Thermal neutron capture cross section for 56 Fe (n, γ)

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The ⁵⁶Fe(n, γ) thermal neutron capture cross section and the ⁵⁷Fe level scheme populated by this reaction have been investigated in this work. Singles γ -ray spectra were measured with an isotopically enriched ⁵⁶Fe target using the guided cold neutron beam at the Budapest Reactor, and $\gamma\gamma$ -coincidence data were measured with a natural Fe target at the LWR-15 research reactor in Řež, Czech Republic. A detailed level scheme consisting of 448 γ rays populating/depopulating 97 levels and the capture state in ⁵⁷Fe has been constructed, and \approx 99% of the total transition intensity has been placed. The transition probability of the 352-keV γ ray was determined to be $P_{\gamma}(352) = 11.90 \pm 0.07$ per 100 neutron captures. The ⁵⁷Fe level scheme is substantially revised from earlier work and \approx 33 previously assigned levels could not be confirmed while a comparable number of new levels were added. The ⁵⁷Fe γ -ray cross sections were internally calibrated with respect to ¹H and ³²S γ -ray cross section standards using iron(III) acetylacetonate (C₁₅H₂₁FeO₆) and iron pyrite (FeS₂) targets. The thermal neutron cross section for production of the 352-keV γ -ray cross section was determined to be $\sigma_{\gamma}(352) = 0.2849 \pm 0.015$ b. The total ⁵⁶Fe(n, γ) thermal radiative neutron cross section is derived from the 352-keV γ -ray cross section and transition probability as $\sigma_0 = 2.394 \pm 0.019$ b. A least-squares fit of the γ rays to the level scheme gives the ⁵⁷Fe neutron separation energy $S_n = 7646.183 \pm 0.018$ keV.

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I. INTRODUCTION

Precise thermal neutron capture γ -ray spectra were measured for all elements with Z = 1-83, 90, and 92, except for He and Pm, using neutron beams at the Budapest Reactor [1,2]. The γ -ray energies and cross sections were determined and combined, together with additional information from the literature, to generate the Evaluated Gamma-ray Activation File (EGAF) [3] and they were also published in the Handbook of Prompt Gamma Activation Analysis with Neutron Beams [4]. These data can be used to determine total radiative thermal neutron capture cross sections, σ_0 . When the level scheme is complete, σ_0 equals both the sum of transition cross sections, γ -ray plus conversion electron, feeding the ground state (GS), $\Sigma \sigma_{\nu+e}$ (GS), and the sum of transition cross sections deexciting the capture state (CS), $\Sigma \sigma_{\nu+e}$ (CS). Thermal neutron capture decay schemes are typically completely determined for low-Z elements where all of the transitions are observed.

Iron is an important structural and shielding material in nuclear reactors and other nuclear installations that has an important impact on thermal neutron flux distribution in a reactor pressure vessel [5]. Despite its importance, the ⁵⁶Fe(n, γ) total radiative thermal neutron cross section, σ_0 , is only known to an accuracy of $\approx 5\%$ based on only two early measurements from over 40 years ago. In this work the ⁵⁶Fe(n, γ) reaction has been studied with a thermal equivalent neutron beam impinging on an enriched ⁵⁶Fe target. The corresponding ⁵⁷Fe γ -ray decay scheme has been nearly completely determined with only minor corrections necessary to account for the weak, missing, or unplaced γ -ray intensity. The new γ -ray data have been internally calibrated with thermal cross section γ -ray standards to determine a new value of the total radiative thermal neutron cross section accurate to $\approx 0.8\%$.

The ⁵⁶Fe(n, γ) reaction was previously studied by Vennink et al. [6], who placed 191 γ rays that populated/depopulated 62 levels in ⁵⁷Fe. Levels and γ rays were assigned by Vennink et al. on the basis of γ -ray energy sums but without the aid of $\gamma\gamma$ coincidence data. That procedure can be unreliable due to a high probability of chance energy sums matching known level energies resulting from the complexity of the (n,γ) spectrum. In this work we have also exploited $\gamma\gamma$ coincidence spectra, originally measured for studying two-step γ cascades [7] using a natural Fe target, to confirm the placement of more than 70% of the transitions observed in γ -ray singles measurements, add new transitions, and divide the intensities of γ rays that could be multiply placed in the decay scheme.

II. EXPERIMENT

The singles ${}^{56}\text{Fe}(n,\gamma)$ neutron capture γ -ray spectrum was measured in the guided cold neutron beam at the 10-MW Budapest Reactor [1]. Neutrons entered the evacuated target holder and continued to the beam stop at the rear wall of the guide hall. The target station, where both primary and secondary γ rays can be measured in low background conditions, is located 30 m from the reactor. The thermalequivalent neutron flux at the target was $1.2 \times 10^8 \text{ cm}^{-2} \text{ s}^{-1}$ during this experiment.

Prompt γ rays from the target were measured with an *n*-type high-purity, 27% efficient, germanium (HPGe) detector with closed-end coaxial geometry located 23.5 cm from the target. The detector is Compton-suppressed by a bismuth germanate

TABLE I. 50 Fe (n, γ) the	hermal neutron capture γ ray e	nergies and relative int	tensities measured in t	his work for γ energies	s from 14 to 352 keV
with detailed transition ch	aracteristics.				

$\overline{\frac{E_{\gamma}}{(\text{keV})}}$	$I_{\gamma}{}^{\mathrm{a}}$	Multipolarity [12]	Mixing ratio δ [12]	ICC [13]	Placement (initial \rightarrow final)
14.4130(3) ^{b,c}	55.0(4)	M1 + E2	0.00223(1)	8.54(2)	$14 \rightarrow 0$
$92(1)^{d}$	0.08(3)	[<i>M</i> 1]		0.044(2)	$7646 \rightarrow 7554$
105.5(3)	0.051(17)	[]			unplaced
$119.86(11)^{e}$	0.172(25)	<i>M</i> 1		0.0218(3)	$3547 \rightarrow 3428$
122.026(14) ^c	35.4(6)	M1 + E2	0.120(1)	0.0238(4)	$136 \rightarrow 14$
134.00(24)	0.046(12)				unplaced
136.441(16) ^c	4.51(8)	E2		0.149(2)	$136 \rightarrow 0$
186.7(4) ^e	0.020(10)	[<i>M</i> 1]		0.007(1)	$5495 \rightarrow 5308$
200.60(21)	0.068(13)				unplaced
204.52(24)	0.064(13)				unplaced
230.298(13) ^c	9.70(14)	[<i>M</i> 1]		0.0042(1)	$367 \rightarrow 136$
318.96(6) ^e	0.131(11)	[<i>M</i> 1]		0.00190(3)	$3240 \rightarrow 2921$
$325(1)^{d}$	0.5(2)	[<i>M</i> 1]		0.00181(3)	$7646 \rightarrow 7321$
333(1) ^c	0.22(8)	[<i>M</i> 1]		0.00171(3)	$7646 \rightarrow 7313$
339.618(14) ^f	1.61(3)	[<i>M</i> 1]		0.00164(2)	$706 \rightarrow 367$
350(1) ^g	0.29(10)	[<i>M</i> 1]		0.00152(2)	$1357 \rightarrow 1007$
352.347(13)°	100.0(14)	M1 + E2	0.025(9)	0.0029(15)	$367 \rightarrow 14$

^aRelative intensity. For multiply placed transitions the singles γ -ray intensity has been divided on the basis of intensity balance and coincidence data. Multiply by 0.1190(7) for transition probability per 100 neutron captures, $P_{\gamma}(\%)$.

^bNot observed. Intensity calculated from intensity balance feeding the 14.4-keV level and corrected for unobserved continuum feeding (see text).

^cTransition confirmed by coincidence data.

^dExpected primary γ -ray transition, see text.

^eTransition placed by energy sums.

^fTransition adopted from ENSDF [12].

^gTransition proposed from intensity balance but likely obscured by strong 352-keV γ -ray.

(BGO) scintillator guard detector annulus surrounded by 10-cm-thick lead shielding. Relative detection efficiency was calibrated from 50 keV to 10 MeV with radioactive sources and (n, γ) reaction γ rays to a precision of better than 1% from 500 keV to 6 MeV and better than 2% at 100–500 keV and >6 MeV [8]. The γ -ray spectra were analyzed using the HYPERMET PC program [8,9].

An FeO target enriched to 99.94% in ⁵⁶Fe, suspended in a Teflon bag to minimize background from the target holder, was irradiated to obtain a high statistics, impurity free ⁵⁷Fe spectrum. No target impurity γ rays were observed in the prompt γ -ray spectrum, verifying that nearly all of the observed γ rays could be assigned to ⁵⁷Fe. Elemental radiative thermal neutron γ -ray cross sections were normalized, with respect to hydrogen and sulfur standard γ rays, using stoichiometric high purity iron(III) acetylacetonate (C₁₅H₂₁FeO₆) and iron pyrite (FeS₂) targets where the isotopic cross sections were determined from the ⁵⁶Fe natural abundance [10].

Coincidence data were measured at the LWR-15 research reactor in Řež with two HPGe detectors, with efficiencies of 20% and 25% respectively, placed above and below the horizontally situated target with their axes parallel to each other. Sum coincidence gates were set on γ rays deexciting the capture state and populating levels at 0, 14, 136, 367, 706, 1265, 1627, 1725, 2118, and 2207 keV in ⁵⁷Fe via two-step cascades. The two-step coincidence method is described in detail by Honzátko *et al.* [11].

III. ⁵⁷Fe DECAY SCHEME

A total of 472 γ -ray transitions, including numerous unresolved multiplets, were assigned to the 56 Fe (n, γ) reaction and 448 γ -rays were placed in the ⁵⁷Fe level scheme; they are summarized in Tables I and II. The low energy 14.4-keV transition connecting the first excited and ground states was not observed in this work, and its intensity has been inferred from the total intensity feeding the 14.4-keV level. Most transition placements were confirmed by the sum coincidence data. Other γ rays were previously placed on the basis of previous work in the Evaluated Nuclear Structure Data File (ENSDF) evaluation [12]. Some γ rays were placed on the basis of energy sums and intensity balance considerations. The intensities of the unresolved multiplets were divided on the basis of coincidence data and the decay scheme intensity balance. The 92-, 325-, and 333-keV primary γ rays were too weak to be observed but are assumed to exist because they feed levels that are too high in excitation energy to be significantly populated by other weakly fed, higher-lying states. The γ -rays at 7313 and 7554 keV are arbitrarily assumed to populate the GS. They are too weak to be observed in the coincidence data. The level at 7321 keV was placed on the basis that the 7306.5-keV transition is very weakly observed in sum coincidence with the 14-keV level, and a 1346.58-keV γ ray can be placed deexciting this level to the 5975-keV level on the basis of energy sums. Expected E1 primary γ rays populating the 2554.12-, 2574.07-, and

TABLE II. ⁵⁶Fe(n, γ) thermal neutron capture γ ray energies and relative intensities measured in this work for γ energies of 366 keV and higher.

TABLE II. (Continued.)

and higher.			E_{γ} (keV)	$I_{\gamma}{}^{\mathrm{a}}$	Placement (initial \rightarrow final)	
E_{γ} (keV)	I_{γ}^{a}	Placement (initial \rightarrow final)	1062.05(24) ^d	0.056(13)	$1198 \rightarrow 136$	
(KCV)		(IIIIdal > IIIda)	1069.98(13) ^c	0.089(13)	$2697 \rightarrow 1627$	
366.752(13) ^b	18.03(25)	$367 \rightarrow 0$	1094.53(6) ^c	0.328(18)	$3792 \rightarrow 2697$	
460.42(7) ^b	0.685(23)	$1725 \rightarrow 1265$	$1099.6(5)^{c}$	0.230(18)	$6408 \rightarrow 5308$	
487.9(4)	0.013(9)	unplaced	1102.24(23) ^c	0.092(15)	$5084 \rightarrow 3982$	
490.92(11) ^b	0.061(14)	$2118 \rightarrow 1627$	1110.95(3) ^b	7.7(3)	$2836 \rightarrow 1725$	
525.91(10) ^b	0.063(12)	$7646 \rightarrow 7120$	1130.49(6) ^b	0.216(16)	$7646 \rightarrow 6516$	
566.4(3) ^c	0.024(8)	$4548 \rightarrow 3982$	1162.36(22)°	0.061(11)	$4460 \rightarrow 3298$	
569.966(15) ^d	4.78(7)	$706 \rightarrow 136$	1164.4(5) ^b	0.171(15)	$3371 \rightarrow 2207$	
628.59(9) ^b	0.112(11)	$2836 \rightarrow 2207$	1165(1) ^b	0.06(3)	$7646 \rightarrow 6481$	
635.33(8) ^c	0.104(11)	$6676 \rightarrow 6040$	1193.6(3) ^c	0.068(20)	$5886 \rightarrow 4692$	
640.50(18) ^d	0.051(11)	$1007 \rightarrow 367$	1196.87(4) ^c	2.15(4)	$2554 \rightarrow 1357$	
650.70(3) ^d	1.71(3)	$1357 \rightarrow 706$	1200.04(4) ^a	0.789(24)	$2207 \rightarrow 1007$	
665.66(7) ^c	0.184(18)	$3240 \rightarrow 2574$	1208.70(12)	0.169(16)	$2836 \rightarrow 1627$	
689.8(5) ^c	0.16(4)	$5238 \rightarrow 4548$	1217.61(5) ^c	0.557(21)	$3792 \rightarrow 2574$	
692.005(14) ^b	50.9(7)	$706 \rightarrow 14$	1221.54(15) ^b	0.141(16)	$3428 \rightarrow 2207$	
706.42(4) ^b	2.14(4)	$706 \rightarrow 0$	1237.55(6) ^b	0.87(6)	$7646 \rightarrow 6408$	
717.9(4) ^b	0.070(17)	$2836 \rightarrow 2118$	1238.73(15) ^c	0.31(6)	$4209 \rightarrow 2971$	
731.07(10) ^c	0.179(16)	$6160 \rightarrow 5429$	1250.68(3) ^b	1.14(3)	$1265 \rightarrow 14$	
734.90(8) ^d	0.617(23)	$3240 \rightarrow 2505$	1253.9(3) ^c	0.067(16)	$6746 \rightarrow 5492$	
746.49(12)	0.082(21)	unplaced	1256.83(20) ^c	0.104(17)	$5238 \rightarrow 3982$	
761.10(4) ^c	0.273(19)	$2118 \rightarrow 1357$	1260.535(21)	25.2(3)	$1627 \rightarrow 367$	
779.68(14) ^b	0.063(9)	$2505 \rightarrow 1725$	1264.96(5)	0.403(18)	$1265 \rightarrow 0$	
809(1) ^b	0.44(15)	$7646 \rightarrow 6837$	1268.38(19) ^c	0.090(18)	$6314 \rightarrow 5046$	
821.04(6) ^c	0.171(15)	$3792 \rightarrow 2971$	1277.15(11) ^c	0.125(15)	$4460 \rightarrow 3183$	
834.9(5) ^c	0.014(13)	$5084 \rightarrow 4249$	1281.31(4) ⁶	0.851(23)	$7646 \rightarrow 6365$	
849.7(4) ^c	0.050(14)	$3547 \rightarrow 2697$	1284.0(5) ^d	0.5(2)	$3982 \rightarrow 2697$	
853.0(6) ^c	0.024(13)	$3428 \rightarrow 2574$	1288.61(20) ^c	0.065(13)	$4209 \rightarrow 2921$	
855.89(17) ^b	0.095(15)	$7646 \rightarrow 6790$	1293.32(4)	0.299(25)	$2921 \rightarrow 1627$	
867.82(22) ^b	0.086(19)	$7646 \rightarrow 6778$	1000 0 c (17)h	1.09(3)	$7646 \rightarrow 6353$	
870.68(8) ^d	1.21(4)	$1007 \rightarrow 136$	1300.06(17) ^b	0.110(14)	$7646 \rightarrow 6346$	
873.2(4) ^c	0.047(15)	$3428 \rightarrow 2554$	1309.77(17)	0.078(14)	$3428 \rightarrow 2118$	
877.0(3) ^c	0.083(15)	$4249 \rightarrow 3371$	1324.96(24)	0.078(15)	$6408 \rightarrow 5084$	
894.1(4)	0.060(15)	unplaced	1328.0(3) ^c	0.048(14)	$4249 \rightarrow 2921$	
898.251(15) ^b	19.4(3)	$1265 \rightarrow 367$	1332.34(8) ⁶	0.317(17)	$7646 \rightarrow 6314$	
900.68(6) ^b	0.324(20)	$7646 \rightarrow 6746$	$1342.78(7)^{a}$	0.682(22)	$135 / \rightarrow 14$	
911.67(20)°	0.055(13)	$4209 \rightarrow 3298$	1346.58(10) ^c	0.206(17)	$/321 \rightarrow 59/5$	
920.843(15) ^b	7.71(11)	$1627 \rightarrow 706$	1358.679(22)	7.91(12)	$1/25 \rightarrow 36/$	
922(1) ^b	0.12(6)	$7646 \rightarrow 6724$	1301.0(3)	0.079(20)	$7646 \rightarrow 6285$	
950.2(3) ^c	0.035(13)	$4249 \rightarrow 3298$	1364.69(6)	0.344(19)	$4548 \rightarrow 3183$	
955.79(11) ^c	0.115(17)	$3792 \rightarrow 2836$	$13/3.3(3)^{2}$	0.050(17)	$4209 \rightarrow 2830$	
970.48(12)	0.144(19)	$7646 \rightarrow 6676$	$1360.40(16)^{2}$ $1407.72(5)^{2}$	0.110(19) 0.245(14)	$3029 \rightarrow 4249$	
987.52(20)	0.063(16)	unplaced	$1407.72(5)^{2}$	0.343(14)	$43/9 \rightarrow 29/1$	
990.42(11) ^d	0.574(22)	$1357 \rightarrow 367$	1411.03(4) 1420.74(11)	2.02(5)	$2116 \rightarrow 700$	
992.85(10) ⁶	0.671(25)	$100/ \rightarrow 14$	1430.74(11) 1/33.0(5)	0.407(19) 0.103(15)	$7040 \rightarrow 0213$ 5804 $\rightarrow 4460$	
994.7(3) ⁶	0.19(3)	$7646 \rightarrow 6652$	1455.9(5)	0.103(13) 0.002(15)	$3094 \rightarrow 4400$	
998.0(6) ^c	0.019(13)	$5689 \rightarrow 4692$	1450.75(19) $1457.70(12)^{b}$	0.092(13) 0.242(24)	2182 1725	
1007.09(10)	0.117(12)	$43/9 \rightarrow 33/1$	1437.79(12) $1/63.1/(10)^{\circ}$	0.343(24)	$5103 \rightarrow 1/23$	
1014.11(19)	0.099(13)	unplaced	1486 75(11) ^b	0.007(17) 0.50(3)	$5724 \rightarrow 4400$ $76/6 \rightarrow 6160$	
1010.2(3)	0.12(3)	unplaced	1490.75(11)	1.39(3)	$1627 \rightarrow 126$	
1018.983(19) ⁶	18.28(25)	$1/25 \rightarrow /06$	1511 A0(2)	0.07(3)	$1027 \rightarrow 130$	
1021.93(18)	0.077(12)	$7040 \rightarrow 6024$	1511.79(2) 1513.0(5) ^b	0.07(3)	3240 _ \ 1725	
1028.5(3)	0.43(13)	$00/5 \rightarrow 5046$	1579 15(11) ^c	0.37(3) 0.167(16)	$52+0 \rightarrow 1723$	
1030.73(20)	0.084(14)	unplaced	1527.15(11)	0.167(16)	$7646 \rightarrow 6117$	
$1052.00(21)^{\circ}$ 1056.0(2)°	0.075(14) 0.027(12)	$5240 \rightarrow 2207$		0.107(10)	/070 / 011/	
1000.7001	0.027(13)	$0000 \rightarrow 0000$				

TABLE II. (Continued.)

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$\overline{E_{\gamma}}$	I_{γ}^{a}	Placement	$\overline{E_{\gamma}}$	I_{γ}^{a}	Placement
(keV)	·	$(initial \rightarrow final)$	(keV)		$(initial \rightarrow final)$
1542.18(19) ^b	0.088(16)	$3660 \rightarrow 2118$	1956.81(14) ^b	0.54(3)	$7646 \rightarrow 5689$
1549.36(19) ^c	0.100(16)	$5689 \rightarrow 4140$	1974.88(3) ^b	0.97(3)	$3240 \rightarrow 1265$
1555.70(8) ^b	0.185(17)	$3183 \rightarrow 1627$	1981.78(13) ^c	0.137(15)	$2118 \rightarrow 136$
1571.02(4) ^b	0.513(23)	$7646 \rightarrow 6075$	1991(1) ^b	0.16(6)	$2697 \rightarrow 706$
	0.13(3)	$2836 \rightarrow 1265$	2002.21(5) ^b	2.00(4)	$4209 \rightarrow 2207$
1574.34(21)	0.103(16)	unplaced	2016.94(6) ^b	0.568(22)	$7646 \rightarrow 5629$
1582.82(22) ^c	0.104(23)	$6408 \rightarrow 4826$	2066.29(4) ^b	4.65(8)	$3792 \rightarrow 1725$
1584.60(3) ^b	0.21(3)	$3792 \rightarrow 2207$	2070.77(6) ^c	0.69(3)	$2207 \rightarrow 136$
	0.85(3)	$7646 \rightarrow 6061$	2075.64(12) ^c	0.171(24)	$4773 \rightarrow 2697$
1589.05(3) ^b	0.668(19)	$1725 \rightarrow 136$	2091.18(5) ^b	2.05(4)	$4209 \rightarrow 2118$
1599.09(16) ^c	0.105(14)	$6837 \rightarrow 5238$	2103.83(6) ^d	0.79(3)	$2118 \rightarrow 14$
1605.8(3) ^c	0.102(14)	$7646 \rightarrow 6040$	2106.06(19) ^b	0.182(20)	$3371 \rightarrow 1265$
1608.81(17) ^b	0.136(17)	$7646 \rightarrow 6037$	2124.4(3) ^b	0.086(18)	$7646 \rightarrow 5522$
	0.042(17)	$5429 \rightarrow 3820$	2129.464(23) ^b	7.42(11)	$2836 \rightarrow 706$
1612.918(18) ^b	54.21(13)	$1627 \rightarrow 14$	2138.19(3) ^b	2.40(5)	$2505 \rightarrow 367$
	0.41(9)	$2971 \rightarrow 1357$	2151.61(3) ^b	2.06(4)	$7646 \rightarrow 5495$
	1.25(13)	$3240 \rightarrow 1627$	2154.59(10) ^b	0.353(22)	$7646 \rightarrow 5492$
1616.82(16) ^b	0.114(16)	$7646 \rightarrow 6029$	2157.81(14)°	0.175(19)	$7646 \rightarrow 5488$
1624.28(21) ^c	0.111(20)	$4460 \rightarrow 2836$	2165(1) ^b	0.030(15)	$7646 \rightarrow 5482$
1627.34(4) ^b	3.33(6)	$1627 \rightarrow 0$	2171.10(6) ^b	0.383(21)	$4379 \rightarrow 2207$
1633.4(3) ^b	0.104(25)	$7646 \rightarrow 6013$	2187.17(7) ^c	0.622(20)	$4692 \rightarrow 2505$
1635.26(5) ^c	0.98(3)	$4209 \rightarrow 2574$	$2192.78(7)^{d}$	1.73(3)	$2207 \rightarrow 14$
1646.2(5) ^b	0.384(17)	$3371 \rightarrow 1725$	2197.7(4) ^c	0.036(15)	$6746 \rightarrow 4548$
$1655.44(4)^{d}$	0.402(16)	$2921 \rightarrow 1265$	2207.36(10) ^b	0.48(3)	$2207 \rightarrow 0$
. ,	1.06(3)	$4209 \rightarrow 2554$		0.30(3)	$2574 \rightarrow 367$
1662.6(3) ^c	0.047(14)	$4845 \rightarrow 3183$	2209.90(16) ^c	0.03(3)	$5046 \rightarrow 2836$
1671.49(6) ^b	0.361(16)	$7646 \rightarrow 5975$	2217.26(11) ^b	0.278(22)	$7646 \rightarrow 5429$
1681.96(15) ^d	0.104(14)	$4379 \rightarrow 2697$	2254.60(17)°	0.174(22)	$5495 \rightarrow 3240$
1692.89(9)	0.148(17)	unplaced	2260.18(8) ^b	0.415(25)	$4379 \rightarrow 2118$
1702.35(7) ^b	0.390(18)	$3428 \rightarrow 1725$	2264.28(5) ^b	0.67(3)	$2971 \rightarrow 706$
$1704.8(5)^{d}$	0.197(17)	$4209 \rightarrow 2505$	2308.4(5)°	0.079(23)	$5492 \rightarrow 3183$
1711.09(3) ^b	1.16(3)	$1725 \rightarrow 14$	2330.23(4) ^b	0.72(3)	$2697 \rightarrow 367$
1721.1(3) ^c	0.27(10)	$4692 \rightarrow 2971$	2338.04(6) ^b	0.315(20)	$7646 \rightarrow 5308$
1722.65(4) ^b	3.89(9)	$7646 \rightarrow 5924$	2354.6(3) ^b	0.055(18)	$3982 \rightarrow 1627$
1725.459(18) ^b	64.1(9)	$1725 \rightarrow 0$	2361.77(20)	0.139(18)	unplaced
1736.68(23)	0.095(16)	unplaced	2368.42(4) ^b	0.726(25)	$2505 \rightarrow 136$
1743.85(6) ^b	0.368(18)	$3371 \rightarrow 1627$	2385.824(25) ^b	1.32(3)	$7646 \rightarrow 5260$
1752.64(8) ^b	0.228(16)	$7646 \rightarrow 5894$	2403.8(6) ^c	0.087(23)	$6652 \rightarrow 4249$
1760.06(3) ^b	0.885(23)	$7646 \rightarrow 5886$	2407.79(5) ^b	1.33(4)	$7646 \rightarrow 5238$
1798.85(12) ^b	0.164(16)	$2505 \rightarrow 706$	2414.58(17) ^b	0.190(25)	$4140 \rightarrow 1725$
1824.26(14) ^c	0.154(16)	$4379 \rightarrow 2554$	2419.2(5)	0.035(22)	$5790 \rightarrow 3371$
$1840.62(5)^{d}$	0.592(22)	$2207 \rightarrow 367$	2424.16(5) ^c	1.01(3)	$5260 \rightarrow 2836$
1847.70(14) ^c	0.147(16)	$2554 \rightarrow 706$		0.51(3)	$7646 \rightarrow 5222$
1851.78(4) ^c	0.580(21)	$4773 \rightarrow 2921$	2433.72(14) ^b	0.26(3)	$4159 \rightarrow 1725$
1856.04(4) ^b	0.671(23)	$7646 \rightarrow 5790$	2437.53(13)°	0.25(3)	$2574 \rightarrow 136$
1863.18(21) ^c	0.088(16)	$3982 \rightarrow 2118$	2450.3(9) ^c	0.054(25)	$5689 \rightarrow 3240$
1867.76(25) ^c	0.069(15)	$2574 \rightarrow 706$	2457.55(19) ^b	0.15(3)	$4575 \rightarrow 2118$
1874.28(23) ^c	0.065(14)	$4845 \rightarrow 2971$	2462.53(11) ^c	0.304(25)	$3820 \rightarrow 1357$
1886.15(6) ^c	0.318(20)	$4460 \rightarrow 2574$	2469.10(4) ^b	3.55(7)	$2836 \rightarrow 367$
1894.2(3)	0.056(19)	unplaced	2472.3(3) ^c	0.11(3)	$5308 \rightarrow 2836$
1900.4(3) ^c	0.058(18)	$6746 \rightarrow 4845$	2477.7(10) ^b	0.14(3)	$3183 \rightarrow 706$
1906.05(5) ^c	0.434(23)	$4460 \rightarrow 2554$	2481(1) ^b	0.16(8)	$7646 \rightarrow 5164$
1932.92(16) ^b	0.125(20)	$7646 \rightarrow 5713$	2484.65(7) ^b	0.28(3)	$4209 \rightarrow 1725$
1944.02(21) ^c	0.118(18)	$5492 \rightarrow 3547$. /	0.28(3)	$4692 \rightarrow 2207$
1951.83(20) ^b	0.122(17)	$4159 \rightarrow 2207$	2508.22(13) ^c	0.222(20)	$5429 \rightarrow 2921$

THERMAL NEUTRON CAPTURE CROSS SECTION FOR

TABLE II. (Continued.)

TABLE II. (Continued.)

 F	I a	Dlacement		I a	Placement
L_{γ} (keV)	I_{γ}	(initial \rightarrow final)	L_{γ} (keV)	I_{γ}	(initial \rightarrow final)
2526.678(18) ^b	4.22(7)	$3792 \rightarrow 1265$	3146.3(4)	0.047(22)	unplaced
2532(1) ^b	0.25(12)	$4159 \rightarrow 1627$	3164.02(14)	0.29(3)	unplaced
2540.02(19)°	0.121(19)	$3547 \rightarrow 1007$	3168.58(5) ^b	4.09(8)	$3183 \rightarrow 14$
2553.56(16) ^b	0.140(20)	$2554 \rightarrow 0$	3172(1) ^b	0.22(11)	$7646 \rightarrow 4474$
2562.53(11) ^b	0.41(4)	$7646 \rightarrow 5084$	$3182.7(3)^{\circ}$	0.29(9)	$3183 \rightarrow 0$
2002100(11)	0.16(4)	$2697 \rightarrow 136$	3185.95(4) ^b	7.25(14)	$7646 \rightarrow 4460$
2573 980(25) ^d	1.70(4)	$2574 \rightarrow 0$	$3225 41(6)^{b}$	3 60(7)	$3240 \rightarrow 14$
2575.960(25) 2582.06(4) ^b	0.85(3)	$4209 \rightarrow 1627$	3225.11(0) $3234.4(3)^{b}$	0.184(25)	$3210 \rightarrow 110$ $3371 \rightarrow 136$
2502.00(4) 2600.00(14) ^b	0.03(3)	$7646 \rightarrow 5046$	3239.82(4) ^b	3.25(7)	$3240 \rightarrow 0$
2603.88(4) ^b	0.105(20) 0.78(3)	$\begin{array}{c} 7040 \\ 2971 \\ \rightarrow 367 \end{array}$	$3257.02(4)^{b}$	1333(22)	$7646 \rightarrow 4379$
2603.00(1) 2653 10(7) ^b	0.73(5)	$4379 \rightarrow 1725$	3207.13(1) 3275.4(5)	0.06(3)	unplaced
2655.10(7) 2655.5(4) ^b	0.05(5)	$4773 \rightarrow 2118$	3273.4(3) 3283 71(11) ^b	0.00(3)	$3208 \rightarrow 14$
$2658.7(3)^{\circ}$	0.10(4)	$4773 \rightarrow 2113$ $5620 \rightarrow 2071$	3203.71(11) $3201.26(4)^{b}$	3.28(7)	$3290 \rightarrow 14$
2038.7(3) 2664 30(23) ^b	0.093(23) 0.12(3)	$3371 \rightarrow 706$	3291.20(4) 3208 16(11) ^b	5.26(7)	$3428 \rightarrow 130$
2004.30(23)	0.12(3)	$3371 \rightarrow 700$	3296.10(11) 3256.65(2)b	0.43(3)	$3290 \rightarrow 0$
2082.399(18)	4.30(7)	$2097 \rightarrow 14$	3330.03(3)	5.40(0)	$33/1 \rightarrow 14$
0(0(00/10))	0.25(8)	$7040 \rightarrow 4904$	33/1.21(7)*	0.25(3)	$33/1 \rightarrow 0$
2686.20(10)°	0.268(19)	$5260 \rightarrow 2574$	2207 70(25)h	0.35(3)	$43/9 \rightarrow 100/$
$2692.44(6)^{\circ}$	0.458(20)	$0353 \rightarrow 3000$	$3397.78(25)^{\circ}$	0.154(23)	$7646 \rightarrow 4249$
$2697.02(3)^{6}$	3.11(6)	$269/ \rightarrow 0$	3411(1) ⁶	0.053(12)	$354/ \rightarrow 136$
2699.50(10) ⁶	0.55(4)	$2836 \rightarrow 136$	3413.321(25)	16.9(3)	$3428 \rightarrow 14$
2/15./(3) ^b	0.19(3)	$4923 \rightarrow 2207$	3425(1)	0.19(9)	$3/92 \rightarrow 36/$
2/21.365(22)	14.8(6)	$3428 \rightarrow 706$	3427.58(21)	0.23(3)	$3428 \rightarrow 0$
2724(1) ^b	0.34(11)	$7646 \rightarrow 4923$	3436.77(3) ⁶	17.4(3)	$7646 \rightarrow 4209$
2734.72(4) ^b	1.59(7)	$4460 \rightarrow 1725$	3444.32(20)°	0.21(3)	$6365 \rightarrow 2921$
2751.05(4) ^b	1.43(6)	$4379 \rightarrow 1627$	3452.84(8) ^b	0.60(3)	$3820 \rightarrow 367$
2766.44(19) ^c	0.18(3)	$6314 \rightarrow 3547$	3486.92(5) ^b	4.24(9)	$7646 \rightarrow 4159$
2800.62(6) ^b	0.81(4)	$7646 \rightarrow 4845$	3502.70(5) ^b	1.95(5)	$4209 \rightarrow 706$
2813.77(7) ^b	1.06(5)	$7646 \rightarrow 4832$	3507.45(5) ^b	1.74(6)	$4773 \rightarrow 1265$
2816.1(5) ^b	0.12(5)	$3183 \rightarrow 367$		0.25(6)	$7646 \rightarrow 4140$
2821.88(6) ^b	0.82(3)	$7646 \rightarrow 4826$	3513.0(3) ^b	0.13(3)	$5238 \rightarrow 1725$
2833.01(5) ^b	2.38(12)	$4460 \rightarrow 1627$	3523.7(4) ^c	0.10(3)	$3660 \rightarrow 136$
2834.2(5) ^b	1.34(16)	$2971 \rightarrow 136$	3533.2(3) ^b	0.11(3)	$3547 \rightarrow 14$
2835.9(5) ^b	5.42(10)	$2836 \rightarrow 0$	3581.4(3) ^b	0.18(4)	$3948 \rightarrow 367$
2840.9(3) ^b	0.13(3)	$3547 \rightarrow 706$	3612.0(5) ^c	0.11(3)	$6117 \rightarrow 2505$
2849.9(3) ^b	0.14(3)	$4575 \rightarrow 1725$	3615.03(13) ^b	0.40(3)	$3982 \rightarrow 367$
2873.49(4) ^b	3.79(7)	$7646 \rightarrow 4773$	3633.11(11) ^b	0.39(3)	$5260 \rightarrow 1627$
2894.12(11) ^b	0.296(22)	$4159 \rightarrow 1265$	3645.8(7)°	0.072(24)	$3660 \rightarrow 14$
2905.96(18) ^b	0.217(23)	$2921 \rightarrow 14$	3654.2(3) ^c	0.043(24)	$6160 \rightarrow 2505$
2920.93(12) ^b	0.30(3)	$2921 \rightarrow 0$	3664.38(5) ^b	1.32(4)	$7646 \rightarrow 3982$
2944.48(8) ^b	0.78(3)	$4209 \rightarrow 1265$	3671.9(3) ^b	0.137(25)	$4379 \rightarrow 706$
2953.97(7) ^b	0.19(9)	$3660 \rightarrow 706$	3684.0(5) ^b	0.049(25)	$3820 \rightarrow 136$
	3.12(12)	$7646 \rightarrow 4692$	3697.57(17) ^b	0.28(3)	$7646 \rightarrow 3948$
2956 18(14) ^b	0.74(9)	$2971 \rightarrow 14$	3710 9(3)°	0.35(4)	$6408 \rightarrow 2697$
2966 83(21) ^b	0.37(4)	$4692 \rightarrow 1725$	3753 57(19) ^b	0.214(25)	$4460 \rightarrow 706$
2900.09(21) 2970.29(7) ^b	1.54(7)	$2971 \rightarrow 0$	3766 5(6)°	0.18(3)	$5492 \rightarrow 1725$
2970.29(7) 3003 7(4) ^b	1.34(7)	$\begin{array}{c} 2971 \rightarrow 0\\ 3371 \rightarrow 367 \end{array}$	3700.5(0) $3772 A(3)^{b}$	0.16(3)	$3492 \rightarrow 1723$ $4140 \rightarrow 367$
$3047 A(3)^{b}$	0.00(3)	$3183 \rightarrow 136$	$3777.26(4)^{b}$	2.83(6)	$\frac{140}{3702} \rightarrow 14$
$3050.6(4)^{\circ}$	0.11(3) 0.07(3)	$\frac{1103}{4240} \rightarrow \frac{1108}{1108}$	$3702 32(4)^{b}$	2.85(0) 2.18(5)	$3792 \rightarrow 14$
3030.0(4)	1.65(4)	$4249 \rightarrow 1190$	5792.52(4)	2.16(3)	$4139 \rightarrow 307$
2070 85(6)b	1.03(4)	$3420 \rightarrow 307$	2805 0(2)b	0.05(1) 0.116(24)	$5/92 \rightarrow 0$
3070.83(0)°	0.89(3)	$7040 \rightarrow 43/0$	$3803.0(3)^{-1}$	0.110(24)	$3924 \rightarrow 2118$
30/4.0(0)°	0.063(23)	$5029 \rightarrow 2554$	3820.04(6) ⁶	0.78(3)	$7046 \rightarrow 3820$
3095.2(3)	0.129(24)	unplaced	3842.48(4) ⁶	5.04(6)	$4209 \rightarrow 367$
3098.38(16) ^b	0.34(3)	$7646 \rightarrow 4548$	3845(1) ⁶	0.06(3)	$3982 \rightarrow 136$
3103.38(4) ^b	6.63(12)	$3240 \rightarrow 136$	3854.36(3) ^b	13.22(21)	$7646 \rightarrow 3792$
3113.36(7) ^b	0.81(4)	$4379 \rightarrow 1265$	3934.4(4) ^b	0.10(3)	$3948 \rightarrow 14$

TABLE II. (Continued.)

TABLE II. (Continued.)

$\overline{E_{\gamma}}$	I_{γ}^{a}	Placement	$\overline{E_{\gamma}}$	I_{γ}^{a}	Placement
(keV)		(initial \rightarrow final)	(keV)		$(initial \rightarrow final)$
3956.77(12) ^b	0.52(3)	$5222 \rightarrow 1265$	4948.81(9) ^b	7.32(13)	$7646 \rightarrow 2697$
3962.6(5)	0.11(3)	unplaced	5069.2(3) ^b	0.26(5)	$5084 \rightarrow 14$
3967.3(3) ^b	0.25(3)	$3982 \rightarrow 14$	5083(1) ^b	0.13(3)	$5084 \rightarrow 0$
3981.50(14) ^b	0.49(4)	$3982 \rightarrow 0$	5100.6(4) ^b	0.13(4)	$5238 \rightarrow 136$
3985.3(4) ^b	0.31(3)	$7646 \rightarrow 3660$	5125(1) ^b	0.12(3)	$5492 \rightarrow 367$
3995.3(4) ^b	0.12(3)	$5260 \rightarrow 1265$	5127.2(6) ^b	0.14(5)	$5495 \rightarrow 367$
4011.9(3) ^b	4.19(8)	$4379 \rightarrow 367$	5140.9(3) ^b	1.61(6)	$7646 \rightarrow 2505$
4072.69(9) ^b	1.96(5)	$4209 \rightarrow 136$	5164(1) ^b	0.16(8)	$5165 \rightarrow 0$
4093.47(19) ^b	0.31(3)	$4460 \rightarrow 367$	5179.46(21) ^b	0.34(4)	$5886 \rightarrow 706$
4098.68(16) ^b	0.34(3)	$7646 \rightarrow 3547$	5216.88(15) ^b	0.35(3)	$5924 \rightarrow 706$
4107(1) ^b	0.22(11)	$4474 \rightarrow 367$	5223.66(21) ^b	0.27(3)	$5238 \rightarrow 14$
4111.8(6) ^b	0.09(3)	$4249 \rightarrow 136$	5357.72(19) ^b	1.20(5)	$5495 \rightarrow 136$
4125.34(20) ^b	0.24(3)	$4832 \rightarrow 706$	$5429.1(4)^{b}$	0.19(4)	$5429 \rightarrow 0$
4145(1) ^b	0.09(3)	$4159 \rightarrow 14$	$5482(1)^{b}$	0.31(15)	$5482 \rightarrow 0$
4159.02(11) ^b	0.86(4)	$4159 \rightarrow 0$	5488(1) ^b	0.17(3)	$5488 \rightarrow 0$
4194.71(7) ^b	0.85(4)	$4209 \rightarrow 14$	5493.0(5) ^b	0.08(3)	$5495 \rightarrow 0$
$42.09.44(18)^{b}$	0.34(4)	$4209 \rightarrow 0$	0.0010(0)	0.18(4)	$5629 \rightarrow 136$
4218.19(4) ^b	36.9(6)	$7646 \rightarrow 3428$	5507.1(3) ^b	0.09(3)	$5522 \rightarrow 14$
$4242(1)^{b}$	0.10(3)	$4379 \rightarrow 136$	5525 2(9)°	0.07(5)	$6790 \rightarrow 1265$
4259 3(5) ^b	0.082(24)	$5886 \rightarrow 1627$	5553(1) ^b	0.07(2)	$5689 \rightarrow 136$
4274 84(4) ^b	4.77(9)	$7646 \rightarrow 3371$	5615(1) ^b	0.07(2)	$5629 \rightarrow 14$
4300 61(4)°	0.35(4)	$5308 \rightarrow 1007$	5646(1) ^b	0.09(3)	$6013 \rightarrow 367$
4324 69(9) ^b	0.33(1) 0.40(3)	$4460 \rightarrow 136$	$5653 4(3)^{b}$	0.09(5) 0.41(6)	$5789 \rightarrow 136$
1321.09(9)	0.10(3) 0.21(3)	$4692 \rightarrow 367$	5673 3(5)°	0.38(6)	$6040 \rightarrow 367$
4347 55(10) ^b	0.58(3)	$7646 \rightarrow 3298$	5698 8(12) ^b	0.07(6)	$5713 \rightarrow 14$
$43644(3)^{b}$	1.00(4)	$4379 \rightarrow 14$	$57495(3)^{b}$	0.07(0) 0.19(4)	$5886 \rightarrow 136$
4378 69(6) ^b	2 35(6)	$4379 \rightarrow 0$	5776(1) ^b	0.17(4) 0.4(2)	$5780 \rightarrow 14$
4406 09(4) ^b	0.44(15)	$4773 \rightarrow 367$	5786 76(10) ^b	0.4(2) 0.88(5)	$5924 \rightarrow 136$
1100.09(1)	16 3(3)	$7646 \rightarrow 3240$	5838 2(4) ^b	0.18(5)	$5921 \rightarrow 130$ $5975 \rightarrow 136$
4411 1(8) ^c	0.12(4)	$4548 \rightarrow 136$	5886(1) ^b	0.10(9) 0.24(8)	$5886 \rightarrow 0$
$4445 48(20)^{b}$	0.12(4) 0.38(4)	$4460 \rightarrow 14$	5893(1) ^b	0.24(0)	$5800 \rightarrow 0$ $5894 \rightarrow 0$
4458 79(20) ^b	1.06(10)	$4824 \rightarrow 367$	5909 7(8) ^b	0.03(2) 0.22(6)	$5924 \rightarrow 14$
4462 60(6) ^b	4 33(20)	$7646 \rightarrow 3183$	5920 20(5) ^b	80.7(16)	$7646 \rightarrow 1725$
4402.00(0)	1.0(3)	$\frac{1}{460} \rightarrow 0$	5920.20(3) 5922 7(3) ^b	1 3(5)	$5024 \rightarrow 0$
4531 9(3) ^b	0.44(3)	$5238 \rightarrow 706$	5998 0(7) ^b	0.14(5)	$6013 \rightarrow 14$
$4548(1)^{b}$	0.19(9)	$4548 \rightarrow 0$	$6018\ 43(5)^{b}$	824(13)	$7646 \rightarrow 1627$
4555 6(3) ^b	0.19(5)	$4692 \rightarrow 136$	$6029(1)^{b}$	0.12(3)	$6029 \rightarrow 0$
4560 2(4) ^b	0.95(3)	$4575 \rightarrow 14$	$6037(1)^{b}$	0.12(3) 0.16(8)	$6038 \rightarrow 0$
4500.2(4)	0.23(3)	$4575 \rightarrow 0$	$6046 \ 9(3)^{b}$	0.10(0) 0.24(4)	$6062 \rightarrow 14$
4575(1) 4588 1(5) ^c	0.13(3)	$4373 \rightarrow 0$ 6215 $\rightarrow 1627$	$6061.07(15)^{b}$	0.24(4) 0.61(5)	$6062 \rightarrow 14$
$4507(1)^{b}$	0.09(3)	$4963 \rightarrow 367$	$6073 8(7)^{b}$	0.01(3) 0.12(4)	$6075 \rightarrow 0$
4639 41(25) ^b	0.25(12)	$6365 \rightarrow 1725$	$6103(1)^{b}$	0.12(4) 0.12(6)	$6117 \rightarrow 14$
4658 52(0) ^b	0.23(3)	$5924 \rightarrow 1265$	$6117(1)^{b}$	0.12(0) 0.21(3)	$6117 \rightarrow 0$
4675 29(6) ^b	(1.03(4))	$7646 \rightarrow 2071$	61/(1) $61/(1)^{b}$	0.21(5) 0.28(5)	$6160 \rightarrow 14$
4075.29(0) $4670(1)^{b}$	4.22(8)	$7040 \rightarrow 2971$ $5046 \rightarrow 367$	$6200.5(4)^{b}$	0.28(5)	$6215 \rightarrow 14$
4079(1)	0.10(3) 0.15(3)	$\frac{3040}{4832} \rightarrow \frac{307}{136}$	6285(1) ^b	0.31(0) 0.08(3)	$0213 \rightarrow 14$
4094.8(4) 4725 60(24) ^b	0.13(3) 0.17(3)	$4052 \rightarrow 150$	$6314(1)^{b}$	0.00(3) 0.17(3)	$\begin{array}{c} 6203 \rightarrow 0 \\ 6314 \rightarrow 0 \end{array}$
4723.09(24) 4772.40(12) ^b	0.17(3)	$\frac{1027}{1027} = 1027$	6338 05(23) ^b	0.17(3) 0.60(3)	$6353 \rightarrow 14$
4772.49(12)	0.00(4) 0.11(3)	$4773 \rightarrow 0$	$6345(1)^{b}$	0.00(3)	$0333 \rightarrow 14$
4800 04(5)b	161(3)	$\frac{100}{7646} \rightarrow \frac{100}{2926}$	63/6(1) ^b	0.00(3)	$0 + 62 \rightarrow 130$
-1007.74(J)	10.1(3) 0.22(2)	$7040 \rightarrow 2000$	6365(1) ^b	0.00(3)	$0340 \rightarrow 0$
-1052.05(17) ²	0.33(3)	$4032 \rightarrow 0$	6280 62/9\b	0.10(0)	$0303 \rightarrow 0$
$+0+3.21(14)^{2}$	0.41(3)	$4043 \rightarrow 0$	$(300.03(8))^{\circ}$	/.10(13)	$7040 \rightarrow 1203$
4909(1)	0.20(9)	$4923 \rightarrow 14$	6407 4(5)b	0.12(4)	$0408 \rightarrow 14$
$4923.1(0)^{\circ}$	0.13(3)	$4923 \rightarrow 0$	$0407.4(3)^{\circ}$	0.20(4)	$0408 \rightarrow 0$
4940.8(3)	0.23(4)	$3308 \rightarrow 36/$	0301.1(0)	0.18(5)	$0310 \rightarrow 14$

TABLE II.	(<i>Continued</i> .)
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E_{γ} (keV)	$I_{\gamma}{}^{\mathrm{a}}$	Placement (initial \rightarrow final)
6610(1) ^b	0.08(3)	$6624 \rightarrow 14$
6652(1) ^b	0.13(3)	$6652 \rightarrow 0$
6661(1) ^b	0.14(3)	$6676 \rightarrow 14$
6701.4(5)	0.12(4)	$6837 \rightarrow 136$
6710(1) ^b	0.12(6)	$6725 \rightarrow 14$
6731(1) ^b	0.24(4)	$6746 \rightarrow 14$
6753.5(5) ^b	0.06(2)	$7120 \rightarrow 367$
6764(1) ^b	0.09(3)	$6778 \rightarrow 14$
6837(1) ^b	0.06(3)	$6837 \rightarrow 0$
6939(1) ^b	0.47(15)	$7646 \rightarrow 706$
7278.76(19) ^b	48(3)	$7646 \rightarrow 367$
7306.5(6) ^b	0.32(7)	$7321 \rightarrow 14$
7312.7(9) ^c	0.22(8)	$7313 \rightarrow 0$
7554.2(5) ^c	0.13(5)	$7555 \rightarrow 0$
7631.06(8) ^b	228(4)	$7646 \rightarrow 14$
7645.48(8) ^b	200(3)	$7646 \rightarrow 0$

^aRelative intensity. For multiply placed transitions the singles γ -ray intensity has been divided on the basis of intensity balance and coincidence data. Multiply by 0.1190(7) for transition probability per 100 neutron captures, $P_{\nu}(\%)$.

^bTransition confirmed by coincidence data.

^cTransition placed by energy sums.

^dTransition adopted from ENSDF [12].

2920.60-keV levels were not seen in either the singles or coincidence measurements. The method of placement of each γ ray in the decay scheme is noted in Tables I and II.

Data for 97 levels and the neutron capture state in 57 Fe are summarized in Table III. Level energies were determined by a least-squares fit of the recoil-corrected γ -ray energies to the level scheme. The spins and parities of the 57 Fe levels in Table III are discussed in the ENSDF evaluation [12] and are based on all experimental reaction and decay data populating 57 Fe, including the results discussed here. The intensity balance reported in Table III has been corrected for internal conversion including internal pair conversion (IPC) [13] which varies 0.13–0.26% for *E*1 and *M*1 transitions with energies of 3.0–7.6 MeV.

We found that ≈ 33 levels assigned to ⁵⁷Fe by Vennink *et al.* [6] could not be confirmed by this work, while an approximately equal number of new levels were added to the ⁵⁷Fe level scheme. Many of the new levels involved different placements of γ rays first observed by Vennink *et al.*, demonstrating the fallibility of relying on energy sums for γ -ray placement and the necessity of coincidence data for reliable construction of a level scheme.

A. Intensity balance

The γ -ray transition intensities have been corrected for a small contribution from internal conversion, calculated with the BRICC code [13], assuming either experimentally determined multipolarities or M1, E1, or E2 depending on the initial and final level spins and parities. When the spin or parity of the initial or final levels was unknown, E1 multipolarity

TABLE III.	Level	energies,	J^{π} , a	nd	intensity	balance	per	100
neutron capture	s feedi	ng/deexcit	ing lev	vels	in ⁵⁷ Fe.			

E_{level} (keV)	J^{π}	$P_{\gamma}(in)$	$P_{\gamma}(\text{out})$	$P_{\gamma}(\text{in-out})$
0.0	$1/2^{-}$	101.0(10) ^a		
14.399(7)	$3/2^{-}$	$62.4(9)^{a}$	$62.4(9)^{a}$	0.0(17)
136.444(10)	$5/2^{-}$	4.67(4)	4.93(7)	-0.26(8)
366.747(9)	$3/2^{-}$	15.2(4)	15.26(17)	0.0(4)
706.418(12)	$5/2^{-}$	6.89(8)	7.07(8)	-0.19(12)
1007.22(5)	$7/2^{-}$	0.227(14)	0.230(6)	-0.003(17)
1198.39(24)	$9'/2^{-}$	0.008(4)	0.0067(15)	0.002(4)
1265.009(15)	$1/2^{-}$	2.256(23)	2.49(4)	-0.24(4)
1357.20(9)	$7'/2^{-}$	0.386(13)	0.388(13)	-0.002(19)
1627.292(16)	$3/2^{-}$	10.79(16)	10.91(4)	-0.11(16)
1725.449(15)	$3/2^{-}$	10.95(19)	11.05(11)	-0.09(22)
2118.27(3)	5/2-	0.383(0)	0.391(6)	0.008(11)
2207.24(4)	$5/2^{-}$	0.438(9)	0.510(7)	-0.071(11)
2504.95(3)	$5/2^+$	0.381(9)	0.399(7)	-0.018(12)
2554.12(25)	$3/2^{-}$	0.209(6)	0.290(6)	-0.081(8)
2574.069(24)	$(3/2)^{-}$	0.277(6)	0.276(7)	0.001(9)
2697 069(17)	$1/2^{-}$	1.05(3)	1.017(14)	0.04(3)
2835 935(22)	3/2(+)	2.09(4)	2.264(21)	-0.18(4)
2920 56(7)	$1/2^{-} 3/2^{-}$	0.150(6)	0.145(6)	0.005(8)
2920.50(7)	$3/2^{-}$	0.653(17)	0.65(3)	0.005(0)
2970.00(7) 3183.07(4)	$1/2^{-} 3/2^{-}$	0.055(17) 0.587(24)	0.63(3)	-0.04(3)
3739911(21)	1/2, $3/21/2^{-}$	1.97(4)	2.030(25)	-0.06(4)
3298 28(8)	$(1/2^+ 3/2^+)$	0.087(4)	0.108(5)	-0.021(7)
3270.20(0) 3371.17(4)	(1/2, 3/2)	0.007(4)	0.100(3)	-0.013(16)
3/27 8/0(17)	$3/2^{-}$	4.42(7)	4 47(8)	-0.05(11)
3547 43(0)	3/2	-1.+2(7)	-4.47(0)	-0.00(11)
3660 23(25)	$(5/2^+)$	0.070(0)	0.070(7)	0.000(9)
3701.747(10)	(3/2)	1.576(25)	1.584(10)	-0.007(18)
3791.747(19) 3810 50(25)	$(5/2^+)$	1.570(25)	1.364(19)	-0.007(18)
3048 40(16)	$(5/2^+)$	0.098(4)	0.114(0) 0.033(6)	-0.10(7)
3081 66(5)	(3/2)	0.033(4)	0.035(0)	0.000(7)
3381.00(3)	$\frac{5}{2^+}$	0.134(0)	0.219(23)	-0.04(3)
4140.01(13)	$\frac{3}{2}$	0.042(7)	0.041(4) 0.486(17)	0.002(8)
4139.20(3)	$\frac{1}{2}, \frac{3}{2}$	2.07(4)	0.480(17) 2.003(18)	0.019(20)
4209.333(23)	5/2	2.07(4)	2.003(18)	0.07(4)
4240.70(7)	3/2(1)	1.50(3)	1.514(18)	0.003(8)
4460 24(2)	$\frac{3/2}{(1/2-3/2-)}$	1.39(3)	1.314(10)	0.07(3)
4400.24(3)	(1/2, 3/2)	0.007(17)	0.07(4)	0.02(4)
4474.0(10)	$(3/2^{+})$	0.020(13)	0.020(13)	0.000(18)
4347.79(7)	1/2, $3/21/2 - 3/2$	0.004(0) 0.106(4)	0.081(12)	-0.017(13)
43/3.8/(1/)	$\frac{1}{2}, \frac{3}{2}$	0.100(4)	0.080(7)	0.020(8)
4092.13(3)	$(3/2)^{+}$	0.382(13)	0.527(10)	0.033(22)
4772.02(4)	$(3/2^{+})$	0.431(8)	0.440(21)	0.011(22)
4823.3(3)	$1/2^+, 3/2^+$	0.12(4)	0.120(12)	-0.01(4)
4832.30(8)	5/2 1/2 2/2	0.120(0)	0.080(0)	0.040(9)
4845.47(6)	1/2,5/2	0.103(5)	0.062(4)	0.041(7)
4922.9(3)	1/2, 3/2	0.040(13)	0.071(12)	-0.031(18)
4903.0(3)	$(5/2^{+})$	0.030(10)	0.030(14)	0.000(17)
5082 (2(10)	(1/2) 1 (2+ 2 /2)	0.084(10)	0.013(7)	0.009(17)
5164 0(10)	$1/2^{+}, 3/2$	0.038(5)	0.039(7)	-0.001(8)
5104.0(10)	1/2'	0.019(10)	0.019(10)	0.000(14)
5221.75(25)	1/2,3/2	0.001(4)	0.062(4)	-0.001(6)
5258.54(6)	1/2 ,3/2	0.1/1(5)	0.14/(9)	0.024(11)
5260.31(3)	1/2,3/2	0.15/(4)	0.213(7)	-0.056(7)
5308.08(6)	$(3/2^{-})$	0.090(4)	0.082(8)	0.008(9)
5428.82(10)	5/2*	0.054(3)	0.054(6)	0.000(7)
5482.0(7)	1/2,3/2	0.0036(18)	0.037(18)	-0.033(18)

TABLE III. (Continued.)

E_{level} (keV)	J^{π}	$P_{\gamma}(in)$	$P_{\gamma}(\text{out})$	$P_{\gamma}(\text{in-out})$
5488.37(25)	1/2,3/2	0.0208(23)	0.020(4)	0.001(4)
5491.55(10)	1/2,3/2	0.050(3)	0.059(6)	-0.009(7)
5494.53(4)	$1/2^{-},3/2$	0.245(5)	0.192(10)	0.053(11)
5521.8(3)	$1/2^{+}$	0.0102(21)	0.011(4)	-0.001(4)
5629.23(7)	3/2	0.068(3)	0.058(7)	0.010(7)
5689.40(14)	3/2	0.064(4)	0.029(5)	0.035(6)
5713.23(18)	$(1/2^+)$	0.0149(24)	0.008(7)	0.007(8)
5790.1(3)	1/2,3/2	0.080(3)	0.101(25)	0.021(25)
5886.10(4)	1/2-,3/2	0.105(3)	0.109(12)	-0.004(12)
5893.53(9)	1/2,3/2	0.0271(19)	0.018(3)	0.009(4)
5923.51(4)	1/2-,3/2	0.463(11)	0.45(6)	0.01(6)
5974.67(7)	$(3/2^+)$	0.067(3)	0.021(6)	0.046(7)
6012.8(3)	1/2,3/2	0.012(3)	0.027(7)	-0.015(8)
6029.36(25)	$3/2^{+}$	0.0136(19)	0.014(4)	0.000(4)
6037.4(3)	1/2,3/2	0.0162(20)	0.019(10)	-0.003(10)
6040.3(3)	1/2,3/2	0.0245(21)	0.045(7)	-0.021(7)
6061.47(15)	1/2,3/2	0.101(4)	0.101(8)	0.000(9)
6074.7(3)	1/2,3/2	0.061(3)	0.065(16)	-0.004(16)
6117.02(12)	$1/2^+, 3/2$	0.0199(19)	0.052(9)	-0.032(9)
6159.55(13)	$3/2^{-}$	0.070(4)	0.073(8)	-0.003(9)
6215.42(12)	$1/2^{+}$	0.0484(23)	0.048(8)	0.000(8)
6284.6(6)	1/2,3/2	0.0094(24)	0.0010(4)	-0.0006(24)
6313.86(9)	1/2,3/2	0.0377(20)	0.052(6)	-0.015(6)
6346.11(19)	1/2,3/2	0.0131(17)	0.010(4)	-0.004(4)
6352.85(5)	1/2,3/2	0.130(4)	0.146(6)	-0.016(7)
6364.87(5)	$3/2^{+}$	0.101(3)	0.077(11)	0.024(11)
6408.36(17)	$3/2^{+}$	0.104(7)	0.129(9)	-0.025(12)
6481.0(10)	1/2,3/2	0.007(4)	0.007(4)	0.000(6) ^c
6515.68(7)	$3/2^{+}$	0.0257(19)	0.021(6)	-0.004(6)
6624.2(3)	1/2,3/2	0.0092(14)	0.010(4)	-0.001(4)
6651.7(3)	$1/2^+, 3/2$	0.023(4)	0.026(5)	-0.003(6)
6675.70(25)	$3/2^{+}$	0.0171(23)	0.017(4)	0.000(4)
6724.0(10)	1/2,3/2	0.014(7)	0.014(7)	$0.000(1)^{c}$
6745.50(7)	1/2,3/2	0.0386(24)	0.048(6)	-0.009(6)
6778.4(3)	1/2,3/2	0.0102(23)	0.011(4)	-0.001(4)
6790.29(19)	1/2,3/2	0.0113(18)	0.008(6)	-0.003(6)
6837.34(11)	$1/2^{-},3/2$	0.055(18)	0.054(7)	0.000(19) ^c
7120.3(3)	1/2,3/2	0.0075(14)	0.0071(24)	0.000(3)
7313.2(8)	1/2,3/2	0.026(10) ^c	0.026(10)	0.000(14) ^c
7321.27(13)	1/2,3/2	0.063(24) ^c	0.063(24)	0.00(3) ^c
7554.4(3)	1/2,3/2	0.015(6) ^c	0.015(6)	0.000(9) ^c
7646.183(18) ^b	$1/2^{+}$		99.5(8)	

^aCorrected for unobserved statistical feeding as described in the text. ^bNeutron capture energy.

^ePrimary γ -ray populating level was not observed. The intensity is from the intensity balance.

was assumed. The total observed primary transition intensity depopulating the capture state is $98.5 \pm 1.3\%$ of that seen feeding the ground and 14-keV states, indicating that the level scheme is nearly complete. The intensity of the 23 unplaced transitions is only 0.14% of the total placed transition intensity.

To estimate the unobserved transition intensity contribution to the ⁵⁷Fe decay scheme, we have plotted the intensity per 100 neutron captures, $P_{\gamma}(\%)$, from the renormalized intensities in Tables I and II (see footnote "a"), for all γ rays, primary γ



FIG. 1. Plot of ⁵⁷Fe transition probabilities, $P_{\gamma}(\%)$, ordered by their decreasing value, for all, primary, ground state (GS), and 14-keV level feeding γ rays. The solid lines through each plot represent an exponential fit through the data below N_{cut} , indicated by the vertical lines in each curve. Extrapolation of the fit to higher γ -ray numbers gives an estimate of the unobserved feeding. The parameters of each exponential fit are given in Table IV.

rays, and γ rays feeding the GS and 14-keV levels in order of decreasing $P_{\gamma}(\%)$ value in Fig. 1. Each of these $P_{\gamma}(\%)$ distributions can be fit to a simple exponential. The fitting parameters for these four exponential fits are summarized in Table IV. In each fit we have ignored both the most intense γ rays, which deviate from an exponential fit, and the least intense $\approx 10\%$ transitions, above a cutoff N_{cut} . The weakest transitions may not all be observed, which is consistent with Fig. 1 where, above N_{cut} , the $P_{\gamma}(\%)$ values begin to fall below the exponential trend. Integrating the exponential fits from N_{cut} to a maximum number of transitions, N_{max} gives an estimate of the total missing transition probability. For the primary, GS, and 14-keV level transitions we assume $N_{\text{max}} = 330$,

TABLE IV. The $P_{\gamma}(\mathscr{B})$ distribution for all, primary (CS), ground state (GS), and 14-keV level feeding γ rays have been fit to an exponential defined as $P_{\gamma}(\mathscr{B}) = ae^{-bN}$ where N is the γ -ray number in decreasing intensity. N_{γ} is the total number of transitions observed in each category. The unobserved contribution was calculated by integrating the exponential from a cutoff transition number, N_{cut} , to a maximum number of transitions, N_{max} , and subtracting the intensity of transitions experimentally observed above N_{cut} .

	Paran a	neters b	Nγ	N _{cut}	$\sum_{\substack{N_{\rm cut}\\{\rm expt}}}^{N_{\gamma}}$	$P_{\gamma}(\%)$ calc	$\frac{\sum_{N_{\text{cut}}}^{N_{\text{max}}} P_{\gamma}(\%)}{\text{netcalc}^{a}}$	netcalc-expt ^b
All	0.015	0.071	448	397	0.28	0.37	1.27	0.99
CS	0.35	0.041	89	80	0.08	0.11	0.32	0.25
GS	0.12	0.049	55	42	0.08	0.11	0.32	0.18
14	0.098	0.042	51	46	0.040	0.058	0.33	0.29

 $^{a}N_{max} = 330$ for GS, 14 keV, and CS transitions, and 1000 for all transitions.

^bTotal unobserved percent transition probability.



FIG. 2. The $P_{\gamma}(\%)$ balance populating/depopulating levels in ⁵⁷Fe following thermal neutron capture.

the number of levels that can be fed by a dipole transition according to the constant temperature (CT) model prediction, and we arbitrarily limit the total number of transitions to $N_{\text{max}} = 1000$. The integral is not very sensitive to the choice of N_{max} because the transition probability is observed to fall off very rapidly with transition number. The theoretical justification for this estimate is discussed below.

The calculated missing transition probabilities are summarized in Table IV. For the total observed γ -ray spectrum we estimate that $\approx 1\%$ of the total transition probability is missing. This is remarkably consistent with the total observed γ -ray energy production, $\Sigma P_{\gamma}(\%)E_{\gamma}/(100 \times S_n) =$ 0.989 ± 0.014 , where S_n is the neutron separation energy. We calculate the total missing primary γ -ray transition probability ΔP_{γ} (%)(CS) = 0.25%. For γ rays feeding the GS + 14 keV levels the missing transition probability is $\Delta P_{\gamma}(\%)(\text{GS} +$ 14) = 0.47%. This missing transition probability is consistent with the variations in the transition probability balance shown in Fig. 2 and lower than the statistical uncertainty in the total primary and GS + 14 keV level feedings. For the ⁵⁶Fe(n,γ) decay scheme the average γ -ray multiplicity per neutron capture is $M_{\gamma} = \sum P_{\gamma}(\%)/100 = 1.83$ and the total multiplicity, including internal conversion, is $M_{\gamma+e} =$ $\sum P_{\gamma+e}(\%)/100 = 2.39.$

The γ -ray intensities in Tables I and II are normalized relative to 100 for the 352.347-keV γ -ray and can be renormalized to percent transition probabilities, $P_{\gamma}(\%)$, by the factor 0.1190 \pm 0.0007, assuming that the sum of the observed GS + 14 keV level feedings and CS deexcitation transition probabilities, $P_{\gamma}(\text{GS} + 14 + \text{CS})\% = 200$, after correcting for the missing transition probabilities as described above. The transition probability balance through all proposed levels in 57 Fe is shown in Table III and summarized in Fig. 2. The decay scheme is very well balanced, with discrepancies of $\Delta P_{\gamma}(\%) \lesssim 0.3\%$ through all levels.

B. ⁵⁶Fe(n, γ) cross section

Two independent internal calibrations of the ${}^{56}\text{Fe}(n,\gamma){}^{57}\text{Fe}$ γ -ray cross sections were performed with iron(III) acetylacetonate (C₁₅H₂₁FeO₆) and iron pyrite

PHYSICAL REVIEW C 95, 014328 (2017)

(FeS₂) targets. The iron(III) acetylacetonate target, provided by Sigma-Aldrich, was certified as 99.9% pure on a trace metals basis, but the purity of the Fe(III) oxidation state was not explicitly given. Iron(III) acetylacetonate is 15.812(2)% Fe by weight; however, the certified Fe content was 16.0(2)%, which is consistent with the target containing < 6.1% iron(II) acetylacetonate (C₁₀H₁₄FeO₄). This suggests a target H/Fe ratio of 20.78 ± 0.22. Using the 2223.2-keV γ ray from the ¹H(n,γ) reaction, assuming $\sigma_{\gamma}(2223) = 0.3325(7)$ b [14], we determined the 352.3-keV γ -ray cross section to be 0.2844(19) b.

Iron pyrite occurs only in the Fe(II) oxidation state since the Fe(III) sulfide is unstable and does not appear in nature. From our prompt γ -ray measurements on the pyrite target we set a limit of <0.5% for sulfide impurities. Using the 841-keV γ ray from the ${}^{32}S(n,\gamma)$ reaction, assuming $\sigma_{\gamma}(841) = 0.353(2)$ b [15], we determined $\sigma_{\nu}(352) = 0.2858(26)$ b. The weighted average of these two measurements is $\sigma_{\nu}(352) = 0.2849(15)$ b. This value together with $P_{\nu}(352) = 11.90 \pm 0.07\%$ from the level scheme normalization gives the 56 Fe (n, γ) total radiative cross section as $\sigma_0 = 2.394(19)$ b. This measured cross section is independent of the neutron flux for a homogenous target since it is only dependent on the ratio of ${}^{1}H$ and ${}^{32}S$ standardization cross sections to the 352-keV γ -ray transition probability. The guided neutron beam energy used in these measurements is subthermal energy so no correction was necessary for epithermal contributions to the measured γ -ray cross sections.

Only three measurements of ${}^{56}\text{Fe}(n,\gamma)$ were found in the literature, 2.65(8) b by Pomerance [16] based on the pile oscillator method, which has been renormalized to the modern ${}^{197}\text{Au}(n,\gamma)$ cross section calibration standard [17], 2.57(14) b by Shcherbokov *et al.* [18], based on a time-of-flight measurement, and 2.51(4) b [15] by Revay and Molnár based on an earlier prompt γ -ray measurement. The recommended cross section from Mughabghab [17] is 2.59(14) b. All previous values are significantly higher than our measurement, which has a considerably smaller uncertainty.

C. ⁵⁷Fe neutron separation energy

A weighted least-squares fit of the recoil-corrected γ -ray energies to obtain the level energies in ⁵⁷Fe determined the neutron separation energy for the capture state to be 7646.183(18) keV. This value is slightly higher than the adopted value of 7646.08(4) keV from the 2013 mass evaluation by Wang *et al.* [19].

IV. STATISTICAL MODEL TESTS

The transition probabilities observed in this work can be compared with calculated values using the Monte Carlo computer code DICEBOX [20]. DICEBOX is based on the generalization of the extreme statistical model embodying Bohr's idea of a compound nucleus [21]. We have simulated the decay of the ⁵⁷Fe capture state with several photon strength function models. Here we show results only for simulations with a combination of the Kadmenskij-Markushev-Furman (KMF) *E*1 photon strength function (PSF) [22] and the



FIG. 3. Plot of simulated ⁵⁷Fe transition probabilities, $P_{\gamma}(\%)$, ordered by decreasing value for all, primary, and GS + 14 keV level feeding γ rays and averaged over 40 realizations with model A. The dashed black lines through each plot are an exponential fit through the predictions.

single-particle (SP) model [23] M1 PSF, labeled model A, and a PSF model based on the Oslo data [24] with an "upbend" of M1 origin, labeled model B. Levels in both models were generated using the constant temperature (CT) level density (LD) model [25]. The spins and parities of levels below an excitation energy $E_{crit} = 2.56$ MeV, where the level scheme is believed to be complete, are from the recent ⁵⁷Fe ENSDF evaluation [12], while the γ -ray transition probabilities deexciting levels below E_{crit} and primary transition probabilities feeding these levels are taken from this work. Above E_{crit} , individual levels were generated using the LD model, and transition probabilities were obtained using Monte Carlo method assuming the Porter-Thomas (PT) distribution [26] around expectation values given by the PSF model. Random fluctuations can produce an infinite number of different artificial sets of levels and decay intensities called nuclear realizations. Typically 40 different nuclear realizations were simulated for each combination of PSFs and LD models. The number of cascades in each realization was 10^6 .

In Fig. 3 we have plotted ordered transition probabilities, averaged over 40 nuclear realizations, for all γ rays, primary γ rays, and γ rays feeding the GS + 14 keV levels, as predicted by model A. Each set of transitions can reasonably be fit with an exponential, as we observed in Fig. 1 and discussed in Sec. III A. Predictions for individual nuclear realizations significantly vary in magnitude, some agreeing with experiment. However, the shapes of predictions are similar for all nuclear realizations. Predictions with model B show a similar exponential trend although the absolute magnitude does not agree as well with experiment. These calculations reinforce the validity of our method for estimating the missing transition intensity.

Simulations can also be used to investigate the intensity balance through levels below E_{crit} . We can compare the simulated feeding of these levels from levels above E_{crit} , excluding the capture state that is taken from experiment,



FIG. 4. Simulated vs experimental side-feeding transition probabilities, $P_{\gamma}(\%)$. The modeled side-feeding corresponds to the predicted feeding from levels above $E_{\rm crit}$ except for the capture state. Experimental side-feeding corresponds to the difference between the intensity deexciting levels below $E_{\rm crit}$, minus the capture state feeding, and the feeding intensity from levels below $E_{\rm crit}$. Calculations were done using models A (blue markers) and B (green markers) that are described in the text. The observed side-feeding is shown (red markers) for comparison.

with the missing experimental feeding from levels below $E_{\rm crit}$. The missing experimental feeding is defined as the difference between the intensity deexciting a level and the intensity populating that level from levels below E_{crit} and from the capture state. We call these quantities the modeled and experimental side-feedings, which should ideally be equal. The side-feeding comparison, expressed as $P_{\nu}(\%)$, for both A and B models is shown in Fig. 4. Modest agreement between the experimental and modeled side-feedings indicates that the statistical model calculations using available models of the PSF and level density are adequate in 57 Fe. There is a general trend for levels with higher experimental side-feeding to have higher simulated side-feedings, indicating that the statistical model can reasonably predict the population of low-lying levels even for light nuclei like ⁵⁷Fe. A better description of experimental data is obtained with model B except for the side-feeding of the $5/2^+$ state. The $5/2^+$ state is the lowest excited positive parity state, suggesting that discrepancies may arise from the LD model, which does not consider the parity distribution. Similar side-feeding agreement was also obtained with the other tested PSF models. The observed side-feeding, defined as above but using the experimental population from levels above E_{crit} instead of the simulated feedings, is also shown in Fig. 4. This side-feeding is well balanced, showing that the experimental side-feeding is well determined and simulated side-feeding discrepancies are largely due to inadequacies in the models.

There are more variables that could be used for testing various PSF and LD models within statistical model calculations and possibly the validity of the statistical model itself. However, such an analysis goes beyond the scope of this paper and will be published separately.

V. CONCLUSIONS

The ⁵⁶Fe(n, γ) reaction has been investigated using cold neutron beams and γ -ray singles and coincidence measurements. A detailed ⁵⁷Fe capture state decay scheme has been constructed where $\approx 99\%$ of the γ -ray transition intensity has been placed. Approximately 33 previously adopted levels in ⁵⁷Fe could not be confirmed in this work while a comparable number of new levels were added. This improvement is largely the result of our coincidence data which was not available in earlier work. Internal standardization of the measured intensities in the singles spectrum with γ -ray cross section standards has determined the ⁵⁷Fe total radiative thermal neutron capture cross section as $\sigma_0 = 2.394 \pm 0.019$ b. This cross section includes a small correction for unobserved continuum transitions. The experimental population of lowlying levels, below $E_{\text{crit}} = 2.56$ MeV, has been compared to statistical model calculations with modest agreement.

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