

**Nuclear, chemical and mechanical instability and the liquid-gas phase transition in nuclei**S. J. Lee<sup>1,2</sup> and A. Z. Mekjian<sup>1</sup><sup>1</sup>*Department of Physics and Astronomy, Rutgers University, Piscataway, New Jersey 08854, USA*<sup>2</sup>*Department of Physics, Kyung Hee University, Yongin, Kyunggi-do, Korea*

(Received 3 September 2007; revised manuscript received 28 March 2008; published 28 May 2008)

The thermodynamic properties of nuclei are studied in a mean-field model by using a Skyrme interaction. Properties of two-component systems are investigated over the complete range of proton fraction from a system of pure neutrons to a system of only protons. Besides volume, symmetry, and Coulomb effects we also include momentum- or velocity-dependent forces. Applications of the results developed are then given and include nuclear mechanical and chemical instability and an associated liquid-gas phase transition in two-component systems. The velocity dependence leads to further changes in the coexistence curve and nuclear mechanical and chemical instability curves.

DOI: [10.1103/PhysRevC.77.054612](https://doi.org/10.1103/PhysRevC.77.054612)

PACS number(s): 24.10.Pa, 21.65.-f, 05.70.-a, 64.10.+h

**I. INTRODUCTION**

One primary goal of medium-energy nuclear collisions is a detailed study of the thermodynamic properties of strongly interacting nuclear matter [1,2]. An important feature of these properties is the existence of the liquid-gas phase transition. The properties of the nuclear force (long-range attraction and short-range repulsion) parallel those of a van der Waals system [3] that qualitatively describes a liquid-gas phase transition in atomic systems. The liquid-gas phase transition in nuclei is the first phase transition seen in a strongly interacting system. Relativistic heavy-ion collisions are being used to explore a second phase transition from hadronic matter made of mesons and baryons to a quark-gluon phase. Important differences exist between the nuclear interaction and the interaction between atoms. Because nuclei are made of neutrons and protons, the phase transition is in a two-component or binary system where symmetry energy effects and Coulomb effects play an important role. Moreover, the nuclear force has a velocity dependence. The presence of symmetry energy and a Coulomb interaction effect and also a velocity dependence in the nuclear interaction make the nuclear case a unique and interesting binary system within the general scope of such systems. Examples of other two-component systems are binary alloys and liquid <sup>3</sup>He. For <sup>3</sup>He the two components are spin-up and spin-down fluids. The phase structure in such two-component systems has some important features. In nuclear systems, isospin fractionation [1,2,4–7] is an example where the monomer gas phase has a large neutron-to-proton ratio. Reference [7] is the most recent reference on isospin fractionation and contains further references to it. Both the symmetry energy and Coulomb energy play an important role in this phenomena of isospin fractionation. Nucleons carry spin, but very little research has been done in understanding the role of spin in the liquid-gas phase structure. However, the crust of neutron stars has features associated with a superfluid phase.

An early study of the nuclear liquid-gas phase transition [3] treated the system as a one-component system of nucleons. This study was then extended to two components by using a Skyrme interaction [8]. A relativistic mean-field model was

also developed in Ref. [9], where the role of the symmetry energy was studied in detail. The addition of the Coulomb energy [10,11] resulted in asymmetries that changed the mechanical and chemical instability regions and binodal surfaces in pressure  $P$ , temperature  $T$ , and proton fraction  $y$  associated with phase coexistence. For one-component systems a phase diagram is the more familiar binodal curve of pressure versus density or volume determined by a Maxwell construction. Some other studies of one- and two-component phase transitions can be found in Refs. [12–21]. The present work is an extension of our research reported in Refs. [10,11]. An extended Skyrme interaction is now used in our present study and, for example, includes effects associated with a velocity dependence in the nuclear interaction. Here we will use a simplified form of the velocity dependence. In particular we will use an effective mass approximation for it that includes a density-dependent behavior. Our primary goal is to see what qualitative effects a momentum dependence has when superimposed upon an interaction model that does not include them. A momentum-dependence study was also given in Ref. [22] using a more refined dependence. Our results differ from that of Ref. [22] since we also include Coulomb and surface effects. Coulomb effects lead to an asymmetric behavior in proton fraction [10,11] of various quantities. In the absence of Coulomb forces a symmetry exists around proton fraction  $y = 1/2$ . The velocity-dependent force modifies nuclear saturation properties and the symmetry energy. Some recent extended studies of symmetry energy can be found in Refs. [23,24]. The results given in the following show modifications in chemical and mechanical instability curves arising from an inclusion of a density-dependent effective mass. The velocity dependence has a larger effect on the proton-rich instability and coexistence features compared to the neutron-rich curves. A detailed discussion is given in Sec. III and in associated figures. The study of two-component nuclear systems with arbitrary neutron/proton ratios will be useful for future RIB (Rare Isotope Beam) Facility experiments and in astrophysical studies such as in neutron stars.

Our paper is divided as follows. The next section discusses the thermodynamic properties of nuclei. It is divided into two subsections. General results based on a mean-field approach

are presented in Sec. IIA. Specific results based on a Skyrme force for the potential terms and low- and high-temperature kinetic energy behavior appear in Sec. IIB, where the effects of a velocity-dependent interaction and related effective mass results are also discussed. Then in Sec. III we apply the results of Secs. IIA and IIB to the specific issues of (A) mechanical and chemical instability of nuclei and (B) the liquid-gas coexistence curve. Results are presented in nine figures and are discussed. Finally, in Sec. IV a summary and conclusions are given.

## II. THERMODYNAMIC PROPERTIES OF NUCLEI IN A MEAN-FIELD DESCRIPTION

### A. General results

In this section we present results for the thermodynamic properties of nuclear matter that are extended from the results of Ref. [10] to include a velocity- or momentum-dependent interaction. The matter is a two-component system of protons and neutrons in equilibrium at some temperature  $T$ . We first develop expressions for the total energy  $E$  as a function of the density  $\rho_q$  of each component  $q$  and temperature  $T$ . The behavior of the energy functional with  $\rho_q$  and  $T$  can be used to obtain the behavior of the pressure  $P$  and chemical potential  $\mu_q$  for each component of type  $q$ . These quantities will also be functions of  $\rho_q$  and  $T$ . They can then be used to study, for example, a phase transition in the nuclear system.

To begin, we use the fact that, at a given temperature  $T = 1/\beta$ , the proton and neutron constituents are distributed in phase space according to the Wigner function  $f$  as

$$f(\vec{r}, \vec{p}) = \sum_q f_q(\vec{r}, \vec{p}), \quad (1)$$

$$f_q(\vec{r}, \vec{p}) = \frac{\gamma}{h^3} \tilde{f}_q(\vec{r}, \vec{p}) = \frac{\gamma}{h^3} \frac{1}{e^{\beta(\epsilon_q - \mu_q)} + 1}.$$

The spin degeneracy factor  $\gamma = 2$  and  $\epsilon_q$  and  $\mu_q$  are the single-particle energy and the chemical potential, respectively, of particle of type  $q$ . Then the particle density  $\rho$  and nucleon number  $A$  are given by the following equations:

$$\rho(\vec{r}) = \sum_q \rho_q(\vec{r}), \quad \rho_q(\vec{r}) = \int d^3p f_q(\vec{r}, \vec{p}), \quad (2)$$

$$A = \sum_q N_q = \int d^3r \rho(\vec{r}), \quad (3)$$

$$N_q = \int d^3r \rho_q(\vec{r}) = \int d^3r \int d^3p f_q(\vec{r}, \vec{p}).$$

Defining  $\tau(\vec{r})$  as

$$\tau(\vec{r}) = \sum_q \tau_q(\vec{r}), \quad \tau_q(\vec{r}) = \int d^3p p \frac{p^2}{h^2} f_q(\vec{r}, \vec{p}) \quad (4)$$

gives the total energy  $E$  as

$$E = \int d^3r \mathcal{E}(\vec{r}) = \int d^3r \int d^3p \frac{p^2}{2m} f(\vec{r}, \vec{p}) + \int d^3r \int d^3p U(\vec{r}, \vec{p}) = \int d^3r [\mathcal{E}_K(\vec{r}) + U(\vec{r})]. \quad (5)$$

The potential energy density is  $U(\vec{r})$ , and the  $\mathcal{E}_K(\vec{r}) = \frac{\hbar^2}{2m} \tau(\vec{r})$  is the kinetic energy density. The single-particle energy  $\epsilon_q$  is given by

$$\epsilon_q = \frac{\delta E}{\delta f_q} = \frac{\delta \mathcal{E}(\vec{r})}{\delta f_q(\vec{r}, \vec{p})} = \frac{p^2}{2m} + \frac{\delta U}{\delta f_q} = \frac{p^2}{2m} + u_q(\vec{r}, \vec{p}). \quad (6)$$

The  $u_q = \frac{\delta U}{\delta f_q}$  is the single-particle potential of particle  $q$ , which may in general be momentum dependent. The chemical potential  $\mu_q$  is given by  $\epsilon_q$  at an effective Fermi momentum  $p = p_{Fq}$  defined by the following equation:

$$\mu_q = \epsilon_q|_{p=p_{Fq}} = \frac{p_{Fq}^2}{2m} + u_q(\vec{r}, \vec{p}_{Fq}). \quad (7)$$

To study a phase transition we need information about the behavior of the pressure when the system is in equilibrium. The general expression for the pressure can be defined dynamically from the total momentum conservation law,  $\frac{d}{dt} [\int d^3r \int d^3p p \vec{p} f] = - \int d^3r \vec{\nabla}_r \cdot \vec{\Pi} = 0$ , by using the Vlasov equation as developed in Ref. [21]:

$$\frac{\partial f_q}{\partial t} + (\vec{\nabla}_p \epsilon_q) \cdot (\vec{\nabla}_r f_q) - (\vec{\nabla}_r \epsilon_q) \cdot (\vec{\nabla}_p f_q) = 0. \quad (8)$$

A more general expression is obtained from the hydrodynamic consideration of time dependent Hartree-Fock (TDHF) in phase space as given in Ref. [25], which reads

$$\begin{aligned} \vec{\nabla}_r \cdot \vec{\Pi} &= -\frac{d}{dt} \left[ \int d^3p p \vec{p} \sum_q f_q(\vec{r}, \vec{p}) \right] \\ &= -\sum_q \int d^3p p \vec{p} \left( \frac{\partial f_q}{\partial t} \right) \\ &= \sum_q \int d^3p p \vec{p} \vec{\nabla}_r \cdot [(\vec{\nabla}_p \epsilon_q) f_q] \\ &\quad + \sum_q \int d^3p p \hat{p} \cdot (\vec{\nabla}_r \epsilon_q) f_q, \end{aligned} \quad (9)$$

where  $\hat{p} = \vec{p}/p$  is a unit vector in the direction of  $\vec{p}$ . By using  $(\vec{\nabla}_r \epsilon_q) f_q = \vec{\nabla}_r (\epsilon_q f_q) - \epsilon_q \vec{\nabla}_r f_q = \vec{\nabla}_r (\epsilon_q f_q) - \vec{\nabla}_r \mathcal{E}$ , the dynamical pressure tensor  $\Pi_{ij}$  is given by

$$\begin{aligned} \Pi_{ij} &= \sum_q \int d^3p p p_i (\nabla_p^j \epsilon_q) f_q + \delta_{ij} \left[ \int d^3p p \sum_q \epsilon_q f_q - \mathcal{E} \right] \\ &= \sum_q \int d^3p p p_i \nabla_p^j \left( \frac{\delta \mathcal{E}}{\delta f_q} \right) f_q \\ &\quad + \delta_{ij} \left[ \sum_q \int d^3p p \left( \frac{\delta \mathcal{E}}{\delta f_q} \right) f_q - \mathcal{E} \right] \\ &= \sum_q \int d^3p p p_i \left[ \frac{p_j}{m} + \nabla_p^j \left( \frac{\delta U}{\delta f_q} \right) \right] f_q \\ &\quad + \delta_{ij} \left[ \sum_q \int d^3p p \left( \frac{\delta U}{\delta f_q} \right) f_q - U \right]. \end{aligned} \quad (10)$$

Our previous study [10] focused on a momentum-independent potential, which gave the following simpler results for the

pressure tensor:

$$\begin{aligned}\Pi_{ij} &= \sum_q \int d^3 p \frac{p_i p_j}{m} f_q + \delta_{ij} \left[ \sum_q \left( \frac{\delta U}{\delta \rho_q} \right) \rho_q - U \right] \\ &= \int d^3 p \sum_q \frac{p_i p_j}{m} f_q + \delta_{ij} \sum_q \rho_q \frac{\delta(U/\rho)}{\delta \rho_q}.\end{aligned}\quad (11)$$

The diagonal element of  $\Pi_{ij}$  is the pressure  $P = \Pi_{ii}$ , which simplifies to

$$\begin{aligned}P &= \Pi_{ii} = \sum_q \int d^3 p \frac{p_i^2}{m} f_q + \sum_q \frac{\delta U}{\delta \rho_q} \rho_q - U \\ &= P_K + \sum_q u_q \rho_q - U = P_K + P_P.\end{aligned}\quad (12)$$

Here  $P_K = \int d^3 p \frac{p_i^2}{m} f = \frac{2}{3} \mathcal{E}_K$  is the kinetic part of the pressure  $P$ , and the interaction potential part is  $P_P = \sum_q u_q \rho_q - U = \rho^2 \frac{\delta(U/\rho)}{\delta \rho}$ . At temperature  $T = 0$  the pressure  $P$  is related to the derivative of the energy per particle,  $E/A$ , with particle number fixed as

$$P = \Pi_{ii} = -\frac{d(E/A)}{dV} = \rho^2 \frac{d(\mathcal{E}/\rho)}{d\rho}.\quad (13)$$

This result applies to a single-component system. In the following we will give results at nonzero temperature for a multicomponent system. We first proceed with a discussion of the role of the momentum dependence and effective mass.

As mentioned, our study is based on a qualitative study of the role of a momentum-dependent interaction and we therefore use a simplifying approximation. Specifically, we use an effective mass with a density dependence and this approximation greatly simplifies our analysis in two-component asymmetric and finite nuclear systems. We still include both Coulomb and surface effects since realistic nuclear systems have such terms that are important in their description and stability properties. More refined studies will be developed in future work. When the momentum-dependent part is of the form  $A(\rho_p, \rho_n) \frac{p^2}{\hbar^2} f$ , then it can be incorporated into the Hamiltonian as an effective mass term. In Ref. [22], the momentum dependence is obtained from

$$\int \int d^3 p d^3 p' \frac{f_\tau(\vec{r}, \vec{p}) f'_\tau(\vec{r}, \vec{p}')}{1 + (\vec{p} - \vec{p}')^2 / \Lambda^2}.\quad (14)$$

We use an effective mass  $m_q^*/m$  approach [26] for Eq. (14), which can further be approximated by expanding the factor  $1/[1 + (\vec{p} - \vec{p}')^2 / \Lambda^2]$  to first order in  $1 - (\vec{p} - \vec{p}')^2 / \Lambda^2$ . Specifically, we write the effective mass behavior of  $m/m_q^*$  as

$$\frac{m}{m_q^*} = 1 + A_q(\rho) \frac{2m}{\hbar^2},\quad (15)$$

$$A_q(\rho) \tau_q(\vec{r}) = \frac{\hbar^2}{2m_q^*} \tau_q(\vec{r}) - \frac{\hbar^2}{2m} \tau_q(\vec{r}).$$

Moreover, we have  $U(\vec{r}) = U(\rho) + A(\rho) \tau(\vec{r}) = U(\rho) + \sum_q A_q(\rho) \tau_q(\vec{r})$  with  $\tau_q(\vec{r})$  of Eq. (4). A momentum-dependent

single-particle potential  $u_q(\vec{r}, \vec{p})$  is given by

$$\begin{aligned}u_q(\vec{r}, \vec{p}) &= \frac{\delta U(\vec{r})}{\delta f_q(\vec{r}, \vec{p})} = \frac{\delta U(\rho)}{\delta \rho_q} + \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho_q} + A_q(\rho) \frac{p^2}{\hbar^2} \\ &= \frac{\delta U(\vec{r})}{\delta \rho_q} + A_q(\rho) \frac{p^2}{\hbar^2}.\end{aligned}\quad (16)$$

The  $\mu_q$  is related to  $u_q(\vec{r}, \vec{p})$  through the result

$$\begin{aligned}\mu_q &= \frac{p_{Fq}^2}{2m} + u_q(\vec{r}, \vec{p}_{Fq}) \\ &= \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \frac{p_{Fq}^2}{2m} + \frac{\delta U(\rho)}{\delta \rho_q} + \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho_q} \\ &= \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \frac{p_{Fq}^2}{2m} + \frac{\delta U(\vec{r})}{\delta \rho_q} = \frac{p_{Fq}^2}{2m_q^*} + \frac{\delta U(\vec{r})}{\delta \rho_q}.\end{aligned}\quad (17)$$

Also

$$\vec{\nabla}_p u_q(\vec{r}, \vec{p}) = \vec{\nabla}_p \left( \frac{\delta U(\vec{r})}{\delta f_q} \right) = A_q(\rho) \frac{2\vec{p}}{\hbar^2}\quad (18)$$

and

$$\begin{aligned}\int d^3 p u_q f_q &= \int d^3 p \left( \frac{\delta U(\vec{r})}{\delta f_q} \right) f_q(\vec{r}, \vec{p}) = \frac{\delta U(\rho)}{\delta \rho_q} \rho_q(\vec{r}) \\ &\quad + \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho_q} \rho_q(\vec{r}) + A_q(\rho) \tau_q(\vec{r}) \\ &= \frac{\delta U(\vec{r})}{\delta \rho_q(\vec{r})} \rho_q(\vec{r}) + A_q(\rho) \tau_q(\vec{r}).\end{aligned}\quad (19)$$

Here  $\rho$  and  $\tau$  are treated as independent variables. Then the pressure tensor  $\Pi_{ij}$  is given by

$$\begin{aligned}\Pi_{ij} &= \sum_q \int d^3 p \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \frac{p_i p_j}{m} f_q \\ &\quad + \delta_{ij} \left[ \sum_q \left( \frac{\delta U(\vec{r})}{\delta \rho_q} \right) \rho_q + A(\rho) \tau(\vec{r}) - U(\vec{r}) \right] \\ &= \int d^3 p \sum_q \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \frac{p_i p_j}{m} f_q \\ &\quad + \delta_{ij} \sum_q \left[ \rho(\vec{r}) \rho_q(\vec{r}) \frac{\delta(U(\rho)/\rho)}{\delta \rho_q} + \rho_q(\vec{r}) \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho_q} \right] \\ &= \int d^3 p \sum_q \frac{p_i p_j}{m_q^*} f_q \\ &\quad + \delta_{ij} \sum_q \left[ \rho(\vec{r}) \rho_q(\vec{r}) \frac{\delta(U(\vec{r})/\rho)}{\delta \rho_q} + A(\rho) \tau(\vec{r}) \right]\end{aligned}\quad (20)$$

and the pressure  $P$  or diagonal element  $\Pi_{ii} = P$  is

$$\begin{aligned}P &= \Pi_{ii} = \sum_q \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \int d^3 p \frac{p_i^2}{m} f_q \\ &\quad + \sum_q \frac{\delta U(\vec{r})}{\delta \rho_q} \rho_q + A(\rho) \tau(\vec{r}) - U(\vec{r})\end{aligned}$$

$$= \sum_q \int d^3p \frac{p_i^2}{m_q^*} f_q + \sum_q \frac{\delta U(\vec{r})}{\delta \rho_q} \rho_q - U(\rho) = P_K^* + P_P. \quad (21)$$

The  $P_K^* = \sum_q P_{Kq}^*$  with

$$\begin{aligned} P_{Kq}^* &= \left(1 + A_q(\rho) \frac{2m}{\hbar^2}\right) \int d^3p \frac{p_i^2}{m} f_q \\ &= \int d^3p \frac{p^2}{3m_q^*} f_q = \frac{2}{3} \mathcal{E}_K^* \end{aligned} \quad (22)$$

is the kinetic pressure with an effective mass correction term, and the second equality is for an isotropic momentum distribution. The potential part of the pressure  $P_P$  is given by

$$\begin{aligned} P_P &= \sum_q \frac{\delta U(\vec{r})}{\delta \rho_q} \rho_q - U(\rho) \\ &= \sum_q \left[ \rho \rho_q \frac{\delta(U(\rho)/\rho)}{\delta \rho_q} + \rho_q \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho_q} \right] \\ &= \sum_q \left[ \rho \rho_q \frac{\delta(U(\vec{r})/\rho)}{\delta \rho_q} + A_q(\rho) \tau_q(\vec{r}) \right] \\ &= \rho^2 \frac{\delta(U(\rho)/\rho)}{\delta \rho} + \rho \frac{\delta A(\rho) \tau(\vec{r})}{\delta \rho} \\ &= \rho^2 \frac{\delta(U(\vec{r})/\rho)}{\delta \rho} + A(\rho) \tau(\vec{r}) = \rho^2 \frac{\delta(U(\vec{r})/\rho)}{\delta \rho} + \mathcal{E}_K^* - \mathcal{E}_K. \end{aligned} \quad (23)$$

Here  $\mathcal{E}_K = \sum_q \frac{\hbar^2}{2m} \tau_q(\vec{r})$  and

$$\mathcal{E}_K^* = \sum_q \frac{\hbar^2}{2m_q^*} \tau_q(\vec{r}) = \sum_q \left(1 + A_q(\rho) \frac{2m}{\hbar^2}\right) \frac{\hbar^2}{2m} \tau_q(\vec{r}). \quad (24)$$

Also in obtaining this result we use the fact that

$$\sum_q \rho_q \frac{\delta U(\rho, \rho_q)}{\delta \rho_q} = \rho \frac{\delta U(\rho, \rho x_q)}{\delta \rho}, \quad (25)$$

which can be shown by looking at the derivative of  $B(\rho)C(\rho_p)D(\rho_n) = B(\rho)C(\rho x_p)D(\rho x_n)$ . Here the variation  $\rho$  must be done after replacing  $\rho_q$  by  $\rho x_q$ .

Other thermodynamic variables, such as  $S$ ,  $\Omega$ ,  $F$ , and  $G$ , are given in Ref. [10]. The entropy  $S$  follows, from the distribution  $\tilde{f}_q$  of Eq. (1), as

$$S = \sum_q S_q = \int d^3r \mathcal{S} = \int d^3r \sum_q \mathcal{S}_q \quad (26)$$

and

$$\begin{aligned} \mathcal{S}_q &= -\frac{\gamma}{h^3} \int d^3p [ \tilde{f}_q \ln \tilde{f}_q + (1 - \tilde{f}_q) \ln(1 - \tilde{f}_q) ] \\ &= \beta \int d^3p \epsilon_q f_q + \beta \int d^3p \frac{\vec{p} \cdot \vec{\nabla}_p \epsilon_q}{3} f_q - \beta \mu_q \int d^3p f_q. \end{aligned} \quad (27)$$

In equilibrium, from Eqs. (10) and (27)

$$\begin{aligned} TS &= \mathcal{E} + P - \sum_q \mu_q \rho_q = \mathcal{E}_K + P_K - \sum_q (\mu_q - u_q) \rho_q \\ &= \mathcal{E}_K + P_K - \sum_q \frac{p_{Fq}^2}{2m} \rho_q. \end{aligned} \quad (28)$$

The last equality of Eq. (28) is the result of using Eq. (7). For a momentum-dependent potential the entropy is now

$$\begin{aligned} TS &= \mathcal{E} + P - \sum_q \mu_q \rho_q \\ &= \mathcal{E}_K^* + P_K^* - \sum_q \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) \rho_q \\ &= \mathcal{E}_K^* + P_K^* - \sum_q \left( 1 + A_q(\rho) \frac{2m}{\hbar^2} \right) \frac{p_{Fq}^2}{2m} \rho_q \\ &= \mathcal{E}_K^* + P_K^* - \sum_q \frac{p_{Fq}^2}{2m_q^*} \rho_q, \end{aligned} \quad (29)$$

where use has been made of Eqs. (17) and (21) to obtain this result. General thermodynamic relations also determine the entropy, pressure, and chemical potential [10].

## B. Thermodynamic properties of nuclear matter based on a Skyrme interaction

We now use a Skyrme interaction to develop expressions for the potential  $U$ . Once the potential energy  $U$  in Eq. (5) is known, then questions related to mechanical and chemical instability and the possibility of a phase transition of the system can be studied by using Eqs. (1)–(29). The potential energy  $U$  determines  $\epsilon_q$  and  $\mu_q$  and the potential energy part of  $E$  and  $P$ . Then for fixed  $T$  and  $N_q$ , the Wigner function  $f$  and  $p_{Fq}$  are determined and thus the kinetic terms of  $E$ ,  $\mu_q$ , and  $P$ . By using these results, the entropy  $S$  can be determined. For a nuclear system of proton ( $\rho_p$ ) and neutron ( $\rho_n$ ), this gives the local potential energy density as

$$\begin{aligned} U(\rho_q) &= \frac{t_0}{2} \left(1 + \frac{x_0}{2}\right) \rho^2 - \frac{t_0}{2} \left(\frac{1}{2} + x_0\right) \sum_q \rho_q^2 \\ &+ \frac{t_3}{12} \left(1 + \frac{x_3}{2}\right) \rho^{\alpha+2} - \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) \rho^\alpha \sum_q \rho_q^2 \\ &+ \frac{1}{4} \left[ t_1 \left(1 + \frac{x_1}{2}\right) + t_2 \left(1 + \frac{x_2}{2}\right) \right] \rho \tau \\ &- \frac{1}{4} \left[ t_1 \left(\frac{1}{2} + x_1\right) - t_2 \left(\frac{1}{2} + x_2\right) \right] \sum_q \rho_q \tau_q \\ &+ C \rho^\beta \rho_p^2 + C_s \rho^\eta. \end{aligned} \quad (30)$$

Here  $C \rho^\beta = \frac{4\pi}{5} e^2 R^2$  and  $C_s \rho^\eta = \frac{4\pi R^2 \sigma(\rho)}{V} = \frac{(4\pi r_0^2 \sigma)}{V^{1/3}} \rho^{2/3}$  when we approximate the Coulomb and surface effects as coming from a finite uniform sphere of radius  $R = r_0 A^{1/3}$  with total charge  $Z$  ( $U_C = \frac{3}{5} \frac{e^2 Z^2}{RV}$ ) [10]. The values for the force parameters used here are given in

TABLE I. Skyrme parameters used here are in MeV and fm units [11]. For  $t_1$  and  $t_2$ , the SkM parameter values are used.

$t_0$	$x_0$	$t_3$	$x_3$	$\alpha$
-1089.0	-1/6	17480.4	-1/2	1
		Momentum dependent	Momentum independent	
$t_1$		251.11	0	
$x_1$		-1/2	-1/2	
$t_2$		-150.66	0	
$x_2$		-1/2	-1/2	
Effective mass $m^*/m$		0.895626	1	
Binding energy $E_B/A$		13.1057	15.54447	
Fermi energy $E_F$		31.8018	34.2101	
Saturation density $\rho_0$		0.1283	0.143145	
Symmetry energy $S_V$		23.4791	24.39379	
Compressibility $\kappa$		307.780	361.9045	

 Table I. We define an effective mass  $m_q^*$  as

$$\frac{m}{m_q^*} = 1 + \frac{2m}{\hbar^2} \left\{ \frac{1}{4} \left[ t_1 \left( 1 + \frac{x_1}{2} \right) + t_2 \left( 1 + \frac{x_2}{2} \right) \right] \rho - \frac{1}{4} \left[ t_1 \left( \frac{1}{2} + x_1 \right) - t_2 \left( \frac{1}{2} + x_2 \right) \right] \rho_q \right\}. \quad (31)$$

Then the momentum-dependent potential term becomes

$$\begin{aligned} A_q(\rho) &= \frac{\hbar^2}{2m_q^*} - \frac{\hbar^2}{2m} = \frac{1}{4} \left[ t_1 \left( 1 + \frac{x_1}{2} \right) + t_2 \left( 1 + \frac{x_2}{2} \right) \right] \rho \\ &\quad - \frac{1}{4} \left[ t_1 \left( \frac{1}{2} + x_1 \right) - t_2 \left( \frac{1}{2} + x_2 \right) \right] \rho_q \\ &= \frac{\hbar^2}{2m} \left[ -1 + 1 + \frac{2m}{\hbar^2} \left\{ \frac{1}{4} \left[ t_1 \left( 1 + \frac{x_1}{2} \right) + t_2 \left( 1 + \frac{x_2}{2} \right) \right] \rho \right. \right. \\ &\quad \left. \left. - \frac{1}{4} \left[ t_1 \left( \frac{1}{2} + x_1 \right) - t_2 \left( \frac{1}{2} + x_2 \right) \right] \rho_q \right\} \right]. \quad (32) \end{aligned}$$

For a symmetric nucleus,  $N = Z$ ,  $\rho_q = \rho/2$ , and thus

$$\begin{aligned} U(\rho) &= \frac{3}{8} t_0 \rho^2 + \frac{3}{48} t_3 \rho^{\alpha+2} \\ &\quad + \frac{3}{16} (t_1 + t_2) \rho \tau + C \rho^\beta \rho_p^2 + C_s \rho^\eta. \quad (33) \end{aligned}$$

This potential energy determines the interaction-dependent terms of  $\mathcal{E}$ ,  $P$ ,  $\epsilon_q$ , and  $\mu_q$ , which depend on densities without an explicit  $T$  dependence.

For a momentum-dependent potential energy as in Eq. (30),  $\epsilon_q - \mu_q = (p^2 - p_{Fq}^2)/(2m_q^*)$ , where the effective mass  $m_q^*$  is independent of the momentum-independent part of the potential and the Wigner function of Eq. (1) becomes

$$\tilde{f}_q(\vec{r}, \vec{p}) = \frac{1}{e^{\beta(\epsilon_q - \mu_q)} + 1} = \frac{1}{e^{\beta(p^2 - p_{Fq}^2)/(2m_q^*)} + 1}. \quad (34)$$

Thus we can evaluate the kinetic terms in  $\mathcal{E}$ ,  $P$ , and  $\mu_q$ , which are functions of  $T$  and  $p_{Fq}$ . Defining the Fermi integral  $F_\alpha(\eta)$ ,

with effective mass  $m_q^*$ , as

$$\begin{aligned} F_\alpha(\eta_q) &= \int_0^\infty \frac{x^\alpha}{1 + e^{x - \eta_q}} dx \\ &= \left( \frac{\lambda_q^2}{4\pi\hbar^2} \right)^{\alpha+1} \int_0^\infty \frac{2p^{2\alpha+1} dp}{1 + e^{\beta p^2/2m_q^* - \eta_q}}, \quad (35) \end{aligned}$$

$$\begin{aligned} \eta_q &= \beta \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) = \beta p_{Fq}^2 / (2m_q^*) \\ &= p_{Fq}^2 / (2m_q^* T) = \ln z_q, \quad (36) \end{aligned}$$

$$\lambda_q = \sqrt{2\pi\hbar^2/m_q^* T}, \quad (37)$$

we can write, for  $f(\vec{r}, \vec{p}) = f(\vec{r}, p)$ ,

$$\begin{aligned} \rho_q &= \int d^3 p f_q(\vec{r}, \vec{p}) = \frac{\gamma}{\hbar^3} \int d^3 p \frac{1}{e^{\beta(p^2 - p_{Fq}^2)/(2m_q^*)} + 1} \\ &= \lambda_q^{-3} \frac{2\gamma}{\sqrt{\pi}} F_{1/2}(\eta_q), \quad (38) \end{aligned}$$

$$\begin{aligned} \epsilon_{Fq}^* &\equiv \frac{p_{Fq}^2}{2m_q^*} = \frac{\hbar^2}{2m_q^*} \left( \frac{6\pi^2}{\gamma} \rho_q \right)^{2/3} = \frac{m}{m_q^*} \epsilon_{Fq}, \\ \epsilon_{Fq} &= \frac{\hbar^2}{2m} \left( \frac{6\pi^2}{\gamma} \rho_q \right)^{2/3}, \quad (39) \end{aligned}$$

$$\begin{aligned} \tau_q &= \int d^3 p p \frac{p^2}{\hbar^2} f_q(\vec{r}, \vec{p}) = \frac{\gamma}{\hbar^3} \int d^3 p p \frac{p^2}{\hbar^2} \frac{1}{e^{\beta(p^2 - p_{Fq}^2)/(2m_q^*)} + 1} \\ &= 8\gamma \sqrt{\pi} \lambda_q^{-5} F_{3/2}(\eta_q) = \frac{1}{\beta} \frac{2m_q^*}{\hbar^2} \frac{2\gamma}{\sqrt{\pi}} \lambda_q^{-3} F_{3/2}(\eta_q) \\ &= \frac{2m}{\hbar^2} \mathcal{E}_{Kq} = \frac{2m_q^*}{\hbar^2} \mathcal{E}_{Kq}^*, \quad (40) \end{aligned}$$

$$\begin{aligned} \mathcal{E}_{Kq} &= \frac{\hbar^2}{2m} \tau_q = \frac{3}{2} P_{Kq} = \int d^3 p p \frac{p^2}{2m} f_q(\vec{r}, \vec{p}) \\ &= \frac{\gamma}{\hbar^3} \int d^3 p p \frac{p^2}{2m} \frac{1}{e^{\beta(p^2 - p_{Fq}^2)/(2m_q^*)} + 1} \\ &= \frac{4\gamma \hbar^2 \sqrt{\pi}}{m} \lambda_q^{-5} F_{3/2}(\eta_q) = \frac{m_q^*}{m} \frac{1}{\beta} \frac{2\gamma}{\sqrt{\pi}} \lambda_q^{-3} F_{3/2}(\eta_q), \quad (41) \end{aligned}$$

$$\begin{aligned} \mathcal{E}_{Kq}^* &= \frac{\hbar^2}{2m_q^*} \tau_q = \frac{3}{2} P_{Kq}^* = \int d^3 p p \frac{p^2}{2m_q^*} f_q(\vec{r}, \vec{p}) \\ &= \frac{\gamma}{\hbar^3} \int d^3 p p \frac{p^2}{2m_q^*} \frac{1}{e^{\beta(p^2 - p_{Fq}^2)/(2m_q^*)} + 1} \\ &= \frac{4\gamma \hbar^2 \sqrt{\pi}}{m_q^*} \lambda_q^{-5} F_{3/2}(\eta_q) = \frac{1}{\beta} \frac{2\gamma}{\sqrt{\pi}} \lambda_q^{-3} F_{3/2}(\eta_q). \quad (42) \end{aligned}$$

Here  $\epsilon_{Fq}$  is the chemical potential at absolute zero or Fermi energy and  $p_{Fq}$  is the effective Fermi momentum at  $T$  [which is related to density  $\rho_q$  through Eq. (38)]. The particle number  $N_q = \int d^3 r \rho(\vec{r})$  determines the effective Fermi momentum  $p_{Fq}(\vec{r})$  or  $\eta_q$  at  $T$ , in terms of density  $\rho_q(\vec{r})$ :

$$\eta_q(\rho_q, T) = \beta \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) = \beta \frac{p_{Fq}^2}{2m_q^*} = F_{1/2}^{-1} \left( \frac{\sqrt{\pi}}{2\gamma} \lambda_q^3 \rho_q \right). \quad (43)$$



For multi(two)-component systems with potential energy given by Eq. (30), with a given  $\rho_q$  (or  $p_{Fq}$ ) and  $T$ , the thermodynamic properties are as follows. The chemical potential is given by

$$\begin{aligned}\mu_q(\rho_q, T) &= T\eta_q(\rho_q, T) + \frac{\delta U(\vec{r})}{\delta \rho_q} \\ &= T\eta_q(\rho_q, T) + t_0 \left(1 + \frac{x_0}{2}\right) \rho + \frac{t_3}{12} \left(1 + \frac{x_3}{2}\right) \\ &\quad \times (\alpha + 2)\rho^{\alpha+1} - \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) \alpha \rho^{\alpha+1} \\ &\quad - t_0 \left(\frac{1}{2} + x_0\right) \rho_q + \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) (\alpha - 1) 2\rho^\alpha \rho_q \\ &\quad - \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) 2\alpha \rho^{\alpha-1} \rho_q^2 \\ &\quad + \frac{1}{4} \left[ t_1 \left(1 + \frac{x_1}{2}\right) + t_2 \left(1 + \frac{x_2}{2}\right) \right] \tau \\ &\quad - \frac{1}{4} \left[ t_1 \left(\frac{1}{2} + x_1\right) - t_2 \left(\frac{1}{2} + x_2\right) \right] \tau_q \\ &\quad + C\beta\rho^{\beta-1} \rho_p^2 + 2C\rho^\beta \rho_p \delta_{q,p} + \eta C_s \rho^{\eta-1}. \quad (44)\end{aligned}$$

The equation of state has a behavior determined by

$$\begin{aligned}P(\rho_q, T) &= \sum_q \frac{2}{3} \mathcal{E}_{Kq}^*(\rho_q, T) + \rho^2 \frac{\delta(U(\rho)/\rho)}{\delta \rho} + \rho \frac{\delta A(\rho)\tau(\vec{r})}{\delta \rho} \\ &= \sum_q \left[ \frac{5}{3} \mathcal{E}_{Kq}^*(\rho_q, T) - \mathcal{E}_{Kq}(\rho_q, T) \right] + \rho^2 \frac{\delta(U(\vec{r})/\rho)}{\delta \rho} \\ &= \sum_q \left[ \frac{5}{3} \mathcal{E}_{Kq}^*(\rho_q, T) - \mathcal{E}_{Kq}(\rho_q, T) \right] \\ &\quad + \frac{t_0}{2} \left(1 + \frac{x_0}{2}\right) \rho^2 \\ &\quad + \frac{t_3}{12} \left(1 + \frac{x_3}{2}\right) (\alpha + 1) \rho^{\alpha+2} \\ &\quad - \frac{t_0}{2} \left(\frac{1}{2} + x_0\right) \sum_q \rho_q^2 - \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) \\ &\quad \times (\alpha + 1) \rho^\alpha \sum_q \rho_q^2 \\ &\quad + C(\beta + 1) \rho^\beta \rho_p^2 + C_s(\eta - 1) \rho^\eta. \quad (45)\end{aligned}$$

The energy density is

$$\begin{aligned}\mathcal{E}(\rho_q, T) &= \sum_q \mathcal{E}_{Kq}(\rho_q, T) + U(\vec{r}) = \sum_q \mathcal{E}_{Kq}^*(\rho_q, T) + U(\rho) \\ &= \sum_q \mathcal{E}_{Kq}^*(\rho_q, T) + \frac{t_0}{2} \left(1 + \frac{x_0}{2}\right) \rho^2 \\ &\quad - \frac{t_0}{2} \left(\frac{1}{2} + x_0\right) \sum_q \rho_q^2 + \frac{t_3}{12} \left(1 + \frac{x_3}{2}\right) \rho^{\alpha+2} \\ &\quad - \frac{t_3}{12} \left(\frac{1}{2} + x_3\right) \rho^\alpha \sum_q \rho_q^2 + C\rho^\beta \rho_p^2 + C_s \rho^\eta \quad (46)\end{aligned}$$

and the entropy can be obtained from

$$\begin{aligned}TS(\rho_q, T) &= \sum_q \frac{5}{3} \mathcal{E}_{Kq}^*(\rho_q, T) - \sum_q \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) \rho_q \\ &= \sum_q \frac{5}{3} \mathcal{E}_{Kq}^*(\rho_q, T) - T \sum_q \eta_q(\rho_q, T) \rho_q. \quad (47)\end{aligned}$$

Once we evaluate  $F_{1/2}(\eta)$  and  $F_{3/2}(\eta)$ , or more directly  $\eta = F_{1/2}^{-1}(\chi)$  and  $F_{3/2}(\eta)$ , we can evaluate various thermodynamic quantities in terms of  $\rho_q$  and  $T$ .

For low-temperature and high-density limit where  $\lambda^3 \rho \gg 1$ , that is, when the average de Broglie thermal wavelength  $\lambda$  is larger than the average interparticle separation  $\rho^{-1/3}$ , we can use a nearly degenerate (Fermi gas) approximations [27] for  $F_{1/2}$  to obtain

$$\begin{aligned}\eta_q(\rho_q, T) &= \beta \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) = \beta \frac{p_{Fq}^2}{2m_q^*} = F_{1/2}^{-1} \left( \frac{\sqrt{\pi}}{2\gamma} \lambda_q^3 \rho_q \right) \\ &= \beta \epsilon_{Fq}^* \left[ 1 - \frac{\pi^2}{12} \left( \frac{T}{\epsilon_{Fq}^*} \right)^2 + \dots \right] \\ &= \beta \frac{\hbar^2}{2m_q^*} \left( \frac{6\pi^2}{\gamma} \right)^{2/3} \left[ \rho_q^{2/3} - \frac{\pi^2 m_q^{*2}}{3\hbar^4} \right. \\ &\quad \left. \times \left( \frac{\gamma}{6\pi^2} \right)^{4/3} T^2 \rho_q^{-2/3} + \dots \right], \quad (48)\end{aligned}$$

$$\begin{aligned}\mathcal{E}_{Kq}^*(\rho_q, T) &= \frac{2\gamma}{\beta \sqrt{\pi}} \lambda_q^{-3} F_{3/2}(\eta_q) = \frac{3}{2} P_{Kq}^* \\ &= \frac{3}{5} \rho_q \epsilon_{Fq}^* \left[ 1 + \frac{5\pi^2}{12} \left( \frac{T}{\epsilon_{Fq}^*} \right)^2 + \dots \right] \\ &= \frac{3\hbar^2}{10m_q^*} \left( \frac{6\pi^2}{\gamma} \right)^{2/3} \left[ \rho_q^{5/3} + \frac{5\pi^2 m_q^{*2}}{3\hbar^4} \right. \\ &\quad \left. \times \left( \frac{\gamma}{6\pi^2} \right)^{4/3} T^2 \rho_q^{1/3} + \dots \right], \quad (49)\end{aligned}$$

$$\begin{aligned}\tau_q(\rho_q, T) &= \frac{2m_q^*}{\hbar^2} \mathcal{E}_{Kq}^* \\ &= \frac{3}{5} \frac{2m_q^*}{\hbar^2} \rho_q \epsilon_{Fq}^* \left[ 1 + \frac{5\pi^2}{12} \left( \frac{T}{\epsilon_{Fq}^*} \right)^2 + \dots \right] \\ &= \frac{3}{5} \left( \frac{6\pi^2}{\gamma} \right)^{2/3} \rho_q^{5/3} \left[ 1 + \frac{5\pi^2}{12} \left( \frac{T}{\epsilon_{Fq}^*} \right)^2 + \dots \right] \\ &= \frac{3}{5} \left( \frac{6\pi^2}{\gamma} \right)^{2/3} \left[ \rho_q^{5/3} + \frac{5\pi^2 m_q^{*2}}{3\hbar^4} \right. \\ &\quad \left. \times \left( \frac{\gamma}{6\pi^2} \right)^{4/3} T^2 \rho_q^{1/3} + \dots \right]. \quad (50)\end{aligned}$$

In the other limit where  $\lambda_q^3 \rho$  is small, we have a nearly nondegenerate Fermi gas (classical ideal gas) and the resulting equations are given by an ideal gas in leading order with higher

order corrections [27] as

$$\begin{aligned}\eta_q(\rho_q, T) &= \beta \left( \mu_q - \frac{\delta U(\vec{r})}{\delta \rho_q} \right) \\ &= \ln \left[ \frac{\rho_q \lambda_q^3}{\gamma} \left( 1 + \frac{1}{2\sqrt{2}} \frac{\rho_q \lambda_q^3}{\gamma} + \dots \right) \right] \\ &\approx \ln \left( \frac{\rho_q \lambda_q^3}{\gamma} \right) + \frac{1}{2\sqrt{2}} \left( \frac{\rho_q \lambda_q^3}{\gamma} \right),\end{aligned}\quad (51)$$

$$\begin{aligned}\mathcal{E}_{Kq}^*(\rho_q, T) &= \frac{3}{2} P_{Kq}^* = \frac{3}{2} \rho_q T \left[ 1 + \frac{1}{2^{5/2}} \frac{\rho_q \lambda_q^3}{\gamma} \right. \\ &\quad \left. + \left( \frac{1}{8} - \frac{2}{3^{5/2}} \right) \left( \frac{\rho_q \lambda_q^3}{\gamma} \right)^2 + \dots \right],\end{aligned}\quad (52)$$

$$\begin{aligned}\tau_q(\rho_q, T) &= \frac{2m_q^*}{\hbar^2} \mathcal{E}_{Kq}^* = \frac{2m_q^*}{\hbar^2} \frac{3}{2} \rho_q T \left[ 1 + \frac{1}{2^{5/2}} \frac{\rho_q \lambda_q^3}{\gamma} \right. \\ &\quad \left. + \left( \frac{1}{8} - \frac{2}{3^{5/2}} \right) \left( \frac{\rho_q \lambda_q^3}{\gamma} \right)^2 + \dots \right].\end{aligned}\quad (53)$$

For a nuclear system with protons and neutrons with the interaction given by Eq. (30), the nondegenerate Fermi gas limit of Eqs. (51), (52), and (53) leads to the following set of equations. The chemical potential has a behavior determined by

$$\begin{aligned}\mu_q(\rho, y, T) &= T \ln \left[ \left( \frac{\lambda_q^3}{\gamma} \right) \rho_q \right] + \frac{T}{2\sqrt{2}} \left( \frac{\lambda_q^3}{\gamma} \right) \rho_q \\ &\quad + \frac{1}{4} \left[ t_1 \left( 1 + \frac{x_1}{2} \right) + t_2 \left( 1 + \frac{x_2}{2} \right) \right] \frac{3}{2} T \sum_q \frac{2m_q^*}{\hbar^2} \\ &\quad \times \left[ \rho_q + \frac{\lambda_q^3}{2^{5/2}\gamma} \rho_q^2 \right] \\ &\quad - \frac{1}{4} \left[ t_1 \left( \frac{1}{2} + x_1 \right) - t_2 \left( \frac{1}{2} + x_2 \right) \right] \frac{3}{2} T \frac{2m_q^*}{\hbar^2} \\ &\quad \times \left[ \rho_q + \frac{\lambda_q^3}{2^{5/2}\gamma} \rho_q^2 \right] + t_0 \left( 1 + \frac{x_0}{2} \right) \rho \\ &\quad + \frac{t_3}{12} \left( 1 + \frac{x_3}{2} \right) (\alpha + 2) \rho^{\alpha+1} \\ &\quad - \frac{t_3}{12} \left( \frac{1}{2} + x_3 \right) \alpha \rho^{\alpha+1} - t_0 \left( \frac{1}{2} + x_0 \right) \rho_q \\ &\quad + \frac{t_3}{12} \left( \frac{1}{2} + x_3 \right) (\alpha - 1) 2 \rho^\alpha \rho_q \\ &\quad - \frac{t_3}{12} \left( \frac{1}{2} + x_3 \right) 2 \alpha \rho^{\alpha-1} \rho_q^2 \\ &\quad + C\beta \rho^{\beta-1} \rho_p^2 + 2C\rho^\beta \rho_p \delta_{q,p} + \eta C_s \rho^{\eta-1}.\end{aligned}\quad (54)$$

The equation of state has a form given by

$$\begin{aligned}P(\rho, y, T) &= \frac{5}{2} T \rho + \frac{5}{2} \frac{T}{2\sqrt{2}} \sum_q \left( \frac{\lambda_q^3}{\gamma} \right) \left( \frac{\rho_q^2}{2} \right) \\ &\quad - \frac{3}{2} T \sum_q \frac{m_q^*}{m} \left[ \rho_q + \frac{1}{2\sqrt{2}} \left( \frac{\lambda_q^3}{\gamma} \right) \left( \frac{\rho_q^2}{2} \right) \right] \\ &\quad + \frac{t_0}{2} \left( 1 + \frac{x_0}{2} \right) \rho^2 + \frac{t_3}{12} \left( 1 + \frac{x_3}{2} \right) (\alpha + 1) \rho^{\alpha+2} \\ &\quad - \frac{t_0}{2} \left( \frac{1}{2} + x_0 \right) \sum_q \rho_q^2 \\ &\quad - \frac{t_3}{12} \left( \frac{1}{2} + x_3 \right) (\alpha + 1) \rho^\alpha \sum_q \rho_q^2 \\ &\quad + C(\beta + 1) \rho^\beta \rho_p^2 + C_s (\eta - 1) \rho^\eta.\end{aligned}\quad (55)$$

The energy density is

$$\begin{aligned}\mathcal{E}(\rho, y, T) &= \frac{3}{2} T \rho + \frac{3}{2} \frac{T}{2\sqrt{2}} \sum_q \left( \frac{\lambda_q^3}{\gamma} \right) \left( \frac{\rho_q^2}{2} \right) \\ &\quad + \frac{t_0}{2} \left( 1 + \frac{x_0}{2} \right) \rho^2 - \frac{t_0}{2} \left( \frac{1}{2} + x_0 \right) \sum_q \rho_q^2 \\ &\quad + \frac{t_3}{12} \left( 1 + \frac{x_3}{2} \right) \rho^{\alpha+2} - \frac{t_3}{12} \left( \frac{1}{2} + x_3 \right) \rho^\alpha \sum_q \rho_q^2 \\ &\quad + C\rho^\beta \rho_p^2 + C_s \rho^\eta\end{aligned}\quad (56)$$

and the entropy is

$$\begin{aligned}TS(\rho, y, T) &= \frac{5}{2} T \rho - T \sum_q \rho_q \ln \left( \frac{\lambda_q^3}{\gamma} \rho_q \right) \\ &\quad + \frac{T}{2\sqrt{2}} \sum_q \left( \frac{\lambda_q^3}{\gamma} \right) \left( \frac{\rho_q^2}{4} \right).\end{aligned}\quad (57)$$

The effective mass  $m_q^*$  and thus  $\lambda_q$  are, in general, isospin dependent [26]. However, we will consider an isospin-independent effective mass here for simplicity in this present study. For the case of  $m_q^* = m^*$  with  $\lambda_q = \lambda$  (such as the case of  $x_1 = x_2 = -1/2$ ), these equations become

$$\begin{aligned}\mu_q(\rho, y, T) &= T \ln \left[ \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \pm (2y - 1) \frac{\rho}{2} \right) \right] \\ &\quad + \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \pm (2y - 1) \frac{\rho}{2} \right) \\ &\quad + \frac{1}{4} \left[ t_1 \left( 1 + \frac{x_1}{2} \right) + t_2 \left( 1 + \frac{x_2}{2} \right) \right] \frac{3}{2} T \frac{2m^*}{\hbar^2} \\ &\quad \times \left[ \rho + \frac{\lambda^3}{2\sqrt{2}\gamma} [1 + (2y - 1)^2] \left( \frac{\rho}{2} \right)^2 \right] \\ &\quad - \frac{1}{4} \left[ t_1 \left( \frac{1}{2} + x_1 \right) - t_2 \left( \frac{1}{2} + x_2 \right) \right] \frac{3}{2} T \frac{2m^*}{\hbar^2} \\ &\quad \times \left[ \left( \frac{\rho}{2} \pm (2y - 1) \frac{\rho}{2} \right) \right. \\ &\quad \left. + \frac{\lambda^3}{2^{5/2}\gamma} \left( \frac{\rho}{2} \pm (2y - 1) \frac{\rho}{2} \right)^2 \right]\end{aligned}$$

$$\begin{aligned}
& + \frac{3}{4} t_0 \rho \mp \left( \frac{1}{2} + x_0 \right) t_0 (2y - 1) \left( \frac{\rho}{2} \right) \\
& + \frac{(\alpha + 2)}{16} t_3 \rho^{\alpha+1} - \frac{1}{6} \left( \frac{1}{2} + x_3 \right) t_3 \\
& \times \left[ \alpha (2y - 1)^2 \left( \frac{\rho}{2} \right)^2 \pm (2y - 1) \left( \frac{\rho}{2} \right) \rho \right] \rho^{\alpha-1} \\
& + \frac{1}{4} C [\beta + 2(1 \pm 1)] \rho^{\beta+1} \\
& + C [(\beta + 1 \pm 1)(2y - 1) \left( \frac{\rho}{2} \right) \rho \\
& + \beta (2y - 1)^2 \left( \frac{\rho}{2} \right)^2] \rho^{\beta-1} + \eta C_s \rho^{\eta-1}, \quad (58)
\end{aligned}$$

$$\begin{aligned}
P(\rho, y, T) &= \left( \frac{5}{2} - \frac{3 m^*}{2 m} \right) T \rho \\
& + \left( \frac{5}{2} - \frac{3 m^*}{2 m} \right) \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \right)^2 \\
& + \frac{3}{8} t_0 \rho^2 + \frac{(\alpha + 1)}{16} t_3 \rho^{\alpha+2} + \frac{(\beta + 1)}{4} C \rho^{\beta+2} \\
& + (\eta - 1) C_s \rho^\eta - \left[ t_0 \left( \frac{1}{2} + x_0 \right) \right. \\
& + \left. \left( \frac{\alpha + 1}{6} \right) t_3 \left( \frac{1}{2} + x_3 \right) \rho^\alpha - \left( \frac{5}{2} - \frac{3 m^*}{2 m} \right) \right. \\
& \times \left. \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) - (\beta + 1) C \rho^\beta \right] (2y - 1)^2 \left( \frac{\rho}{2} \right)^2 \\
& + (\beta + 1) C \rho^{\beta+1} (2y - 1) \left( \frac{\rho}{2} \right), \quad (59)
\end{aligned}$$

$$\begin{aligned}
\mathcal{E}(\rho, y, T) &= \frac{3}{2} T \rho + \frac{3}{8} t_0 \rho^2 + \frac{1}{16} t_3 \rho^{\alpha+2} \\
& + \frac{3}{2} \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \right)^2 + \frac{1}{4} C \rho^{\beta+2} + C_s \rho^\eta \\
& - \left[ t_0 \left( \frac{1}{2} + x_0 \right) + \left( \frac{1}{6} \right) t_3 \left( \frac{1}{2} + x_3 \right) \rho^\alpha \right. \\
& - \left. \frac{3}{2} \frac{kT}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) - C \rho^\beta \right] (2y - 1)^2 \left( \frac{\rho}{2} \right)^2 \\
& + C \rho^{\beta+1} (2y - 1) \left( \frac{\rho}{2} \right), \quad (60)
\end{aligned}$$

$$\begin{aligned}
TS(\rho, y, T) &= T \rho \left[ \frac{5}{2} - y \ln \left( \frac{\lambda^3}{\gamma} y \rho \right) \right. \\
& - \left. (1 - y) \ln \left( \frac{\lambda^3}{\gamma} (1 - y) \rho \right) \right] \\
& + \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \frac{[1 + (2y - 1)^2]}{2} \left( \frac{\rho}{2} \right)^2. \quad (61)
\end{aligned}$$

Here, for the proton density ( $\rho_p$ ) and neutron density ( $\rho_n$ ), we defined the isoscalar density  $\rho$ , isovector density  $\rho_3$ , proton

fraction  $y$ , and related quantities by

$$\begin{aligned}
\rho &= \rho_p + \rho_n, \rho_3 = \rho_p - \rho_n = (2y - 1)\rho, y = \rho_p/\rho, \\
\rho_p &= \frac{1}{2}(\rho + \rho_3) = y\rho, \rho_n = \frac{1}{2}(\rho - \rho_3) = (1 - y)\rho, \\
\sum_q \rho_q^2 &= \frac{1}{2}(\rho^2 + \rho_3^2) \\
&= \frac{[1 + (2y - 1)^2]}{2} \rho^2 = [1 + 2y(y - 1)]\rho^2, \\
\sum_q \rho_q^3 &= \frac{1}{4}\rho(\rho^2 + 3\rho_3^2) \\
&= \frac{[1 + 3(2y - 1)^2]}{4} \rho^3 = [1 + 3y(y - 1)]\rho^3. \quad (62)
\end{aligned}$$

In the expression for  $\mu_q$  [Eq. (58)], the plus sign is for the case  $q = \text{proton}$  and the minus sign is for the case  $q = \text{neutron}$ .

At fixed  $T$  and  $P$ , only one of either  $\rho$  or  $y$  is the independent variable. Thus observables such as  $P$ ,  $\mathcal{E}/\rho$ , and  $\mathcal{S}/\rho$  may have a discontinuity in  $T$  or  $y$  when  $(\frac{\partial \rho}{\partial T})_{y,P}$  or  $(\frac{\partial \rho}{\partial y})_{T,P}$  diverges. We can study the behavior of thermodynamic quantities at a fixed  $P$  using  $dP = 0$  from Eq. (59),

$$\begin{aligned}
dP &= \left\{ \left( \frac{5}{2} - \frac{3 m^*}{2 m} \right) \left[ \rho - \frac{1}{2} \frac{1}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \right)^2 \right. \right. \\
& - \left. \left. \frac{1}{2} \frac{1}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) (2y - 1)^2 \left( \frac{\rho}{2} \right)^2 \right] \right\} dT \\
& + \left\{ \left[ \frac{5}{2} - \frac{3}{2} \left( \frac{m^*}{m} \right)^2 \right] T + \frac{3}{4} t_0 \rho \right. \\
& + \left. \frac{(\alpha + 2)(\alpha + 1)}{16} t_3 \rho^{\alpha+1} \right. \\
& + \left. \left[ \frac{35}{8} - \frac{15 m^*}{4 m} + \frac{3}{8} \left( \frac{m^*}{m} \right)^2 \right] \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \left( \frac{\rho}{2} \right) \right. \\
& + \left. \frac{(\beta + 2)(\beta + 1)}{4} C \rho^{\beta+1} + \eta(\eta - 1) C_s \rho^{\eta-1} \right. \\
& - \left. \left[ t_0 \left( \frac{1}{2} + x_0 \right) + \left( \frac{\alpha + 2}{2} \right) \left( \frac{\alpha + 1}{6} \right) t_3 \left( \frac{1}{2} + x_3 \right) \rho^\alpha \right. \right. \\
& - \left. \left. \left( \frac{\beta + 2}{2} \right) (\beta + 1) C \rho^\beta \right. \right. \\
& - \left. \left. \left( \frac{35}{8} - \frac{15 m^*}{4 m} + \frac{3}{8} \left( \frac{m^*}{m} \right)^2 \right) \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \right] \right. \\
& \times \left. (2y - 1)^2 \left( \frac{\rho}{2} \right) \right. \\
& + \left. (\beta + 2)(\beta + 1) C \rho^\beta (2y - 1) \left( \frac{\rho}{2} \right) \right\} d\rho \\
& - \left\{ \left[ t_0 \left( \frac{1}{2} + x_0 \right) + \left( \frac{\alpha + 1}{6} \right) t_3 \left( \frac{1}{2} + x_3 \right) \rho^\alpha \right. \right. \\
& - \left. \left. (\beta + 1) C \rho^\beta - \left( \frac{5}{2} - \frac{3 m^*}{2 m} \right) \frac{T}{2\sqrt{2}} \left( \frac{\lambda^3}{\gamma} \right) \right] \right. \\
& \times \left. (2y - 1) \left( \frac{\rho}{2} \right)^2 - (\beta + 1) C \rho^\beta \left( \frac{\rho}{2} \right)^2 \right\} 4dy. \quad (63)
\end{aligned}$$



This equation gives  $y_E(\rho)$  where both  $\partial P/\partial y = 0$  and  $\partial \rho/\partial y = 0$ :

$$y_E(\rho) = \frac{1}{2} + \frac{1}{2} \frac{(\beta + 1)C\rho^\beta}{\left[ t_0\left(\frac{1}{2} + x_0\right) + \left(\frac{\alpha+1}{6}\right)t_3\left(\frac{1}{2} + x_3\right)\rho^\alpha - (\beta + 1)C\rho^\beta - \left(\frac{5}{2} - \frac{3m^*}{m}\right)\frac{T}{2\sqrt{2}}\left(\frac{\lambda^3}{\gamma}\right) \right]}. \quad (64)$$

The concentration  $y_E(\rho)$  is independent of  $\rho$  for a momentum-independent Skyrme interaction with  $x_3 = -1/2$  and  $\beta = 0$  as considered in Refs. [10,11]. The  $x_3$  term and the density-dependent effective mass for a momentum-dependent Skyrme force introduce a small  $\rho$  dependence in  $y_E$ . Equation (59) shows that, for  $\rho$ -dependent  $y_E$ , the  $P(\rho)$  curve for different values of  $y$  at fixed  $T$  may cross at some  $\rho$ . Moreover, the minimum pressure for a given  $T$  and  $\rho$  [i.e.,  $(\partial P/\partial y)_{\rho,T} = 0$ ] occurs at  $y = y_E(\rho) \neq 0.5$  owing to the Coulomb effect. These results were not seen in Ref. [9]. At  $y_E$ , the pressure of the coexistence curve is minimum and the liquid and gas phases have the same proton fraction  $y_E$ . The condition  $\partial P/\partial y = 0$  determines the equal fraction point  $y_E$ .

### III. APPLICATIONS TO NUCLEAR MECHANICAL AND CHEMICAL INSTABILITY AND THE LIQUID-GAS PHASE TRANSITION

#### A. Mechanical and chemical instability

We now use the results to discuss features of the instability of nuclei, both mechanical and chemical, and the liquid-gas phase transition. The region of mechanical instability is determined by the condition

$$\left. \frac{dP}{d\rho} \right|_{y,T} = 0. \quad (65)$$

Figure 1 shows the behavior of the pressure  $P(\rho, y, T)$  as a function of  $\rho$  for several values of the proton fraction  $y$ . All curves are at  $T = 10$  MeV. The range of  $y$  is from  $y = 0$ , or pure neutron matter, to  $y = 1$ , or pure proton systems. The point  $y = 1/2$  corresponds to symmetric systems. Without a Coulomb interaction, results would be symmetric about the point  $y = 1/2$ , which would also be the point of equal concentration in a liquid-gas phase coexistence. Including a Coulomb interaction shifts the equal concentration point to a proton fraction of  $y = y_E(\rho) \sim 0.415$  with a momentum dependence included in the interaction and to  $y = y_E = 0.41057$  without a momentum dependence. The  $y = y_E$  curve for both the momentum-dependent and momentum-independent cases has the lowest pressure versus density dependence (i.e., the lowest  $P$  for a given value of  $\rho$  at a given  $T$ ). A higher or lower  $y$  raises the pressure at a given density. Both momentum-dependent and momentum-independent Skyrme interaction results are shown for several values of  $y$  and they are distinguished by the thickness of the lines as described in the figure caption. The momentum dependence increases the pressure in the range shown (thick lines compared to thin lines) and introduces the density dependence of  $y_E(\rho)$  given

by Eq. (64). The mechanical instability densities for each  $y$  curve at  $T = 10$  MeV are the points where the  $P(\rho, y, T)$  curve has zero slope,  $dP/d\rho|_{y,T} = 0$ . The total region of mechanical instability is obtained by a similar calculation of  $P(\rho, y, T)$  at different  $T$ . For a one-component system or a symmetric system the mechanical instability region is a curve somewhat similar to an inverted parabola with its peak at the critical point. Allowing for systems with different values of  $y$  gives a two-dimensional boundary surface for the mechanical instability region. The intersection of the surface with different

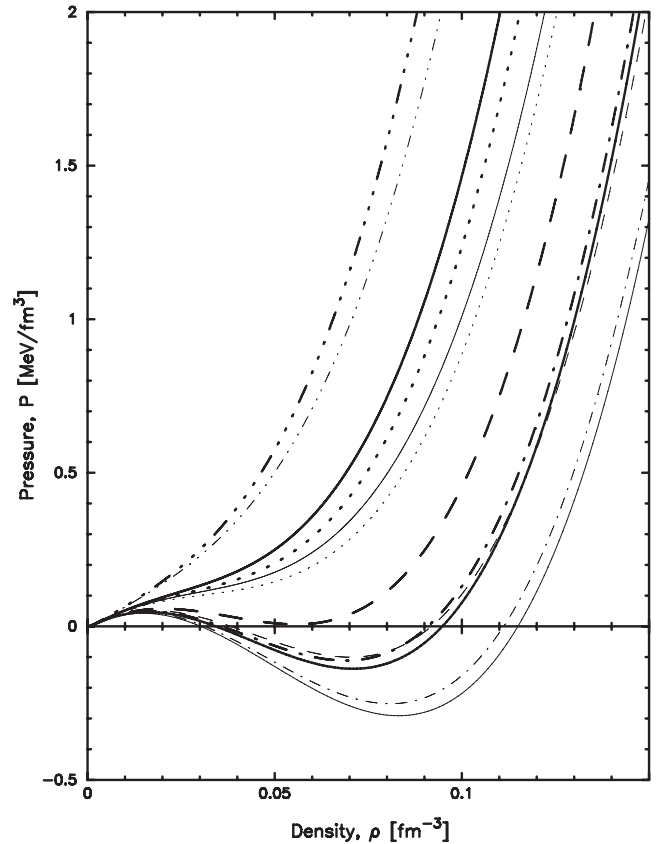


FIG. 1. Pressure  $P(\rho)$  vs  $\rho$  at  $T = 10$  MeV for various proton fractions  $y$ . The upper solid curve is for  $y = 0$ , the dashed curve for  $y = 0.2$ , the dash-dotted curve for  $y = 0.5$ , the dotted curve for  $y = 0.8$ , and the dash-tripled-dotted curve for  $y = 1$ . The thick curves are for the momentum-dependent Skyrme force and the thin curves are for the momentum-independent Skyrme force. The lower thick solid curve is for  $y = y_E(\rho)$  of Eq. (64) ( $y_E = 0.4106-0.4214$  for  $\rho = 0-0.15 \text{ fm}^{-3}$ ) with momentum-dependent Skyrme force and the lower thin solid curve is for  $y = y_E = 0.41057$  with momentum-independent Skyrme force.

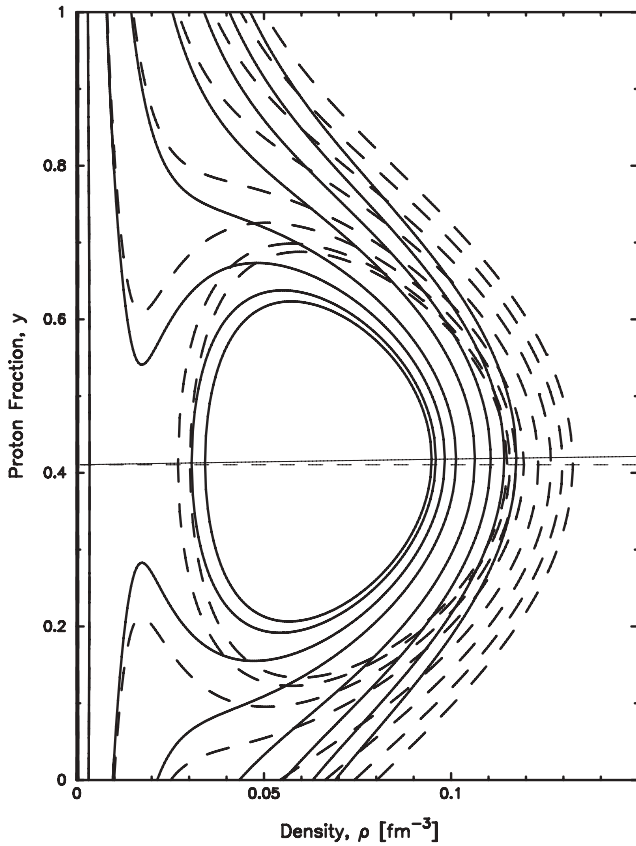


FIG. 2. Proton fraction  $y(\rho)$  for  $P = 0, 0.015, 0.05, 0.1, 0.2, 0.3, 0.4,$  and  $0.5 \text{ MeV/fm}^3$  from inside to outside at  $T = 10 \text{ MeV}$ . The solid curves are for the momentum-dependent Skyrme force and the dashed curves are for the momentum-independent Skyrme force. The thin straight lines are  $y_E(\rho)$  for the corresponding force.

$y$  planes gives the one-dimensional boundary curve or line of mechanical instability for each corresponding value of  $y$ .

Figure 2 shows the proton fraction  $y$  versus the density  $\rho$  for different fixed values of the pressure at a fixed temperature of  $T = 10 \text{ MeV}$ . The loops and curves are determined by solving  $P(\rho, y, T) = P$  for the values of  $P$  listed in the figure caption and at the temperature  $T = 10 \text{ MeV}$ . Figure 2 is obtained from Fig. 1 by drawing a horizontal line and looking at the points where the horizontal line intersects the set of  $P(\rho, y, T)$  curves. This intersection can be at one, two, or three points. Besides the innermost closed loop ( $P = 0$ ) shown in Fig. 2, a vertical line exists at  $\rho = 0$  for  $P = 0$  for all  $y = 0-1$ . Similarly, for the second inner closed loop at  $P = 0.015 \text{ MeV/fm}^3$ , a nearly parallel vertical line is present at very low density. The rightmost point on each curve and the leftmost point on a closed loop with  $d\rho/dy|_{P,T} = 0$  are at the point of equal concentration  $y_E$ . Also shown are two thin lines for  $y_E(\rho)$ . The dashed thin line is at  $y_E = 0.41057$  and is horizontal or density independent and corresponds to the momentum-independent interaction. The solid thin line is nearly horizontal with a slight density dependence and has  $y_E(\rho) = 0.4106-0.4214$  for  $\rho = 0-0.15 \text{ fm}^{-3}$ . Horizontal turning points on each curve occur at  $dy/d\rho|_{P,T} = 0$ . For each  $T$ , there is a curve  $P(\rho)|_{y,T}$  with an inflection point

for a particular  $y$ , which we call  $y_I$ . At the pressure  $P = P(\rho, y_I, T)$ , the closed loop in Fig. 2 just breaks at the point of  $y = y_E$  on the left low-density side and creates two new horizontal turning points with  $\partial y/\partial \rho = 0$ . Figure 2 also shows the result that a momentum-independent force has closed loops outside those of a momentum-dependent force and open curves to the right of those of a momentum-dependent force with the same pressure  $P$ .

The region of chemical instability [spinodal in  $\mu(y)|_{P,T}$ ] is determined by the condition

$$\left. \frac{d\mu_q}{dy} \right|_{P,T} = 0 \quad (66)$$

for each component  $q = p$  or  $n$ . These conditions for either protons or neutrons give the same relation since

$$y d\mu_p + (1-y) d\mu_n = \frac{1}{\rho} dP. \quad (67)$$

This general condition will be used later in our discussion of results given in various figures. The result is also useful for checking numerical results. The chemical instability condition can be rewritten in terms of derivatives of the chemical potential and pressure with respect to the density variable  $\rho$  and proton fraction  $y$ . Namely, the chemical instability condition can be obtained from the following relation [11]:

$$\left. \frac{dP}{d\rho} \right|_{y,T} \left. \frac{d\mu_q}{dy} \right|_{\rho,T} = \left. \frac{dP}{dy} \right|_{\rho,T} \left. \frac{d\mu_q}{d\rho} \right|_{y,T}. \quad (68)$$

The expressions developed for the proton and neutron chemical potentials are functions of the variables  $(\rho, y, T)$ . The equation of state  $P(\rho, y, T)$  can then be used to find their behavior in terms of  $(y, P, T)$  or  $(\rho, P, T)$ . The behavior with  $y$  of the proton chemical potential  $\mu_p(\rho, P, T) \rightarrow \mu_p(y)$  and neutron chemical potential  $\mu_n(\rho, P, T) \rightarrow \mu_n(y)$  at various values of the pressure  $P$  and at a fixed temperature  $T = 10 \text{ MeV}$  is shown in Fig. 3. The chemical instability region boundaries are determined by the points where the slope of each chemical potential with respect to  $y$  is zero. Further discussion of the chemical spinodal line is given in the next section. The behavior of the proton chemical potential  $\mu_p(\rho, P, T) \rightarrow \mu_p(\rho)$  and neutron chemical potential  $\mu_n(\rho, P, T) \rightarrow \mu_n(\rho)$  with density  $\rho$  at various fixed values of the pressure  $P$  and at a fixed temperature  $T = 10 \text{ MeV}$  is shown in Fig. 4. Figures 2 and 4 show some similarities in the behavior of the plotted quantities (i.e., inner closed loops at low pressure, to outer curves that almost form closed loops with increasing pressure, to open curves with further increase in pressure).

## B. Liquid-gas phase transition and the coexistence curve

For a one-component system the coexistence curve is a line obtained by the familiar Maxwell construction, as already noted. For a two-component system the coexistence region is a surface obtained as follows. The condition for coexistence between the two phases requires the proton chemical potentials to be the same in two phases and, similarly, the neutron chemical potentials must be the same in the two phases at a given pressure and temperature. Note that the proton fraction

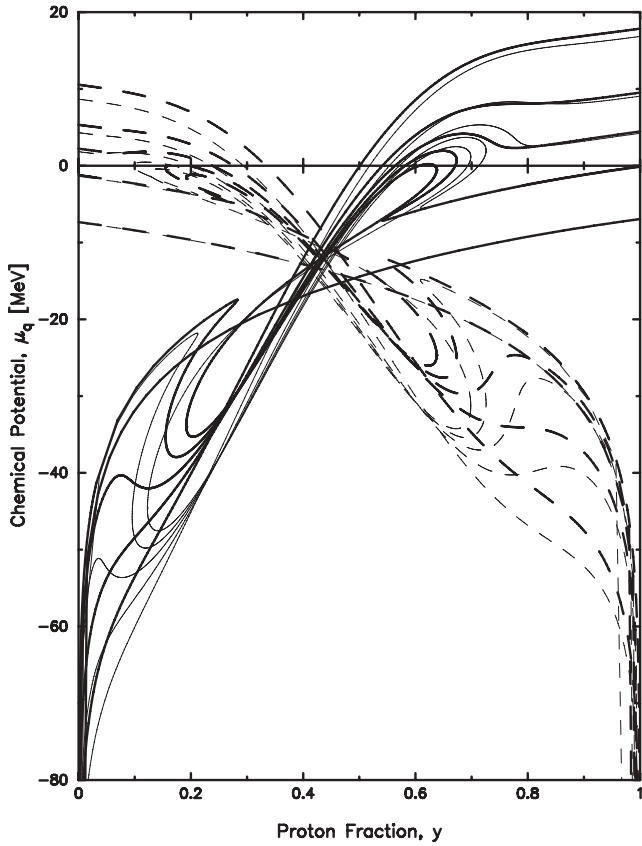


FIG. 3. Chemical potential  $\mu_p(y)$  and  $\mu_n(y)$  for  $P = 0.015, 0.05, 0.1, 0.2,$  and  $0.5$  from top to bottom curves for protons (solid curve) and from bottom to top curves for neutrons (dashed curve) at  $T = 10$  MeV. Thick curves are for the momentum-dependent Skyrme force and the thin curves for the momentum-independent Skyrme force.

need not be the same in each of the two phases. In fact, the liquid phase should be a more symmetric system than the gas phase because of the symmetry potential, as seen in Refs. [10,11]. Figures 5–9 show features of the coexistence curves together with the mechanical and chemical instability curves.

The condition of phase coexistence corresponds to the rectangular box geometrical construction in the chemical potential plots of Fig. 3 or of Fig. 4. Namely, the chemical potential equality condition  $\mu_p(y_1, P, T) = \mu_p(y_2, P, T)$  and  $\mu_n(y_1, P, T) = \mu_n(y_2, P, T)$  leads to a rectangular box in Fig. 3 with vertical sides connecting  $\mu_p(y_1, P, T)$  to  $\mu_n(y_1, P, T)$  for side 1 and  $\mu_p(y_2, P, T)$  to  $\mu_n(y_2, P, T)$  for side 2. The horizontal sides are the chemical potential equality conditions at  $y_1$  and  $y_2$  for neutrons and for protons. The rectangular box shrinks in its horizontal direction in  $\mu_q$ - $y$  plots as the point of equal concentration, where the liquid and gas phases have the same proton fraction, is approached (the lowest point of the coexistence curve in Fig. 5).

Figure 5 shows various features of the coexistence region in pressure versus proton fraction. The coexistence regions are marked by the dark thicker solid line for a momentum-dependent force and the dark thicker dashed line for a

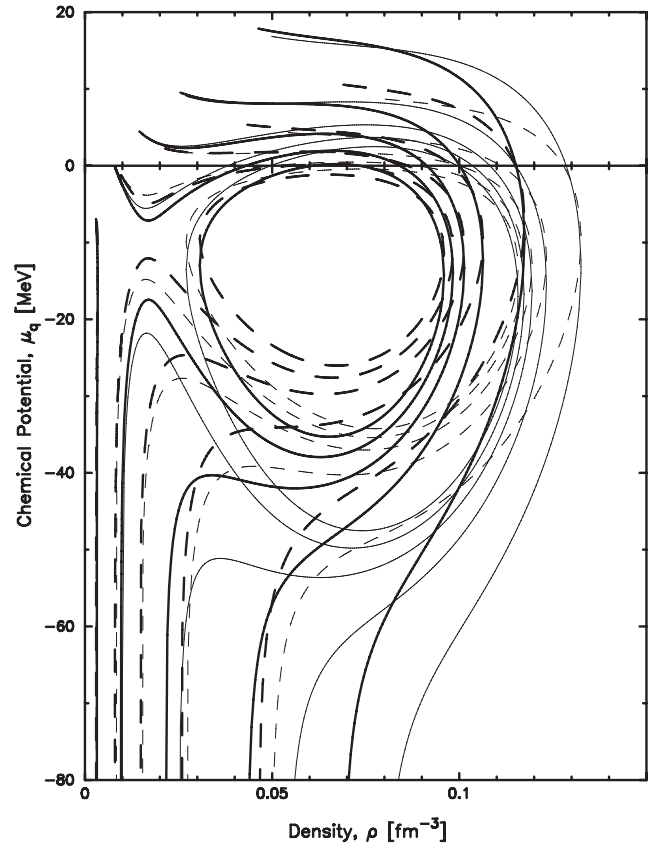


FIG. 4. Same as Fig. 3 but for  $\mu_p(\rho)$  and  $\mu_n(\rho)$  vs  $\rho$ .

momentum-independent force. Also shown are associated chemical instability regions as a thinner solid line and thinner dashed line. The calculations are done at a temperature of 10 MeV. For a two-component system, the coexistence and instability regions are two-dimensional surfaces in pressure, temperature, and proton fraction as previously mentioned. The pressure-proton fraction behavior shown is a consequence of cutting these surfaces with a constant-temperature plane. The results at  $T = 10$  MeV are the loops shown. Other temperatures can be obtained in a similar fashion. For a momentum-independent force the chemical instability region basically lies inside the coexistence curve and peaks at the top of the coexistence loop, the critical points. The condition  $dP/dy|_T = 0$  with  $d^2P/dy^2|_T < 0$  gives a critical point on the coexistence curve and the condition  $dy/dP|_T = 0$  gives the point with maximal asymmetry at the leftmost and rightmost points of the coexistence curve. The proton-rich  $y \geq y_E$  and neutron-rich  $y \leq y_E$  loops are very asymmetric because of the Coulomb interaction. The inclusion of velocity- or momentum-dependent interactions leads to further modification of the coexistence curve and chemical instability curves. This modification is easily seen in the figure by comparing the dashed momentum-independent curves with the solid momentum-dependent case. The figure shows that the momentum-dependent interaction that was used has a larger effect on the asymmetric proton-rich loop ( $y > y_E$ ), significantly reducing its maximum pressure. The maximum of the neutron-rich loop ( $y < y_E$ ) remains somewhat unchanged

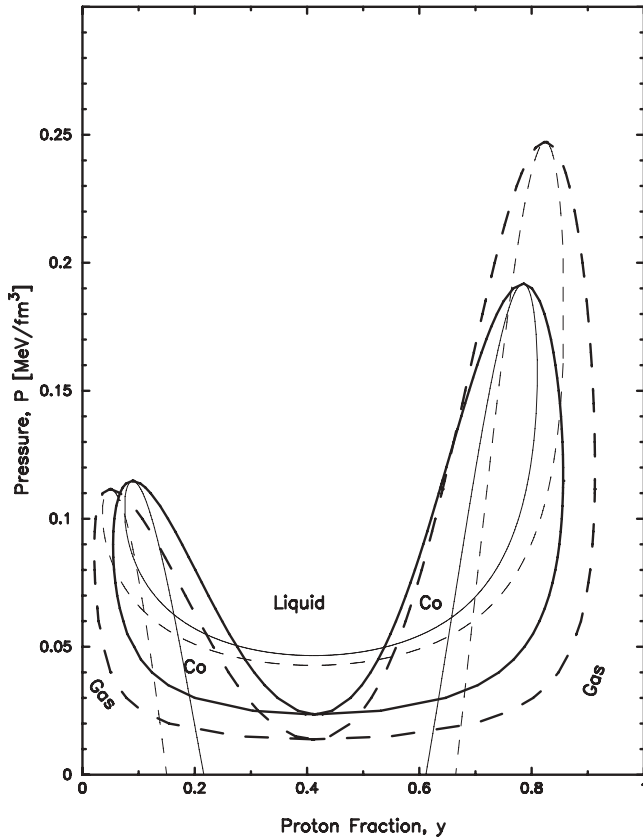


FIG. 5. Pressure  $P$  vs proton fraction  $y$  for coexistence loop (thick curves) at  $T = 10$  MeV. The solid curve is for the momentum-dependent Skyrme force and the dashed curve is for the momentum-independent Skyrme force. The thin curves are the chemical instability boundary curves for each case of Skyrme interaction respectively. For both momentum-dependent and momentum-independent cases the maxima of the chemical instability loop and the coexistence loop occur at the same point where the curves are tangent to each other as discussed in the text. The point of equal concentration is  $y_E \sim 0.415$  for the momentum-dependent case and  $y_E = 0.41057$  for the momentum-independent case.

with a small increase. Another effect is to shift the two loops inward toward the equal concentration point  $y_E$ . A third effect is to shift the lowest pressure point, which occurs at the equal concentration  $y_E$ , upward, with the value of  $y_E$  remaining nearly unchanged. Finally, it should be noted that the peaks of the coexistence and chemical instability curves are at the same point where the curves are tangent to each other. We see no indication of a truncation effect in our model where the coexistence curve intersects the chemical instability curve before reaching the peak critical point. A truncation effect gives a limiting pressure (below the maximum pressure of the chemical instability curve) above which a liquid-gas phase transition cannot take place [22].

Figure 6 shows plots in  $y$  versus  $\rho$  of phase coexistence curves, instability boundary loops for both chemical and mechanical instability, and features of  $\partial\mu_q/\partial\rho|_{y,T} = 0$  for proton and neutrons. The thin curves are for a momentum-independent interaction and the thick curves are for a momentum-dependent interaction. The calculations are done

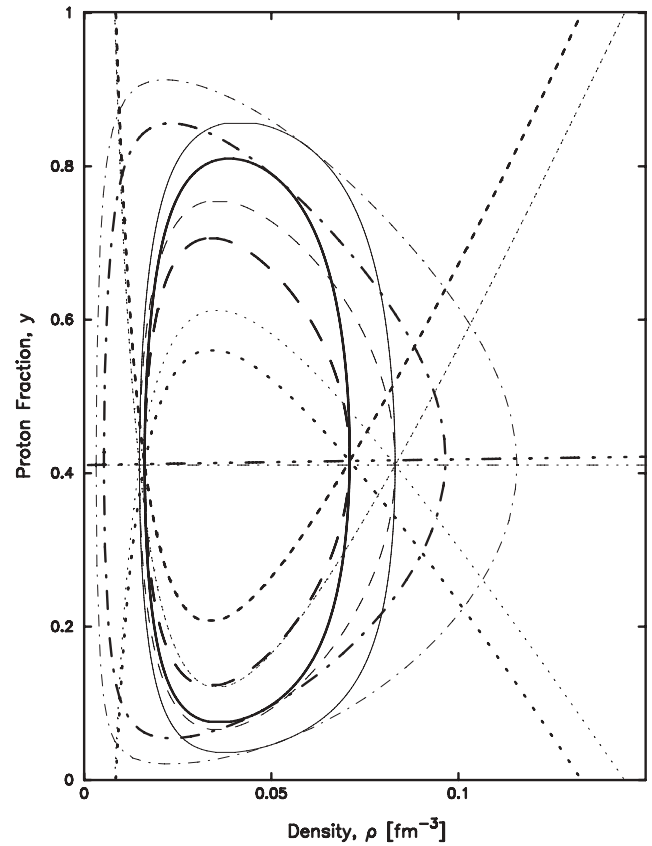


FIG. 6. The coexistence curves (dash-dotted line), chemical instability boundary curves (solid line), and mechanical instability boundary curves (dashed line) at  $T = 10$  MeV. Also shown are the  $\partial\mu_q/\partial\rho = 0$  curves for protons (dotted line) and for neutrons (short dash line) at  $T = 10$  MeV. The dash-triple-dotted line is for  $y_E(\rho)$ . The thick lines are for the momentum-dependent Skyrme force and the thin lines are for the momentum-independent Skyrme force. The momentum-dependent loops are inside the momentum-independent loops.

at a fixed temperature of 10 MeV. Some features common to both cases are as follows: The mechanical and chemical instability boundary curves are closed loops with the mechanical loop (dashed line) inside the chemical instability loop (solid line). These two loops touch at  $y_E$ , the dash-triple-dotted line. The concentration  $y_E(\rho)$  increases slightly with  $\rho$  for a momentum-dependent interaction whereas it is constant (horizontal) for a momentum-independent interaction. The  $\rho$  dependence of  $y_E(\rho)$  come from the  $\rho$  dependence of the effective mass and also from the  $x_3$  term, as can be seen in Eq. (64). Also intersecting at these same points are  $\partial\mu_p/\partial\rho = 0$  and  $\partial\mu_n/\partial\rho = 0$ . Different features and behaviors exist for the two cases. The momentum-dependent case (thick curves) has behaviors that are compressed in these  $y$ - $\rho$  plots. The coexistence curves have a different quantitative but similar qualitative behavior in the two cases. The coexistence loop (dash-dotted line) is outside the other two loops and tangent to chemical instability loop at two points. These two points are the critical points of low and high  $y$ , which are shown in Fig. 5 where the two loops touch at the peak of each loop. Comparing the two cases quantitatively, we see a compression

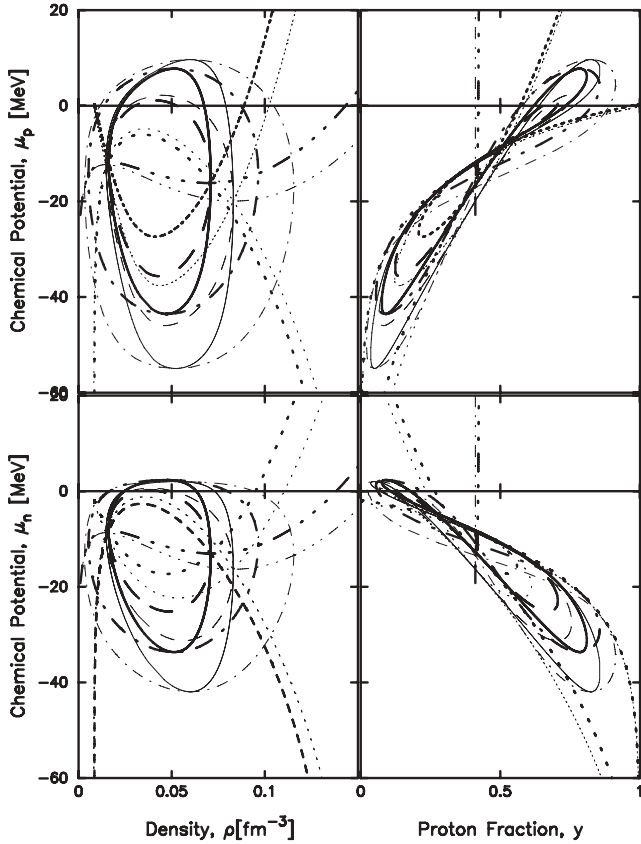


FIG. 7. Chemical potential  $\mu_p$  (upper panel) and  $\mu_n$  (lower panel) for various boundary curves at  $T = 10$  MeV. The meanings of the curves are the same as in Fig. 6.

of the results of the momentum-dependent case (thick curves) with respect to the results of the momentum-independent case (thin curves). The thick loops are inside of thin loops.

Figures 7 and 8 show chemical potentials for both proton  $\mu_p$  and neutron  $\mu_n$  and pressure  $P$  along the various curves of coexistence and chemical and mechanical instabilities. Curves in Fig. 7 illustrate the behavior of each chemical potential with density on the left panel and proton fraction on the right panel.

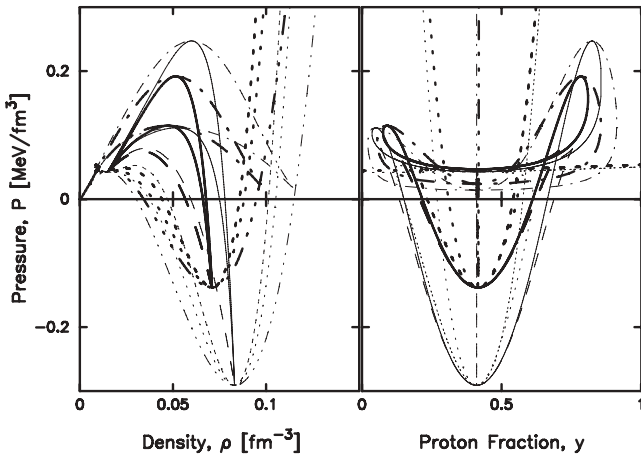


FIG. 8. Pressure  $P$  for various curves. The meanings of the curves are the same as in Fig. 6.

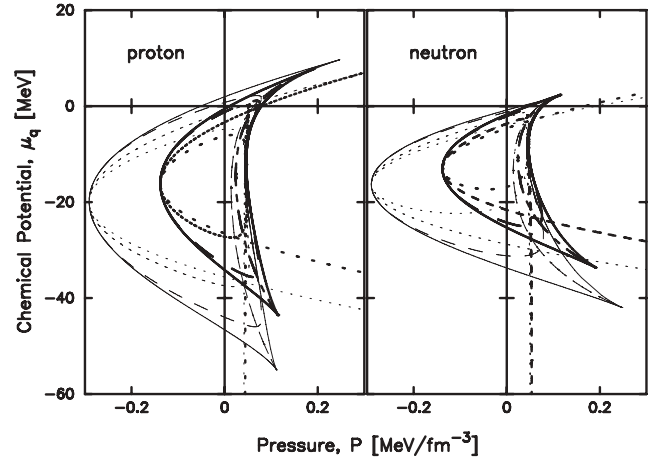


FIG. 9. Chemical pressure  $\mu_q$  vs pressure  $P$  for various boundary curves. The left panel is for the proton  $\mu_p$  and the right panel is for the neutron  $\mu_n$ . The meanings of the curves are the same as in Fig. 6.

Curves in Fig. 8 are pressure versus density on the left side and pressure versus proton fraction on the right. The separate pressure-proton fraction behavior in Fig. 8 was already shown in Fig. 5, but now these two figures contain additional plotted quantities, which are the  $\partial\mu_q/\partial\rho|_{y,T=0}$  curves. The chemical potential density curves in Fig. 7 have features similar to those discussed in Fig. 6. Both momentum-dependent and momentum-independent cases of Fig. 7 and Fig. 8 show tangent points of the solid line and dash-dotted line. Also seen in these figures is the compression or shrinking of various curves for the momentum-dependent case with respect to the momentum-independent case. The thick loops are inside of thin loops. Figure 5 shows that the momentum-dependent interaction leaves the point of equal concentration nearly unchanged (i.e., from  $y = 0.4106$  to  $y \approx 0.415$ ).

Figure 9 shows the behavior of the boundary curves of the proton and neutron chemical potentials with pressure for both momentum-dependent and momentum-independent Skyrme interactions. A comparison of the thick curves (momentum-dependent case) and thin curves (momentum-independent case) shows that the qualitative behavior is the same. Quantitative difference exist with the momentum-independent behavior being an enlargement of the momentum-dependent shape. The coexistence arc and the chemical instability loop meet at the cusp. The behavior shown in these figures also confirms that no truncation effects exist in our study.

#### IV. SUMMARY AND CONCLUSIONS

In this paper we studied the thermodynamic properties of a two-component system of hadronic matter made of protons and neutrons. Our analysis is based on a mean-field model using a local Skyrme interaction and includes both velocity- or momentum-dependent and momentum-independent interactions, besides volume, symmetry, and Coulomb effects. We have used a somewhat simplified description of the velocity dependence of the nuclear interaction. In particular we have used a density-dependent effective mass approximation.



Effective mass approximations are frequently used in physics to capture the main effects and they lead to a simpler set of equations and a corresponding simpler analysis. As noted we still keep Coulomb and surface terms, which are present in realistic nuclear systems. It is the interplay of volume, surface, symmetry, and Coulomb and momentum-dependent terms that is studied here. In fact, the interplay of such terms makes nuclei a unique system for studying phase transitions and chemical and mechanical instability in binary systems. We then applied the basic thermodynamic relations that we developed to issues related to the mechanical and chemical instability of nuclei and features associated with a liquid-gas phase transition in this system.

Because of the two-component nature of real nuclear systems, the analysis involves a study of the behavior in proton fraction, density, and temperature ( $y, \rho, T$ ) and also proton fraction, pressure, and temperature ( $y, P, T$ ). We studied systems with proton fraction  $y = 0-1$ , where  $y = 0$  corresponds to a system of pure neutrons and  $y = 1$  is for a system of pure protons. An important system with large neutron excess is a neutron star. The study of nuclear systems with arbitrary proton/neutron ratios is also important for future RIB experiments and for medium-energy collisions where the liquid-gas phase transition is studied experimentally. In a liquid-gas phase transition the liquid and gas phase have different proton fractions because of symmetry and Coulomb effects. The proton fraction in the liquid phase reflects a more symmetric system than the gas phase where a higher asymmetry exists. The process of producing a larger neutron excess in the gas phase is referred to as isospin fractionation, and a review can be found in Refs. [1,2,4-7]. The process is modified somewhat by the Coulomb interaction, which leads to proton diffusion of some protons from the liquid phase back into the gas phase, as discussed in Refs. [10,11].

One of the unique aspects of nuclear systems is a velocity or momentum dependence in the two-body interaction. Here, we also study the role of this momentum dependence in the thermodynamic properties of the system. Then, we extend the discussion of its role to nuclear instabilities and phase transitions and make a comparison with the case without momentum dependence. A characteristic pattern of qualitative similarities and quantitative differences appears between a

momentum- or velocity-dependent Skryme interaction and a momentum- or velocity-independent Skryme interaction. These patterns can be seen in Figs. 1-9 and are discussed in detail in Sec. III, which we briefly summarize now.

Figure 1 shows that the momentum dependence increases the pressure at a given density. Figures 2 and 4 show proton fraction versus density and chemical potential versus density at several pressures and at a fixed temperature. The qualitative features are the same between momentum-dependent and momentum-independent forces. However, sizable quantitative differences are present between the two types of interactions. For example the solid loops (momentum-dependent interaction) in proton fraction versus density of Fig. 2 are reduced versions of the same dashed loops (momentum-independent interaction). Similarly, the chemical instability boundaries for a momentum-dependent Skryme interaction are found to be reduced versions of the same boundaries for momentum-independent Skryme interactions, as can be seen from Fig. 5 and a comparison of the thin curves of Figs. 6-9 with the corresponding thick curves of these figures. Figure 5 also shows that momentum-dependent terms reduce the height of the proton-rich asymmetric loop ( $y > y_E$ ) and leave the height of the neutron asymmetric loop ( $y < y_E$ ) almost unchanged while the lowest pressure point, which is the point of equal concentration  $y_E$ , is shifted upward with the value of  $y_E$  remaining nearly unchanged. From Fig. 5 we also see that the chemical instability loops lie on top of each other for protons and neutrons, as required by the general connection of Eq. (67). Also seen is that the chemical instability loop is inside the coexistence loop and tangent to it at the maxima of each loop. The largest and smallest  $y$  in the coexistence loops are shifted inward toward the point of equal concentration  $y_E$ . Figures 6 and 7 shows that the mechanical instability loop is inside the chemical instability loop and tangent at the equal proton fraction  $y_E(\rho)$  without touching it at the peak.

#### ACKNOWLEDGMENTS

S.J.L. was on sabbatical leave from Kyung Hee University and spent a sabbatical year at Rutgers University in 2006-2007. This work was supported in part by the US Department of Energy under DOE Grant No. DE-FG02-96ER-40987.

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