

Gravitational wave detection beyond the standard quantum limit using a negative-mass spin system and virtual rigidity

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Gravitational wave detectors (GWDs), which have brought about a new era in astronomy, have reached such a level of maturity that further improvement necessitates quantum-noise-evading techniques. Numerous proposals to this end have been discussed in the literature, e.g., invoking frequency-dependent squeezing or replacing the current Michelson interferometer topology by that of the quantum speedmeter. Recently, a proposal based on the linking of a standard interferometer to a negative-mass spin system via entangled light has offered an unintrusive and small-scale new approach to quantum noise evasion in GWDs [Phys. Rev. Lett. **121**, 031101 (2018)]. The solution proposed therein does not require modifications to the highly refined core optics of the present GWD design and, when compared to previous proposals, is less prone to losses and imperfections of the interferometer. In the present article, we refine this scheme to an extent that the requirements on the auxiliary spin system are feasible with state-of-the-art implementations. This is accomplished by matching the effective (rather than intrinsic) susceptibilities of the interferometer and spin system using the virtual rigidity concept, which, in terms of implementation, requires only suitable choices of the various homodyne, probe, and squeezing phases.

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I. INTRODUCTION

The sensitivity of the contemporary state-of-art optical interferometers is to a large degree limited by quantum fluctuations of the probing light. In particular, in the modern laser interferometric gravitational wave detectors (GWDs), like Advanced LIGO [1] and Advanced VIRGO [2], the dominating noise source in the mid- and high-frequency parts of their sensitivity band (above ~ 100 Hz) is the shot noise, which originates from the quantum fluctuations of the light phase [3]. In the more general context of the theory of linear quantum measurements [4–6], it is known as the measurement imprecision noise. In the lower frequencies band, the technical (that is, nonquantum) noise sources dominate for now.

The resulting sensitivity has proved to be sufficient for direct observation of gravitational waves from astrophysical sources [3] with an event rate which exceeded one per week during the current (as of June 2019) O3 observing run of the Advanced LIGO and Advanced VIRGO interferometers [7]. At the same time, almost all GW signals detected to date came from only one class of cosmic events,

namely, binary black hole coalescences. In order to regularly detect gravitational waves from less powerful events, like neutron star coalescences and supernova explosions, the next major step in increasing the sensitivity of the GWDs is required.

The shot noise can be suppressed either by the brute-force increase of the optical power circulating in the interferometer or by injecting squeezed light into the interferometer dark port, as was proposed in Ref. [8]. Squeezed light is used in the smaller GW detector GEO-600 since 2011 [9,10]. Starting from the beginning of the O3 observing run, it is used in the Advanced LIGO and Advanced VIRGO as well.

Because of the Heisenberg uncertainty relation, suppression of the shot noise leads to the proportional increase of another kind of quantum noise, namely, the radiation pressure noise, also known as the quantum backaction noise [5]. It originates from the quantum fluctuations of the light power in the interferometer, which create a random force perturbing the positions of the interferometer mirrors. Within the sensitivity band of the laser GW detectors ($\gtrsim 10$ Hz), the suspended mirrors of the GW detectors can be treated as free masses. Correspondingly, the massless susceptibility function of the signal mechanical degree of freedom of the interferometer can be approximated as

$$\chi_I(\Omega) = -1/\Omega^2, \quad (1)$$

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where Ω is the observation frequency. Therefore, the radiation pressure noise is most important in the low-frequency part of the GW detectors' sensitivity band. When the Advanced LIGO reaches its design sensitivity, the radiation pressure noise will be the dominating one at low frequencies, i.e., below ~ 100 Hz.

At any given frequency Ω , an optimal value of the optical power exists which provides the minimum of the sum quantum noise at this frequency. In the case where the imprecision noise and the backaction noise are uncorrelated, this minimum is known as the standard quantum limit (SQL) [11]. Being expressed in units of spectral density of the effective position noise, it is equal to [12]

$$S_{\text{SQL}} = \frac{\hbar}{m\Omega^2}. \quad (2)$$

Several methods of overcoming the SQL suitable for laser interferometers are known; see, e.g., the reviews [5,6]. In particular, as early as in 1982, Unruh [13] had shown that, injecting into the interferometer squeezed light with the optimally tuned frequency-dependent squeeze angle (i.e., phase squeezing at higher frequencies and amplitude squeezing at lower ones), it is possible to suppress the quantum noise spectral density by the squeeze factor e^{2r} over the entire band of interest. A practical method for generating frequency-dependent squeezed light was proposed by Kimble and co-workers in Ref. [14]. They have shown that the necessary frequency dependence can be created by reflecting an ordinary frequency-independent squeezed vacuum from an additional Fabry-Pérot cavity (a so-called filter cavity).

This scheme is considered now as one of the most probable candidates for implementation in the next generation of GW detectors. However, it has a significant disadvantage, namely, vulnerability to optical losses in the filter cavity. In order to “dilute” them, long (and therefore expensive) filter cavities with high-reflectivity mirrors have to be used. In fact, filter cavities with the same 4 km length as the main interferometer arms were considered in Ref. [14]. Currently, a more modest but still long (tens of meters) cavity is discussed as an option for the future upgrade of the Advanced LIGO detectors [15,16].

In Ref. [17], a different approach to the preparation of the necessary quantum state of light was proposed. In this scheme, two entangled light beams are prepared using an optical parametric oscillator. One of them (“signal”) probes the interferometer, and the second one (“idler”) the filter cavity. The output beams are then measured by two homodyne detectors. Because of the entanglement, measurement of the idler beam prepares the signal beam in the required frequency-dependent squeezed quantum state. Taking into account that the wavelengths of the signal and the idler beam could be different (the nondegenerate regime), some additional mode of the interferometer can be

used as the filter cavity; it is this option that was considered in detail in Ref. [17]. This scheme does not require a dedicated filter cavity, but it requires instead the additional squeezed light injection and the additional readout optical paths which could hinder its practical application.

Instead of the passive filter cavity, a much more compact active “negative effective mass” atomic spin ensemble has been shown to cancel quantum backaction noise, generate entanglement, and perform sensing beyond the SQL. First experiments were performed with purely atomic systems [18,19]. Later, the idea was applied to a mechanical system [20] in the spirit of trajectories without quantum uncertainties based on the establishment of entanglement between a mechanical oscillator and a spin system [21]. There, it has been shown that an ensemble of spins oriented (anti)parallel to the axis of the magnetic field behaves as an effective (positive-) negative-mass oscillator within the Holstein-Primakoff approximation. Those early papers utilized the “sequential” layout, where the same light interacts with the mechanical mode and the spin ensemble. Recently, suppression of the backaction noise using the atomic spin ensemble scheme was demonstrated experimentally, with a nanomechanical membrane playing the role of the mechanical object [22].

This scheme cannot be used directly in the laser GW detectors, because, in order to interact effectively with the atomic spin ensemble, the optical wavelength must be close to that of the atomic transition ($\lambda_S \approx 850$ nm), while in the contemporary GW detectors the wavelength is equal to $\lambda_I = 1064$ nm, and longer wavelengths are planned for future upgrades. To circumvent this problem, a “parallel” layout (similar to the one of Ref. [17]) was proposed in Ref. [23]. It was shown that, using demanding but realistic parameters of the spin system, it is possible to improve the sensitivity by 6 dB over the entire frequency band of the GWD.

In order to effectively suppress the quantum noise, two conditions have to be satisfied for the interferometer and the spin system. First, the readout rates (the measurement strengths) in the subsystems have to match each other. Second, the susceptibility of the spin system has to match that of the relevant mechanical degree of freedom in the interferometer. In Ref. [23], a brute-force approach to satisfying these conditions was used, which resulted in a very demanding value of the quantum cooperativity factor \mathcal{C}_S of the spin system (denoted as d_0 in Ref. [23]), about 10^2 (see details in Sec. II A). Such a high value of \mathcal{C}_S requires that the spin ensemble should be placed inside an optical cavity, which inevitably increases the optical losses, greatly hindering the implementation of this scheme.

In the present paper, we introduce an additional mechanism, the *virtual optical rigidity* effect (see Sec. 4.4 of Ref. [5]), into the combined GWD and spin system. We show that this idea dramatically relaxes the requirement on \mathcal{C}_S . The new mechanism can be implemented by

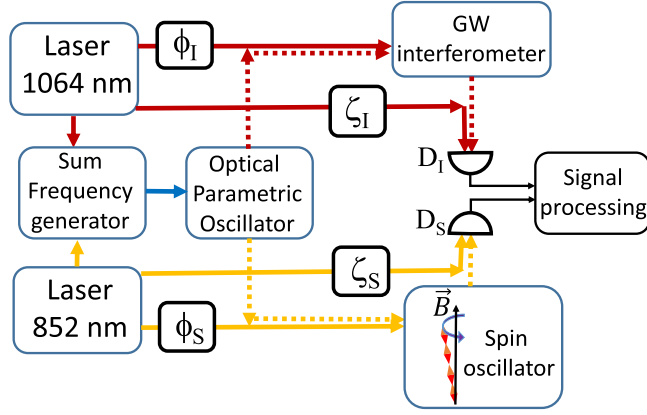


FIG. 1. The GW interferometer (I) and the spin oscillator (S) are probed and detected in parallel by laser beams (solid arrows) with different wavelengths but entangled fluctuations (dashed arrows). These two-mode-squeezing correlations are achieved by means of a sum frequency generator in combination with an optical parametric oscillator. The collective spin of the atomic ensemble precesses around the magnetic field \vec{B} , forming a spin oscillator. With respect to the squeeze angle of this process, we reference the probe $\phi_{I,S}$ and detection $\zeta_{I,S}$ phases of the respective systems. The output fields impinge on detectors $D_{I,S}$, and the resulting measurements are suitably combined to cancel the joint meter noise. A possible practical implementation of the present conceptual schematic is presented in Ref. [23].

experimentally straightforward phase shifts of the optical carrier and homodyne detection. In the following, we provide the general analysis of the parallel spin-system-based scheme shown in Fig. 1, assuming full freedom in our choice of the relevant phases, namely, two homodyne angles and two optical carriers relative to the squeezing phase. We then show that the virtual rigidity effect can induce effective frequency shifts in the mechanical and spin system susceptibilities. Finally, we derive a simple closed equation (57) for the sensitivity gain provided by our scheme, which clearly shows the comparative role of the optical and the spin system losses at different frequencies.

The paper is organized as follows. In Sec. II, we familiarize the readers with the “brute-force” matching conditions of Ref. [23], introduce the virtual rigidity concept and use it to derive conditions for quantum noise

suppression under ideal conditions. In Sec. III, we present the full expression for the sensitivity of our scheme accounting for various imperfections, including finite entanglement between the probe fields, optical losses, the spin system thermal noise, and response mismatch due to the spin system dissipation. We then evaluate the sensitivity in Sec. IV using state-of-the-art parameters for interferometer and spin systems to assess the potential of our scheme. Finally, we conclude and give an outlook in Sec. V.

The main parameters used in this paper are listed in Table I. For the GW interferometer parameters, we use the values which correspond to the Advanced LIGO design goal [24]. We would like to note, however, that our results explicitly depend only on one parameter of the interferometer, namely, the readout rate

$$\Omega_{qI} = \sqrt{\frac{16\omega_o I_c}{mcL\gamma}}, \quad (3)$$

which is equal to $\Omega_{qI} \approx 2\pi \times 60$ Hz for the parameters listed in Table I. Taking into account that for future interferometers higher optical power but at the same time heavier test masses and longer arms are planned, it is reasonable to expect that this parameter will not change drastically. For the intrinsic spin linewidth we assume $\gamma_{S,0} = 2\pi \times 1$ Hz as has been demonstrated in an experiment [25].

II. QUANTUM NOISE MATCHING

A. Matching conditions for the interferometer and spin systems without virtual rigidity

A schematic of the experimental layout is shown in Fig. 1. To set the stage for this extended scheme, we start by reviewing the simpler scheme introduced in Ref. [23]. In essence, it differs from the one considered here and shown in Fig. 1 only by the specific choice of the homodyne and the carrier angles:

$$\phi_I = \phi_S = 0, \quad \zeta_I = \zeta_S = \frac{\pi}{2}. \quad (4)$$

TABLE I. The main parameters and their numerical values used in this paper.

Notation	Quantity	Value used for estimates
ω_o	Optical frequency	$2\pi c/(1064 \text{ nm})$
L	Interferometer arm length	4000 m
m	Mirror mass	40 kg
γ	Interferometer bandwidth (half width at half maximum, HWHM)	$2\pi \times 500$ Hz
I_c	Optical power circulating in each of the arms	840 kW
$\gamma_{S,0}$	Spin system “dark” damping rate (HWHM)	$2\pi \times 1$ Hz
η_{iI}, η_{oI}	Input and output quantum efficiencies of the interferometer	0.95
η_{iS}, η_{oS}	Input and output quantum efficiencies of the spin system	0.95

In this limiting case, relations for the input $\hat{a}_{I,S}$ and output $\hat{b}_{I,S}$ light quadratures for the interferometer and spins, respectively, are [23]

$$\hat{b}_I^s = \hat{a}_I^s + \chi_I \left(\frac{\Omega_{qI}}{\sqrt{\hbar m}} F_s + \Omega_{qI}^2 \hat{a}_I^c \right), \quad (5a)$$

$$\hat{b}_S^s = \hat{a}_S^s + \chi_S (\Omega_{qS} \hat{f}_T + \Omega_{qS}^2 \hat{a}_S^c), \quad (5b)$$

where Ω_{qS} and Ω_{qI} are the readout rates, F_s is the signal (GW) force, \hat{f}_T is the normalized thermal noise of the spin system, χ_I and χ_S are the massless susceptibilities, and the superscripts c and s denote the cosine (amplitude) and sine (phase) quadratures, respectively.

The analysis of the work [23] was based on two conditions for the negative-mass spin system parameters, which allow us to provide the required conditional frequency-dependent squeezing across the entire bandwidth of interest. The first one is the equality of the readout rates in the two subsystems:

$$\Omega_{qS} = \Omega_{qI}, \quad (6)$$

where

$$\Omega_{qS} = \sqrt{4\Gamma_S \Omega_S} \quad (7)$$

is the spin system readout rate, Ω_S is the spin system (Larmor) resonance frequency, and Γ_S is the spin-light coupling factor proportional to the optical power probing the spin system. Both Ω_S and Γ_S are typically highly tunable parameters for a collective spin oscillator [22], the former by the dc magnetic bias field and the latter by the optical probe power. However, the readout of the spin oscillator entails an increase of its bandwidth beyond its intrinsic value $\gamma_{S,0}$ due to induced spontaneous emission (i.e., power broadening)

$$\gamma_S - \gamma_{S,0} = \gamma_{S,\text{pb}} = \Gamma_S / \mathcal{C}_S, \quad (8)$$

where the spin oscillator cooperativity \mathcal{C}_S depends on factors such as atomic density, the atomic species, optional cavity enhancement, and probe detuning from atomic resonance but is independent of probe power. Since it is desirable to keep the spin decay γ_S small, due to the noise and response mismatch it otherwise entails, we are motivated to realize the condition (6) by means of a relatively small Γ_S (so as to keep $\gamma_{S,\text{pb}}$ small) and a large Ω_S . However, this strategy raises another problem pertaining to the second matching condition which must be fulfilled for broadband noise cancellation:

$$\chi_I(\Omega) = \frac{1}{-\Omega^2} \approx -\chi_S(\Omega) = \frac{1}{\Omega_S^2 - \Omega^2 - 2i\gamma_S\Omega}, \quad (9)$$

where χ_S is the spin system (massless) susceptibility. In addition to showing the need for small γ_S , this condition prompts us to employ a small $\Omega_S \rightarrow 0$, contrary to what was suggested by the first condition [Eq. (6)]. These two opposing requirements can, in principle, be accommodated by a compromise involving a small, finite Ω_S as in the original proposal [23], where the value $2\pi \times 3$ Hz was used. But this strategy demands a highly refined spin system with $\mathcal{C}_S \sim 10^2$ to avoid an excessively power-broadened γ_S (8), thus posing a significant practical challenge.

B. Virtual rigidity representation

Let us start with a standard optomechanical setup consisting of a mechanical object (free mass or harmonic oscillator) whose motion modulates the eigenfrequency of an optical cavity probed by a pump laser. Using the well-known analogy between the mechanical system and the collective spin mode of the atomic ensemble [22,26], our treatment here can be extended to the latter, as we will make use of in Sec. II C. For simplicity, we neglect here the optical and mechanical losses (they will be taken into account later). Also for simplicity, we assume that our frequency band of interest is well within the cavity half bandwidth γ (the bad-cavity approximation):

$$\Omega \ll \gamma. \quad (10)$$

This assumption, which we retain throughout this work, will be discussed in more detail in Sec. III A.

The input-output relation for this system can be presented as follows:

$$\begin{aligned} \hat{b}^\zeta &= \hat{b}^c \cos \zeta + \hat{b}^s \sin \zeta \\ &= \hat{a}^\zeta + \chi \left(\frac{\Omega_q}{\sqrt{\hbar m}} F_s + \Omega_q^2 \hat{a}^\phi \right) \sin(\zeta - \phi); \end{aligned} \quad (11)$$

see, e.g., the review papers [5,27]. Here ζ is the homodyne angle, ϕ is the optical carrier phase, $\hat{a}^{c,s}$ are the cosine and the sine quadratures of input light, respectively, satisfying the commutation relation $[\hat{a}^c, \hat{a}^s] = i$ [28], $\hat{b}^{c,s}$ are the corresponding amplitudes of the output light, and $\hat{a}^\psi, \hat{b}^\psi$, etc., are the rotated quadratures in terms of an angle ψ , e.g.,

$$\hat{a}^\psi = \hat{a}^c \cos \psi + \hat{a}^s \sin \psi. \quad (12)$$

It is easy to see that Eqs. (5) correspond to the particular case of Eq. (11) where $\phi = 0$ and $\zeta = \pi/2$.

From the output field (11), the signal force is estimated as

$$\tilde{F}_s = F_s + \sqrt{\hbar m} \hat{f}, \quad (13)$$

where

$$\hat{f} = \frac{\chi^{-1}}{\Omega_q \sin(\zeta - \phi)} \hat{a}^\zeta + \Omega_q \hat{a}^\phi \quad (14)$$

is the normalized sum quantum noise of our system. The two components of this equation describe the imprecision noise and the backaction noise, respectively; in general, these are correlated with each other.

The consequences of the correlations can be elucidated by introducing the orthonormal quadrature basis defined by the detection angle ζ :

$$\hat{a}^{c'} \equiv \hat{a}^{(\zeta - \pi/2)} = \hat{a}^c \sin \zeta - \hat{a}^s \cos \zeta, \quad (15a)$$

$$\hat{a}^{s'} \equiv \hat{a}^\zeta = \hat{a}^c \cos \zeta + \hat{a}^s \sin \zeta. \quad (15b)$$

The resulting form of \hat{f} (14) is

$$\hat{f} = \frac{\chi_{\text{eff}}^{-1}}{\beta} \hat{a}^{s'} + \beta \hat{a}^{c'}, \quad (16)$$

where

$$\beta = \Omega_q \sin(\zeta - \phi) \quad (17)$$

is the effective readout rate and

$$\chi_{\text{eff}}^{-1} \equiv \chi^{-1} + \frac{\Omega_q^2}{2} \sin 2(\zeta - \phi) \quad (18)$$

is the *effective susceptibility* of the scheme. It follows from Eq. (16) that the orthonormal basis (15) introduces the effective, *uncorrelated* imprecision and backaction noise terms constructed by absorbing the part of the backaction correlated with the nominal imprecision noise into an effective imprecision noise term. A by-product of this transformation is the modified effective susceptibility χ_{eff} . Since the modification term in Eq. (18) is real and independent of the Fourier frequency, it corresponds to a shift in the resonance frequency of χ , whence it is referred to as *virtual rigidity* (see Sec. 4.4 of Ref. [5]).

We conclude that, in the absence of optical losses, the probing of a system characterized by χ and probe parameters Ω_q , ζ , and ϕ is indistinguishable from the scenario resulting from using the scheme with effective parameters χ_{eff} , $\Omega_{q\text{eff}} = \beta$, and $\zeta_{\text{eff}} - \phi_{\text{eff}} = \pi/2$.

C. Quantum noise matching using virtual rigidity for two systems probed by entangled light

Consider now two systems—the interferometer and the spin system, denoted by the subscripts I and S , respectively. Suppose that they are probed by individual optical meters, described by the four quadratures $\hat{a}_I^{c,s}$ and $\hat{a}_S^{c,s}$, in the manner described in Sec. II B. The two systems are not interacting, but the fluctuations of the two light meters are

assumed to be entangled by a nondegenerate parametric down-conversion process (see Fig. 1). We will use the parametric pump phase as the phase reference point (that is, the squeeze angle defines zero phase). In this case, the noise spectral densities of all four quadratures are equal to

$$S_{a_I^c} = S_{a_I^s} = S_{a_S^c} = S_{a_S^s} = \frac{\cosh 2r}{2}, \quad (19a)$$

and the cosine quadratures of the beams are correlated, whereas the sine counterparts are anticorrelated:

$$S_{a_I^c a_S^c} = -S_{a_I^s a_S^s} = \frac{\sinh 2r}{2}, \quad (19b)$$

where r is the squeeze factor. All other components of the correlation matrix vanish.

Assume now that we wish to measure a force signal acting on system I . Because of the meter noise correlations, the sensitivity to this signal can be improved by exploiting the additional probing on system S by adding the corresponding additional output signal to the main interferometer signal with some optimal weight function Λ . The equations for the normalized meter noise (14) for the two systems are

$$\hat{f}_I = \frac{\chi_I^{-1}}{\Omega_{qI} \sin(\zeta_I - \phi_I)} \hat{a}_I^{\zeta_I} + \Omega_{qI} \hat{a}_I^{\phi_I}, \quad (20a)$$

$$\hat{f}_S = \frac{\chi_S^{-1}}{\Omega_{qS} \sin(\zeta_S - \phi_S)} \hat{a}_S^{\zeta_S} + \Omega_{qS} \hat{a}_S^{\phi_S}, \quad (20b)$$

respectively, where $\zeta_{I,S}$ are the homodyne angles in the interferometer and the spin system channels, respectively, and $\phi_{I,S}$ are the corresponding probe phases of the carrier fields. In Ref. [23], the simplest particular case of measuring the phase quadratures of light while probing with the (orthogonal) amplitude fluctuations was considered:

$$\zeta_I = \zeta_S = \frac{\pi}{2}, \quad \phi_I = \phi_S = 0, \quad (21)$$

which corresponds to

$$\hat{f}_I = \frac{\chi_I^{-1}}{\Omega_{qI}} \hat{a}_I^s + \Omega_{qI} \hat{a}_I^c, \quad (22a)$$

$$\hat{f}_S = \frac{\chi_S^{-1}}{\Omega_{qS}} \hat{a}_S^s + \Omega_{qS} \hat{a}_S^c. \quad (22b)$$

Taking into account Eqs. (19), it is easy to see that if

$$\Omega_{qS}^2 = \Omega_{qI}^2 \quad \text{and} \quad \chi_S = -\chi_I, \quad (23)$$

then the simple subtraction of \hat{f}_S from \hat{f}_I (which corresponds to the choice of the above-mentioned weight

function $\Lambda = -1$) allows us to reduce the resulting noise spectral density by the factor $e^{2r}/2$ relative to a standard interferometer subject to vacuum noise. The optimal weight function $\Lambda = -\tanh 2r$ gives the slightly better suppression factor $\cosh 2r$.

As was discussed in Sec. II A, implementation of the near antisymmetric susceptibilities (23) could be problematic due to technological limitations. However, the virtual rigidity approach can be used to make the effective susceptibilities (18) match each other. Here we demonstrate how the complete cancellation of quantum noise at all Fourier frequencies can be engineered in the limit of a lossless negative-mass spin system with

$$\chi_S^{-1} = -(\Omega_S^2 - \Omega^2), \quad (24a)$$

where the overall sign stems from the negative mass (the general case is considered in Sec. III). For the interferometer, we suppose that

$$\chi_I^{-1} = -\Omega^2 \quad (24b)$$

(the ideal free mass).

In general, the phase rotation transformations (15) in terms of $\zeta_{I,S}$ alter the cross-correlation entries in the spectral density matrix of the light quadratures. However, an interesting feature of the two-mode squeezed light generated in a nondegenerate parametric process is that if the homodyne angles ζ_I and ζ_S are antisymmetric with respect to the phase of the parametric pump (modulo π),

$$\zeta_I + \zeta_S = \pi n, \quad (25)$$

where n is an integer, then the matrix remains invariant and, in particular, Eqs. (19) remain valid. This follows from the simple geometrical observation that Eq. (19b) implies that the quadrature pairs $(\hat{a}_I^s, \hat{a}_S^c)$ and $(\hat{a}_I^c, -\hat{a}_S^s)$ are correlated. The minus sign in the latter pair effectively inverts the sense of rotation (15), $\zeta_S \rightarrow -\zeta_S$, resulting in the antisymmetric condition (25) for invariance of the correlation matrix. Let us, without the loss of generality, take $n = 1$ in Eq. (25) in order to provide a smooth transition from the case of Ref. [23], as stated in Eqs. (21).

Assuming the condition (25), we can rewrite Eqs. (20) in the virtual rigidity form (16):

$$\hat{f}_I = \frac{\chi_{\text{eff}I}^{-1}}{\beta_I} \hat{a}_I^s + \beta_I \hat{a}_I^c, \quad (26a)$$

$$\hat{f}_S = \frac{\chi_{\text{eff}S}^{-1}}{\beta_S} \hat{a}_S^s + \beta_S \hat{a}_S^c, \quad (26b)$$

where

$$\beta_{I,S} = \Omega_{qI,S} \sin(\zeta_{I,S} - \phi_{I,S}) \quad (27)$$

and

$$\chi_{\text{eff}I}^{-1} = -\Omega^2 + \frac{\Omega_{qI}^2}{2} \sin 2(\zeta_I - \phi_I), \quad (28a)$$

$$\chi_{\text{eff}S}^{-1} = \Omega^2 - \Omega_S^2 + \frac{\Omega_{qS}^2}{2} \sin 2(\zeta_S - \phi_S). \quad (28b)$$

Therefore, the setting

$$\frac{\Omega_{qI}^2}{2} \sin 2(\zeta_I - \phi_I) = \Omega_S^2 - \frac{\Omega_{qS}^2}{2} \sin 2(\zeta_S - \phi_S) \quad (29)$$

provides the effective response functions matching condition $\chi_{\text{eff}S}^{-1} = -\chi_{\text{eff}I}^{-1}$.

Finally, we have to make the effective coupling factors equal to each other, which gives the following condition:

$$\beta_I^2 = \beta_S^2. \quad (30)$$

In order to simplify the equations, it is convenient to introduce the following combined angles:

$$\zeta \equiv \zeta_I - \phi_I, \quad \phi \equiv \phi_I + \phi_S. \quad (31)$$

In these notations, the conditions (25), (29), and (30) can be reexpressed and summarized, respectively, as

$$\zeta + \phi_I + \zeta_S = \pi, \quad (32a)$$

$$\Omega_{qS}^2 = \frac{\sin^2 \zeta}{\sin^2(\zeta + \phi)} \Omega_{qI}^2, \quad (32b)$$

$$\Omega_S^2 = \frac{\sin \zeta \sin \phi}{\sin(\zeta + \phi)} \Omega_{qI}^2. \quad (32c)$$

These conditions generalize those of the simpler scheme, Eqs. (6) and (9), which are recovered from Eqs. (32b) and (32c) as the special case $\zeta = \pi/2$ and $\phi = 0$.

D. Geometrical interpretation of noise cancellation using virtual rigidity

We now provide a geometrical interpretation of the conditions for quantum noise cancellation arrived at above. To this end, we focus on the case $\zeta = \pi/2$, which is the natural choice for purposes of broadband sensing enhancement (as will be discussed below). In view of Eqs. (31), we may choose $\phi_I = 0$ as a matter of convention, since this is without consequences for Ω_{qS} and Ω_S [Eqs. (32b) and (32c)]; it follows that $\phi = \phi_S$ and, from Eq. (32a), $\zeta_S = \pi/2$. Conveniently, this implies equality between the original and primed quadrature bases $\hat{a}_{I,S}^{c,s}$ [Eqs. (15)].

In this scenario, the backaction matching condition (32b) can be written [cf. Eq. (6)]

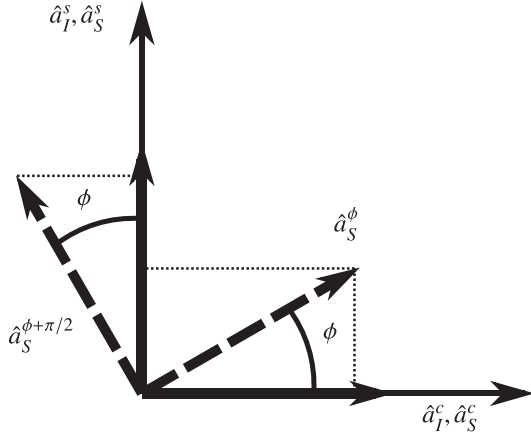


FIG. 2. Geometrical representation of the virtual rigidity effect. The backaction and imprecision noise quadratures for I and S are depicted with respect to the quadrature bases $(\hat{a}_{I,S}^c, \hat{a}_{I,S}^s)$, respectively. Homodyne measurement quadratures are chosen to be \hat{b}_I^s and \hat{b}_S^s (i.e., $\zeta_I = \zeta_S = \pi/2$) so that the corresponding imprecision noise quadratures (vertical bold arrow) coincide with the vertical axes, \hat{a}_I^s and \hat{a}_S^s . For I , we make the “standard” choice of probe phase $\phi_I = 0$ such that the orthogonal quadrature \hat{a}_I^c acts as backaction. However, for S , a probe phase $\phi = \phi_S$ relative to \hat{a}_S^c is introduced.

$$\Omega_{qI}^2 = \Omega_{qS}^2 \cos^2 \phi = 4\Omega_S \Gamma_S \cos^2 \phi, \quad (33)$$

where only the component $\Gamma_S \cos^2 \phi$ of the spin backaction \hat{a}_S^{ϕ} overlapping with that of the interferometer \hat{a}_I^c contributes (Fig. 2); the projection factor is $\cos \phi$ in terms of amplitude and, thus, $\cos^2 \phi$ in terms of power. However, the power broadening of γ_S and associated noise are still proportional to the full backaction rate Γ_S according to Eq. (8).

The virtual rigidity effect results in an effective spin resonance frequency Ω_{Seff} as found in Eq. (28b):

$$\Omega_{\text{Seff}}^2 = \Omega_S^2 - \frac{\Omega_{qS}^2}{2} \sin 2\phi = \Omega_S^2 - \Omega_{qI}^2 \tan \phi, \quad (34)$$

where the condition (33) was used to obtain the last expression. This shift can be understood geometrically from Fig. 2 as follows: The state of S is mapped with strength Ω_{qS}^2 onto the output quadrature $\hat{b}_S^{\phi+\pi/2}$ whose imprecision noise $\hat{a}_S^{\phi+\pi/2}$ (orthogonal to the backaction \hat{a}_S^{ϕ}) has the projection factor $\cos \phi$ onto \hat{a}_S^s , the imprecision noise of the chosen measurement quadrature. Meanwhile, the part of the backaction \hat{a}_S^{ϕ} correlated with \hat{a}_S^s is the projection $\sin \phi$. Combining these factors, the resulting interference is found to be equivalent to a shift in the resonance frequency squared by $-\Omega_{qS}^2 \cos \phi \sin \phi = -(\Omega_{qS}^2/2) \sin 2\phi$ [see Eq. (34)], where the minus sign arises from the negative effective mass; cf. Eq. (24). Matching requires $\Omega_{\text{Seff}} = 0$ as discussed above, thus, according to Eq. (34), fixing

$$\Omega_S = \Omega_{qI} \sqrt{\tan \phi}, \quad (35)$$

which is consistent with Eq. (32c) for $\zeta = \pi/2$.

E. Optimal ϕ for minimizing spin decay γ_S

Continuing to focus on the choice $\zeta = \pi/2$ relevant for broadband quantum noise evasion, we now finally address to which extent the virtual rigidity effect can alleviate the limitation of the original scheme reviewed in Sec. II A. Our goal is to approach the quantum noise matching conditions while minimizing γ_S and, hence, Γ_S ; see Eq. (8). As is clear from Eq. (35), the virtual rigidity effect allows us (in principle) to work at an arbitrarily large Ω_S for a given Ω_{qI} by letting $\phi \rightarrow \pi/2$. But the projection factor $\cos^2 \phi$ in Eq. (33) entails that under the constraint of matching (32) the minimum of γ_S occurs at a finite value of Ω_S . Combining Eqs. (33) and (35), we find that

$$\Gamma_S = \frac{\Omega_{qI}}{4\sqrt{\sin \phi \cos^3 \phi}}, \quad (36)$$

which is minimal at $\phi = \pi/6$, resulting in

$$\Gamma_S = \Omega_{qI}/3^{3/4}, \quad \Omega_S = \Omega_{qI}/3^{1/4}, \quad (37)$$

and, hence, in view of Eq. (8), the minimized spin decay γ_S . Since this is the main bottleneck parameter, as will be clear from the full sensitivity calculation below, the parameters $\zeta = \pi/2$, $\phi = \pi/6$, and (37) constitute a quasioptimal set for broadband quantum noise evasion resulting in a much less stringent requirement for the spin cooperativity \mathcal{C}_S and/or the intrinsic decay rate $\gamma_{S,0}$ compared to the original proposal [23].

III. CALCULATION OF THE SENSITIVITY

A. Assumptions and approximations

In the analysis above, we arrived at the conditions for perfect quantum noise cancellation while elucidating the essential physics of our scheme. However, this was done in the idealized limit of dissipationless mechanical and spin degrees of freedom. While the mechanical losses in modern gravitational wave detectors are very small and can safely be neglected in our analysis, the imperfections brought about by finite bandwidth γ_S of the spin system as well as by the optical losses must be accounted for in order to assess the feasibility of the scheme.

A finite γ_S will impact performance in two ways. First, it will introduce a nonzero imaginary part to the spin system susceptibility:

$$\chi_S^{-1} = -(\Omega_S^2 - \Omega^2 - 2i\Omega\gamma_S), \quad (38)$$

which cannot be countered by the virtual rigidity effect and, hence, will render perfect broadband matching of the

effective susceptibilities $\chi_{\text{eff}I}^{-1}$ and $\chi_{\text{eff}S}^{-1}$ impossible. Second, on account of the dissipation-fluctuation theorem, spin noise uncorrelated with the meter noise will degrade the sensitivity.

The optical losses can in a natural way be divided into three parts: the losses in the input paths of the interferometer and the spin system, the light absorption inside these two subsystems (e.g., the intracavity losses), and the losses in their output paths. The input losses include, in particular, the imperfections of the squeezer, whereas the output losses include, in particular, the finite quantum efficiency of the detectors. In order to simplify the equations, we neglect the intracavity losses. In the contemporary GW interferometers, the influence of these losses is small in comparison with the input and the output counterparts. Concerning the spin system, the virtual rigidity approach requires only the modest quantum cooperativity $C_S \sim 10$, which allows the use of a small-finesse cavity or even a cavityless path-through topology, which also makes the internal optical losses much smaller than those at the input and the output.

In our analysis here and below, we still assume the bad-cavity approximation (10). This approach is justified by the following reasoning. The spectral shape of the quantum noise of interferometers depends on the two characteristic frequencies Ω_q and γ . Below Ω_q , the radiation pressure noise dominates over the imprecision shot noise (if no backaction cancellation techniques are used). Above γ , the normalized noise increases due to the signal cutting by the interferometer bandwidth. In all contemporary and planned GWDs, $\Omega_q \ll \gamma$. If frequency-independent squeezing is used, then the effective Ω_q scales up as e^{2r} . However, in *frequency-dependent* squeezing schemes like the one considered here, both the backaction noise and the imprecision shot noise are suppressed, leaving Ω_q unchanged. Therefore, all nontrivial behavior of the backaction cancellation schemes is concentrated in the frequency band $\Omega \sim \Omega_q \ll \gamma$. In particular, it is easy to show that, at higher frequencies, the scheme which we consider here provides only the trivial (but desirable) frequency-independent suppression of the sum quantum noise, which consists only of the imprecision shot noise in this frequency band, by a frequency-independent factor defined by the squeezing rate and the optical losses.

B. Effects of dissipation and losses

With account of optical losses and spin dissipation, the input-output relations for the interferometer and the spin system take the following form:

$$\hat{b}_I^{\zeta_I} = \sqrt{\eta_{ol}} \left[\hat{a}_I^{\zeta_I} + \chi_I \left(\frac{\Omega_{qI}}{\sqrt{\hbar m}} F_s + \Omega_{qI}^2 \hat{a}_I^{\phi_I} \right) \sin(\zeta_I - \phi_I) \right] + \sqrt{1 - \eta_{ol}} \hat{z}_I^{\zeta_I}, \quad (39a)$$

$$\hat{b}_S^{\zeta_S} = \sqrt{\eta_{oS}} [\hat{a}_S^{\zeta_S} + \chi_S (\Omega_{qS} \hat{f}_T + \Omega_{qS}^2 \hat{a}_S^{\phi_S}) \sin(\zeta_S - \phi_S)] + \sqrt{1 - \eta_{oS}} \hat{z}_S^{\zeta_S}; \quad (39b)$$

compare with Eq. (11). Here $\hat{z}_{I,S}$ are the vacuum fields associated with the output optical losses of the interferometer and the spin system channels, and \hat{f}_T is the normalized thermal force of the spin system with the spectral density defined by the fluctuation-dissipation theorem:

$$\sigma_T \geq 2\gamma_S \Omega. \quad (40)$$

We assume that this noise is ground-state noise, i.e., with equality in the above equation. Accounting for the input optical losses, the spectral densities and correlations (19) of the incident optical fields generalize to

$$S_{a_I^c} = S_{a_I^s} = \eta_{il} \sinh^2 r + 1/2, \quad (41a)$$

$$S_{a_S^c} = S_{a_S^s} = \eta_{is} \sinh^2 r + 1/2, \quad (41b)$$

$$S_{a_I^c a_S^c} = -S_{a_I^s a_S^s} = \frac{1}{2} \sqrt{\eta_{il} \eta_{is}} \sinh 2r. \quad (41c)$$

Similar to our treatment in Sec. II C, we introduce the normalized noise forces

$$\hat{f}_I = \frac{\chi_{\text{eff}I}^{-1} \hat{a}_I^{sI} + \chi_I^{-1} \epsilon_{ol} \hat{z}_I^{\zeta_I}}{\beta_I} + \beta_I \hat{a}_I^c, \quad (42a)$$

$$\hat{f}_S = \frac{\chi_{\text{eff}S}^{-1} \hat{a}_S^{sS} + \chi_S^{-1} \epsilon_{oS} \hat{z}_S^{\zeta_S}}{\beta_S} + \beta_S \hat{a}_S^c + \hat{f}_T, \quad (42b)$$

where

$$\epsilon_{ol,S} = \sqrt{\frac{1 - \eta_{ol,S}}{\eta_{ol,S}}}, \quad (43)$$

compare with Eqs. (26). The spectral densities of \hat{f}_I and \hat{f}_S and their cross-spectral density are equal to

$$\sigma_I = \frac{\eta_{il} K_I}{2} (\cosh 2r + \kappa_I), \quad (44a)$$

$$\sigma_S = \frac{\eta_{is} K_S}{2} (\cosh 2r + \kappa_S), \quad (44b)$$

$$\sigma_{IS} = \frac{1}{2} \sqrt{\eta_{il} \eta_{is}} K_{IS} \sinh 2r, \quad (44c)$$

where we have introduced the factors

$$\kappa_I = \epsilon_{II}^2 + \frac{k_I \epsilon_{oI}^2}{K_I \eta_{II}}, \quad (45a)$$

$$\kappa_S = \epsilon_{IS}^2 + \frac{k_S \epsilon_{oS}^2 + 2\sigma_T}{K_S \eta_{IS}}, \quad (45b)$$

describing the total imperfections in each of the channels, and the coefficients

$$K_{I,S} = \frac{|\chi_{\text{eff},I,S}^{-1}|^2}{\beta_{I,S}^2} + \beta_{I,S}^2, \quad (46a)$$

$$K_{IS} = K_{IS}^c \cos(\zeta_I + \zeta_S) + K_{IS}^s \sin(\zeta_I + \zeta_S), \quad (46b)$$

$$k_{I,S} = \frac{|\chi_{I,S}^{-1}|^2}{\beta_{I,S}^2}, \quad (46c)$$

with

$$K_{IS}^c = \frac{\chi_{\text{eff},I}^{-1} \chi_{\text{eff},S}^{-1*}}{\beta_I \beta_S} - \beta_I \beta_S, \quad K_{IS}^s = \frac{\beta_S}{\beta_I} \chi_{\text{eff},I}^{-1} + \frac{\beta_I}{\beta_S} \chi_{\text{eff},S}^{-1*}. \quad (47)$$

The optimally combined sum noise spectral density of the two meters is given by

$$\frac{S}{\hbar m} = \sigma_I - \frac{|\sigma_{IS}|^2}{\sigma_S} = \frac{\eta_{II}}{2K_S(\cosh 2r + \kappa_S)} \{ |K_{\text{res}}|^2 \cosh^2 2r + |K_{IS}|^2 + K_I K_S [(\kappa_I + \kappa_S) \cosh 2r + \kappa_I \kappa_S] \}, \quad (48)$$

where

$$|K_{\text{res}}|^2 = K_I K_S - |K_{IS}|^2. \quad (49)$$

Note that the structure of Eq. (48) suggests that an optimal value of squeezing providing the minimum of S should exist. This optimization is done in the following subsection.

C. Squeezing optimization

Here we derive the optimal value of the squeezing parameter r based on the general expressions given in Sec. III B. To be precise, we derive the value of r that minimizes the sensitivity $S(\Omega)$ (48) at a given Fourier component Ω . Nonzero squeezing (and, hence, introducing the spin system) can improve the sensitivity only if the extraneous noise in the spin system uncorrelated with the interferometer is sufficiently small; from Eq. (48), we find the following condition on κ_S (45b):

$$\kappa_S < 1 - 2 \frac{|K_{\text{res}}|^2}{K_I K_S}. \quad (50)$$

Recall that these quantities depend on the Fourier frequency Ω . Provided that the condition (50) is fulfilled, the

squeeze parameter $r_{\text{opt}}(\Omega)$ that minimizes the sensitivity $S(\Omega)$ is specified by

$$\cosh 2r_{\text{opt}}(\Omega) = \frac{|K_{IS}|}{|K_{\text{res}}|} \sqrt{1 - \kappa_S^2} - \kappa_S. \quad (51)$$

Note that Eqs. (50) and (51) are both independent of the extraneous noise in the *interferometer* due to optical losses, $\eta_{II}, \eta_{oI} < 1$. If the source of entangled light is broadband, as assumed throughout this work, it is characterized by a squeeze factor r which is independent of the Fourier frequency; accordingly, the chosen r will not be optimal for all Fourier frequencies Ω . With this in mind, we may nonetheless evaluate $S(\Omega)$ (48) at $r = r_{\text{opt}}(\Omega)$ to achieve an expression for the optimized sensitivity at each Fourier frequency:

$$\left. \frac{S}{\hbar m} \right|_{r=r_{\text{opt}}} = \frac{\eta_{II}}{2K_S} [2|K_{\text{res}}|^2 \cosh 2r_{\text{opt}} + K_I K_S (\kappa_I + \kappa_S)], \quad (52)$$

with $\cosh 2r_{\text{opt}}$ given by Eq. (51), suppressing the Ω dependence of the involved quantities for brevity.

D. Quasioptimal noise cancellation in the large-squeezing limit

We now optimize the full sensitivity (48) in the large-squeezing limit $e^{2r} \gg 1$. While the parameters which provide this optimum are not strictly the best ones for finite squeezing and in the presence of optical and spin losses and noise, it is still a reasonable working point when these detrimental effects are relatively small.

In the limit of $r \rightarrow \infty$, Eq. (48) simplifies to

$$\frac{S}{\hbar m} = \frac{\eta_{II} e^{2r}}{4} \frac{|K_{\text{res}}|^2}{K_S}. \quad (53)$$

In order to minimize this expression, the cross-correlation term $|K_{IS}|$ has to be maximized. In principle, its rigorous maximization in $\zeta_I + \zeta_S$ is possible, but its maximum corresponds to frequency-dependent homodyne angles. We assume instead that the condition (25) is fulfilled. In this case,

$$|K_{\text{res}}|^2 = \left| \frac{\beta_S}{\beta_I} \chi_{\text{eff},I}^{-1} + \frac{\beta_I}{\beta_S} \chi_{\text{eff},S}^{-1} \right|^2. \quad (54)$$

It is easy to see that, in the ideal lossless case of (24), the conditions (29) and (30) make K_{res} equal to zero.

Unfortunately, the imaginary part of the realistic spin system susceptibility (38) does not allow us to cancel K_{res} completely. Taking it into account and still assuming the conditions (25), (29), and (30), we obtain that

$$K_S = K_I + \frac{4\Omega^2\gamma_S^2}{\beta_I^2}, \quad (55a)$$

$$|K_{IS}|^2 = K_I^2 + \frac{4\chi_{\text{eff}I}^{-2}\Omega^2\gamma_S^2}{\beta_I^4}, \quad (55b)$$

$$|K_{\text{res}}|^2 = 4\Omega^2\gamma_S^2. \quad (55c)$$

Note that $\chi_{\text{eff}I}$ depends only on the angle ζ , as is clear from Eqs. (18) and (31). We thus remark that the optimized noise spectral density (48) depends on the angle ϕ only via χ_S^{-1} , as this dictates our choice of Ω_S according to Eq. (32c). The only term in Eq. (48) that contains χ_S^{-1} represents the vacuum noise due to optical losses at the output of the spin system and is minimal at the peak of $\chi_S(\Omega)$ ($\Omega \sim \Omega_S$ provided that $\Omega_S \gg \gamma_S$). Hence, in the absence of such losses, $\eta_{oS} \rightarrow 1 \Rightarrow \epsilon_{oS} \rightarrow 0$, the sensitivity is independent of both ϕ and Ω_S . Crucially, this allows a significant extent of freedom in choosing the (bare) spin resonance Ω_S , since the appropriate effective (virtual) resonance can be achieved by the proper choice of ϕ ; this is a great advantage for purposes of practical implementation and is a central result of this work.

IV. DISCUSSION OF THE SENSITIVITY

We now explore this central idea in a case of particular interest $\zeta = \pi/2$, so that $\chi_{\text{eff}I} = \chi_I$, which means that the standard phase configuration of orthogonal probe and homodyne quadratures is used for the main interferometer; this is exactly the scenario discussed in Sec. II D. As for an interferometer without a spin system, this yields the most flat shape of the sum quantum noise spectral density, as well as the best performance in the shot-noise-dominated high-frequency band. Moreover, in all plots we choose $\phi = \pi/6$ in order to minimize γ_S for fixed C_S according to the discussion in Sec. II E; hence, the quasioptimal Ω_S and Γ_S are given as functions of Ω_{qI} alone; see Eqs. (37).

Prior to plotting the sensitivity resulting from these parameters, let us discuss the choice of squeezing r in the presence of imperfections. The optimal degree of two-mode squeezing r_{opt} depends on the signal Fourier frequency Ω ; see Sec. III C. This function is plotted in Fig. 3 for different spin cooperativities C_S and exhibits a minimum near $\Omega \sim \Omega_S$ for the present parameters, as will be discussed below in this section.

Taking into account that in GWDs the main interest is in broadband sensing enhancement, we will here choose the

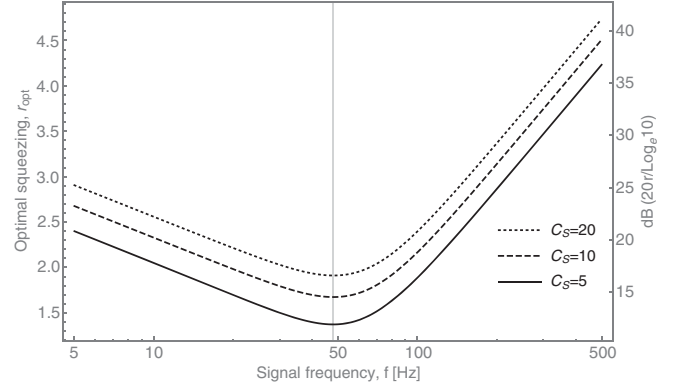


FIG. 3. Optimal squeezing as a function of the Fourier frequency for different values of the spin cooperativity C_S . The bare spin resonance $\Omega_S/(2\pi)$ is indicated by the vertical line and coincides to a good approximation with the minimum of $r_{\text{opt}}(\Omega)$.

squeezing $r = r_{\text{min}}$ that maximizes the minimal sensitivity gain within the signal bandwidth. This will tend to flatten the gain curve and will in some sense represent a conservative assessment of the scheme in that the chosen squeezing is optimal only for a single point on the gain curve.

The degree of two-mode squeezing r , defined in Eqs. (19) and shown in Fig. 3, corresponds to the pure state generated by the optical parametric oscillator and not to what is actually observed given the losses and imperfections which are taken into account separately. Therefore, it essentially is limited only by the pumping power. More specifically, the expression for the degree of squeezing in a pure state as a function of the ratio of the pump power to the threshold pump power, P/P_{th} , is $\exp 2r = (1 + \sqrt{P/P_{\text{th}}})^2 / (1 - \sqrt{P/P_{\text{th}}})^2$ [29]. It follows that the degree of squeezing of 15 dB is achieved at half threshold power, and 20 dB can be achieved at 67% of threshold power, which is well within the experimental reach.

In Fig. 4, the normalized quantum noise spectral density is plotted for the parameters discussed above and for three realistic values of C_S . For comparison, the spectral density S_{std} of the standard interferometer, which corresponds to $r \rightarrow 0$ and $\zeta = \pi/2$, is also shown in this plot. It can be seen that a broadband sensing gain is possible relative to a standard interferometer, surpassing the SQL over a broad band, as also demonstrated in the original proposal [23].

To further illustrate the sensitivity gain relative to the standard interferometer, we introduce the gain factor

$$G = \frac{S_{\text{std}}}{S} = \frac{K_I K_S (1 + \chi_I) (\cosh 2r + \chi_S)}{|K_{\text{res}}|^2 \cosh^2 2r + |K_{IS}|^2 + K_I K_S [(\chi_I + \chi_S) \cosh 2r + \chi_I \chi_S]}. \quad (56)$$

It is plotted in Fig. 5 for the same values of the parameters as in Fig. 4. Note that, since the event rate of GWDs scales as the volume within which the GWD is sensitive, it is proportional to $G^{3/2}$.

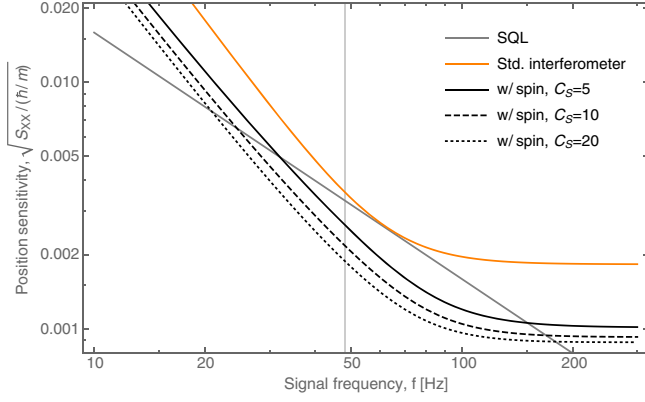


FIG. 4. Normalized position sensitivity $\sqrt{|\chi_I(\Omega)|^2 S}$ for the spin-GWD scheme benchmarked against a standard interferometer. Also shown is the SQL.

Equation (56) is quite cumbersome. However, for the reasonable values of the parameters which we use for our estimates, it can be significantly simplified, providing insight into the comparative influence of the optical losses and the spin system bandwidth on the sensitivity. Focusing on the case $\zeta = \pi/2$ and making the reasonable assumptions that $\chi_{I,S} \ll \cosh 2r$, $\gamma_S \ll \Omega_{qI}$, and $\epsilon_{iS}^2 \ll 1$, Eq. (56) can be approximated as

$$G \approx G_{\text{approx}} = \frac{1 + \chi_I}{\left(\frac{1}{\cosh 2r} + \frac{2\gamma_S \Omega \sqrt{\cosh 2r}}{K_I}\right)^2 + \chi_I + \chi_{\text{Sopt}}}, \quad (57)$$

where

$$\chi_{\text{Sopt}} = \epsilon_{iS}^2 + \frac{k_S \epsilon_{oS}^2}{K_S \eta_{iS}} \quad (58)$$

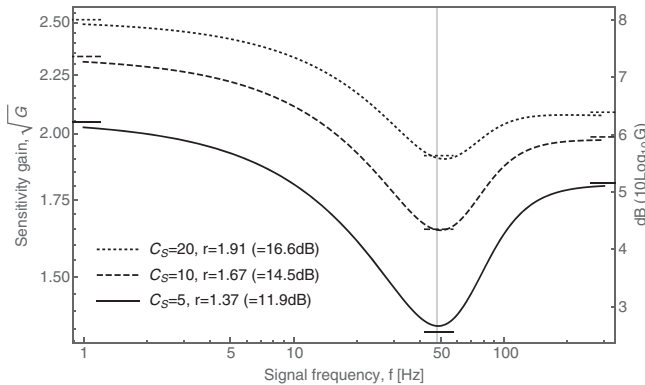


FIG. 5. Sensitivity gain relative to standard interferometer $\sqrt{G} \equiv \sqrt{S_{\text{std}}/S}$. The vertical line indicates $\Omega_S/(2\pi)$. Gain values predicted by simplified expressions for low (61) and high (62) frequencies are indicated by horizontal line segments. We also indicate the gain at $\Omega = \Omega_S$, near the minimum, according to the approximate formula Eq. (57).

is the part of χ_S imposed by the optical losses (note that it still depends on γ_S through the factor k_S , but this dependence is relatively weak).

Equation (57) succinctly expresses the impact of spin decay γ_S , optical losses χ_I and χ_{Sopt} , and finite squeezing r on the performance of our scheme. It shows that, at the price of introducing the additional optical losses χ_{Sopt} , the essential quantum noise contribution (i.e., in the absence of losses) is reduced by the factor given by the parenthesis squared in the denominator of Eq. (57). The squeeze parameter $r_{\text{opt}}(\Omega)$ that maximizes G_{approx} at a given Fourier frequency Ω is simply given by $\cosh 2r_{\text{opt}}(\Omega) = K_I/\sigma_T$ [using Eq. (40) with equality]; this is consistent with the general result (51) within the regime of validity of $G \approx G_{\text{approx}}$ insofar as $\chi_S^2 \ll 1$.

Equation (57) clearly shows also that the characteristic dip in the frequency dependence of G (see Fig. 5) is created by the spin system damping and corresponds, to a good approximation, to the maximum of the ratio Ω/K_I , which occurs at the frequency

$$\Omega_{\text{min}} = \Omega_{qI}/3^{1/4}. \quad (59)$$

It can be seen from Eq. (37) that Ω_{min} coincides with the bare spin resonance $\Omega_{\text{min}} = \Omega_S$ when $\phi = \pi/6$, the choice that minimizes γ_S . For our values of the parameters, it evaluates to $\Omega_{\text{min}} \approx 2\pi \times 48$ Hz. Estimates show that, around this frequency, the value of G is limited mostly by the spin system damping. Because of the increase of the spin system damping influence around Ω_{min} , a smaller degree of squeezing (that is, less entangled optical fields in the interferometer and the spin system channels) becomes optimal in this frequency band, creating the aforementioned dip in Fig. 3.

At the same time, for low and high signal frequencies, $K_I \gg 2\gamma_S \Omega \cosh 2r$ and

$$G \approx \frac{1 + \chi_I}{1/\cosh 2r + \chi_I + \chi_{\text{Sopt}}}; \quad (60)$$

that is, the sensitivity gain is primarily defined by the optical losses. Keeping only the lowest-order terms in $\epsilon_{iI,S}^2$ and $\epsilon_{oI,S}^2$ in the numerator and denominator of Eq. (60), we find for low (backaction-dominated) frequencies $\Omega \ll \Omega_{qI}$

$$G \approx \frac{1 + \epsilon_{iI}^2}{1/\cosh 2r + \epsilon_{iI}^2 + \epsilon_{iS}^2 + \epsilon_{oS}^2 \tan^2 \phi}, \quad (61)$$

whereas for high (imprecision-noise-dominated) frequencies $\Omega \gg \Omega_{qI}$

$$G \approx \frac{1 + \epsilon_{iI}^2 + \epsilon_{oI}^2}{1/\cosh 2r + \epsilon_{iI}^2 + \epsilon_{oI}^2 + \epsilon_{iS}^2 + \epsilon_{oS}^2}. \quad (62)$$

The approximate Eqs. (61) and (62) are compared to the exact sensitivity gain in Fig. 5.

V. CONCLUSION AND OUTLOOK

We have discussed a scheme that promises to push gravitational wave detectors into a new realm of broadband sub-SQL sensitivity by means of a flexible and unintrusive extension of existing interferometer topologies by a negative effective mass spin oscillator. The physical resources required by this approach are relatively low cost compared to other candidate techniques for quantum noise evasion proposed for future GWDs.

We have shown that the addition of the virtual rigidity technique to the scheme first proposed in Ref. [23] allows one to achieve a tangible sensitivity gain even for modest values of the atomic cooperativity, $\mathcal{C}_S \sim 10$, which dramatically facilitates practical implementation of this scheme.

The value of the resulting sensitivity crucially depends on two factors: optical losses in the scheme and the dissipation rate in the atomic spin system. For the reasonably optimistic values of these parameters used

for our estimates, the sensitivity gain (in comparison with an “ordinary” interferometer) could reach 6–7 dB.

While our modeling and assessment of the scheme is reasonably detailed, it is beyond the scope of the present work to exhaustively account for all realistic imperfections of gravitational wave interferometers. A first step towards the practical implementation of the scheme would be a proof-of-principle demonstration of the spin subsystem subject to a two-mode-squeezed input field. The modular nature of the setup allows such separate characterization and optimization of the spin subsystem. Given a spin system fine-tuned in this manner, work towards integration with an actual GWD could commence.

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