Adiabatic fission barriers in superheavy nuclei

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Using the microscopic-macroscopic model based on the deformed Woods-Saxon single-particle potential and the Yukawa-plus-exponential macroscopic energy, we calculated static fission barriers B_f for 1305 heavy and superheavy nuclei $98 \le Z \le 126$, including even-even, odd-even, even-odd and odd-odd systems. For odd and odd-odd nuclei, adiabatic potential-energy surfaces were calculated by a minimization over configurations with one blocked neutron or/and proton on a level from the 10th below to the 10th above the Fermi level. The parameters of the model that have been fixed previously by a fit to masses of even-even heavy nuclei were kept unchanged. A search for saddle points has been performed by the "imaginary water flow" method on a basic five-dimensional deformation grid, including triaxiality. Two auxiliary grids were used for checking the effects of the mass asymmetry and hexadecapole nonaxiality. The ground states (g.s.) were found by energy minimization over configurations and deformations. We find that the nonaxiality significantly changes first and second fission saddle in many nuclei. The effect of the mass asymmetry, known to lower the second, very deformed saddles in actinides, in the heaviest nuclei appears at the less deformed saddles in more than 100 nuclei. It happens for those saddles in which the triaxiality does not play any role, which suggests a decoupling between effects of the mass asymmetry and triaxiality. We studied also the influence of the pairing interaction strength on the staggering of B_f for odd- and even-particle numbers. Finally, we provide a comparison of our results with other theoretical fission barrier evaluations and with available experimental estimates.

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I. INTRODUCTION

Although fission barrier heights B_f are not directly measurable quantities, i.e., are not quantum observables, they are very useful in estimating nuclear fission rates. As the activation energy E_a (per mole) in chemistry gives a rate k of a chemical reaction at temperature T via the Arrhenius law $k = Ae^{-E_a/RT}$ (where R is the gas constant and A is the frequency factor) [1,2], the fission barrier gives the fission rate Γ_f of an excited (as they usually are in nuclear reactions) nucleus via: $\Gamma_f \sim e^{-B_f/kT_{\text{eff}}}$, where T_{eff} is an effective temperature derived from the excitation energy, and k is the Boltzmann constant. For example, knowing fission barriers of possible fusion products helps to predict a cross section for a production of a given evaporation residue in a heavy-ion reaction: one can figure out whether neutron or alpha emission wins a competition with fission at each stage of the deexcitation of a compound nucleus. Moreover, one can try to understand the experimentally established intriguing growth of the total cross sections around Z = 118; for its correlation with B_f ; see, e.g., Fig. 6 and the related discussion in Ref. [3]. On the other hand, the prediction of the spontaneous or low-energy (i.e., from a weakly excited state) fission rates, governed by the regime of the collective quantum tunneling, requires an additional knowledge of the barrier shape and mass parameters.

A nonobservable status of the fission barrier, again in analogy to that of the activation energy in chemistry, is reflected in its possible dependence on a reaction type and/or the excitation energy (effective temperature) range. This leads to some uncertainty in calculations of fission barriers. In particular, it is not clear whether intrinsic configurations should be conserved along the level crossings, which increases B_f , or the adiabatic state should be followed. This is especially relevant for odd-A and odd-odd nuclei, in which sharp crossings of levels occupied by the odd particle exclude the strictly adiabatic scenario. It is known that, if the projection of the single-particle angular momentum Ω on the symmetry axis of a nucleus is conserved, the diabatic effect on the fission barrier can be huge; see, e.g., Ref. [4]. As there is no accepted formula for a barrier correction due to the nonadiabaticity, it is usually ignored, even in odd-N and/or odd-Z nuclei.

A general idea is that, at the excitation energies close to and higher than the barrier but still not inducing sizable dissipative corrections, the adiabatic barrier could be used for calculating fission rates.

Since calculations of potential-energy surfaces (PESs) for odd-A and odd-odd nuclei involve a repetition of calculations for many low-lying quasiparticle states which multiplies the effort (especially in odd-odd systems), systematic studies of their fission barriers are rather scarce. Up to now, they were provided mainly by the Los Alamos microscopic-macroscopic (MM) model and recently by some self-consistent models [5]. The current state of theoretical predictions in fission of even-even nuclei (with $Z \ge 100$) has been discussed recently in Ref. [6].

In the present paper we extend our MM model based on the deformed Woods–Saxon potential, which up to now was applied mainly to even-even nuclei [7], to odd-A and odd-odd

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superheavy (SH) systems. We study a wide range of isotopes which, perhaps, may be of some use for astrophysical purposes. The fission barriers are calculated by using the adiabatic assumption, i.e., they are the smallest possible. Since the model has been quite reasonable, in particular in reproducing first [7] and second [8] fission barriers in actinides, as well as super-[9] and hyper-deformed [10,11] minima, we prefer to keep its parameters unchanged. The shell and pairing correction for an odd-nucleon system is done by blocking the lowest-lying quasiparticle states. The modification of the macroscopic energy by including the average pairing energy contribution which we introduced for nuclear masses in Ref. [12] is irrelevant for fission barriers.

The other aim of our study is to improve the predictions for the fission saddles. This requires simultaneously taking into account a large number of shape variables [8,11] and relying on an in principle exact method for finding saddles to escape errors inherent in the mostly used constrained minimization method; see Refs. [13,14]. As usual, to make the involved computational effort manageable one has to make some compromises which will be discussed in detail. The need for a simultaneous consideration of many shape variables in PES calculations is common to all nuclear models, including self-consistent theories based on some effective interactions [15]. The results for fission saddles obtained up to now in the SH region clearly show the great importance of triaxial deformation, which is neglected in many published works. A recent study [16] of fission barriers within both the MM Woods-Saxon and Skyrme SLy6 Hartree-Fock plus BCS models shows that triaxiality is even more crucial beyond Z = 126.

A description of our method of calculation is given in Sec. II. The results, details of the additional calculations, and comparisons with other calculated barriers are presented and discussed in Sec. III. Finally, the conclusions are summarized in Sec. IV.

II. THE METHOD

Multidimensional energy landscapes are calculated within the MM model based on the deformed Woods–Saxon potential [17]. The Strutinsky shell and pairing correction [18] is taken for the microscopic part. For the macroscopic part we used the Yukawa plus exponential model [19] with parameters specified in Ref. [20]. Thus, all parameter values are kept exactly the same as in all recent applications of the model to heavy and superheavy nuclei.

Of main importance in fission-barrier calculations is their reliability which, once the model for calculating energy of a nucleus as a function of deformation is fixed, depends on two main ingredients: (1) the type and dimension of the admitted deformation space and (2) a method applied to the search for saddles.

Mononuclear shapes can be parametrized via spherical harmonics $Y_{\lambda\mu}(\vartheta,\varphi)$ (for brevity we just use the symbol $Y_{\lambda\mu}$) by the following equation of the nuclear surface:

$$R(\vartheta,\varphi) = c(\{\beta\})R_0 \left\{ 1 + \sum_{\lambda=1}^{\infty} \sum_{\mu=-\lambda}^{+\lambda} \beta_{\lambda\mu} \mathbf{Y}_{\lambda\mu} \right\}, \qquad (1)$$

where $c(\{\beta\})$ is the volume-conservation factor and R_0 is the radius of a spherical nucleus. This parametrization has its limitations; certainly, it is not suitable for too-elongated shapes. However, for moderately deformed saddle points in superheavy nuclei it excellently reproduces all shapes generated by other parametrizations, e.g., by Ref. [21], as we checked in numerous tests.

For nuclear ground states it is possible to confine the analysis to axially symmetric shapes, with the expansion truncated at β_{80} :

$$R(\vartheta,\varphi) = c(\{\beta\})R_0\{1 + \beta_{20}Y_{20} + \beta_{30}Y_{30} + \beta_{40}Y_{40} + \beta_{50}Y_{50} + \beta_{60}Y_{60} + \beta_{70}Y_{70} + \beta_{80}Y_{80}\}.$$
 (2)

Thus, a seven-dimensional minimization is performed by using the gradient method. At least thirty minimizations with different initial deformations were performed for each nucleus. Some of the initial conditions were chosen randomly (within reasonable limits). The lowest minima were verified by performing additional minimizations with initial deformations found for neighboring nuclei. Finally, the minima were checked against the results of minimization over the 5DIM mesh used for the saddle calculation (see below). For odd systems, the additional minimizations over configurations were performed at every step of the gradient procedure. Considered configurations consist of the odd particle occupying one of the levels close to the Fermi level and the rest of the particles forming a paired BCS state on the remaining levels. Ten states above and ten states below the Fermi level have been blocked and energy minimized over these configurations.

The main problem in a search for saddle points is that, since they are neither minima nor maxima, one has to know energy on a multidimensional grid of deformations (the often used and much simpler method of minimization with imposed constraints may produce invalid results, cf. Refs. [8,13–15]). To find saddles on a grid we used the imaginary water flow (IWF) technique. This conceptually simple and at the same time very efficient (from a numerical point of view) method was widely used and discussed before [8,13,22-25]. The number of numerically tractable deformation parameters $\{\beta_{\lambda\mu}\}$ is practically limited. Girds with more than five dimensions, keeping in mind a subsequent interpolation, are intractable in calculations for many (~1000) nuclei. Including mass symmetric and axially symmetric deformations ($\beta_{20}, \beta_{40}, \beta_{60}$, β_{80} ; see Refs. [26–29]) together with both mass asymmetry $(\beta_{30}, \beta_{50}, \beta_{70})$ and triaxiality (at least β_{22}) would mean at least an eight-dimensional mesh and is impossible at present.

Based on our previous results showing that triaxial saddles are abundant in SH nuclei [7], we consider that quadrupole triaxial shapes have to be necessarily included. We treated the effects of mass-asymmetry and nonaxial higher multipoles as corrections and analyzed them at the second stage of calculations. A rationale for a lesser importance of massasymmetric saddles is that, while they constitute a second, more deformed ($\beta_{20} \approx 0.7$ –0.8), prominent barrier peak in actinides, their heights are much reduced in SH nuclei where they become irrelevant. In the remaining, less deformed saddles, the mass asymmetry occurs less frequently. As to the nonaxial multipoles of higher order, they are less important for saddles with small to moderate γ [where γ is the Bohr quadrupole nonaxiality parameter, cf. Eq. (7)]. They become important for γ closer to 60° where they are needed to produce oblate shapes having *x* as the symmetry axis. Thus, they should be included for nuclei with a large oblate ground-state (g.s.) deformation and a short triaxial fission path. The additional studies of the mass asymmetry and higher nonaxial multipoles are described in the proper sections of the results section.

Thus, at the first stage, for all 1305 investigated nuclei the saddle points were searched in a five-dimensional deformation space spanned by β_{20} , β_{22} , β_{40} , β_{60} , β_{80} by using the IWF technique. The appropriate nuclear radius expansion has the form

$$R(\vartheta,\varphi) = c(\{\beta\})R_0 \left\{ 1 + \beta_{20}Y_{20} + \frac{\beta_{22}}{\sqrt{2}}[Y_{22} + Y_{2-2}] + \beta_{40}Y_{40} + \beta_{60}Y_{60} + \beta_{80}Y_{80} \right\}.$$
 (3)

The five-dimensional calculations are performed on the following deformation mesh:

$$\beta_{20} = 0.00 (0.05) 0.60,$$

$$\beta_{22} = 0.00 (0.05) 0.45,$$

$$\beta_{40} = -0.20 (0.05) 0.20,$$
 (4)

$$\beta_{60} = -0.10 (0.05) 0.10,$$

$$\beta_{80} = -0.10 (0.05) 0.10.$$

This makes a grid of 29 250 points which was subsequently interpolated to a fivefold-denser grid of 50 735 286 points with the step 0.01 in each dimension. On the latter, the saddle point, or rather several saddle points—if there were a few of comparable heights within the 0.5 MeV energy window—were searched for by means of the IWF procedure. We have checked that every ground-state minimum found by the minimization corresponds to a minimum on the mesh with a similar deformation. This latter mesh point was used as the initial one in the IWF method. For odd or odd-odd nuclei, at each grid point we were looking for low-lying configurations by blocking particles on levels from the 10th below to the 10th above the Fermi level (in neutrons or/and protons).

The fact that searches for ground states and for saddles are separated—performed using different deformation spaces—allows saving some number of deformation parameters in Eq. (3). This is equivalent to assuming that the fission saddles have mostly prolate deformations large enough to make nonaxial deformations of multipolarity $\lambda \ge 3$ less important. One has to check this assumption afterwards and separately treat nuclei in which the inclusion of nonaxial deformations with $\lambda \ge 4$ is necessary.

Although, as mentioned before, in SH nuclei the second barriers at large deformations are usually smaller than the first one or do not exist at all, for Z = 98-101 the mesh (4) was extended to $\beta_{20} = 1.5$ and the second saddles were searched for by the IWF technique. It turned out that they are indeed mostly lower than the first ones and their heights decrease with increasing Z. Only in Cf isotopes with N = 134-160 were there some second saddles (at $\beta_{20} \approx 0.9$) higher than the

first one by at most 0.5 MeV. However, even those saddles were lowered by at least 1 MeV after including the mass asymmetry. Therefore, we have reason to believe that the range of β_{20} in Eq. (4) is sufficient for determining the height of the fission barrier in the whole studied region.

III. RESULTS AND DISCUSSION

In the present paper we have systematically calculated fission barrier heights B_f as the energy difference between the saddle point and the ground state. The saddle point is defined as the minimum over possible fission paths of the maximal energy along the path. Let us emphasize that the calculations presented here have been performed without adding any zero-point vibration energy. We included 1305 heavy and superheavy nuclei with proton numbers $98 \le Z \le 126$ and neutron numbers in the range $134 \le N \le 192$, with the smallest *N* for a given *Z* increasing by one with every step in *Z*. All obtained barriers have been collected in Table III. On all PESs presented here, energy is normalized in such a way that its macroscopic part is set to zero at the spherical shape.

A. Potential-energy surfaces

Some idea about the ground-state deformations, secondary minima, and saddles may be gained from the PESs. Chosen examples are shown in figures for 252 Lr (Fig. 1), 270 Db (Fig. 2), 276 Mt (Fig. 3), 280 Cn (Fig. 4), and 297 119 (Fig. 5). Overall evolution of ground-state shapes with increasing Z from prolate to spherical can be seen there. In some nuclei one can see multiple saddles of which the one defining the fission barrier should be properly chosen. Sometimes the saddles between competing minima can be important, therefore the determination of all saddles on the map is necessarily needed.

The energy landscapes (Figs. 1–5) were obtained by minimizing energy on the five-dimensional (5D) grid (4) with respect to β_{40} , β_{60} , and β_{80} . One should be aware



FIG. 1. Energy surface, $E - E_{\text{mac}}$ (sphere), for Z = 103 and N = 149.



FIG. 2. The same as in Fig. 1 but for Z = 105 and N = 165.

of two related circumstances: (1) As the grid (3) does not include nonaxial deformations $\lambda \ge 4$, the axial deformations $\lambda = 4, 6, 8$ with respect to the x axis cannot be reproduced, so the landscapes are inexact around the oblate $\gamma = 60^{\circ}$ axis. (2) A reduction of an *n*-dimensional grid of energy values via the minimization over n - 2 deformations sometimes leads to an energy surface composed from portions corresponding to minima which are disconnected in the auxiliary (those minimized over) dimensions. This can distort the picture of the barrier (actually, a reduction of multidimensional data to a two-dimensional map is a general problem).

With these reservations in mind, one can still explore some of the details shown in the maps. In particular, the prolate g.s. minimum with strongly nonaxial first saddle point at $\beta_{20} = 0.41$ and $\beta_{22} = 0.18$ is visible in ²⁵²Lr. One can notice that the axially symmetric saddle lies more than 2 MeV higher. A





FIG. 4. The same as in Fig. 1 but for Z = 112 and N = 168.

slightly wider, prolate g.s. minimum and an emerging second minimum are visible in Fig. 2 for ²⁷⁰Db. The triaxial saddle at $\beta_{20} = 0.52$ and $\beta_{22} = 0.13$ has a smaller triaxiality γ than the saddle in ²⁵²Lr. A decrease in barrier height due to triaxiality is ≈ 2 MeV; see Fig. 2.

In a heavier nucleus ²⁷⁶Mt, a prolate deformation of the g.s. is clearly smaller than in ²⁵²Lr; see Fig. 3. The second minimum, which was barely outlined in ²⁷⁰Db, is more pronounced here, giving the fission barrier a double-hump structure. The deformation $\beta_{20} \approx 0.5$ of the second saddle is much smaller than that of the second saddles in actinides. Thus, a two-peak structure of the barrier in SH nuclei may be viewed as a result of a division (split) of the first hump, occurring with growing Z. The higher second axial saddle is lowered by triaxiality by ≈ 1.5 MeV, but eventually is still higher than the first axial saddle.



FIG. 3. The same as in Fig. 1 but for Z = 109 and N = 167.



FIG. 5. The same as in Fig. 1 but for Z = 119 and N = 178.

For ²⁸⁰Ds, a topology of the PES is even more complicated. We see several minima: prolate—the g.s. and a superdeformed one—and a shallow oblate. The map also shows a few saddles. The axially deformed saddle point at $\beta_{20} = 0.3$ has a similar height as the nonaxial saddle at $\beta_{20} = 0.54$ and $\beta_{22} = 0.12$. It follows from the IWF calculation that the second fission saddle is nonaxial in this case. The axial second saddle is lowered by ≈ 1 MeV owing to the nonaxiality.

The nucleus Z = 119, N = 178 is spherical in its g.s.; see Fig. 5. There is a secondary oblate minimum (whose depth is underestimated in the map due to omission of nonaxial $\lambda = 4,6$ deformations). There is a low triaxial second saddle at $\beta_{20} \approx 0.5$ and two "first saddles" with different triaxiality, of which the one with a larger γ is the fission saddle.

Still another type of PES, typical of nuclei with the superdeformed oblate g.s., is presented in Fig. 8 in Sec. III.C.

B. Role of mass asymmetry

To study the effect of the reflection (mass) asymmetry on the fission saddles, a two-step procedure has been performed. At the first stage, we checked the stability of all the saddles found on the basic 5D mesh (the first, the second, ..., axially symmetric or triaxial, of energy within 0.5 MeV of the highest saddle) against the mass asymmetry. This was done by a threedimensional (3D) energy minimization with respect to β_{30} , β_{50} , and β_{70} around each saddle. Since most of the saddles are nonaxial, the most general version of our Woods–Saxon code had to be used. In this case, when both symmetries (axial and mass symmetry) are broken simultaneously, the nuclear shapes are defined by the following equation of the nuclear surface:

$$R(\vartheta,\varphi) = R_0 c(\{\beta\}) \left\{ 1 + \beta_{20} Y_{20} + \frac{\beta_{22}}{\sqrt{2}} [Y_{22} + Y_{2-2}] + \beta_{30} Y_{30} + \beta_{40} Y_{40} + \beta_{50} Y_{50} + \beta_{60} Y_{60} + \beta_{70} Y_{70} + \beta_{80} Y_{80} \right\}.$$
(5)

It turned out that this minimization lowers the energy of only those saddles in which: (i) there is no triaxiality, and (ii) deformation $\beta_{20} \approx 0.3$. This supports an often expressed conventional "wisdom" that the mass-asymmetry and triaxiality effects on the fission saddle are decoupled. This is why, at the second step of the procedure, we could carry out a full IWF analysis on a grid including only axially symmetric deformations: β_{20} , β_{30} , β_{40} , β_{50} , β_{60} , β_{70} , β_{80} , with β_{20} restricted to a quite short interval 0.25–0.40:

$$\beta_{20} = 0.25 (0.05) 0.40,$$

$$\beta_{30} = 0.00 (0.05) 0.25,$$

$$\beta_{40} = -0.15 (0.05) 0.20,$$

$$\beta_{50} = 0.00 (0.05) 0.15,$$

$$\beta_{60} = -0.10 (0.05) 0.10,$$

$$\beta_{70} = 0.00 (0.05) 0.15,$$

$$\beta_{80} = -0.10 (0.05) 0.10.$$

(6)

This seven-dimensional grid, composed of 76 800 deformations, was subject to the fivefold interpolation in all directions before it was used in the IWF procedure. This means that the IWF calculations have been performed on the grid containing 1 690 730 496(!) points. We have made such seven-dimensional analysis for more than 100 nuclei, for which the effect of minimization was greater than 300 keV. Results for these nuclei are shown in Table I. The rest of 127 cases shown in Table I are the test nuclei, in which the effect of the minimization was smaller than 0.3 MeV. The results for these additional nuclei allow us to appreciate whether the (in principle exact) IWF method could produce a greater effect that the (inexact) minimization.

As one can see, the adopted procedure allowed us to omit the problem of searching for a saddle by using the (inexact) minimization method which is not always reliable [8,13]. For example, for Z = 118 and N = 165, the discussed effect resulting from the minimization amounts to 0.44 MeV, which, just in this case, is quite similar to 0.46 MeV obtained from the IWF technique; however, in Z = 113 and N = 163 one obtains ≈ 0.5 MeV difference between saddles obtained by both methods. In this particular nucleus, the ≈ 0.77 MeV barrier lowering by the mass asymmetry is the largest among all studied nuclei. It should be also noted that, for the isotopes of Z = 113, the effect of the mass asymmetry is particularly large; see the the top panel in Fig. 6.

In the bottom panel of Fig. 6, we show the difference between the results of the both methods—the minimization (MIN) and imaginary water flow (IWF). One can see that this difference increases with the neutron number. In particular, there is practically no effect derived from the mass asymmetry in ²⁸¹113 when IWF is used. On the contrary, the approach based on minimization suggests still a quite substantial (spurious) effect (0.55 MeV). One might notice that our conclusion concerning decoupling of the variables describing the axial and reflection asymmetries is in a delicate contradiction with the studies [30].

C. Role of triaxiality

The importance of including triaxiality in a calculation of fission-barrier heights was indicated many times before [31–40]. In particular, it was shown that the effect of *both* quadrupole and a general hexadecapole nonaxiality, when accounted for within the *nonexact* method of constrained minimization (used generally in all self-consistent studies), may reach 2.5 MeV for some superheavy even-even nuclei; see Fig. 5 in Ref. [7]. Here, we extend our previous discussion of its role to the odd and odd-odd nuclei and, at the same time, improve the treatment by employing the exact IWF method in potentially most interesting cases.

By using the original 5D mesh (4) we obtained saddles with *quadrupole* nonaxiality for about 900 nuclei, what constitutes more than 70% of all cases. We illustrate this conspicuous effect in Fig. 7 on the example of two isotopic chains, Z = 103 and 113.

We show the difference between axial and nonaxial barriers in these nuclei. One can see that, for lighter lawrencium isotopes the effect of nonaxiality is quite considerable. Starting TABLE I. Mass-asymmetry (reflection-asymmetry) effect on the fission saddle from the minimization (MIN) and from the imaginary water flow method (IWF), in MeV.

N	IWF	MIN	Ν	IWF	MIN	Ν	IWF	MIN
	Z = 109			Z = 114			Z = 117	
157	0.39	0.81	155	0.28	0.59	157	0.24	0.34
158	0.22	0.42	156	0.14	< 0.30	158	0.28	< 0.30
159	0.54	0.45	157	0.72	0.83	159	0.24	0.34
160	0.31	0.54	158	0.46	0.46	160	0.12	< 0.30
	$\mathbf{Z} = 110$		159	0.67	0.68	161	0.26	< 0.30
157	0.41	0.69	160	0.45	0.66	165	0.36	0.39
158	0.19	0.31	161	0.53	0.79	166	0.23	< 0.30
159	0.52	0.46	162	0.42	0.64	167	0.19	0.50
160	0.50	0.40	163	0.58	0.65	168	0.07	< 0.30
161	0.43	0.47	164	0.40	0.63	169	0.05	0.37
162	0.35	0.31	165	0.42	0.65		$\mathbf{Z} = 118$	
	$\mathbf{Z} = 111$		166	0.38	0.53	163	0.30	0.32
157	0.49	0.97	167	0.11	0.68	164	0.23	< 0.30
158	0.36	0.78	168	0.06	0.41	165	0.46	0.44
159	0.61	0.83		Z = 115		166	0.28	0.31
160	0.67	0.85	157	0.28	0.64	167	0.20	0.63
161	0.87	0.89	158	0.25	0.50	168	0.15	0.39
162	0.66	0.80	159	0.34	0.49		Z = 119	
163	0.56	0.83	160	0.39	0.38	165	0.46	0.57
164	0.58	0.68	161	0.56	0.58	166	0.33	0.37
166	0.48	0.49	162	0.42	0.39	167	0.34	0.49
	Z = 112		163	0.46	0.54	168	0.27	0.32
157	0.57	0.83	164	0.49	0.45	169	0.31	0.57
158	0.32	0.45	165	0.47	0.60	170	0.24	0.38
159	0.58	0.55	166	0.53	0.54	171	0.23	0.32
160	0.60	0.49	167	0.42	0.80		Z = 120	
161	0.51	0.60	168	0.20	0.55	165	0.39	0.38
162	0.53	0.48	169	0.13	0.31	166	0.17	< 0.30
163	0.56	0.64	170	0.07	0.30	167	0.20	0.49
164	0.44	0.43		Z = 116		168	0.15	< 0.30
165	0.33	0.48	155	0.40	0.41	169	0.10	0.46
166	0.34	0.34	156	0.19	< 0.30		Z = 121	
167	0.20	0.35	157	0.36	0.52	165	0.25	0.40
	$\mathbf{Z} = 113$		158	0.26	0.34	166	0.23	< 0.30
155	0.14	0.49	159	0.35	0.44	167	0.38	0.52
156	0.24	0.34	160	0.28	0.49	168	0.31	0.34
157	0.80	0.98	161	0.40	0.44	169	0.36	0.60
158	0.50	0.75	162	0.33	0.37	170	0.30	0.43
159	0.56	0.91	163	0.48	0.54		$\mathbf{Z} = 122$	
160	0.61	0.88	164	0.40	0.38	164	0.00	< 0.30
161	0.72	1.06	165	0.46	0.50	165	0.21	< 0.30
162	0.57	0.93	166	0.33	0.40	166	0.12	< 0.30
163	0.76	1.25	167	0.30	0.38	167	0.19	0.31
164	0.49	0.89	168	0.11	< 0.30	168	0.11	< 0.30
165	0.54	0.98	169	0.09	0.32	169	0.10	0.45
166	0.40	0.86					Z = 123	
167	0.19	0.78				166	0.06	< 0.30
168	0.10	0.55				167	0.08	0.35
							Z = 124	
						165	0.23	0.31
						166	0.06	< 0.30
						167	0.10	0.32



FIG. 6. (top panel) The fission-saddle lowering by the mass asymmetry obtained by the (in principle exact) imaginary water flow method (IWF) and by the (easier, but sometimes misleading) minimization method (MIN). (bottom panel) The difference between both methods in MeV (in principle, the error in the saddle energy due to the minimization method).

with N = 164, it is weakening quickly and finally vanishes for $N \ge 176$. Somewhat different dependence of the effect on the neutron number occurs in Z = 113 isotopes. The maximum lowering of the barrier of more than 1.5 MeV occurs for $N \approx 165$, there is a second maximum at N = 179, and the effect becomes large again at N = 192. For $N \approx 154$ and



FIG. 7. Effect of the nonaxiality on the saddle energy (see text for further explanations).

 $N \approx 174$, there is no effect at all. Thus, the effect of nonaxiality has to be studied carefully, indeed.

Another task is to consider the influence of the hexadecapole nonaxiality; namely, β_{42} , β_{44} in Eq. (1), on the fission barriers. The unconstrained inclusion of these shapes would lead to a seven-dimensional (7D) grid which is too much for now. To evaluate the effect without increasing the grid dimension, we constrained β_{42} and β_{44} to be functions of the quadrupole nonaxial deformation β_{22} , or actually γ , and β_{40} , in a well-known manner [41]. By using the conventional notation

$$\beta = \sqrt{\beta_{20}^2 + \beta_{22}^2},$$

$$\gamma = \operatorname{arctg} \frac{\beta_{22}}{\beta_{20}},$$
(7)

the following form of Eq. (1) was used:

$$R(\vartheta,\varphi) = c(\beta)R_0 \left\{ 1 + \beta \cos(\gamma)Y_{20} + \frac{\beta \sin(\gamma)}{\sqrt{2}} [Y_{22} + Y_{2-2}] + \beta_{40}\frac{1}{6} [5\cos^2(\gamma) + 1]Y_{40} - \beta_{40}\frac{1}{6}\sqrt{\frac{15}{2}}\sin(2\gamma)[Y_{42} + Y_{4-2}] + \beta_{40}\frac{1}{6}\sqrt{\frac{35}{2}}\sin^2(\gamma)[Y_{44} + Y_{4-4}] + \beta_{60}Y_{60} + \beta_{80}Y_{80} \right\}.$$
(8)

On this 5D grid, the hexadecapole nonaxiality (but not the β_{60} and β_{80} terms) preserves the modulo-60° invariance in γ so, in particular, the parameter β_{40} describes a deformation which is axially symmetric around the *z* axis at $\gamma = 0^{\circ}$ and around the *x* axis at $\gamma = 60^{\circ}$, which allows us to better approximate energy at oblate shapes. For this reason, while the original mesh (3) may be expected more reliable for barriers at small γ , the one of Eq. (8) is better for saddles closer to $\gamma = 60^{\circ}$, like those in nuclei with well- or superdeformed oblate ground states.

Our method of proceeding is analogous to that used in the study of the mass asymmetry. The difference is that we do not have to perform the first step: a minimization with respect to β_{42} and β_{44} at the saddles found from the grid (3). Such calculations were already done in the previous studies of the effect of nonaxial deformations of higher multipolarity on the fission barrier in heaviest nuclei [40,42–44]. We know that the minimization gave the largest effect in the following four regions of nuclei, see Fig. 2 in Ref. [44]: (I) $Z \approx 122$, $N \approx 160$: up to 1.5 MeV, and a ~3 times smaller effect for nuclei with larger N and Z > 120; (II) $Z \approx 110$, $N \approx 146$: up to 1 MeV; (III) $Z \approx 114$, $N \approx 184$: up to 1 MeV; and (IV) $Z \approx 104$, $N \approx 170$; up to 0.4 MeV.

By applying the IWF method on the mesh (8) we found the saddles for a dozen of nuclei from the last three regions, for which the effect of the minimization was the largest. It turned out that, compared with saddles found on the original grid (3), they were lowered by less than 150 keV in region (II), by less then 100 keV in region (III), and even increased by ~ 100 keV



FIG. 8. Energy surface, $E - E_{\text{mac}}$ (sphere), for the nucleus Z = 122, N = 163, resulting from the calculation according to Eq. (8).

in region (IV). On this basis we conclude that the lowering of the fission saddles found by the minimization in Refs. [7,40] in these three regions is in a large measure a spurious effect which mostly vanishes when saddles are fixed by a proper method.

On the contrary, the substantial effect (up to ≈ 1 MeV) of the nonaxial hexadecapole in the region (I), although smaller than found by the minimization, survives in the exact IWF treatment. This might be expected because these are very heavy $Z \ge 119$ nuclei with short barriers and oblate (also superdeformed) ground states, so β_{42} and β_{44} are necessary to reproduce energy in the vicinity of the oblate axis. Therefore, in the whole region of nuclei with $Z \ge 118$ we calculated triaxial saddles by the IWF method by using the mesh (8) and then selected the proper fission barriers from two 5D calculations.

Three types of saddles in nuclei from the region (I) are shown for a very heavy and exotic nucleus $^{285}122$ in Fig. 8. The landscape was created from the 5D mesh Eq. (8).

This nucleus has a global superdeformed oblate (SDO) minimum with the quadrupole deformation $\beta_{20} = -0.455$ (spheroid with the axis ratio $\approx 3:2$). Such ground states are typical in the neutron-deficient area of superheavy nuclei according to recent predictions [45]. These intriguing SDO minima were already reproduced by various self-consistent models [46,47]. There is a saddle close to the oblate axis, separating the SDO g.s. from the wide minimum near the spherical shape-type (a); the axially symmetric saddle is designated as (b). One fission path may go through the saddles (a) and (b), the higher of which would define the barrier along this path. The second fission path goes through a triaxial saddle of type (c) at $\beta_{20} \approx 0.4$, $\gamma \approx 35^{\circ}$. The fission barrier of $B_f = 3.6$ MeV corresponds to saddle (c) as found by using the grid (8). It turns out that saddles of types (a) and (c) are much lowered by including β_{42} , β_{44} ; the first usually more than the second.

Table II summarizes the effect of the nonaxial hexadecapoles on the barriers in the region (I). It contains 75 nuclei

TABLE II. The lowering of the saddle (greater than 0.3 MeV) by the nonaxial hexadecapole deformation in nuclei $Z \ge 118$, in particular in those with SDO ground states, from the IWF calculations on the 5D mesh including β_{42} and β_{44} according to Eq. (8). Also reported is the associated change in the saddle type (for a description of saddle types see text); no entry means that a (c)-type saddle results from both grids (3) and (8).

Ν	ΔB_f	Saddle	Ν	ΔB_f	Saddle	Ν	ΔB_f	Saddle
	$\mathbf{Z} = 1$	19		$\mathbf{Z} = 1$	22		$\mathbf{Z} = 1$	25
155	0.597		158	0.779		161	1.083	
156	0.482		159	0.959		162	0.958	
157	0.472		160	0.807		163	1.167	
158	0.566		161	0.731		164	0.936	
159	0.585		162	0.690		165	0.439	$a \rightarrow c$
160	0.508		163	0.469	$a \rightarrow c$	166	0.806	$b \to c$
161	0.315	$b \rightarrow c$	164	0.364	$b \rightarrow c$	167	0.806	
162	0.471	a ightarrow c	169	0.403	$b \rightarrow c$	168	0.800	
170	0.343	$b \rightarrow c$	170	0.365		169	0.714	
172	0.480	$b \rightarrow c$		$\mathbf{Z} = 1$	23	170	0.551	
173	0.501		159	0.831			$\mathbf{Z} = 1$	26
174	0.400		160	0.821		162	0.995	
	$\mathbf{Z} = 1$	20	161	0.863		163	1.099	
156	0.613		162	0.924		164	1.034	
157	0.731		163	0.496	$a \rightarrow c$	165	0.802	
158	0.652		164	0.480	$a \rightarrow c$	166	0.912	
159	0.778		168	0.357	$b \rightarrow c$	167	0.807	
160	0.696		169	0.300	$b \rightarrow c$	168	0.845	
161	0.658			$\mathbf{Z} = 1\mathbf{Z}$	24	169	0.911	
162	0.581	a ightarrow c	160	0.819		170	0.735	
163	0.323	$a \rightarrow b$	161	0.868		171	0.534	
	$\mathbf{Z} = 1$	21	162	0.896		172	0.434	
157	0.747		163	0.741				
158	0.774		164	0.739	$\mathbf{a} \rightarrow \mathbf{c}$			
159	0.690		165	0.333	$b \rightarrow c$			
160	0.830		166	0.334	$b \to c$			
161	0.688		167	0.455	$b \to c$			
162	0.633	$b \to c$	168	0.519	$b \to c$			
			169	0.459				
			170	0.328				

in which the barrier lowering is greater than 300 keV. The most frequent saddle type in region (I), on both grids, is (c), but there are also more complicated cases in which the saddle type changes when β_{42} and β_{44} are included. The largest effect of 1.167 MeV occurs in the nucleus Z = 125, N = 163.

Let us remark that the difference between the results of the constrained minimization and the IWF method for the nonaxial hexadecapole is the main source of the discrepancy between the current fission barriers and those published in Ref. [7] for even-even nuclei.

D. Isotopic dependence

Calculated fission barriers given in Table III are illustrated along isotopic chains in Figures 9–18. Generally, it can be

TABLE III. Calculated fission-barrier heights (in MeV).

N	Α	B_f	N	Α	B_f	N	Α	B_f	N	Α	B_f	N	Α	B_f
	Z = 98			Z = 99			Z = 100)		Z = 101			Z = 102	
134	232	2.28												
135	233	2.74	135	234	2.82									
136	234	2.83	136	235	3.30	136	236	2.62						
137	235	3.45	137	236	4.18	137	237	3.30	137	238	3.29			
138	236	3.62	138	237	4.37	138	238	3.58	138	239	3.33	138	240	2.87
139	237	4.64	139	238	5.32	139	239	4.64	139	240	4.13	139	241	3.81
140	238	4.78	140	239	5.23	140	240	4.61	140	241	4.05	140	242	3.63
141	239	5.86	141	240	6.14	141	241	5.60	141	242	4.94	141	243	4.47
142	240	5.90	142	241	6.01	142	242	5.38	142	243	4.85	142	244	4.42
143	241	6.71	143	242	7.01	143	243	6.23	143	244	5.70	143	245	5.18
144	242	6.61	144	243	6.72	144	244	6.07	144	245	5.59	144	246	5.10
145	243	7.35	145	244	7.72	145	245	7.09	145	246	6.48	145	247	5.90
146	244	6.88	146	245	7.25	146	246	6.61	146	247	6.23	146	248	5.66
147	245	7.41	147	246	7.99	147	247	7.32	147	248	6.94	147	249	6.39
148	246	6.86	148	247	7.50	148	248	6.89	148	249	6.72	148	250	6.14
149	247	7.08	149	248	7.87	149	249	7.40	149	250	7.45	149	251	6.92
150	248	6.79	150	249	7.53	150	250	6.99	150	251	7.09	150	252	6.59
151	249	7.36	151	250	8.06	151	251	7.60	151	252	7.91	151	253	7.42
152	250	6.67	152	251	7.42	152	252	6.98	152	253	7.38	152	254	6.88
153	251	6.26	153	252	6.95	153	253	6.55	153	254	7.03	153	255	6.53
154	252	5.98	154	253	6.66	154	254	6.21	154	255	6.69	154	256	6.23
155	253	5.62	155	254	5.88	155	255	5.71	155	256	6.06	155	257	5.81
156	254	5.19	156	255	5.69	156	256	5.40	156	257	5.82	156	258	5.46
157	255	5.00	157	256	5.32	157	257	5.14	157	258	5.77	157	259	5.59
158	256	4.73	158	257	5.04	158	258	4.82	158	259	5.36	158	260	5.15
159	257	4.99	159	258	5.26	159	259	5.08	159	260	5.30	159	261	5.30
160	258	4.48	160	259	4.63	160	260	4.56	160	261	4.95	160	262	5.02
161	259	5.06	161	260	5 19	161	261	5 17	161	262	5.61	161	263	5 46
162	260	4.60	162	261	4.71	162	262	4.74	162	263	5.23	162	264	4.96
163	261	4 4 1	163	262	4 58	163	263	4 54	163	264	4 97	163	265	4 71
164	262	4 10	164	263	4 20	164	263	4 14	163	265	4 56	164	266	4 29
165	262	3.97	165	263	3 99	165	265	3.85	165	266	4 15	165	267	3.86
166	263	3 71	166	265	3 78	165	265	3.62	165	267	3.92	166	268	3.69
167	265	3 71	167	265	3.65	167	267	3.51	167	268	3.64	167	260	3 52
168	265	3.62	168	267	3.50	168	268	3 38	168	269	3 55	168	270	3 27
169	267	4 38	160	268	3.78	169	260	3.84	169	270	3.69	169	270	3.51
170	267	3.85	170	260	3 52	170	20)	3.43	170	270	3 35	170	271	3 10
171	260	4 81	170	20)	4 20	170	270	4 36	170	271	3.92	170	272	3.03
172	20)	4.01	172	270	3 79	172	271	3.94	172	272	3.50	172	273	3 46
172	270	5 13	172	271	4 46	172	272	4.62	172	273	4 31	172	274	4 08
174	271	5.13	173	272	1 31	174	273	4.02	173	274	3 00	174	275	3.01
175	272	6.00	174	273	5.18	174	274	5 37	174	275	1.99	174	270	1 72
176	273	5 58	175	274	1 80	175	275	5.01	175	270	4.60	175	277	4.72
177	274	6.63	170	275	4 .09	170	270	6.01	170	277	1 .00	170	270	5 41
178	275	6.17	179	270	5.41	178	277	5.52	179	270	5.04	178	219	1 86
170	270	672	170	277	5.41 6.02	170	270	5.00	170	219	5.04	170	200	4.00
19	277	6.40	1/9	270	0.03 5.72	1/9	219	5.99	1/9	200	5.45	1/9	201	5.57
100	270	7.95	100	219	5.75	100	200	5.00	100	201	5.10	100	202	5.04
101	219	6.02	101	20U 201	5 00	101	201	5.06	101	202 282	5.71	101	203 281	5 21
102	200	0.93 7 45	102	201	J.99 6 60	102	202	J.90 6.65	102	203	5.15	102	204	2.51
185	281	7.05	185	282	0.08	183	283	0.05	185	284	5.95	185	283	0.11
184	282	1.14	184	283	0.19	184	284	0.1/	184	283	5.30	184	280	5.48
100	283	5.15	185	284	4.19	185	283	4./0	185	280	4.29	185	287	4.29
180	284	5.43	180	285	4.54	180	286	4.4/	180	287	4.02	180	288	3.97
18/	285	4.59	187	286	3.76	18/	287	3.60	18/	288	3.38	18/	289	3.20
188	286	4.00	188	287	3.30	188	288	3.09	188	289	3.00	188	290	2.73
189	287	4.13	189	288	3.30	189	289	3.10	189	290	2.88	189	291	2.48

TABLE III. (Continued.)

N	Α	B_f	N	Α	B_f	N	Α	B_f	N	Α	B_{f}	N	Α	B_f
190	288	3.52	190	289	2.79	190	290	2.48	190	291	2.42	190	292	2.09
191	289	3.53	191	290	2.69	191	291	2.57	191	292	2.64	191	293	2.24
192	290	3.08	192	291	2.17	192	292	2.05	192	293	2.13	192	294	1.73
	$\mathbf{Z} = 103$			Z = 104			Z = 105	i		$\mathbf{Z} = 106$	j		Z = 107	
139	242	3.13												
140	243	3.14	140	244	2.69									
141	244	4.01	141	245	3.58	141	246	2.89	1.40	240	2.44			
142	245	3.92	142	246	3.46	142	247	3.09	142	248	2.66	142	250	2 20
145	240	4.55	145	247	4.10	145	248	3.// 2.75	145	249	3.37 2.25	145	250	3.30 2.21
144	247	4.00	144	240 240	4.15	144	249	5.75	144	250	5.55 4 21	144	251	3.31
145	248	5.19	145	249	4.95	145	251	4.08	145	252	4.21	145	252	4.17
147	250	6.10	147	250	5.47	147	252	5.57	147	252	5.01	147	253	5.19
148	251	5.79	148	252	5.36	148	253	5.62	148	254	4.98	148	255	5.08
149	252	6.54	149	253	6.16	149	254	6.77	149	255	5.98	149	256	6.22
150	253	6.28	150	254	5.93	150	255	6.43	150	256	5.76	150	257	5.92
151	254	7.26	151	255	6.93	151	256	7.50	151	257	6.85	151	258	7.17
152	255	6.81	152	256	6.44	152	257	7.04	152	258	6.37	152	259	6.70
153	256	6.62	153	257	6.36	153	258	7.18	153	259	6.58	153	260	6.83
154	257	6.45	154	258	6.11	154	259	6.99	154	260	6.49	154	261	6.70
155	258	6.49	155	259	6.14	155	260	7.18	155	261	6.61	155	262	6.69
156	259	6.30	156	260	5.96	156	261	6.82	156	262	6.30	156	263	6.53
157	260	6.33	157	261	6.01	157	262	6.84	157	263	6.37	157	264	6.74
158	261	6.10	158	262	5.73	158	263	6.56	158	264	6.03	158	265	6.44
159	262	6.15	159	263	5.68	159	264	6.53	159	265	5.97	159	266	6.92
160	263	5.89	160	264	5.45	160	265	6.31	160	266	5.83	160	267	0.72
162	204	0.50 5.83	162	205	5.91	162	200	0.85 6.40	162	267	0.45 5.05	162	208	7.00
162	205	5.05	162	200	5.40	162	267	5.90	162	208	5.60	162	209	6.95
164	200	4.83	164	267	2.14 4.59	164	269	5 37	165	209	5.09	164	270	6.27
165	268	4.17	165	269	4.13	165	270	4.71	165	271	4.50	165	272	5.61
166	269	3.97	166	270	3.85	166	271	4.43	166	272	4.17	166	273	5.30
167	270	3.82	167	271	3.67	167	272	4.00	167	273	3.85	167	274	4.67
168	271	3.41	168	272	3.33	168	273	3.70	168	274	3.54	168	275	4.38
169	272	3.52	169	273	3.44	169	274	3.67	169	275	3.44	169	276	3.93
170	273	3.19	170	274	3.12	170	275	3.37	170	276	3.20	170	277	3.72
171	274	3.68	171	275	3.65	171	276	3.81	171	277	3.56	171	278	4.11
172	275	3.30	172	276	3.20	172	277	3.36	172	278	3.24	172	279	3.70
173	276	4.07	173	277	3.83	173	278	4.08	173	279	3.89	173	280	4.33
174	277	3.67	174	278	3.48	174	279	3.72	174	280	3.55	174	281	4.10
175	278	4.55	175	279	4.55	175	280	4.73	175	281	4.71	175	282	5.15
176	279	4.00	176	280	4.12	176	281	4.10	176	282	4.15	176	283	4.64
1//	280	4.97	1//	281	5.24	1//	282	5.03	1//	283	5.29	1//	284	5.27
170	281	4.40	1/8	282	4.//	1/8	283	4.51	1/8	284	4.78	1/8	285	4.05
1/9	202	J.01 4.68	179	203	J.19 1 80	1/9	204	5.25 4.75	1/9	285	5.20	1/9	280	J.49 1 00
181	285	4.00 5.62	180	285	1 .09 5.69	180	285	5 71	180	280	5.00	180	287	+.99 5 84
182	285	5.02	182	285	5.09	182	280	5.13	182	287	5.05	182	288	5.04
183	286	5.91	183	287	5.89	183	288	5.87	183	289	6.01	183	290	6.13
184	287	5.31	184	288	5.36	184	289	5.34	184	290	5.41	184	291	5.52
185	288	4.38	185	289	4.27	185	290	4.32	185	291	4.26	185	292	4.25
186	289	4.17	186	290	4.01	186	291	4.11	186	292	4.11	186	293	4.26
187	290	2.74	187	291	3.05	187	292	3.24	187	293	2.99	187	294	3.19
188	291	2.76	188	292	2.57	188	293	2.83	188	294	2.67	188	295	2.91
189	292	2.44	189	293	2.23	189	294	2.18	189	295	1.88	189	296	1.86
190	293	2.20	190	294	1.81	190	295	1.92	190	296	1.56	190	297	1.61
191	294	2.21	191	295	1.89	191	296	1.73	191	297	1.48	191	298	1.40

N	Α	B_f	Ν	Α	B_f	Ν	A	B_f	N	A	B_f	Ν	Α	B_f
192	295 Z = 108	1.70	192	296 Z = 109	1.44	192	297 Z = 110	1.37	192	298 $\mathbf{Z} = 111$	1.12	192	299 Z = 112	1.06
144	252	2.72												
145	253	3.49	145	254	2.72									
146	254	3.58	146	255	3.06	146	256	2.47						
147	255	4.50	147	256	3.71	147	257	3.29	147	258	2.60			
148	256	4.48	148	257	3.70	148	258	3.32	148	259	2.50	148	260	2.21
149	257	5.60	149	258	4.88	149	259	4.26	149	260	3.33	149	261	2.96
150	258	5.29	150	259	4.53	150	260	4.05	150	261	3.27	150	262	2.77
151	259	6.40 5.09	151	260	5.55	151	261	5.12	151	262	4.10	151	263	3.92
152	200	5.98	152	201	5.17	152	262	4.08	152	203	3.07	152	204	3.47
155	201	6.07	153	262	3.00 4.07	153	203	4.08	153	204	3.75	155	203	3.40
155	263	6.07	155	263 264	5.01	154	265	4 50	155	265	3.65	155	267	3 22
156	263	5.93	155	265	4 92	155	265	4 39	155	267	3 74	155	268	3.26
157	265	6.09	157	266	5.29	157	267	4.50	157	268	3.65	157	269	3.21
158	266	5.83	158	267	5.11	158	268	4.38	158	269	3.68	158	270	3.31
159	267	6.19	159	268	5.85	159	269	5.04	159	270	4.52	159	271	3.98
160	268	5.93	160	269	5.65	160	270	4.86	160	271	4.26	160	272	3.78
161	269	6.87	161	270	6.72	161	271	5.91	161	272	5.58	161	273	5.02
162	270	6.46	162	271	6.44	162	272	5.62	162	273	5.30	162	274	4.72
163	271	6.28	163	272	6.48	163	273	5.85	163	274	5.70	163	275	5.00
164	272	5.52	164	273	5.85	164	274	5.22	164	275	5.03	164	276	4.46
165	273	5.00	165	274	5.56	165	275	4.87	165	276	5.05	165	277	4.46
166	274	4.62	166	275	5.14	166	276	4.47	166	277	4.62	166	278	4.01
167	275	4.16	167	276	4.90	167	277	4.16	167	278	4.61	167	279	3.99
168	276	3.80	168	277	4.45	168	278	3.73	168	279	4.13	168	280	3.78
169	277	3.40	169	278	4.14	169	279	3.44	169	280	4.35	169	281	3.88
170	278	3.20	170	279	3.84	170	280	3.29	170	281	4.19	170	282	3.74
171	279	5.60 3.31	171	280	4.09	171	201	5.95 3.72	171	282	4.74	171	283	4.30
172	280	4 20	172	281	3.87 4.55	172	282	5.72 4.68	172	285	4.07 5.32	172	285	5 26
174	282	3.88	174	283	4 22	174	284	4 40	173	285	5.07	173	286	5.03
175	283	5.00	175	283	5.37	175	285	5.51	175	286	5.83	175	287	6.04
176	284	4.50	176	285	4.91	176	286	5.04	176	287	5.37	176	288	5.60
177	285	5.43	177	286	5.74	177	287	5.86	177	288	6.39	177	289	6.29
178	286	4.93	178	287	5.17	178	288	5.33	178	289	5.93	178	290	5.87
179	287	5.61	179	288	6.03	179	289	5.96	179	290	6.60	179	291	6.32
180	288	5.29	180	289	5.66	180	290	5.61	180	291	6.23	180	292	5.94
181	289	6.06	181	290	6.19	181	291	6.12	181	292	6.59	181	293	6.29
182	290	5.47	182	291	5.70	182	292	5.63	182	293	6.18	182	294	5.89
183	291	6.05	183	292	6.46	183	293	6.20	183	294	6.75	183	295	6.48
184	292	5.61	184	293	5.95	184	294	5.68	184	295	6.20	184	296	5.91
185	293	4.20	185	294	4.51	185	295	4.38	185	296	4.79	185	297	4.54
186	294	4.23	186	295	4.68	186	296	4.50	186	297	5.04	186	298	4.74
187	295	3.04	187	296	3.09	187	297	3.07	187	298	3.73	187	299	3.39
188	296	2.83	188	297	3.11	188	298	3.01	188	299	3.76	188	300	3.44
189	297	1.75	189	298	1.80	189	299	1.79	189	300	2.20	189	301	1.92
190	298	1.44	190	299	1.74	190	201	1.58	190	301	2.28	190	302	2.02
191	299	0.75	191	300	1.21	191	302	1.28	191	302	1.05	191	303	1.07
192	Z = 113	0.75	192	Z = 114	0.74	192	Z = 115	0.70	192	Z = 116	0.99	192	Z = 117	0.70
149	262	2.02												
150	263	2.02	150	264	1.72									
151	264	2.95	151	265	2.75	151	266	1.54						
152	265	2.44	152	266	2.27	152	267	1.17	152	268	1.08			
153	266	2.33	153	267	2.15	153	268	0.90	153	269	0.96	153	270	0.76

TABLE III. (Continued.)

TABLE III. (Continued.)

Ν	A	B_f	Ν	A	B_f	Ν	A	B_f	Ν	A	B_f	Ν	Α	B_f
154	267	2.25	154	268	2.14	154	269	1.34	154	270	1.01	154	271	0.87
155	268	2.44	155	269	2.13	155	270	2.14	155	271	1.39	155	272	1.93
156	269	2.34	156	270	2.27	156	271	2.29	156	272	1.72	156	273	1.99
157	270	2.55	157	271	2.36	157	272	2.81	157	273	2.24	157	274	2.58
158	271	2.66	158	272	2.50	158	273	2.89	158	274	2.37	158	275	2.91
159	272	3.65	159	273	3.25	159	274	3.67	159	275	3.13	159	276	3.33
160	273	3.45	160	274	3.39	160	275	3.81	160	276	3.27	160	277	3.69
161	274	4.58	161	275	4.53	161	276	4.88	161	277	4.45	161	278	4.74
162	275	4.41	162	276	4.35	162	277	4.68	162	278	4.18	162	279	4.35
163	276	4.88	163	277	4.75	163	278	5.30	163	279	4.//	163	280	5.10
164	277	4.44	164	278	4.32	164	279	4.79	164	280	4.34	164	281	4.60
165	270	4.38	105	279	4.29	165	260	4.07	105	201	4.50	105	282	4.47
167	279	4.25	167	280	5.99 1 37	167	201	4.30	167	282	4.10	167	205	4.33
168	280	4.07	168	281	4.57	168	282	4.90	168	285	4.52	168	285	4.77
169	281	4.34	169	282	4.03	169	285	5 29	169	285	4.40	160	285	5 23
170	282	4 46	170	285	4.32	170	285	4.98	170	286	4.05	170	287	5 30
171	284	5 19	171	285	5.16	171	286	5 70	171	287	5 76	171	288	6.21
172	285	4.98	172	286	4.83	172	287	5.56	172	288	5.45	172	289	5.95
173	286	5.74	173	287	5.76	173	288	6.21	173	289	6.18	173	290	6.81
174	287	5.54	174	288	5.52	174	289	6.02	174	290	5.93	174	291	6.46
175	288	6.43	175	289	6.43	175	290	6.68	175	291	6.67	175	292	7.04
176	289	6.28	176	290	6.04	176	291	6.55	176	292	6.31	176	293	6.56
177	290	6.95	177	291	6.67	177	292	7.46	177	293	6.82	177	294	7.31
178	291	6.61	178	292	6.58	178	293	6.80	178	294	6.37	178	295	6.64
179	292	7.26	179	293	6.75	179	294	7.08	179	295	6.64	179	296	6.88
180	293	6.82	180	294	6.45	180	295	6.69	180	296	6.25	180	297	6.32
181	294	6.93	181	295	6.64	181	296	7.00	181	297	6.51	181	298	6.70
182	295	6.71	182	296	6.29	182	297	6.48	182	298	6.10	182	299	6.12
183	296	7.13	183	297	6.58	183	298	6.75	183	299	6.35	183	300	6.32
184	297	6.63	184	298	6.10	184	299	6.23	184	300	5.84	184	301	5.81
185	298	5.36	185	299	4.72	185	300	4.97	185	301	4.39	185	302	4.27
186	299	5.43	186	300	4.92	186	301	5.01	186	302	4.64	186	303	4.61
187	300	4.11	187	301	3.52	187	302	3.85	187	303	3.27	187	304	3.32
188	301	4.14	188	302	3.66	188	303	3.74	188	304	3.40	188	305	3.34
189	302	2.67	189	303	2.26	189	304	2.53	189	305	2.04	189	306	2.28
190	303	2.70	190	304	2.36	190	305	2.34	190	306	2.16	190	307	2.07
191	304	1.30	191	305	0.78	191	306	1.53	191	307	0.90	191	308	1.25
192	305	1.28	192	306	0.91	192	307	1.23	192	308	0.75	192	309	1.18
	L = 118			L = 119			L = 120			L = 121			L = 122	
154	272	0.66												
155	273	1.39	155	274	1.82									
156	274	1.41	156	275	1.83	156	276	1.38						
157	275	2.30	157	276	2.26	157	277	1.79	157	278	1.96	1.50	• • • •	
158	276	2.25	158	277	2.25	158	278	1.88	158	279	2.11	158	280	1.47
159	277	3.06	159	278	2.78	159	279	2.39	159	280	2.72	159	281	1.94
160	278	3.15	160	279	2.79	160	280	2.44	160	281	2.75	160	282	2.15
161	279	4.30	161	280	3.49	161	281	3.23	161	282	3.66	161	283	3.07
162	280	3.94	162	281	3.27	162	282	3.07	162	283	5.50 4.56	162	284	2.94
103	201	4.32	103	282	3.90 2.40	103	283 201	5.89 2.57	103	284 285	4.30	103	283	3.88 2.41
164	282	4.15	164	205	5.08 2.97	165	204	2.57	165	285	4.10	104	280	5.01
165	203 281	3.19	165	∠04 285	3.67	165	20J 286	3.05	165	200 287	4.07	165	207 288	4.40
167	20 4 285	4 00	167	205 286	2.07 4.43	167	280 287	2.43 4.08	167	207	4.30 4.40	167	200 280	2.91 4.06
168	285	4.09	168	280	4 45	168	287	4 21	168	280	4 37	168	209	4.00
169	280	5.03	169	288	5 21	169	289	5.01	169	290	5 35	169	291	4 83
170	288	5.05	170	289	5.23	170	290	5.01	170	291	5.41	170	292	4.80
		2.00								- / -			_/_	

N	Α	B_f	Ν	Α	B_f									
171	289	6.03	171	290	6.26	171	291	6.08	171	292	6.56	171	293	5.96
172	290	5.75	172	291	5.75	172	292	5.48	172	293	5.90	172	294	5.36
173	291	6.40	173	292	6.55	173	293	6.06	173	294	6.15	173	295	5.54
174	292	6.09	174	293	6.21	174	294	5.62	174	295	5.89	174	296	5.28
175	293	6.62	1/5	294	6.95	1/5	295	6.28 5.70	1/5	296	6.00 5.60	1/5	297	5.48
170	294	6.09	170	295	6.32	1/0	296	5.79	1/0	297	5.69	1/0	298	5.10
170	295	6.04	170	290	6.71	1//	297	0.02 5.56	170	298	5.90	1//	299	J.30
170	290	6.12	170	297	6.20	1/8	298	5.50	170	299	5.38	1/8	201	4.80
100	297	0.21 5.70	1/9	298	0.20 5.70	1/9	299	5.09	1/9	201	J.38 4.82	1/9	202	4.73
100	298	5.79	100	299	5.12	180	201	5.08	100	202	4.82	180	302	4.20
101	299	5.52	101	300	J.00 5 38	101	301	J.24 4 71	101	302	4.99	101	303	4.45
102	201	5.52	102	202	5.50	102	202	4.71	102	204	4.37	102	205	2 70
105	301	5.71	105	302	1.08	183	303	4.01	105	304	4.27	105	305	3.10
104	302	3.20	104	303	4.90	104	304	4.50	104	305	2.04	104	300	2.10
185	303	J.95 4 03	185	304	3.82	185	305	3.02	185	300	2.90	185	307	2.27
187	305	2.80	187	305	2.05	187	307	2.17	187	307	2.00	187	300	2.00
188	305	2.80	187	307	2.78	187	307	1.05	187	300	2.13	188	310	1.00
180	307	2.78	180	308	2.03	180	300	1.95	180	310	1.04	180	311	1.30
100	308	1.70	100	300	2.05	100	310	1.31	100	311	1.50	100	312	1.51
190	300	0.79	190	310	1.57	190	311	1.59	190	312	1.45	190	313	0.68
192	310	0.75	191	311	1.67	192	312	1.05	192	313	1.20	192	314	0.00
172	Z = 123	0.00	172	Z = 124	1.05	172	Z = 125	1.05	172	Z = 126	1.20	172	514	0.00
159	282	2.14												
160	283	2.25	160	284	1.78									
161	284	3.01	161	285	2.51	161	286	2.47						
162	285	2.87	162	286	2.44	162	287	2.44	162	288	1.89			
163	286	4.03	163	287	3.46	163	288	3.18	163	289	2.64			
164	287	3.69	164	288	3.24	164	289	3.18	164	290	2.58			
165	288	4.75	165	289	4.43	165	290	4.43	165	291	3.85			
166	289	4.15	166	290	3.78	166	291	3.76	166	292	3.24			
167	290	4.43	167	291	4.08	167	292	4.14	167	293	3.69			
168	291	4.08	168	292	3.54	168	293	3.64	168	294	3.15			
169	292	5.10	169	293	4.44	169	294	4.34	169	295	3.48			
170	293	4.94	170	294	4.38	170	295	4.35	170	296	3.49			
171	294	5.96	171	295	5.44	171	296	5.47	171	297	4.62			
172	295	5.52	172	296	5.01	172	297	5.06	172	298	4.20			
173	296	5.52	173	297	5.10	173	298	5.30	173	299	4.84			
174	297	5.23	174	298	4.81	174	299	5.02	174	300	4.52			
175	298	5.16	175	299	4.82	175	300	5.13	175	301	4.65			
176	299	4.82	176	300	4.51	176	301	4.76	176	302	4.37			
177	300	5.26	177	301	4.92	177	302	5.14	177	303	4.75			
178	301	4.75	178	302	4.48	178	303	4.66	178	304	4.28			
179	302	4.83	179	303	4.55	179	304	4.68	179	305	4.33			
180	303	4.07	180	304	3.84	180	305	4.03	180	306	3.66			
181	304	3.90	181	305	3.39	181	306	3.45	181	307	2.96			
182	305	3.39	182	306	2.95	182	307	3.17	182	308	2.79			
183	306	3.54	183	307	2.78	183	308	3.02	183	309	2.21			
184	307	2.91	184	308	2.25	184	309	2.53	184	310	2.08			
185	308	2.20	185	309	2.07	185	310	2.40	185	311	2.05			
186	309	2.01	186	310	1.96	186	311	2.37	186	312	1.90			
187	310	1.89	187	311	1.69	187	312	1.90	187	313	1.39			
188	311	1.85	188	312	1.62	188	313	1.76	188	314	1.26			
189	312	1.47	189	313	1.16	189	314	1.36	189	315	0.90			
190	313	1.31	190	314	0.98	190	315	1.10	190	316	0.80			
191	314	0.90	191	315	0.68	191	316	0.91	191	317	0.81			
192	315	0.76	192	316	0.62	192	317	0.84	192	318	0.70			

8

7

6

З

2

136

144

152

B, [MeV]



160

Ν

168

Z=98

Z=99

Z=100

176

184

192

seen that: (i) in the whole region Z = 98-126 the fission barrier heights are limited by: $B_f \leq 8.06$ MeV; (ii) there are characteristic maxima of fission barriers at $Z \approx 100$, $N \approx 150$, near Z = 108, N = 162 (deformed magic shells) and Z = 114, N = 178 (not 184); high barriers occur also at the border of the studied region, for Z = 98, $N \approx 183$; (iii) over intervals of N where $B_f(N)$ increase or are on average constant, the fission barriers in a neighboring system $N_{\text{even}} + 1$ are higher than $B_f(N_{\text{even}})$; it may be the opposite over intervals where $B_f(N)$ strongly decrease; the same behavior can be seen when comparing barriers for isotones; see Fig. 20. This quite pronounced odd-even staggering in barriers is related to a decrease in the pairing gap due to blocking as will be discussed in the next section.

In the isotopic dependence of the fission barriers for Cf, Es, and Fm nuclei, shown in Fig. 9, there are two peaks of a similar size, at N = 152 and N = 184. The minima of $B_f(N)$ occur at $N \approx 170$. Odd-even staggering in B_f for Es is stronger around N = 152, while for Cf it is stronger near N = 184.



FIG. 11. The same as in Fig. 9 but for Z = 104, 105 and Z = 106.

For Md, No, and Lr isotopes (Fig. 10), the second maximum around N = 184 becomes lower. A maximum associated with the semimagic deformed shell at N = 162 appears. As before, the minima of $B_f(N)$ are located at $N \approx 170$. For Rf, Db, Sg, Bh, and Hs nuclei (Fig. 11 and 12), previously distinct maximum at N = 152 becomes more flat, and a kind of plateau forms between N = 152 and 162. For Mt isotopes this plateau changes into a local minimum in the isotopic dependence $B_f(N)$, located around N = 155. The highest barriers in Bh, Hs, and Mt isotopic sets occur at $N \approx 162$.

For Ds, Rg, and Cn nuclei (Fig. 13), with increasing proton number, the N = 184 spherical shell starts to dominate. However, not-much-lower barriers are obtained near the deformed gap N = 162.

For nuclei Z = Nh, Fl, Mc (Fig. 14), one can see one region with high barriers, around N = 180. One can notice that the maxima in $B_f(N)$ are already shifted toward N < 184. Slight residues of the formerly observed shells at N = 152 and N =162 can be spotted.



FIG. 10. The same as in Fig. 9 but for Z = 101, 102 and Z = 103.



FIG. 12. The same as in Fig. 9 but for Z = 107, 108 and Z = 109.



FIG. 13. The same as in Fig. 9 but for Z = 110, 111 and Z = 112.

For nuclei Z = Lv, Ts, Og (Fig. 15), the main maximum in B_f shifts further towards smaller N, reaching finally $N \approx 175$. The minima in $B_f(N)$, observed before at N = 172, gradually disappear. For nuclei Z = 119, Z = 120, Z = 121 (Fig. 16), the situation is similar to that described above. Barriers in nuclei Z = 122, 123, 124 (Fig. 17), compared with the previous set, are clearly lower. The maximum is even more shifted towards smaller N. For nuclei Z = 125, 126 (Fig. 18) the fission barriers are still lower. Their maxima occur at N = 171 and 173.

All calculated fission-barrier heights are collected and shown as a map $B_f(Z, N)$ in Fig. 19. One can see three areas with clearly raised barriers: around $N \approx 152$, N = 162, and $N \approx 180$, and the region of low barriers around N = 170, as discussed above. The effect of the odd particle, i.e., an often (but not always) higher barrier in a neighboring odd-particle system can also be seen in Fig. 19.





FIG. 15. The same as in Fig. 9 but for Z = 116, 117 and Z = 118.

E. Role of the pairing interaction and the odd-even barrier staggering

It is known that the blocking procedure often causes an excessive reduction of the pairing gap in systems with an odd particle number. This effect is much more pronounced in the g.s. than in the fission saddle, because the pairing gap is never small in the latter. One device to avoid an excessive even-odd staggering in nuclear binding was to assume a stronger (typically by $\sim 5\%$) pairing interaction for odd-particle-number systems; see Refs. [48–51]. Here, instead of performing another grid calculation with modified pairing strengths, we tested the magnitude of their effect on fission barriers by increasing them by 5% and 10% for odd particle numbers (neutrons or protons) at previously found ground states and saddle points. The results of this test are presented in Fig. 20 for the N = 169 isotones and in Fig. 21 for the Z = 109 isotopic chain.

Both the isotopic and isotonic dependence show that increasing the intensity of pairing leads to a reduction of



FIG. 14. The same as in Fig. 9 but for Z = 113, 114 and Z = 115.



FIG. 16. The same as in Fig. 9 but for Z = 119, 120 and Z = 121.



FIG. 17. The same as in Fig. 9 but for Z = 122, 123 and Z = 124.

the fission barrier by a variable amount. When the pairing strengths are increased by 5% for odd particle numbers, the fission barriers decrease in odd-even, even-odd, and odd-odd systems by up to 0.5 MeV; the 10% increase in the pairing strengths can decrease the barriers at most by about 1 MeV. The same pairing change leads to the suppression, and then the inversion of the staggering effect.

The even-odd barrier staggering related to pairing is convoluted with the isotopic or isotonic dependence related to the mean field. With the original pairing, when one separates a linear part of the latter by calculating: $B_f(Z_{odd}, N) - 1/2[B_f(Z_{odd} + 1, N) + B_f(Z_{odd} - 1, N)]$, and an analogous quantity for odd neutron numbers, one obtains numbers between 1.053 and -0.947 MeV, with the average of ≈ 0.22 MeV for protons and ≈ 0.26 MeV for neutrons. As shown by black points in Fig. 20 and 21, the effect is indeed irregular and, when present, typically at the level of several hundred keV.



FIG. 18. The same as in Fig. 9 but for Z = 125 and Z = 126.

The 5% increase in pairing for odd particle numbers reduces the staggering in N = 169 isotones and nearly cancels it in Z = 109 isotopes (red points in Figs. 20 and 21). The important point is that the 10% increase in pairing for an odd number of particles *inverts* the staggering, at least locally: near Z = 120 in N = 169 isotones and near N = 153, N = 162, and N = 180 in Mt isotopes (green points in Figs. 20 and 21).

Although the spontaneous fission rates of odd-particle number nuclei are smaller by 3-5 orders of magnitude than those of their even neighbors, the experimental fission barriers in actinides show only a moderate odd-even staggering, cf. Refs. [23,52]. Still, it is inconceivable that the fission barriers in odd-Z or odd-N systems should be on average smaller than in their even neighbors. This indicates that the 10% increase in pairing strengths in odd-N or odd-Z systems would be too large. A qualitative argument which follows is that, even if the blocking method overestimates the pairing decrease, the fission barriers of odd-Z or/and odd-N nuclei should fall in a strip between the black and red points in Figs. 20 and 21. Thus, the test of the pairing influence on barriers indicates that a possible overestimate of barriers in odd-A and odd-odd nuclei, induced by the blocking, should not be much larger than 0.5 MeV. One may add in this context that the barriers from the finite-range liquid drop model (FRLDM) do not show any even-odd staggering due to the way the pairing was included there.

F. Comparison with other theoretical calculations and some empirical data

Let us discuss the results in Table III in relation to available empirical data and to the other theoretical estimates.

As an empirical check of our model, one can use the barriers in the actinide region. We have reported quite a spectacular agreement of the calculated first [7] and second [8] fission barriers in even-even actinides with the data [23,52], with root mean square deviation 0.5 and 0.7 MeV, respectively.

The heaviest nucleus in which the fission barrier height has been measured recently is ²⁵⁴No. The value $B_f =$ 6.0 ± 0.5 MeV at spin 15 \hbar , giving by extrapolation $B_f =$ 6.6 ± 0.9 MeV at the spin 0 \hbar , has been deduced from the measured distribution of entry points in the excitation energy vs angular-momentum plane [53]. This result perfectly agrees with our evaluation: $B_f = 6.88$ MeV (at spin 0 \hbar) and with the MM model [54] which gives: $B_f = 6.76$ MeV. The self-consistent calculations, mainly based on the Skyrme interaction, overestimate this barrier significantly [37,55,56] (9.6 and 8.6 or 12.5 MeV, respectively). There are experimental estimates of barriers in a few SH nuclei, based on observed ER production probabilities [57], which again agree well with our barriers; see Ref. [7]. Apart from those, fission barriers in the SH region are generally unknown.

As a supplementary insight, one can cross-check barriers evaluated within various models. Quite recently we noted a dramatic divergence in calculated fission barriers [58]. Since, as discussed previously, the inclusion of triaxiality is absolutely necessary in the SH region, we have chosen only models which take this into account. In fact, there is only one systematic calculation including triaxiality and



FIG. 19. Calculated fission-barrier heights B_f for superheavy nuclei.

odd-particle-number nuclei: the finite-range liquid drop model [13,54,59] (FRLDM) developed by the Los Alamos group. It can be noted though, that the inner fission barrier is fixed there in only three-dimensional deformation space, what is certainly not enough.

The first conclusion from the comparison between our results and those of the FRLDM is that a conspicuous barrier staggering between odd- and even-particle-number nuclei is obtained in the Woods–Saxon model. As mentioned before, this results from the blocking treatment of pairing. At present it is not certain how large this staggering should be.

One can include more models for comparison if one confines it to even-even nuclei. Here we take the covariant density functional model [60] with the nonlinear meson-nucleon coupling, represented by the NL3* parametrization of the relativistic mean-field (RMF) Lagrangian and the

Hartree–Fock–Bogoliubov (HFB) approach with the SkM^{*} Skyrme energy density functional [61].

As can be seen in Fig. 22, fission barriers in Hassium nuclei are quite similar in all models. The values of B_f differ up to 2 MeV, but never more. Regarded as a function of N, they show a maximum close to the semimagic number N = 162 while the second maximum is related with the N = 184 spherical gap. In the FRLDM, this maximum is barely outlined and slightly shifted to the neutron-deficient side. The minimum in barriers is obtained in both MM models at the similar place (N = 170), while the RMF gives the smallest barriers at Z = 174.

As one can see in Fig. 23, for flerovium isotopes the barriers calculated here are in agreement with the experimental (empirical) estimates [57] and with the self-consistent calculations [61] based on the SkM* interaction. The FRLDM [54] overestimates these quasi-empirical barriers [57] significantly. Although only the lower limit for the barrier height has been



FIG. 20. Effect of pairing-strength increase (while keeping fixed the g.s. and saddle deformations) in N = 169 isotones: standard G_n and G_p (black points), red (green) points show G_n and G_p increased by 5% (10%) for odd-*Z* and odd-*N* nuclei.



FIG. 21. Effect of the pairing-strength increase (while keeping fixed the g.s. and saddle deformations) in Z = 109 isotopes: standard G_n and G_p (black points), red (green) points show G_n and G_p increased by 5% (10%) for odd-Z and odd-N nuclei.



FIG. 22. Fission barriers predicted by various models for Hassium isotopes: WS model (black), FRLDM (green) [54], SkM* (blue) [61], RMF with NL3 parametrization (red) [60]. Experimental data taken from Ref. [57]. (For interpretation of the references to color in this figure legend, the reader is referred to the online version of this article.)

estimated in Ref. [57], which would reproduce the known cross sections on the picobarn level, such a high barrier seems problematic, see discussion in Refs. [62,63]. On the other hand, with extremely small barriers obtained within the RMF model one cannot explain experimentally known millisecond fission half-life in ²⁸⁴Fl. One should note, however, that a slight tuning of the RMF model [64] gives higher barriers, closer to ours, especially in Cn and Fl isotopes; see details in Fig. 5 of Ref. [64] and in the discussion included there.

For Z = 120 our results, shown in Fig. 24, are very close to those obtained within the RMF model. The results of Ref. [54] are systematically higher by ≈ 1 MeV. This is in an evident contrast to the Skyrme SkM* prediction [61] of the highest barriers for Z = 120 [61] related to the proton magic gap.



FIG. 23. The same as in Fig. 22 but for Z = 114.



FIG. 24. The same as in Fig. 22 but for Z = 120.

Three models: FRLDM, RMF, and ours converge at N = 182-184 to $B_f \simeq 5$ MeV. The nucleus $^{302}120$ is particularly interesting, because two unsuccessful attempts to produce it have already taken place in GSI, providing a cross-section limit of 560 fb [65] or 90 fb in Ref. [66], and in Dubna [67], providing the limit of 400 fb. The cross-section estimates [68] do not support a possibility of an easy production of this SH isotope in the laboratory. It seems that, with the barrier of the order of 10 MeV, as obtained in the frame of the self-consistent theory, producing superheavy Z = 120 nuclei should not pose any difficulties.

In the case of Z = 126, shown in Fig. 25, both MM models give significantly smaller barriers than the model based on the SkM^{*} force. For example, the barrier $B_f \approx 9$ MeV for ³¹⁰126, calculated with this Skyrme interaction, is still impressively large. This might induce thoughts on the ways of synthesis of such superheavy systems, but one has to remember that the predicted half-lives with respect to the α decay are



FIG. 25. The same as in Fig. 22 but for Z = 126.

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below the present-day 10^{-5} s time limit for the experimental identification. On the contrary, $B_f \approx 2$ MeV obtained in the MM approach does not induce any hopes; it only points to a quite striking disagreement between models.

IV. CONCLUSIONS

We have determined fission barriers for 1305 heavy and superheavy nuclei, including odd-A and odd-odd systems, within the macroscopic-microscopic method by following the adiabatic configuration in each nucleus. The applied Woods-Saxon model was widely used for heavy nuclei and well reproduces experimental fission barriers in actinides. For odd-Z or/and odd-N nuclei, pairing was included within the blocking procedure. Triaxial and mass-asymmetric deformations were included and the IWF method used for finding the saddles which allowed us to escape errors inherent in the constrained minimization approach. To find saddles, energy for each nucleus was calculated on a 5D deformation grid and then fivefold interpolated in each dimension for the IWF search. Two additional energy grids, a second 5D and another 7D, were calculated in order to include nonaxial hexadecapole and mass-asymmetry effects on fission saddles. The following conclusions can be drawn from our investigation:

- (i) Global calculations confirm the existence of two physically important areas in the Z-N plane with prominent barriers: one located around the semimagic quantum numbers Z = 100-108 and N = 150-162 (connected with deformed closed shells), and the second of nearly spherical nuclei around Z = 114 and N = 176-180. The highest fission barrier among the studied nuclei occurs in very exotic ²⁸⁰Es.
- (ii) The well-known effect of the mass asymmetry on the second barrier in actinides is not very relevant for the heaviest nuclei since the heights of very deformed saddles at $\beta_{20} \approx 0.8$ decrease with increasing Z and fission barriers are fixed by the less deformed saddles. However, in some nuclei with $Z \ge 109$ the

mass-asymmetry (reflection-asymmetry) effect lowers the first saddles which are sometimes split into two humps. It seems that this concerns only axially symmetric saddles. The largest barrier lowering (by 0.8 MeV) has been observed for Z = 113 and N = 157.

- (iii) It has been demonstrated that the inclusion of triaxial shapes significantly reduces the fission barriers by up to 2.5 MeV; about 70% of the found fission barriers correspond to triaxial saddles. Besides the quadrupole nonaxiality we checked also the effect of hexadecapole nonaxiality, which significantly lowers the fission barrier in $Z \ge 119$ nuclei, especially neutron-deficient ones.
- (iv) Rather strong, irregular odd-even Z or N barrier staggering effect resulted from the blocking formalism used for pairing. The barrier of an odd nucleus $Z_{\text{even}} + 1$ or $N_{\text{even}} + 1$ is typically by several hundred keV higher than that of its even neighbor.
- (v) The existing theoretical evaluations of fission barriers differ significantly. Even the results of the two models based on the microscopic-macroscopic approach differ dramatically for some nuclei. Our calculations indicate, in contrast to the self-consistent mean-field studies, that fission barriers, still quite substantial for some Z = 118 nuclei, become lower than 5.5 MeV for Z = 126.

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