneously being robust against mirror imperfections.

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APPENDIX: CONTRAST DEFECT

Here we show that the contrast defects defined in Eqs. (15) and (14) are equivalent in the limit of small perturbations. We denote the input and output field for the two cavities (X and Y) as $|\text{in}\rangle_X$, $|\text{out}\rangle_X$, $|\text{in}\rangle_Y$, $|\text{out}\rangle_Y$. In our analytical calculation, we assume the input and output fields of each cavity are normalized, because we ignore transmissivity of the ETM, and the diffraction loss, so that we have

$$\langle \text{in}|\text{in}\rangle_X = \langle \text{in}|\text{in}\rangle_Y = \langle \text{out}|\text{out}\rangle_X = \langle \text{out}|\text{out}\rangle_Y = 1.$$
 (A1)

We can then write

$$P_X = \langle \text{in}|\text{in}\rangle_X = 1, \qquad P_Y = \langle \text{in}|\text{in}\rangle_Y = 1$$
 (A2)

and the power at the antisymmetric port can be written as

$$P_{AS} = \| |\operatorname{out}\rangle_{X} - |\operatorname{out}\rangle_{Y} \|^{2}$$

$$= 2 - \langle \operatorname{out}|\operatorname{out}\rangle_{XY} - \langle \operatorname{out}|\operatorname{out}\rangle_{YX}.$$
 (A3)

With the definition of contrast defect in Eq. (15), we have

$$\epsilon_X = 1 - |\langle \text{in} | \text{out} \rangle_X|, \qquad \epsilon_Y = 1 - |\langle \text{in} | \text{out} \rangle_Y| \quad (A4)$$

so that we can write the output field as

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$$\begin{aligned} |\text{out}\rangle_X &= (1 - \epsilon_X)e^{i\phi_X}|\text{in}\rangle_X + |\delta_X\rangle \\ |\text{out}\rangle_Y &= (1 - \epsilon_Y)e^{i\phi_Y}|\text{in}\rangle_Y + |\delta_Y\rangle, \end{aligned} \tag{A5}$$

where

$$\langle \delta_X | \text{in} \rangle_X = 0,$$
 $\langle \delta_X | \delta_X \rangle = \epsilon_X$ $\langle \delta_Y | \text{in} \rangle_Y = 0,$ $\langle \delta_Y | \delta_Y \rangle = \epsilon_Y$ $\langle \delta_X | \text{in} \rangle_Y = \langle \delta_Y | \text{in} \rangle_X = 0.$ (A6)

In both the analytical and numerical calculations, we assume one of the two interferometer cavities is perfect and the other is with mirror figure errors, so here we can write $\epsilon_Y=1, |\delta_Y\rangle=0$, therefore, to the first-order approximation ($\epsilon_X\ll 1$), we obtain

$$P_{\rm AS} = 2\epsilon_X \tag{A7}$$

which shows that the contrast defect defined in Eq. (14) is the same as the analytical definition in Eq. (15).

When we consider two cavities both with imperfections, if they are statistically independent, we can write $\langle \delta_X | \delta_Y \rangle = 0$, so that the average value of the contrast defect of the system is

$$P_{\rm AS} = 2(\epsilon_X + \epsilon_Y). \tag{A8}$$

We now show that Eq. (15) can be approximately written as given in Eq. (16). From Eq. (13), we have

$$\langle \text{in} | \text{out} \rangle = \sum_{n'} \frac{\gamma + i(\omega - \omega_n')}{\gamma - i(\omega - \omega_{n'})} \langle \text{in} | n' \rangle \langle n' | \text{in} \rangle$$
 (A9)

when $\omega - \omega_{n'} \ll \gamma$, Eq. (A9) can be expanded as

$$\sum_{n'} \left[1 + \frac{2i(\omega - \omega_{n'})}{\gamma} - \frac{2(\omega - \omega_{n'})^2}{\gamma^2} \right] \langle \operatorname{in}|n'\rangle \langle n'|\operatorname{in}\rangle. \tag{A10}$$

Note that when the mode frequency is shifted $\omega_{n'}$, the optical power in the cavity is maximized, so that the linear term vanishes, therefore that the modulated frequency of the beam ω can be given by

$$\omega = \frac{kc}{L} \langle 33 | \delta h | 33 \rangle. \tag{A11}$$

The contrast defect defined in Eq. (15) is

$$\epsilon = \sum_{n'} \frac{2(\omega - \omega_{n'})^2}{\gamma^2} \langle \text{in} | n' \rangle \langle n' | \text{in} \rangle$$

$$= \frac{2}{\gamma^2} \left(\sum_{n'} \langle \text{in} | n' \rangle \omega_{n'}^2 \langle n' | \text{in} \rangle - \omega^2 \right). \tag{A12}$$

After perturbation, the frequency split is the eigenvalue of the matrix given in Eq. (9) and the eigenvector of the matrix is the real eigenmode of the cavity, thus we can write

$$\sum_{n'} \langle \operatorname{in}|n' \rangle \omega_{n'}^{2} \langle n'|\operatorname{in} \rangle = \left(\frac{2\pi c}{\lambda L}\right)^{2} \sum_{n'm'l'} \langle \operatorname{in}|n' \rangle \langle n'|\delta h|m' \rangle$$

$$\times \langle m'|\delta h|l' \rangle \langle l'|\operatorname{in} \rangle$$

$$= \left(\frac{2\pi c}{\lambda L}\right)^{2} \sum_{m'} \langle \operatorname{in}|\delta h|m' \rangle \langle m'|\delta h|\operatorname{in} \rangle,$$
(A13)

where $\gamma = cT/4L$. Then, in this limit, when the injected field is $|33\rangle$, the contrast defect can be written as in Eq. (16).

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