First principles determination of bubble wall velocity

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The terminal wall velocity of a first-order phase transition bubble in the early Universe can be calculated from a set of fluid equations describing the scalar fields and the plasma's state. We rederive these equations from the energy-momentum tensor conservation and the Boltzmann equation, without linearizing in the background temperature and fluid velocity. The resulting equations have a finite solution for any wall velocity. We propose a spectral method to integrate the Boltzmann equation, which is simple, efficient, and accurate. As an example, we apply this new methodology to the singlet scalar extension of the standard model. We find that all solutions are naturally categorized as deflagrations ($v_w \sim c_s$) or ultrarelativistic detonations ($\gamma_w \gtrsim 10$). Furthermore, the contributions from out-of-equilibrium effects are, most of the time, subdominant. Finally, we use these results to propose several approximation schemes with increasing levels of complexity and accuracy. They can be used to considerably simplify the methodology, while correctly describing the qualitative behavior of the bubble wall.

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I. INTRODUCTION

First-order phase transitions (FOPTs) can produce striking cosmological signatures that may provide a window into high-energy physics and the history of the early Universe. Recently, the prospect of probing these signals for the first time through the upcoming space-based gravitational wave (GW) detector LISA [1–3], DECIGO [4,5], and BBO [6,7] has stimulated a great interest in models that predict strong FOPTs [8–19]. Such FOPTs can also potentially provide the departure from equilibrium needed for baryogenesis and thereby explain the origin of the baryon asymmetry of the Universe. One of the popular scenarios is electroweak baryogenesis [20–23] because of its testability in collider experiments, in realizations involving simple or well-motivated extensions of the Standard Model (SM) [9,24–52].

To accurately predict the cosmological signature of a FOPT, it is important to understand its dynamics in some detail. An essential quantity, which is also notoriously challenging to compute, is the bubble wall terminal velocity v_w . Several methods have been developed to determine it, as described below, which all essentially consist in requiring that the driving force on the wall be equal to the friction, or "backreaction," force from the plasma. The main

differences between the methods is in how the plasma's distribution functions are represented and calculated.

A common strategy is to assume that all the species in the plasma are in local thermal equilibrium at the same temperature and fluid velocity [53–56]. These two thermodynamic quantities can then be computed from a set of hydrodynamic equations derived from the conservation of the energy-momentum tensor (EMT). A more general approach is to allow the heavy species to be out of equilibrium, with the remaining degrees of freedom forming a "background" plasma in equilibrium [57–63]. These distribution functions are usually computed from a set of Boltzmann equations. The procedure introduced in this work uses some aspects of both of these methods.¹

The standard formalism to solve the Boltzmann equations consists in using an ansatz for the distribution function. In the seminal Refs. [57,58], the out-ofequilibrium species were only allowed to deviate from the background distribution function by a perturbation of the temperature, velocity, and chemical potential. The Boltzmann equation was then linearized in these perturbations and truncated by taking three linearly independent moments. This procedure yields a set of three moment equations that can be solved for the perturbations.

Strikingly, these equations suffer from a singularity when the wall velocity v_w reaches the speed of sound $c_s \approx 1/\sqrt{3}$, which makes the background perturbations diverge. This prevents an accurate description of fast-moving walls,

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¹See also Ref. [64] for a derivation of the bubble wall velocity from the holographic correspondence.

which has given rise to two schools of thought. The first one considers that this singularity of the moment equations is unphysical and is merely an artifact of an unsuitable representation of the full Boltzmann equation [61,65]. More specifically, it was argued that the singularity is a consequence of a bad choice of moments or ansatz and, instead, a truncation scheme for the moment expansion was proposed, which yields finite solutions even at $v_w = c_s$. On the other hand, Refs. [62,66] argued that the singularity is caused by the linearization of the Boltzmann equation, and they proposed a generalized ansatz for the out-ofequilibrium distribution functions to more accurately represent the full Boltzmann equation, while interpreting that the singularity has a physical origin: a "sonic boom."

In this work, we advocate a middle ground by maintaining that the singularity of the moment expansion is unphysical and can be induced by an overly restrictive ansatz, while recognizing that the linearization of the background perturbations is the root of the problem, as was argued in Ref. [62]. (In contrast, the out-of-equilibrium perturbations can be safely linearized.) Based on this interpretation, we propose a solution to the problem of supersonic walls by solving nonlinearly for the background perturbations. Then the only danger in choosing a particular ansatz is that it may not give a very accurate representation of the exact solution. Our method will also avoid this pitfall by expanding the perturbations in a large enough basis of orthogonal polynomials so that convergence to the exact solution is achieved.

We start in Sec. II by rederiving the fluid equations used to compute the wall velocity. Our methodology differs from the standard approach by linearizing only when necessary to obtain equations that are numerically tractable. This strategy leads to a set of Boltzmann equations for each heavy out-of-equilibrium species, in which we only linearize the collision operators, and a set of hydrodynamic equations that describe the background fluid in local thermal equilibrium. We do not linearize the latter, which yields a finite solution for every wall velocity.

Then, we propose in Sec. III a novel spectral method to solve the Boltzmann equations. It uses a spectral ansatz that can be as general as needed and yields a high accuracy with great efficiency. Moreover, we believe it simpler to implement than the standard moment expansion. In Sec. IV, we apply this new methodology to a benchmark model: the Z_2 -symmetric singlet scalar extension of the SM. We study its consequences for the wall velocity and shape and reassess the importance of the out-of-equilibrium contributions. We use these results in Sec. V to motivate several approximation schemes with increasing levels of complexity and accuracy. They allow to correctly describe the qualitative behavior of the wall dynamics, while substantially simplifying the fluid equations. Conclusions are given in Sec. VI. Finally, details about the calculation of the collision integrals are presented in Appendix A, and the boundary conditions of the hydrodynamic equations are computed in Appendix B.

II. FLUID EQUATIONS

The wall terminal velocity and shape can be determined by solving a set of fluid equations describing the evolution of the plasma and the scalar fields. These equations consist of the EMT conservation and a set of Boltzmann equations describing the plasma's departure from equilibrium. In general, a static solution corresponding to the terminal state of the wall can only be found for discrete values of v_w .

In this section, we derive these fluid equations in a completely Lorentz invariant way. They form a highly nontrivial nonlinear eigenvalue problem that must be solved for the wall velocity.

A. Boltzmann equation

The relativistic Boltzmann equation that describes the evolution of the distribution functions $f_i(p^{\mu}, x^{\mu})$ takes the form

$$(p^{\mu}\partial_{\mu} + m_i F^{\mu}_i \partial_{p^{\mu}}) f_i(p^{\mu}, x^{\mu}) = -\mathcal{C}_i[f_j], \qquad (1)$$

where $m_i F_i^{\mu} = \partial^{\mu}(m_i^2)/2$ is the *CP*-even force applied on the particles by the moving wall,² and $C[f_j]$ is a nonlinear collision integral. To keep Lorentz invariance manifest, the 4-momenta p^{μ} is set to its on-shell value $(p^0 = \sqrt{m^2 + |\mathbf{p}|^2})$ only after the derivatives of f_i are taken, so that one can assume $\partial_{\mu} p^{\nu} = 0$ and $\partial_{p^{\mu}} p^{\nu} = \delta_{\mu}^{\nu}$.

If the bubble radius is much larger than its width, the wall can be approximated to be planar and moving in the +zdirection. In that case, translational invariance in the plane parallel to the wall implies that none of the quantities in Eq. (1) depend on the x and y coordinates. Furthermore, they should only depend on the distance from the wall $\xi \equiv -\bar{u}_w^{\mu} x_{\mu} = \gamma_w (z - v_w t)$, where $\bar{u}_w^{\mu} = \gamma_w (v_w, 0, 0, 1)$ is the 4-velocity perpendicular to the wall 4-velocity $u_w^{\mu} = \gamma_w (1, 0, 0, v_w)$. This allows us to write the derivative with respect to the coordinates as

$$\partial^{\mu} = \partial^{\mu} \xi \partial_{\xi} = -\bar{u}^{\mu}_{w} \partial_{\xi}. \tag{2}$$

In general, the distribution functions can be written as the sum of an equilibrium distribution,

$$f_i^{\rm eq}(p^{\mu},\xi) = \frac{1}{\exp[p_{\mu}u_{\rm pl}^{\mu}(\xi)/T(\xi)] \pm 1},$$
 (3)

and some function describing the deviation from equilibrium $\delta f_i(\vec{p},\xi)$:

$$f_i(p^{\mu},\xi) = f_i^{\text{eq}}(p^{\mu},\xi) + \delta f_i(p^{\mu},\xi).$$
(4)

In this parametrization, all the species share the same local temperature $T(\xi)$ and local plasma 4-velocity

 $^{^{2}}$ A more general expression would also include a *CP*-odd force, which plays an important role in baryogenesis.

 $u_{\rm pl}^{\mu}(\xi) \equiv \gamma_{\rm pl}(\xi)(1,0,0,v_{\rm pl}(\xi))$, which can both depend on ξ . We use the convention where $v_{\rm pl} \leq 0$ and $v_w \geq 0$, which corresponds to the wall moving in the positive *z* direction.

In previous studies, the position-dependent temperature was generally written as $T(\xi) = T + \delta T_{bg}(\xi)$ [and similarly for $v_{\rm pl}(\xi)$], where \bar{T} is an arbitrary constant temperature, and $\delta T_{\rm bg}$ is a small temperature deviation of the background species (the light species in local thermal equilibrium). This deviation was found by solving a Boltzmann equation similar to Eq. (1) and linearized in $\delta T_{\rm bg}$. However, Ref. [62] has argued that this linearization leads to a singularity of the fluid equations which makes the fluid temperature and velocity diverge when the wall velocity approaches the speed of sound. Fortunately for us, it is not necessary to linearize the Boltzmann in the background perturbations to make it numerically tractable. It is sufficient to linearize only the collision operator $C_i[\delta f_i]$, in terms of δf_i (see Appendix A), which does not induce any singularity in the equations.³

One might wonder whence this fundamental difference between the background and out-of-equilibrium perturbations arises, that only the former causes a singularity when linearized. There are two main reasons for the differing behaviors: the background perturbations are constrained by EMT conservation, and they are the only perturbations undamped by $C_i[f_i]$. The constraints from EMT conservation lead to a set of hydrodynamic equations derived in the next subsection. Reference [62] has shown that, when linearized, these equations are singular at $v_w = c_s$, if local thermal equilibrium is assumed. One could try to solve the problem by relaxing this last assumption, by allowing the background fluid to be out of equilibrium. While this might work close to the wall, it is doomed to fail away from it since all these out-of-equilibrium perturbations are exponentially damped by $C_i[f_i]$, which ensures that the plasma is in local thermal equilibrium at infinity.

Therefore, the only way to remove the unphysical singularity is to keep the full nonlinear dependence on $T(\xi)$ and $v_{\rm pl}(\xi)$. We determine these directly from the hydrodynamic equations,⁴ which will be derived in the next subsection.

Substituting Eqs. (2) and (4) into Eq. (1), one obtains

$$\left(\mathcal{P}_{w}\partial_{\xi} - \frac{1}{2}\partial_{\xi}(m_{i}^{2})\bar{u}_{w}^{\mu}\partial_{p^{\mu}}\right)\delta f_{i} = -\mathcal{C}_{i}^{\mathrm{lin}}[\delta f_{j}] + \mathcal{S}_{i}, \quad (5)$$

where we introduce the notation $\mathcal{E}_a \equiv p_\mu u_a^\mu$ and $\mathcal{P}_a \equiv -p_\mu \bar{u}_a^\mu$ with $a \in \{\text{pl}, w\}$, which are Lorentz invariant

quantities corresponding, respectively, to the energy and *z*-momentum in the plasma (pl) and wall (*w*) frames. Note that $C^{\text{lin}}[\delta f]$ is the linearized collision operator, which can safely be used instead of $C[\delta f]$ since δf is not subject to the same constraint as the background perturbations that caused the singularity. Moreover, the deviation from equilibrium is expected to be small, so neglecting the higher order terms should be a reasonable approximation. See Appendix A for more details about $C^{\text{lin}}[\delta f]$. The source term in Eq. (5) is

$$S_{i} = -\left(\mathcal{P}_{w}\partial_{\xi} - \frac{1}{2}\partial_{\xi}(m_{i}^{2})\bar{u}_{w}^{\mu}\partial_{p^{\mu}}\right)f_{i}^{\mathrm{eq}}$$

$$= f_{i}^{\prime}\frac{\mathcal{P}_{w}}{T}\left[\gamma_{\mathrm{pl}}^{2}\mathcal{P}_{\mathrm{pl}}\partial_{\xi}v_{\mathrm{pl}} + \mathcal{E}_{\mathrm{pl}}\frac{\partial_{\xi}T}{T}\right] + \frac{1}{2}\partial_{\xi}(m_{i}^{2})\bar{u}_{w,\mu}u_{\mathrm{pl}}^{\mu}\frac{f_{i}^{\prime}}{T},$$

(6)

with

$$f'_{i} \equiv -\frac{e^{\mathcal{E}_{\rm pl}/T}}{(e^{\mathcal{E}_{\rm pl}/T} \pm 1)^{2}}.$$
(7)

B. Hydrodynamic equations

The starting point to derive the hydrodynamic equations and the scalar fields' equations of motion is the conservation of stress energy. The EMT of the vacuum contribution from N scalar fields ϕ_i is

$$T^{\mu\nu}_{\phi} = \partial^{\mu}\phi_{i}\partial^{\nu}\phi_{i} - \eta^{\mu\nu} \bigg[\frac{1}{2}\partial_{\alpha}\phi_{i}\partial^{\alpha}\phi_{i} - V_{0}(\phi_{j}) \bigg], \quad (8)$$

where repeated indices are summed over, and $V_0(\phi_j)$ is the scalar fields' vacuum potential, including loop corrections. One also needs to include the contribution from the plasma, which can be written in terms of the distribution functions f_i as

$$T_{\rm pl}^{\mu\nu} = \sum_{i} \int \frac{d^3 p}{(2\pi)^3 E_i} p^{\mu} p^{\nu} f_i(p^{\mu}, \xi), \qquad (9)$$

where the sum is over all the plasma's degrees of freedom.

One can substitute the ansatz (4) to express $T_{pl}^{\mu\nu}$ as a sum of equilibrium and out-of-equilibrium contributions:

$$T_{\rm pl}^{\mu\nu} = T_{\rm eq}^{\mu\nu} + T_{\rm out}^{\mu\nu},$$

$$T_{\rm eq}^{\mu\nu} = \sum_{i} \int \frac{d^{3}p}{(2\pi)^{3}E_{i}} p^{\mu}p^{\nu}f_{i}^{\rm eq}(p^{\mu},\xi),$$

$$T_{\rm out}^{\mu\nu} = \sum_{i} \int \frac{d^{3}p}{(2\pi)^{3}E_{i}} p^{\mu}p^{\nu}\delta f_{i}(p^{\mu},\xi).$$
 (10)

Using Lorentz covariance, one can write $T_{eq}^{\mu\nu}$ as

³The failure of linearization in $\delta T_{\rm bg}$ and $\delta v_{\rm bg}$ occurs not because these quantities ever become large, but rather because the Liouville operator of the Boltzmann equation becomes singular, unless higher order terms are retained [62].

⁴This method has already been used in Refs. [55,56] for a plasma in local thermal equilibrium. We here extend their derivation to include out-of-equilibrium perturbations.

$$T_{\rm eq}^{\mu\nu} = w u_{\rm pl}^{\mu} u_{\rm pl}^{\nu} - p \eta^{\mu\nu}, \qquad (11)$$

where the thermal pressure p and enthalpy w are

$$p = \pm T \sum_{i} \int \frac{d^{3}p}{(2\pi)^{3}} \log \left[1 \pm \exp(-E_{i}/T)\right],$$
$$w = T \frac{\partial p}{\partial T},$$
(12)

with E_i defined in the plasma rest frame and the +/- signs denoting fermions/bosons.

Similarly to Eq. (11), one can use Lorentz covariance and the symmetry of the EMT under $\mu \leftrightarrow \nu$ to express $T_{out}^{\mu\nu}$ as a linear combination of the tensors $\eta^{\mu\nu}$, $u_{pl}^{\mu}u_{pl}^{\nu}$, $\bar{u}_{pl}^{\mu}\bar{u}_{pl}^{\nu}$, and $(u_{pl}^{\mu}\bar{u}_{pl}^{\nu} + \bar{u}_{pl}^{\mu}u_{pl}^{\nu})$:

$$T_{\text{out}}^{\mu\nu} = T_{\text{out},\eta}\eta^{\mu\nu} + T_{\text{out},u}^{\mu\nu}, \qquad (13)$$

with

$$\begin{split} T_{\text{out},\eta} &= \frac{1}{2} \sum_{i} (m_{i}^{2} \Delta_{00}^{i} + \Delta_{02}^{i} - \Delta_{20}^{i}), \\ T_{\text{out},u}^{\mu\nu} &= \frac{1}{2} \sum_{i} [(3\Delta_{20}^{i} - \Delta_{02}^{i} - m_{i}^{2} \Delta_{00}^{i}) u_{\text{pl}}^{\mu} u_{\text{pl}}^{\nu} \\ &+ (3\Delta_{02}^{i} - \Delta_{20}^{i} + m_{i}^{2} \Delta_{00}^{i}) \bar{u}_{\text{pl}}^{\mu} \bar{u}_{\text{pl}}^{\nu} \\ &+ 2\Delta_{11}^{i} (u_{\text{pl}}^{\mu} \bar{u}_{\text{pl}}^{\nu} + \bar{u}_{\text{pl}}^{\mu} u_{\text{pl}}^{\nu})], \end{split}$$
(14)

and

$$\Delta_{mn}^{i}(\xi) = \int \frac{d^{3}p}{(2\pi)^{3}E} \mathcal{E}_{pl}^{m} \mathcal{P}_{pl}^{n} \delta f_{i}(p^{\mu},\xi).$$
(15)

Conservation of the EMT is then given by

$$0 = \partial_{\mu}T^{\mu\nu} = \partial_{\mu}(T^{\mu\nu}_{\phi} + T^{\mu\nu}_{eq} + T^{\mu\nu}_{out})$$

$$= \partial^{\nu}\phi_{i}\left[\partial^{2}\phi_{i} + \frac{\partial V_{T}(\phi_{j}, T)}{\partial\phi_{i}} + \frac{\partial T_{out,\eta}}{\partial\phi_{i}}\right] - \partial^{\nu}T\frac{\partial p}{\partial T}$$

$$+ (\partial^{\nu}T_{out,\eta})_{\phi} + \partial_{\mu}(wu^{\mu}_{pl}u^{\nu}_{pl} + T^{\mu\nu}_{out,u}), \qquad (16)$$

where $V_T \equiv V_0 - p$, and the subscript ϕ indicates that the scalar fields ϕ_i are kept constant. We recognize the quantity in brackets as the equation of motion for the scalar fields, which must vanish independently of the rest of Eq. (16):

$$\partial^2 \phi_i + \frac{\partial V_T(\phi_j, T)}{\partial \phi_i} + \sum_j \frac{\partial (m_j^2)}{\partial \phi_i} \frac{\Delta_{00}^j}{2} = 0, \quad (17)$$

where we assume that the only dependence of $T_{\text{out},\eta}$ on ϕ_i comes from the explicit factor of m_i^2 multiplying Δ_{00}^j .

To derive the last two equations that describe the evolution of $T(\xi)$ and $v_{\rm pl}(\xi)$, it is convenient to write Eq. (16) in the frame of the wall, where all the quantities depend only on the *z* coordinate. Conservation of the EMT can then be written as

$$T^{30} = w\gamma_{\rm pl}^2 v_{\rm pl} + T_{\rm out}^{30} = c_1,$$

$$T^{33} = \frac{1}{2} (\partial_z \phi_i)^2 - V_T(\phi_j, T) + w\gamma_{\rm pl}^2 v_{\rm pl}^2 + T_{\rm out}^{33} = c_2, \quad (18)$$

where c_1 and c_2 are constants that depend on T_- and v_- (or alternatively on T_+ and v_+), which denote the fluid temperature and velocity at $z \to \mp \infty$. These can be computed as functions of v_w using the method described in Ref. [67], which is summarized in Appendix B.

In practice, one can directly solve the first line of Eq. (18) for v_{pl} :

$$v_{\rm pl} = \frac{-w + \sqrt{4s_1^2 + w^2}}{2s_1},\tag{19}$$

with $s_1 = c_1 - T_{out}^{30}$. Substituting v_{pl} into the equation for T^{33} yields

$$\frac{1}{2}(\partial_z \phi_i)^2 - V_T - \frac{1}{2}w + \frac{1}{2}\sqrt{4s_1^2 + w^2} - s_2 = 0, \quad (20)$$

where $s_2 = c_2 - T_{out}^{33}$; this can be solved numerically for the temperature as a function of the scalar fields.

In addition to Eqs. (17) and (20), one must impose boundary conditions on the scalar fields to insure that they start and end in the false and true vacua, respectively:

$$\phi_i(z \to \pm \infty) = \phi_i^{\pm},\tag{21}$$

where ϕ_i^{\pm} satisfy

$$0 = \frac{\partial V_T}{\partial \phi_i} \bigg|_{\phi_i = \phi_i^{\pm}, T = T_{\pm}}.$$
 (22)

However, the boundary conditions (21) are insufficient for specifying a unique solution. Effectively, all the hydrodynamic equations and boundary conditions derived so far are invariant under translations along the z axis. This implies that there exists a continuous family of solutions related to one another via the substitution $z \rightarrow z + a$, $a \in \mathbb{R}$. To remove this degeneracy, one must give an additional boundary condition that specifies the position of the wall. We choose here to impose

$$\phi_1(z=0) = \frac{\phi_1^- + \phi_1^+}{2}.$$
 (23)

The resulting system of equations naively appears to be overconstrained, as there are now more boundary conditions than the number of differential equations. The additional constraint serves to determine the unknown wall velocity v_w , which plays the role of a nonlinear eigenvalue for the system of equations (17), (18), (21), and (23). Formally, this can be handled by promoting v_w to an undetermined function $v_w(z)$ with the differential equation

$$\partial_z v_w(z) = 0, \tag{24}$$

which, of course, enforces that v_w is a constant.

III. SPECTRAL SOLUTION OF THE BOLTZMANN EQUATION

The Boltzmann equation (5) is notoriously difficult to solve, being a partial integrodifferential equation involving the nonlocal collision operator C[f], which can be laborious to compute. We present here a spectral method that can efficiently deal with such difficulties. The basic idea behind the spectral method is to expand the unknown functions in series of orthogonal polynomials. Doing this transforms the differential equation into an algebraic equation that can be solved for the series' coefficients. For smooth functions, the convergence of the spectral series is exponential, promoting a high level of accuracy in the solutions.

There is no unique way to define the spectral expansion; in principle, any set of orthogonal polynomials can be used, and most of them have similar convergence properties. The optimal choice ultimately depends on the domain of integration and the nature of the solution. Fortunately, there exists a significant body of empirical evidence to help optimize the choice of basis polynomials. We refer the reader to Ref. [68] for more details.

For the expansion of the function $\delta f(p^{\mu}, \xi)$, the first thing one must consider is the choice of independent variables to represent the momentum p^{μ} . The symmetries of Eq. (5) dictate that δf should be independent of the azimuthal angle, determined by p_y/p_x . Moreover, it greatly simplifies the equations to choose variables that are independent of the position, Lorentz invariant, that can efficiently represent the fluid's state, and that are defined on a simple domain. A simple choice that satisfies these criteria is the component parallel to the wall p_{\parallel} and the z component in the frame of the fluid at $\xi = 0$, $\mathcal{P}_{pl_0} \equiv$ $-p_{\mu} \bar{u}^{\mu}_{pl_0}$ with $\bar{u}^{\mu}_{pl_0} \equiv \bar{u}^{\mu}_{pl}|_{\xi=0}$. For the system of basis functions, we choose the

For the system of basis functions, we choose the Chebyshev polynomials with an appropriate change of variables to map the infinite domain to [-1, 1]. For the momenta, we choose the exponential mappings

$$\rho_{z}(\mathcal{P}_{\mathrm{pl}_{0}}) = \tanh\left(\frac{\mathcal{P}_{\mathrm{pl}_{0}}}{2T_{0}}\right), \quad \rho_{\parallel}(p_{\parallel}) = 1 - 2e^{-p_{\parallel}/T_{0}}, \quad (25)$$

with $T_0 \equiv T_{\xi=0}$,⁵ which ensure that δf decays asymptotically like e^{-p/T_0} for $p \to \infty$. Since the decay length in the ξ direction is *a priori* unknown, we prefer to use an algebraic mapping for this variable, as it offers more flexibility than the exponential one:

$$\chi(\xi) = \frac{\xi}{\sqrt{\xi^2 + L_{\xi}^2}},\tag{26}$$

where L_{ξ} is a constant that should be similar in magnitude to the decay length of δf in the ξ direction.

Expressed in this set of variables, and omitting the species index, the spectral expansion of δf is

$$\delta f(\chi, \rho_z, \rho_{\parallel}) = \sum_{i=2}^{M} \sum_{j=2}^{N} \sum_{k=1}^{N-1} a_{ijk} \bar{T}_i(\chi) \bar{T}_j(\rho_z) \tilde{T}_k(\rho_{\parallel}), \quad (27)$$

where \overline{T} and \widetilde{T} are two sets of restricted Chebyshev polynomials defined by

$$\bar{T}_{i}(x) = \begin{cases} T_{i}(x) - T_{0}(x), & i \text{ even} \\ T_{i}(x) - T_{1}(x), & i \text{ odd}, \end{cases}$$
$$\tilde{T}_{i}(x) = T_{i}(x) - T_{0}(x), \qquad (28)$$

which are constructed in such a way that δf automatically satisfies the boundary conditions

$$\delta f(\xi \to \pm \infty, \mathbf{p}) = \delta f(\xi, |\mathbf{p}| \to \infty) = 0.$$
 (29)

The linearized collision integral $C_{\text{lin}}[\delta f]$ can also be expressed as a spectral series by using Eq. (27) and the properties of linear operators:

$$\mathcal{C}[\delta f] = \mathcal{C}\left[\sum_{i=2}^{M}\sum_{j=2}^{N}\sum_{k=1}^{N-1}a_{ijk}\bar{T}_{i}(\chi)\bar{T}_{j}(\rho_{z})\tilde{T}_{k}(\rho_{\parallel})\right]$$
$$= \sum_{i=2}^{M}\sum_{j=2}^{N}\sum_{k=1}^{N-1}a_{ijk}\bar{T}_{i}(\chi)\mathcal{C}[\bar{T}_{j}(\rho_{z})\tilde{T}_{k}(\rho_{\parallel})].$$
(30)

The functions $C[\bar{T}_j(\rho_z)\tilde{T}_k(\rho_{\parallel})]$ depend only on the momenta and not on δf ; hence one need compute them only once. These functions can be approximated as another spectral series,

⁵We use T_0 instead of $T(\xi)$ to avoid having ξ dependence in the momentum mapping. Since $T(\xi)$ varies only slightly across the wall, this does not significantly affect the convergence of the spectral method.

$$\mathcal{C}[\bar{T}_j(\rho_z)\tilde{T}_k(\rho_{\parallel})] \cong \sum_{l=2}^N \sum_{m=1}^{N-1} c_{lm}^{jk} \bar{T}_l(\rho_z)\tilde{T}_m(\rho_{\parallel}), \quad (31)$$

where the coefficients c_{lm}^{jk} can be determined using the method described below. This procedure requires the values of $C[\bar{T}_j(\rho_z)\tilde{T}_k(\rho_{\parallel})]$ with j = 2, ..., N and k = 1, ..., N - 1, each on a grid of $(N-1)^2$ points, for a total of $\mathcal{O}(N^4)$ terms. These can be computed with the method described in Appendix A.

The Boltzmann equation (5) can finally be written in terms of the spectral expansions (27), (30), and (31) as

$$0 = S(\chi, \rho_z, \rho_{\parallel}) - \sum_{ijk} a_{ijk} \left\{ \bar{T}_i(\chi) \sum_{lm} c_{lm}^{jk} \bar{T}_l(\rho_z) \tilde{T}_m(\rho_{\parallel}) \right. \\ \left. + \partial_{\xi} \chi \left[\mathcal{P}_w \partial_{\chi} - \frac{\gamma_w}{2} \partial_{\chi}(m^2) (\partial_{p_z} \rho_z) \partial_{\rho_z} \right] \right.$$

$$\left. \times \bar{T}_i(\chi) \bar{T}_j(\rho_z) \tilde{T}_k(\rho_{\parallel}) \right\}.$$

$$(32)$$

There exist several methods to determine the coefficients a_{ijk} . All of them aim at minimizing a residue function that measures the error of Eq. (32) (see Ref. [68] for more details). The two most common are the Galerkin method, which consists of taking moments of the differential equation and setting them to zero, and the collocation (or pseudospectral) method, which requires the equation to be exactly satisfied on a discrete grid of well-chosen points. One can show that both algorithms approximately minimize the residue

$$\int_{-1}^{1} d\chi d\rho_z d\rho_{\parallel} w(\chi) w(\rho_z) w(\rho_{\parallel}) \times [\text{Eq. (32)}]^2, \quad (33)$$

where $w(x) = 1/\sqrt{1-x^2}$ is the weight function under which the Chebyshev polynomials are orthogonal. Both methods have similar convergence properties, but the collocation method does not require carrying out the integral (33); hence we choose collocation.

To minimize the residue (33), one can show that the optimal collocation grid is given by the abscissas of the Gaussian quadrature associated with the Chebyshev polynomials. In the most common version of Gaussian quadrature, these points are the roots of T_{N+1} . However, it is more convenient to use, instead, the Gauss-Lobatto points, which are given by the extrema and endpoints of T_{N+1} . The collocation grid is therefore formed by the points $(\chi^{(i)}, \rho_z^{(j)}, \rho_{\parallel}^{(k)})$, with⁶

$$\chi^{(i)} = \cos\left(\frac{\pi i}{M}\right), \quad i = 1, ..., M - 1,$$

$$\rho_z^{(j)} = \cos\left(\frac{\pi j}{N}\right), \quad j = 1, ..., N - 1,$$

$$\rho_{\parallel}^{(k)} = \cos\left(\frac{\pi k}{N - 1}\right), \quad k = 1, ..., N - 1.$$
(34)

Requiring Eq. (32) to be satisfied on the grid (34) yields $(M-1)(N-1)^2$ linear algebraic equations that can easily be solved for the $(M-1)(N-1)^2$ unknown coefficients a_{ijk} by doing a single matrix inversion.

The accuracy of this spectral method is expected to increase exponentially with M and N. One can generally obtain an error of less than 1%, which we judge to be satisfactory, with $M \sim 20$ and $N \sim 10$. This allows for a fast and accurate solution of the Boltzmann equation.

It may not be obvious in what ways this spectral method is superior to the standard moment expansion of the Boltzmann equation, used in previous studies. Seemingly, the latter is closely related to the Galerkin method by a change of weight functions and a trivial basis transformation. Indeed, if performed with exact arithmetic, these two methods show similar convergence properties. The superiority of the Galerkin or collocation methods manifests itself when numerical algorithms are used to do the matrix inversion. For large $N \gtrsim 5$, the high-order terms in the basis functions of the moment expansion become nearly linearly dependent. This results in ill-conditioned matrices that yield large roundoff errors when inverted [68]. The Galerkin and collocation methods avoid this problem by using orthogonal polynomials, which are, in some way, maximally linearly independent. To prevent the round-off error from becoming prohibitively large when N is large, one should therefore avoid the moment expansion in favor of one of the spectral methods presented in this section.

There are further reasons to prefer the collocation method over the moment expansion. As previously mentioned, the former does not require integrating the Boltzmann equation, which significantly reduces the numerical overhead. One could argue that this benefit is offset by the calculation of the collision integrals, which requires the evaluation of $\mathcal{O}(N^4)$ terms for the collocation method, compared to $\mathcal{O}(N^2)$ terms for the moment expansion. However, the former consist in four-dimensional integrals, while the latter are seven dimensional. This implies that the convergence rate of the Monte Carlo algorithm used to compute the collision integrals (see Appendix A) is better for the former, which makes up for the larger number of terms to evaluate. Finally, several previous studies used additional approximations to simplify the moment equations (e.g., neglecting the mass dependence and the terms proportional to $\partial_{\varepsilon}(m^2)\delta f$). By not having to perform any integration, these approximations become unnecessary, and one can easily retain the full

⁶The collocation grid does not include the boundary points $\chi, \rho_z = \pm 1$ or $\rho_{\parallel} = 1$ because our choice of restricted basis Eq. (28) automatically satisfies the boundary conditions at these points.



FIG. 1. Exemplary solution of the Boltzmann equation for the top quark out-of-equilibrium perturbation δf_t , computed with the spectral method using N = 11 and M = 22. We show the moments of δf_t defined in Eq. (15), which appear in the hydrodynamic equations. The units of the *y* axis are GeV⁴. The Lorentz-invariant wall coordinate ξ is defined above Eq. (2).

Boltzmann equation. This further improves the overall accuracy of the algorithm.

An example of the results from this procedure is shown in Fig. 1, for the moments of the top quark perturbation δf_t as a function of ξ . The numbers of basis polynomials N = 11 and M = 22 were found to give a high degree of convergence, resulting in an average error of only 0.1%. The solution shown corresponds to values of the model parameters, to be described in the following section: $m_s = 103.8$ GeV, $\lambda_{hs} = 0.72$, and $\lambda_s = 1$. The terminal wall velocity for this model is $v_w = 0.57$.

IV. BENCHMARK MODEL: Z₂-SYMMETRIC SINGLET SCALAR EXTENSION

To illustrate the methodology discussed earlier, we consider the Z_2 -symmetric singlet scalar extension of the SM. This model can render the electroweak phase transition, strongly first order, with a modest input of new physics [26,27,69–76], which makes it attractive for studying general properties of FOPTs. Moreover, it has been shown that it can generate gravitational waves that could potentially be probed by future detectors [10,14,77–81], and it can provide a successful mechanism for baryogenesis by coupling it to a simple source of *CP* violation [31,36,49,65,82].

The singlet scalar extension consists of augmenting the SM by a new scalar field *s*, a singlet under the SM gauge group, and coupling it to the Higgs boson *h*. In its Z_2 -symmetric version, the tree-level scalar potential of this model takes the general form

$$V_{\text{tree}}(h,s) = \frac{\mu_h^2}{2}h^2 + \frac{\lambda_h}{4}h^4 + \frac{\mu_s^2}{2}s^2 + \frac{\lambda_s}{4}s^4 + \frac{\lambda_{hs}}{4}h^2s^2.$$
 (35)

To make quantitative predictions, we add to this potential the one-loop vacuum and thermal corrections, which are described in the appendix of Ref. [83].

We are interested in the region of parameter space where the phase transition occurs in a two-step process, which first breaks the *s* field's Z_2 symmetry and subsequently that of the Higgs field. Electroweak symmetry breaking occurs at the second step, so we only consider the second phase transition in the following. Electroweak bubbles appear at the nucleation temperature T_n , which is always below the critical temperature T_c , where the two vacua are degenerate. Further details about the electroweak phase transition and bubble nucleation in the singlet scalar extension can be found in Refs. [49,60,74,75,82–85].

A. Solution of fluid equations for SM-like plasma

To determine the wall velocity v_w , one needs to solve simultaneously a set of equations consisting of the scalar fields' equations of motion (EOMs) (17), the conservation of the EMT (20), and the spectral Boltzmann equation (32). In practice, the out-of-equilibrium perturbations contribute only slightly to the EOMs and the EMT. This allows one to solve the whole system iteratively, by first solving the EOMs and EMT with $\delta f = 0$, then using the resulting fields, temperature, and velocity profiles to solve the Boltzmann equation for an updated δf . We iterate this process with the new δf until convergence is achieved. This algorithm allows one to separate the problem into solutions of two subsystems: the spectral Boltzmann equation, which can be solved with the method described in Sec. III, and the EOMs + EMT system. We show how to solve the latter in this subsection.

To simplify the analysis, we only consider the out-ofequilibrium contribution from the top quark, which is the dominant one. In a more complete treatment, the other massive degrees of freedom including the W and Z bosons and the scalar fields should also be taken into account. We defer such improvements to future investigation. With this simplification, the scalar fields' EOMs in the wall frame become

$$E_{h} = -\partial_{z}^{2}h + \frac{\partial V_{T}(h, s; T)}{\partial h} + N_{t}\frac{\partial (m_{t}^{2})}{\partial h}\frac{\Delta_{00}^{t}}{2} = 0,$$

$$E_{s} = -\partial_{z}^{2}s + \frac{\partial V_{T}(h, s; T)}{\partial s} = 0,$$
(36)

where V_T is the effective potential, including the one-loop vacuum and thermal corrections, and $N_t = 12$ is the top quark's number of degrees of freedom.

A simple approximate solution to these equations is the tanh ansatz

$$h(z) = \frac{h_0}{2} [1 - \tanh(z/L_h)],$$

$$s(z) = \frac{s_0}{2} [1 + \tanh(z/L_s + \delta_s)],$$
(37)

where h_0 and s_0 are the scalar field vacuum expectation values (VEVs) in the true and false vacua, respectively, given appropriate choices for the coupling constants in the potential (35). They satisfy

$$\frac{\partial V}{\partial h}(h_0, 0; T_-) = \frac{\partial V}{\partial h}(0, s_0; T_+) = 0,$$
$$\frac{\partial V}{\partial s}(h_0, 0; T_-) = \frac{\partial V}{\partial s}(0, s_0; T_+) = 0.$$

The VEVs depend on the plasma's asymptotic temperatures T_{\pm} far from the wall, which are themselves a function of the wall velocity v_w .

Once a tentative field profile has been proposed, one can determine the temperature profile by solving Eq. (20). Since no derivative of T is involved, it forms a set of uncoupled algebraic equations for each value of z. Therefore, it can be solved with a standard root-finding algorithm, like a Newton or bracketing method.⁷

To get an accurate estimate of the solution, it is essential to allow the two scalar fields to have different wall thicknesses L_h and L_s , and even more so to allow an offset δ_s between the two wall positions. One could also use a more general ansatz than Eq. (37) with more free parameters. However, we find that the main features of the fields' profiles are well approximated by (37), and it is therefore sufficient for obtaining a good enough initial estimate of the solution.

The general strategy for determining the optimal values of v_w , L_h , L_s , and δ_s is to take moments of E_h and E_s in Eq. (36) and algebraically solve for the vanishing of the moments. The choice of the moments is to some extent arbitrary, as long as they are sensitive to independent linear combinations of the unknown parameters. A convenient choice is [59]

$$P_{h}(v_{w}, L_{h}, L_{s}, \delta_{s}) = -\int dz E_{h} h' = 0,$$

$$G_{h}(v_{w}, L_{h}, L_{s}, \delta_{s}) = \int dz E_{h} (2h/h_{0} - 1)h' = 0, \quad (38)$$

and similarly for P_s and G_s . These moments have intuitive physical interpretations that naturally distinguish them as good predictors of the wall speed and thickness, respectively. P_i is a measure of the net pressure on the wall, so that $P_i = 0$ can be interpreted as the requirement that a stationary wall should have a vanishing total pressure; nonvanishing P_i would cause it to accelerate. It can also create an offset between the two walls if $P_h \neq P_s$, which can be used to determine δ_s . On the other hand, G_i measures the pressure gradient in the wall. If nonvanishing, then it would lead to compression or stretching of the wall, causing L_i to change.

The system of moment equations (38) can be solved with a Newton algorithm. If needed, the resulting approximate solution can then be improved with a few relaxation steps. Generally, we find that it only changes the wall velocity by a few percent, so the tanh ansatz is sufficient for most applications.

B. Classification of solutions

To better understand how the wall velocity of first-order phase transition bubbles is determined by the departure from equilibrium, it is convenient to define the total pressure,

$$P_{\text{tot}}(v_w) = P_h(v_w, L_h^*, L_s^*, \delta_s^*) + P_s(v_w, L_h^*, L_s^*, \delta_s^*), \quad (39)$$

where L_h^* , L_s^* , and δ_s^* solve the equations $P_h - P_s = G_h = G_s = 0$. This quantity measures the total pressure on the bubble wall as a function of the wall velocity, when the dependence on the wall shape is eliminated in favor of v_w .

The total pressure for two different models is shown in Fig. 2, illustrating deflagration and detonation transitions, respectively. A striking nontrivial feature in both curves is the large pressure peak maximized at the Jouguet velocity v_J , which is the smallest wall velocity that can yield a detonation solution. This pressure barrier was predicted in Ref. [53], and observed in Ref. [49], and is confirmed by the present analysis. It plays an essential role, being a general feature of first-order phase transitions, and naturally dividing the bubbles into two qualitatively distinct categories: deflagration (which also includes hybrid walls) and ultrarelativistic detonation solutions.⁸

A phase transition corresponds to a deflagration solution if it is too weak to overcome the pressure barrier at v_I . This is the case for the model shown in Fig. 2(a), which solves $P_{\text{tot}} = 0$ at approximately $v_w = 0.57$. It is no coincidence that the terminal wall velocity in this example ends up being so close to the sound speed in the plasma. The pressure peak is a consequence of hydrodynamic effects that heat the plasma, increasing the pressure on the wall. These effects become especially important for hybrid walls, when the shock wave in front of the wall becomes thin. This causes the pressure to start to rise rapidly only around $v_w \sim c_s \sim 0.58$, when the wall becomes a hybrid solution (a supersonic deflagration which has both a shock and rarefaction wave). Since the acceleration of most deflagration solutions is stopped by the pressure peak, it implies that a large fraction of the walls in that category satisfies $c_s \lesssim v_w \leq v_J$.

⁷For some tentative field profiles and wall velocities (mainly for hybrid walls), Eq. (20) does not have any solution. In this situation, we choose the value of T that minimizes the error. Of course, the exact solution of the EOMs (36) must allow a solution for Eq. (20).

⁸For more formal definitions of deflagration, hybrid, and detonation solutions, see Appendix B.



FIG. 2. Total pressure as a function of the wall velocity for a deflagration wall (a) and a detonation wall (b). The dashed (red) line only contains the contribution from the equilibrium distribution function, while the solid (blue) line also includes the top quark's out-of-equilibrium contribution. The shaded region corresponds to hybrid walls. It is bounded on the right by the Jouguet velocity v_J .

For stronger phase transitions, the pressure peak is not high enough to impede the wall's acceleration since P_{tot} remains negative, leading to detonation solutions. This is the case for the model shown in Fig. 2(b). Since the pressure at v_J is higher than in the range $v_J < v_w \leq 1$ and yet insufficient to decelerate the wall, it will continue accelerating until it is stopped by the friction coming from out-of-equilibrium effects. These become important only at ultrarelativistic velocities; in general, detonation solutions always satisfy $\gamma_w \gtrsim 10$. The asymptotic behavior of this ultrarelativistic friction force is still being debated [86,87], as Refs. [88,89] found different scaling relations $P_{tot}(v_w \rightarrow 1) \sim \gamma_w, \gamma_w^2$, respectively. Nevertheless, they both agree that it will eventually become high enough to stop the wall with $\gamma_w \gg 1$.

One can also appreciate the role played by the deviation from equilibrium in Fig. 2, as it shows the pressure computed with or without the out-of-equilibrium contribution [the term proportional to Δ_{00} in Eq. (36)]. Strikingly, the out-of-equilibrium pressure is much smaller than the equilibrium one.⁹ The latter can accurately reproduce the most important feature of the pressure curve, namely the pressure peak at v_J . Therefore, it could be a good approximation to neglect the deviations from equilibrium altogether, considerably simplifying the fluid equations since no Boltzmann equation would have to be solved.

However, there are some situations where the out-ofequilibrium pressure can be quantitatively important. For slow walls ($v_w \leq 0.5$), the error in the wall velocity Δv_w caused by neglecting this contribution can become large, even if the pressure difference is small. One can show that $\Delta v_w \sim (dP_{\text{tot}}/dv_w)^{-1}$, which increases at small velocities. But as previously argued, most deflagration solutions are stopped by the pressure peak, at which point $(dP_{tot}/dv_w)^{-1}$ is small; thus, Δv_w is expected to be unimportant for typical deflagrations.

One can also see from Fig. 2 that the approximation of ignoring the out-of-equilibrium pressure contribution becomes poor when $v_w > v_J$. But, ultimately, this has a small effect since all detonation walls become ultrarelativistic, irrespective of their pressure profile. Possibly the most important distinction between the equilibrium and total pressure is the magnitude of the peak pressure, which determines the type of solution: deflagration for $P_{\text{tot}}(v_J) > 0$ and detonation, otherwise. Even if the out-of-equilibrium contribution is small, it is possible that neglecting it erroneously transforms a deflagration into a detonation, resulting in a large Δv_w . We will later estimate how likely this is to happen and propose a simple fix to approximate the out-of-equilibrium pressure without solving the Boltzmann equation.

From Fig. 2, it is apparent that the total pressure is discontinuous at $v_w = v_J$. However, we now obtain a finite discontinuity rather than a divergent one, such as was found in previous studies that were based on a perturbative treatment of $\delta v_{\rm bg}$ and $\delta T_{\rm bg}$. By virtue of its finiteness, the pressure discontinuity is no longer conceptually nor numerically problematic. Unlike in earlier work, we do not find that it arises from the fluid equations (5), (17), and (18). Rather, its origin is in the initial conditions T_{\pm} and v_{\pm} , which vary discontinuously when the wall goes from a hybrid to a detonation solution. Ultimately, this is caused by the shock wave disappearing for detonations.

C. Scan results

We now turn to a more specific discussion about the singlet scalar extension. To study the consequences of the

⁹However, one should keep in mind that we only include the out-of-equilibrium contribution of the top quark, which slightly underestimates the actual total pressure.



FIG. 3. Scan of the parameter space with $\lambda_s = 1$. Red points are ultrarelativistic detonation solutions.

methodology discussed in this paper for the wall velocity and shape, we performed a random scan over the region in parameter space constrained by $\lambda_s = 1$ and $m_s \in [62.5, 160]$ GeV, where $m_s = \mu_s^2 - \lambda_{hs} \mu_h^2 / (2\lambda_h)$ is the physical mass of the *s* particle at T = 0, and its lower bound is chosen to avoid collider constraints from Higgs boson decays $h \rightarrow ss$. To ensure a more uniform exploration of the parameter space, we sampled the points from a Sobol sequence, which prevents two points from being arbitrarily close to one another. The result of this scan is shown in Fig. 3, where v_w is indicated in the $\lambda_{hs} - m_s$ plane for models giving a first-order phase transition.

Of the 2860 points sampled, roughly 70% are deflagration walls. Although this ratio is model dependent, it suggests that both types of solution should be relatively common for generic models. The qualitative analysis of the last subsection is validated: we find that all the detonation solutions have $\gamma_w > 10$ (hence ultrarelativistic), and a large fraction of the deflagration walls have a terminal velocity close to the speed of sound, the slowest being $v_w \approx 0.4$. More precisely, 83% of the deflagration walls have a velocity greater than 0.55, and 97% are greater than 0.5.

The classification of walls is strongly correlated with the strength of the phase transitions, which we quantify by α , the ratio of released vacuum energy density to the radiation energy density. A histogram of α is shown in Fig. 4. It clearly shows that the phase transition of detonation solutions is, in general, stronger than for deflagration walls. There is some overlap between the two groups, but as a rough rule of thumb, one can say that deflagrations satisfy $\alpha_{def} \lesssim 10^{-2}$ and detonations $\alpha_{det} \gtrsim 10^{-2}$.

We quantify the effect of neglecting the out-of-equilibrium pressure in Fig. 5, which shows the relative errors induced for the wall velocity and thickness. The absolute error is defined as $\Delta v_w = v_w^{\text{eq}} - v_w^{\text{total}}$, and similarly for L_h ; thus Fig. 5 shows that the out-of-equilibrium contributions slow down the wall while making it thicker. As expected, the error is small for hybrid walls and becomes larger as v_w decreases. Even in the



FIG. 4. Histogram of α (latent heat divided by radiation energy density) for deflagration (blue) and detonation (orange) solutions. Overlap region is shown in darker red.



FIG. 5. Scatter plot of relative errors of the wall velocity (blue points) and thickness (red points) due to neglecting the out-of-equilibrium pressure contribution, as a function of v_w .

extreme cases, the relative error never exceeds 15% for v_w and 20% for L_h , and the mean errors are 2% and 5%, respectively.

The out-of-equilibrium pressure also has an impact on the classification of the solutions, as 9% of the deflagration walls would be incorrectly identified as detonations if one neglected this contribution. This last consequence could be more problematic since it has a significant qualitative impact on the behavior of the misidentified solution. The errors presented here somewhat underestimate the true error that would be obtained by considering the full out-ofequilibrium contributions beyond those of the top quark.⁹

V. APPROXIMATION SCHEMES

For some applications, a qualitative understanding of the bubble wall's behavior may be sufficient; for example, one might be content to know whether the wall speed is subsonic or ultrarelativistic, without needing its precise value. With that in mind, in this section we propose several approximation schemes with increasing levels of complexity and accuracy. Each method can be separated into two parts: first classifying the wall as a deflagration or detonation solution, and second computing the wall velocity.¹⁰

A. Fixed wall velocity

The wall velocity is often needed to study the cosmological signatures of first-order phase transitions (e.g., baryogenesis and gravitational waves). To simplify the analysis, several past studies have assumed a fixed value for the wall velocity instead of computing it from the fluid equations. Unfortunately, the chosen value was often motivated by the strength of the cosmological signature studied, instead of the likelihood of having such a velocity, simply because this likelihood was unknown.

For example, baryogenesis studies frequently adopt a small wall velocity ($v_w \leq 0.1$) to maximize the resulting baryon asymmetry. As we have seen in Sec. IV, it is actually very unlikely to have $v_w < 0.5$, and the smallest velocity found out of 2860 models is $v_w = 0.4$. Instead of this arbitrary (and inaccurate) assumption, we propose here to use the most likely wall velocity, which is $v_w = c_s = 1/\sqrt{3}$ for deflagrations and $v_w = 1$ for detonations. It is harder to suggest a fixed wall thickness since this typically depends rather sensitively on the specific model being studied. Generally, values between $5/T_n$ and $20/T_n$ are realistic. One can classify the solutions using the α parameter, with phase transitions satisfying $\alpha < 10^{-2}$ corresponding to deflagrations and $\alpha > 10^{-2}$ as detonations.

Using these approximations, we correctly classify 86% of the models sampled in the last section. Moreover, the mean error in the wall velocity of deflagration walls is only 5%. Of course, the main advantage of this approximation is that it requires almost no calculation. Yet, it is able to reproduce the correct qualitative behavior most of the time. For higher accuracy, or an estimation of the wall thickness, we recommend one of the subsequent approximations.

B. Local thermal equilibrium

The next step towards a better approximation of the fluid equations is to assume the plasma to be in local thermal equilibrium (LTE). This strategy has already been studied in Refs. [54–56], and we showed in Sec. IV that it correctly reproduces the qualitative features of the pressure curve. To implement it, one needs to solve Eqs. (17) and (20), while neglecting all the out-of-equilibrium terms involving the Δ_{mn} functions. The type of solution can be classified by computing the sign of $P_{\text{tot}}(v_J)$.

Using a tanh ansatz to solve the equilibrium fluid equations, one can in this way correctly classify 94% of the solutions. The mean error on the deflagration wall velocity is 2%, and the wall thickness estimate has an accuracy of 13%. This level of accuracy represents a net improvement compared to the previous approximation, in addition to providing an estimation of the wall shape. However, it requires computing v_J , v_{\pm} , T_{\pm} and solving a set of fluid equations, which requires significant additional computational effort.

C. Numerical fit of out-of-equilibrium pressure

It is possible to substantially improve the last approximation by estimating the out-of-equilibrium pressure from a numerical fit. Since the Boltzmann equation does not depend on the potential V_T , these out-of-equilibrium contributions are, to some extent, model independent.

An excellent representation of out-of-equilibrium contributions to the moments of Eq. (38) can be obtained using a power-law proportional to h_0^4 , $v_+^{1.5}$, $T_+^{-0.5}$, and L_h^{-1} . (Recall that v_+ , T_+ are the fluid velocity and temperature at $z \to \infty$.) The best fits of the out-of-equilibrium pressure and pressure gradient are

$$\begin{split} P_{h}^{\text{out}} &\equiv -\frac{N_{t}}{2} \int dz h' \frac{\partial (m_{t}^{2})}{\partial h} \Delta_{00}^{t} \\ &\approx (1.04 \times 10^{-4} \text{ GeV}^{-0.5}) \frac{N_{t} y_{t}^{4} h_{0}^{4} v_{+}^{1.5}}{T_{+}^{0.5} L_{h}}, \\ G_{h}^{\text{out}} &\equiv \frac{N_{t}}{2} \int dz (2h/h_{0}-1) h' \frac{\partial (m_{t}^{2})}{\partial h} \Delta_{00}^{t} \\ &\approx (-3.95 \times 10^{-5} \text{ GeV}^{-0.5}) \frac{N_{t} y_{t}^{4} h_{0}^{4} v_{+}^{1.5}}{T_{+}^{0.5} L_{h}}, \end{split}$$
(40)

where y_t is the top Yukawa coupling. We calibrated these fits on the deflagration walls found in the scan of Sec. IV, so they should not be trusted for ultrarelativistic detonation solutions. They both have a coefficient of determination of $R^2 = 0.999$, and the fits are shown in Fig. 6.

One can substitute the fits (40) in the moment equations (38) to obtain an improved set of fluid equations that include the estimate of the out-of-equilibrium contributions.¹¹ Using this approximation, we can correctly classify 98% of the walls and the mean errors on v_w and L_h are, respectively, 0.4% and 9.8%.

At this stage, the numerical fits (40) are only valid for the singlet scalar extension presented in Sec. IV. It is possible to generalize them by identifying the origin of the h_0^4/L_h factor, which is model dependent. First, the $dzh'\partial(m^2)/\partial h$ factor in the definitions of P_h^{out} and G_h^{out} scales like h_0^2 . Second, the magnitude of deviation from equilibrium is

¹⁰For detonations, the wall velocity is always $v_w \approx 1$, so this second part becomes trivial. For estimations of the terminal Lorentz factor γ_w and for detonation solutions, see Refs. [88,89].

¹¹Since this approximation is obtained from the moment equations (38), it requires a tanh ansatz for the fields' profiles.



FIG. 6. Out-of-equilibrium pressure (blue points) and pressure gradient (red points) of the deflagration solutions, obtained in the scan of Sec. IV, and the corresponding best fits Eq. (40) (lines). The units of the y axis are GeV^4 .

proportional to the amplitude of the Boltzmann equation's source term S_i , Eq. (6). The dominant contribution to S_i is the term proportional to $\partial_{\xi}(m_t^2)$, which scales like h_0^2/L_h .

In a more general treatment, one should include the pressure from all the massive degrees of freedom. Furthermore, the masses can depend on the VEVs of several scalar fields. To be as general as possible, we keep the masses unspecified and replace the h_0^4/L_h factor in Eq. (40) by the following scaling relations:

$$\begin{split} \Delta_{00}^{j} &\sim \partial_{\xi}(m_{j}^{2}) \sim \sum_{k} \frac{\beta_{jk}}{L_{k}}, \\ \beta_{ij} &\equiv \Delta \left[\phi_{j} \frac{\partial(m_{i}^{2})}{\partial \phi_{j}} \right], \end{split} \tag{41}$$

and

$$P_{i}^{\text{out}} = -\sum_{j} \frac{N_{j}}{2} \int dz \phi_{i}^{\prime} \frac{\partial(m_{j}^{2})}{\partial \phi_{i}} \Delta_{00}^{j}$$
$$\sim \sum_{j} N_{j} \beta_{ji} \sum_{k} \frac{\beta_{jk}}{L_{k}}, \qquad (42)$$

where the Δ operator denotes the variation of its argument across the wall, and L_k is the thickness of the ϕ_k wall profile. The factors β_{ij} can be interpreted as the variation of m_i^2 during the phase transition, due to the variation of ϕ_j 's VEV.

The $v_{+}^{1.5}/T_{+}^{0.5}$ factor appearing in the fits does not depend on the masses, but rather on the structure of the Boltzmann equation. Therefore, we expect it to be model independent. This is a reasonable assumption for SM-like plasmas since they all share similar collision operators. Demanding that Eq. (42) reduces to Eq. (40) in the case where only the contribution from the top quark is included, the fits for the pressure and pressure gradient become

$$P_{i}^{\text{out}} \approx \frac{1.04 \times 10^{-4}}{\text{GeV}^{0.5}} \frac{v_{+}^{1.5}}{T_{+}^{0.5}} \sum_{j,k} \frac{N_{j}}{L_{k}} \beta_{ji} \beta_{jk},$$

$$G_{i}^{\text{out}} \approx \frac{-3.95 \times 10^{-5}}{\text{GeV}^{0.5}} \frac{v_{+}^{1.5}}{T_{+}^{0.5}} \sum_{j,k} \frac{N_{j}}{L_{k}} \beta_{ji} \beta_{jk}, \qquad (43)$$

where j is summed over all the massive species and k over all the scalar fields that have VEVs in the wall.

As an exemplary application, we use the fits (43) to estimate the out-of-equilibrium contributions from the h and s scalar fields, and the W and Z bosons, which were previously neglected.

The contribution from the gauge bosons is the easiest to estimate since their mass is not affected by the singlet scalar. Their out-of-equilibrium pressure can simply be related to the top's by

$$\frac{P_{h,W}^{\text{out}} + P_{h,Z}^{\text{out}}}{P_{h,t}^{\text{out}}} \approx \frac{N_W m_W^4 + N_Z m_Z^4}{N_t m_t^4} \approx 0.04, \qquad (44)$$

where $P_{i,j}^{\text{out}}$ is the out-of-equilibrium pressure of the *j* species on the ϕ_i wall. This shows that it is a reasonable approximation to neglect the gauge bosons' contribution.

The scalar fields' masses depend on *h* and *s*, so they contribute to both P_h^{out} and P_s^{out} . Before estimating these pressures, it is convenient to compute the relevant β_{ij} factors from Eqs. (35) and (41):

$$\beta_{hh} = 6\lambda_h h_0^2, \qquad \beta_{hs} = \lambda_{hs} s_0^2, \beta_{ss} = 6\lambda_s s_0^2, \qquad \beta_{sh} = \lambda_{hs} h_0^2.$$
 (45)

The fractional contribution from the scalar particles to the pressure, relative to that of the top quark, can then be estimated as

$$\frac{L_h}{N_t(y_t h_0)^4} \left[\frac{1}{L_h} (\beta_{hh}^2 + \beta_{sh}^2) + \frac{1}{L_s} (\beta_{hh} \beta_{hs} + \beta_{sh} \beta_{ss}) \right] \sim 0.3,$$

$$\frac{L_h}{N_t(y_t h_0)^4} \left[\frac{1}{L_s} (\beta_{ss}^2 + \beta_{hs}^2) + \frac{1}{L_h} (\beta_{hh} \beta_{hs} + \beta_{sh} \beta_{ss}) \right] \sim 0.5$$
(46)

for the *h* and *s* walls, respectively. The numbers on the right-hand sides are averages over all the deflagrations found in Sec. IV. Due to the large value of $\lambda_s = 1$ used for the scan, the magnitude of this out-of-equilibrium pressure is significantly larger. Incidentally, nearly all the contribution comes from the *s* field's departure from equilibrium. Therefore, it is still a good approximation to assume the Higgs to be in LTE (because $\lambda_h \sim 0.1$ is small), but it seems

harder to justify it for the singlet scalar, as long as λ_s is large.

We finally study the effect of these additional sources of pressure on the wall velocity. Despite the large contribution from the *s* field, the average v_w for deflagration solutions is only decreased by 0.5%, compared to the case where only the top's pressure is included. This is not surprising since we already found that v_w is mainly determined by the equilibrium contribution. However, the additional pressure increases the number of deflagration solutions by 7%, which could have an important effect on the predicted terminal velocity if a high accuracy is needed.

D. Discussion

Table I shows a summary of the accuracy of each approximation scheme. For applications requiring only a qualitative understanding, we recommend the fixed wall velocity method, as it requires practically no calculations, while correctly describing the bubble's qualitative dynamics. For higher accuracy, we recommend solving the fluid equations with the numerical fits (43) to estimate the out-of-equilibrium terms since it is much more precise than the LTE method, without increasing the complexity of the equations that must be solved. However, these fits should only be trusted for a SM-like plasma; the LTE method should be used for a plasma whose constituents differ significantly from the SM.

Finally, for the highest level of accuracy, one should compute the deviation from equilibrium by solving a set of Boltzmann equations for each massive species in the plasma. This can be done efficiently with the spectral method described in Sec. III.

It is worthwhile to keep in mind that the Boltzmann equation is not an exact predictor of the distribution functions and is subject to various sources of uncertainty. It is an approximation to the Kadanoff-Baym equations, which is obtained by performing a gradient expansion [90], that is only trustworthy for $L_i \gtrsim 2/T_+$ [91]. Moreover, the collision integrals are computed to leading log accuracy, which has large uncertainties [57,60,61,92]. This can

TABLE I. Accuracy of the different approximation schemes for the scan of Sec. IV. All the numbers are percentages and are compared to the complete solution of the fluid equations, including the Boltzmann equation of the top quark only. The numbers in parentheses were computed with a tanh ansatz.

Approximation	Correct classification (%)	$\Delta v_w/v_w$ (%)	$\Delta L_h/L_h \ (\%)$
Fixed wall velocity	86	4.7	
Local thermal equilibrium	94 (94)	1.6 (2.2)	4.7 (13)
Numerical fits	(98)	(0.4)	(9.8)
Full Boltzmann equations	100 (98)	0 (0.5)	0 (9.6)

induce significant errors in the out-of-equilibrium contributions since they are typically inversely proportional to the collision terms.

VI. SUMMARY AND CONCLUSIONS

In this work we have rederived the fluid equations used to determine the wall velocity of a first-order phase transition bubble. Contrary to the standard methodology, we exactly solved the equations for the background temperature and fluid velocity, without linearizing in these quantities. This ensures the existence of nonsingular solutions regardless of the wall velocity, in particular, for $v_w \gtrsim c_s$. We thereby overcome an important limitation of the standard formalism introduced in Ref. [57], which prevented the accurate description of supersonic walls.

Furthermore, the Lorentz invariant fluid equations are derived from first principles; EMT conservation is used to calculate the background temperature, fluid velocity, and scalar field profiles, and a set of Boltzmann equations determines the deviation from thermal equilibrium of each species in the plasma. We proposed a spectral method to solve the Boltzmann equations, which has the attractive features of being simple, efficient, rapidly converging, and accurate. It allows one to approximately solve the Boltzmann equation directly with arbitrary accuracy, requiring just a single matrix inversion.

To explore the consequences of this new formalism on the dynamics of the bubble wall, we applied it to the singlet scalar extension of the SM. A key finding is that all bubble walls fall into one of two qualitatively distinct groups: either deflagrations with $c_s \lesssim v_w \leq v_J$ (the Jouguet velocity), or ultrarelativistic detonations with $\gamma_w \gtrsim 10$. Hence, generic transitions will give bubble walls traveling either near the speed of sound or that of light. Although the result was derived in a specific model, we expect this classification to be a general feature of first-order phase transitions; it is a consequence of general equilibrium hydrodynamic effects. Since it mainly comes from equilibrium physics, departure from equilibrium has little impact on the terminal wall velocity. Rather than making a dominant contribution to the friction on the wall, as standard lore suggested, we find that it only gives a small correction, which changes the wall velocity by 2% on average. However, in some borderline situations, it can generate a small additional pressure that transforms a would-be detonation into a deflagration; the outof-equilibrium effects are significant in such cases.

Finally, we proposed several approximation schemes with increasing levels of complexity and accuracy. The simplest of these can, in most cases, correctly reproduce the qualitative behavior of the full treatment, while requiring almost no calculation. We also performed a numerical fit of the out-of-equilibrium pressure and pressure gradient from the present study. This allows future practitioners to quantitatively estimate the effects of friction, without having to solve the Boltzmann equations. They can thereby improve the (already good) estimates from the local thermal equilibrium approximation, with modest additional effort, to get accurate estimates of the wall speed. It should be noted, however, that the methods discussed here do not address the question of how large γ_w is in the case of highly relativistic walls.

A natural next step would be to extend the fluid equations derived in this work to *CP*-odd perturbations. This would be relevant to the study of electroweak baryogenesis, which is one of the primary applications of a firstorder electroweak phase transition. Although generalizing the hydrodynamic and Boltzmann equations is straightforward, the calculation of the collision integrals presents a challenge. In particular, some of the processes relevant for the *CP*-odd perturbations (such as those involving weak and strong sphalerons) should properly be calculated using lattice gauge theory since they require matrix elements that are not simply related to the total sphaleron rate. This is a problem we hope to investigate in future work.

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APPENDIX A: COLLISION INTEGRALS

We discuss here the calculation of the collision integrals by adapting the method used in Ref. [61] to be used with the spectral method discussed in Sec. III. The collision term for a given particle species is

$$\mathcal{C}[f] = \sum_{i} \frac{1}{2N_{p}} \int \frac{d^{3}k d^{3} p' d^{3} k'}{(2\pi)^{5} 2E_{k} 2E_{p'} 2E_{k'}} |\mathcal{M}_{i}|^{2} \times \delta^{4}(p+k-p'-k')\mathcal{P}[f];$$
(A1)

$$\mathcal{P}[f(p)] = f(p)f(k)(1 \pm f(p'))(1 \pm f(k')) - f(p')f(k')(1 \pm f(p))(1 \pm f(k)), \quad (A2)$$

where the sum is over all the relevant processes. Note that p is the momentum of the incoming particle, whose distribution is being computed, N_p is its number of degrees of freedom, k is the momentum of the other incoming particle, and p', k' are the momenta of the outgoing particles. $|\mathcal{M}_i|^2$ is the squared scattering amplitude, summed over the helicities and colors of all the external particles. Finally, the \pm appearing in population factor \mathcal{P} is + for bosons and – for fermions.

To make the Boltzmann equation numerically tractable, \mathcal{P} can be simplified by expanding it to linear order in the perturbations. Using the definition (4) of the distribution function and conservation of energy, one can show that \mathcal{P} becomes

$$\mathcal{P}_{\rm lin}[f] = f_p f_k f_{p'} f_{k'} \left(\frac{e^{\mathcal{E}_k^{\rm pl}/T}}{f_p^2} \delta f_p + \frac{e^{\mathcal{E}_p^{\rm pl}/T}}{f_k^2} \delta f_k - \frac{e^{\mathcal{E}_{k'}^{\rm pl}/T}}{f_{p'}^2} \delta f_{p'} - \frac{e^{\mathcal{E}_{p'}^{\rm pl}/T}}{f_{k'}^2} \delta f_{k'} \right),$$
(A3)

where $f_p \equiv f_{eq}(p)$.

Following the treatment of Ref. [57], the calculation of the collision rates has been done to leading log accuracy, where it is justified to neglect the masses of all the external particles, which implies $E_p = p$. One can also neglect *s*-channel contributions and the interference between diagrams because they are not logarithmic. To account for thermal effects, we use propagators of the form $1/(t - m^2)$ or $1/(u - m^2)$, where *m* is the exchanged particle's thermal mass. It is given by $m_g^2 = 2g_s^2 T^2$ for gluons and $m_q^2 = g_s^2 T^2/6$ for quarks [93].

As previously discussed, we only consider the collision terms of the top quark. They are dominated by their strong interactions; we include only contributions to $|\mathcal{M}|^2$ of order g_s^4 . There are three relevant processes: top annihilation into gluons¹² $\bar{t}t \rightarrow gg$ and the two scattering $tg \rightarrow tg$ and $tq \rightarrow tq$. Their respective amplitudes are [57]

$$\frac{1}{N_t} |\mathcal{M}_{tt \to gg}|^2 = -\frac{64}{9} g_s^4 \frac{st}{(t - m_q^2)^2},$$

$$\frac{1}{N_t} |\mathcal{M}_{tg \to tg}|^2 = -\frac{64}{9} g_s^4 \frac{su}{(u - m_q^2)^2} + 16g_s^4 \frac{s^2 + u^2}{(t - m_g^2)^2},$$

$$\frac{1}{N_t} |\mathcal{M}_{tq \to tq}|^2 = \frac{80}{3} g_s^4 \frac{s^2 + u^2}{(t - m_q^2)^2}.$$
 (A4)

To evaluate the integrals in (A1), one can first use the delta function and the symmetry of the integrand to analytically perform five of the nine integrals. The remaining four integrals can be evaluated numerically with a Monte Carlo algorithm like VEGAS [95].

To use the spectral method described in Sec. III, one needs to compute $C_{\text{lin}}[\bar{T}_m(\rho_z^{(j)})\tilde{T}_n(\rho_{\parallel}^{(k)})]$ on a grid of $(N-1)^2$ points given by Eq. (34), for a total of $\mathcal{O}(N^4)$ integrals to evaluate. However, the linearity of C_{lin} and the symmetries of \bar{T}_m imply

$$\mathcal{C}_{\mathrm{lin}}[\bar{T}_m(-\rho_z)\tilde{T}_n(\rho_{\parallel})] = (-1)^m \mathcal{C}_{\mathrm{lin}}[\bar{T}_m(\rho_z)\tilde{T}_n(\rho_{\parallel})],$$

which reduces by half the number of independent components to calculate. Furthermore, one can show that $C_{\text{lin}}[\bar{T}_m(0)\tilde{T}_n(\rho_{\parallel})] = 0$ if *m* is odd or if $\rho_{\parallel} = 0$.

The calculation of these $O(N^4)$ integrals may appear to be numerically expensive. For example, for N = 20

 $^{^{12}}$ As pointed out in Ref. [94], Ref. [57] inadvertently omitted a 1/2 symmetry factor in this amplitude.

(the highest value used in this paper), there are 65151 independent coefficients. However, the collision integrals are model independent, which means that they only have to be computed once. It therefore represents an important initial calculational cost, but once they are known, they can be used for any model with the same plasma content (in this approximation, only the top quark). We still recommend using an integration algorithm adapted for these large-scale problems, like the Monte Carlo algorithm VEGAS [95].

APPENDIX B: BOUNDARY CONDITIONS OF THE HYDRODYNAMIC EQUATIONS

For the convenience of the reader, we here reproduce the method of Ref. [67] to calculate the boundary conditions of the hydrodynamic equations (18). The quantities of interest are the temperatures $T_{\pm} \equiv T(\pm \infty)$ and the velocities of the plasma measured in the wall frame $v_{\pm} \equiv v(\pm \infty)$.

By integrating the conservation equation for the energymomentum tensor across the wall, one can show that the quantities T_{\pm} and v_{\pm} are related by the equations

$$v_{+}v_{-} = \frac{1 - (1 - 3\alpha_{+})r}{3 - 3(1 + \alpha_{+})r},$$

$$\frac{v_{+}}{v_{-}} = \frac{3 + (1 - 3\alpha_{+})r}{1 + 3(1 + \alpha_{+})r},$$
(B1)

where α_{+} and *r* are defined as

$$\begin{aligned} \alpha_{+} &\equiv \frac{\epsilon_{+} - \epsilon_{-}}{a_{+}T_{+}^{4}}, \qquad r \equiv \frac{a_{+}T_{+}^{4}}{a_{-}T_{-}^{4}}, \\ a_{\pm} &\equiv -\frac{3}{4T_{\pm}^{3}} \frac{\partial V_{\text{eff}}}{\partial T} \Big|_{\pm}, \\ \epsilon_{\pm} &\equiv \left(-\frac{T_{\pm}}{4} \frac{\partial V_{\text{eff}}}{\partial T} + V_{\text{eff}} \right) \Big|_{\pm}. \end{aligned} \tag{B2}$$

These quantities are often approximated by the so-called bag equation of state, which is given in Ref. [67]. This approximation is expected to hold when the masses of the plasma's degrees of freedom are very different from T, which is not necessarily true in the broken phase. Therefore, we keep the full relations (B2) in our calculations.

Subsonic walls always come with a shock wave preceding the phase transition front. Equations (B1) can be used to relate T_{\pm} and v_{\pm} at the wall and the shock wave, but we need to understand how T and v evolve between these two regions. Assuming a spherical bubble and a thin wall, one can derive from the conservation of $T^{\mu\nu}$ the differential equations

$$2\frac{v}{\xi} = \gamma^2 (1 - v\xi) \left(\frac{\mu^2}{c_s^2} - 1\right) \partial_{\xi} v,$$

$$\partial_{\xi} T = T \gamma^2 \mu \partial_{\xi} v,$$
 (B3)

where v is the fluid velocity in the frame of the bubble's center, and $\xi = r/t$ is the independent variable [not to be confused with ξ in Eq. (2)], with r being the distance from the bubble center and t the time since the bubble nucleation. In these coordinates, the wall is located at $\xi = v_w$. Note that μ is the Lorentz-transformed fluid velocity,

$$\mu(\xi, v) = \frac{\xi - v}{1 - \xi v},\tag{B4}$$

and c_s is the speed of sound in the plasma,

$$c_s^2 = \frac{\partial V_{\rm eff}/\partial T}{T\partial^2 V_{\rm eff}/\partial T^2} \approx \frac{1}{3}.$$
 (B5)

The last approximation is valid for relativistic fluids, which is applicable in the unbroken phase. In the broken phase, some particles get a mass that can be of the same order as the temperature, somewhat reducing the speed of sound for those species.

One can find three different types of solutions for the fluid's velocity profile: deflagrations $(v_w < c_s^-)$ have a shock wave propagating in front of the wall, detonations $(v_w > v_J)$ have a rarefaction wave behind it, and hybrid transitions $(c_s^- < v_w < v_J)$ have both shock and rarefaction waves. v_J is the model-dependent Jouguet velocity, which is defined as the smallest velocity a detonation solution can have. Each type of wall has different boundary conditions that determine the characteristics of the solution. Detonation walls are supersonic solutions where the fluid in front of the wall is unperturbed. Therefore, it satisfies the boundary conditions $v_+ = v_w$ and $T_+ = T_n$. For that type of solution, Eqs. (B1) can be solved directly for v_- and T_- .

Subsonic walls always have a deflagration solution with a shock wave at position $\xi_{\rm sh}$ that satisfies $v_{\rm sh}^-\xi_{\rm sh}=(c_s^+)^2$, where $v_{\rm sh}^-$ is the fluid's velocity just behind the shock wave, measured in the shock wave's frame. It also satisfies the boundary conditions $v_{-} = v_{w}$ and $T_{sh}^{+} = T_{n}$. Because these boundary conditions are given at two different points, the solution of this system can be somewhat more involved than for the detonation case. We use a shooting method, which consists of making a guess for T_{-} , solving Eqs. (B1) for T_+ and v_+ , and integrating Eqs. (B3) with the initial values $T(v_w) = T_+$ and $v(v_w) = \mu(v_w, v_+)$ for ξ up to the point where $\mu(\xi, v(\xi))\xi = (c_s^+)^2$ is satisfied. This procedure is iterated with different values of T_{-} until Eqs. (B1) are satisfied at the shock wave. Hybrid walls are characterized by $v_{+} < c_{s}^{-} < v_{w}$, with boundary conditions $v_{-} = c_{s}^{-}$ and $T_{sh}^{+} = T_{n}$, which make them similar to deflagrations.

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