

Study of dissipative collisions of ^{20}Ne ($\approx 7\text{--}11$ MeV/nucleon) + ^{27}Al

Aparajita Dey, C. Bhattacharya, S. Bhattacharya, T. K. Rana, S. Kundu, K. Banerjee, S. Mukhopadhyay, S. R. Banerjee, D. Gupta, and R. Saha

Variable Energy Cyclotron Centre, Sector-1, Block-AF, Bidhan Nagar, Kolkata-700 064, India

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The inclusive energy distributions of complex fragments ($3 \leq 9$) emitted in the reactions ^{20}Ne (145, 158, 200, 218 MeV) + ^{27}Al have been measured in the angular range $10^\circ\text{--}50^\circ$. The fusion-fission and the deep-inelastic components of the fragment yield have been extracted using multiple Gaussian functions from the experimental fragment energy spectra. The elemental yields of the fusion-fission component have been found to be fairly well explained in the framework of the standard statistical model. It is found that strong competition occurs between the fusion-fission and the deep-inelastic processes at these energies. The time scale of the deep-inelastic process was estimated to be typically in the range of $\sim 10^{-21}\text{--}10^{-22}$ s, and it was found to decrease with increasing fragment mass. The angular momentum dissipations in the fully energy damped deep-inelastic process have been estimated from the average energies of the deep-inelastic components of the fragment energy spectra. The estimated angular momentum dissipations, for lighter fragments in particular, are found to be greater than those predicted by the empirical sticking limit.

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I. INTRODUCTION

Complex fragment emission in heavy ion induced reactions involving light nuclei ($A_{\text{target}} + A_{\text{projectile}} \lesssim 60$) at bombarding energies well above the Coulomb barrier has been studied quite extensively in recent years [1–16] to understand the origin of fragment emission and the role of the underlying dynamics. It is well known that different types of reaction mechanisms contribute to fragment emission at different energy regions. At bombarding energies near the Coulomb barriers, the complete fusion (CF) process is the dominant reaction mechanism. At higher energies, this process is limited by the contributions of other competing processes, such as quasielastic (QE) and deep-inelastic (DI) collisions. The CF cross section increases with incident energy at lower energies and reaches a near-saturation value at higher energies. On the other hand, nonfusion processes become increasingly dominant at higher energies. Thus, the fragments emitted in light heavy ion collisions at energies well above the Coulomb barrier may have different origins, which extend from partially relaxed processes—such as QE collision/projectile breakup [17,18] and DI transfer and orbiting [8,9,19–22]—to fully relaxed fusion-fission (FF) [23–28] processes. In some cases, the structure of the nuclei has also been found to play an important role. Therefore, the characterization of the origin of fragments is of utmost importance to extracting information on the relaxation of various degrees of freedom (energy and angular momentum dissipation, for example) in heavy ion collision in this energy domain. However, for light systems, the distinction between different reaction mechanisms, FF and orbiting or DI processes in particular, is very difficult, as there is a strong overlap in the elemental distributions of the fragments emitted in these processes.

Binary decay of the light composite system ^{47}V has been investigated quite extensively in the past years. In some cases (where the composite system ^{47}V was produced through inverse kinematic reactions, such as $^{35}\text{Cl} + ^{12}\text{C}$ [4,5,29,30],

$^{31}\text{P} + ^{16}\text{O}$ [7], and $^{23}\text{Na} + ^{24}\text{Mg}$ [6]), the ^{47}V composite system was found to deexcite statistically. In these cases, the emitted fragment yields show $1/\sin \Theta_{\text{c.m.}}$ -like angular dependence and have angle-independent mean total kinetic energy (TKE) values in agreement with the decay of a fully energy equilibrated composite system. The experimental cross sections are well explained with the predictions of the extended Hauser-Feshbach method (EHFM) [25] and thus suggest a fusion-fission origin. It was further concluded that the orbiting process [9] does not play a significant role in the decay of the ^{47}V composite system. On the other hand, studies on the same system, produced through direct kinematic reactions ($^{20}\text{Ne} + ^{27}\text{Al}$ [31–33]), showed that the angular distributions of fully damped fragments are forward peaked and fall off faster than $1/\sin \Theta_{\text{c.m.}}$, which behaviors are characteristic of DI processes. Subsequently, assuming the fragment yield to be of DI origin (and assuming the sticking limit for the angular momentum dissipation), a highly elongated configuration for the $^{20}\text{Ne} + ^{27}\text{Al}$ dinuclear system was conjectured [32].

It is clearly evident from the above that some degree of ambiguity prevails over the interpretation of fragment yield data in the decay of ^{47}V composite system. To resolve the ambiguity, it is necessary to understand the roles played by various competing processes in this energy regime. For example, there is strong competition between FF and DI processes at these energies, which should be deciphered properly to extract meaningful information about the reaction mechanism. In recent years, we have developed a scheme for the decomposition of FF and DI components of the fragment yield [14,20] in order to study systematically the competition between FF and DI processes in light heavy ion collisions at energies well above the barrier. In this paper, we report an experimental study of fragment emission in the decay of the ^{47}V composite system, produced through ^{20}Ne (145–218 MeV) + ^{27}Al reactions. Some of the ^{20}Ne (145 MeV) + ^{27}Al data have already been published [20].

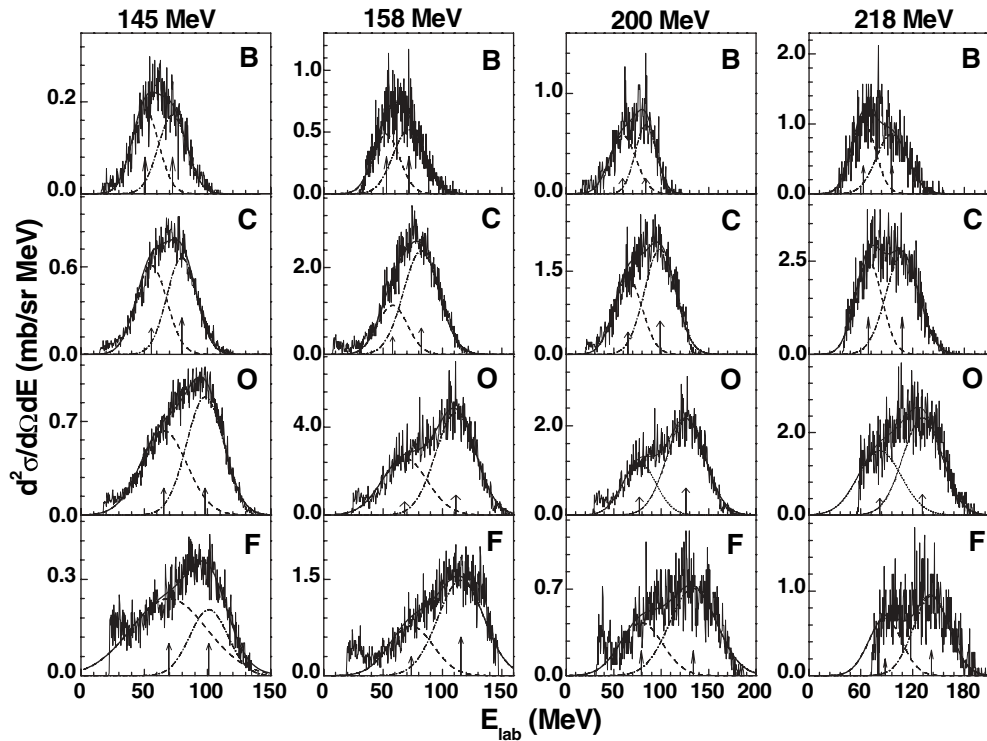


FIG. 1. Inclusive energy distributions for different fragments emitted in $^{20}\text{Ne} + ^{27}\text{Al}$ reaction at different bombarding energies at an angle $\theta_{\text{lab}} = 15^\circ$. Curves show the FF (dashed) and DI (dash-dotted) components and their sum (FF + DI) (solid). Arrows indicate the centroids of the fitted Gaussians.

The FF and DI components of the fragment yields have been extracted in each case to study the systematics of the two processes in the above energy range.

The paper is arranged as follows. The experimental procedures are given in the next section. The experimental results are presented in Sec. III. Finally, the discussion and conclusion are given in Sec. IV.

II. EXPERIMENTAL PROCEDURES

The experiments were performed using the accelerated ^{20}Ne ion beams from the variable energy cyclotron at Kolkata. The beam energies were 145, 158, 200, and 218 MeV; the target was made of self-supporting ^{27}Al of thickness $\sim 515 \mu\text{g}/\text{cm}^2$. Fragments were detected using two types of solid state telescopes: telescopes with $\sim 10 \mu\text{m} \Delta E$ [Si(SB)], $300 \mu\text{m} E$ [Si(SB)] were used to detect heavier fragments ($5 \leq Z \leq 9$), whereas telescopes with $\sim 10 \mu\text{m} \Delta E$ [Si(SB)], $5 \text{ mm} E$ [Si(Li)] were used for the detection of lighter fragments ($3 \leq Z \leq 5$). The two types of telescopes were mounted on two arms of the scattering chamber which could move independently. Typical solid angle subtended by each detector was $\sim 0.6 \text{ msr}$. The telescopes were calibrated using elastically scattered ^{20}Ne ion from Au, Al targets and Th- α source. The systematic errors in the data, arising from the uncertainties in the measurements of the solid angle, target thickness, and the calibration of current digitizer have been estimated to be $\approx 15\%$.

III. EXPERIMENTAL RESULTS

A. Energy distribution

The inclusive energy distributions were measured for the fragments ($3 \leq Z \leq 9$) emitted in the reaction $^{20}\text{Ne} + ^{27}\text{Al}$ at the bombarding energies 145, 158, 200, and 218 MeV in the angular range 10° – 50° . Typical fragment energy spectra (at $\theta_{\text{lab}} = 15^\circ$) are displayed in Fig. 1 for different bombarding energies. It is evident from Fig. 1 that the shapes of the energy spectra of the heavier fragments (*viz.*, F) are quite different from those of the lighter fragments, such as B and C, at all bombarding energies. This difference is mainly due to the variation of the relative contributions of DI and FF processes for different fragments. The contributions of FF and DI components have been estimated by fitting the measured energy spectra with Gaussian functions as per the procedure in Ref. [14]. The energy spectra of different fragments at each angle have been fitted with two Gaussian functions in two steps. In the first step, the FF component of the fragment energy distribution has been extracted in the following way; the energy distribution of the FF component was taken to be a Gaussian. The centroid of the Gaussian was obtained from Viola systematics [34,35], adapted for light nuclear systems [36], of total kinetic energies of mass-symmetric fission fragments duly corrected for asymmetric factor [15]. The FF component of the energy spectrum thus obtained was then subtracted from the full energy spectrum. In the next step, the DI component was obtained by fitting the subtracted energy spectrum with a second Gaussian. This is illustrated in Fig. 1, where the extracted FF (dashed curve) and DI

(dash-dotted curve) components are displayed along with the experimental data for all bombarding energies. It is clear from Fig. 1 that the experimental energy spectra, for all fragments at all bombarding energies, may be explained fairly well as the sum of two Gaussian functions representing the FF and DI components (sums of FF and DI are shown by the solid curves). In each spectrum, the arrow at the lower energy corresponds to the centroid of the Gaussian for the FF component and the arrow at the higher energy corresponds to the centroid of the Gaussian for the DI component.

B. Angular distribution

The FF and the DI components of the fragment angular distributions were obtained by integrating the respective energy distributions. The center-of-mass (c.m.) angular distributions of the FF components of various fragments for all bombarding energies are displayed as a function of c.m. angle ($\Theta_{\text{c.m.}}$) in Fig. 2. The transformation from the laboratory system to the c.m. system was done with the assumption of a two-body kinematics averaged over total kinetic energy distributions. The angular distributions of FF components exhibit $d\sigma/d\Omega \sim 1/\sin \Theta_{\text{c.m.}}$ -like dependence (solid lines in Fig. 2), which conform with the systematics of fission decay of a fully equilibrated system.

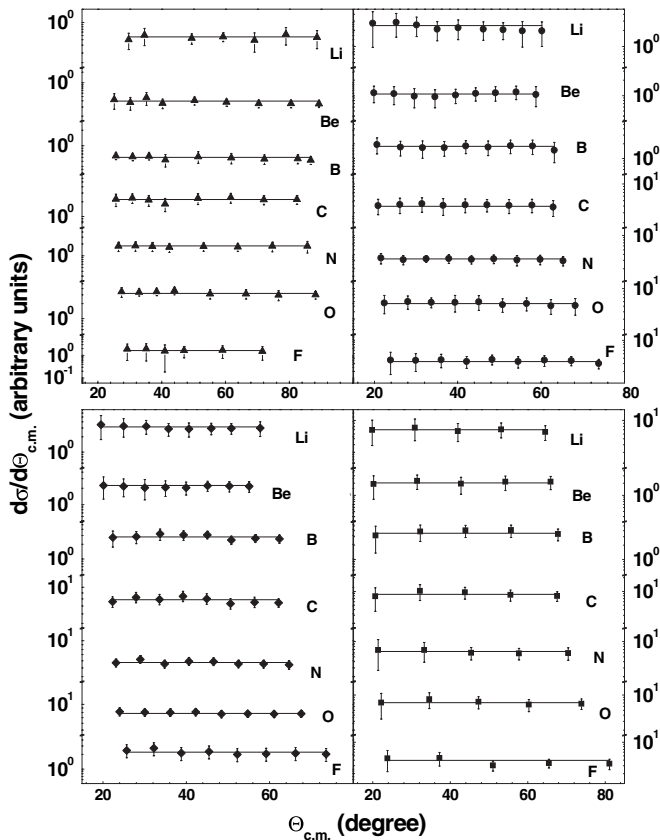


FIG. 2. c.m. angular distributions of the fusion-fission component for different fragments at the bombarding energies 145 (triangle), 158 (circle), 200 (diamond), and 218 MeV (square). Lines correspond to fissionlike angular distribution ($d\sigma/d\Omega \sim 1/\sin \Theta_{\text{c.m.}}$) fit to the data.

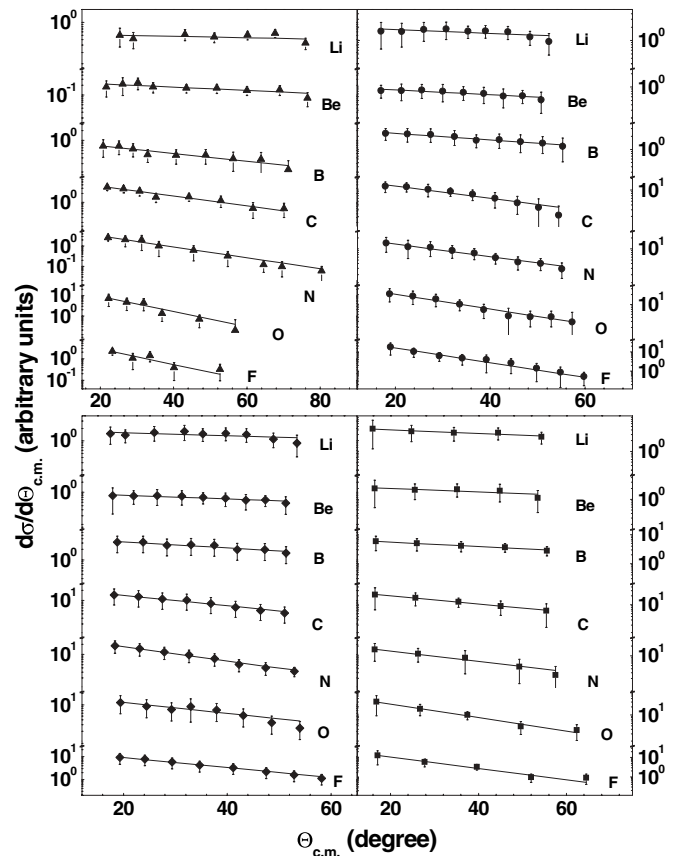


FIG. 3. c.m. angular distributions of the deep-inelastic component for different fragments at the bombarding energies 145 (triangle), 158 (circle), 200 (diamond), and 218 MeV (square). Lines are exponential fit [Eq. (1)] to the data.

The c.m. angular distributions of the DI components of different fragments for all bombarding energies have been displayed as a function of c.m. angle in Fig. 3. A rapid fall of the angular distribution (faster than $d\sigma/d\Omega \sim 1/\sin \Theta_{\text{c.m.}}$) indicates a shorter lifetime of the composite system. Such lifetimes are incompatible with the formation of an equilibrated compound nucleus but may still reflect significant energy damping within a deep-inelastic mechanism. From the measured forward-peaked angular distribution, it is possible to estimate the lifetime of the intermediate dinuclear complex using a diffractive Regge-pole model [15,37]. The angular distributions have been fitted with the following expression:

$$\frac{d\sigma}{d\Omega} \propto \frac{C}{\sin \Theta_{\text{c.m.}}} e^{-\Theta_{\text{c.m.}}/\Theta_o}, \quad (1)$$

where, Θ_o is called the “life angle,” which is the angle of rotation of the dinuclear composite during the time interval between its formation and the decay into two fragments. The fit to the DI angular distribution with Eq. (1) is shown in Fig. 3 (solid line). The values of Θ_o thus obtained are given in Table I.

C. Average Q value distribution

The average Q value $\langle Q \rangle$ was estimated from the total average kinetic energy of the fragments, E_K^{tot} , using the

TABLE I. Time scales for emission of different DI fragments. Upper (lower) limit corresponds to l_{cr} (l_{gr}). Numbers in brackets denote corresponding uncertainties.

E_{lab} (MeV)	l_{cr} (\hbar)	l_{gr} (\hbar)	Fragment	Θ_o (radian)	τ (10^{-22} s)
145	37	51	Li	7.68(1)	20.85(3)–15.13(2)
			Be	1.99(1)	5.94(2)–4.31(2)
			B	0.67(2)	2.16(7)–1.57(5)
			C	0.43(1)	1.44(3)–1.04(3)
			N	0.31(1)	1.10(3)–0.80(2)
			O	0.22(1)	0.82(3)–0.59(3)
			F	0.21(1)	0.82(4)–0.60(2)
158	38	54	Li	3.36(1)	8.88(3)–6.25(2)
			Be	1.76(1)	5.11(3)–3.60(2)
			B	1.10(1)	3.46(3)–2.43(2)
			C	0.54(2)	1.76(6)–1.24(4)
			N	0.47(1)	1.62(3)–1.14(2)
			O	0.35(2)	1.26(8)–0.89(5)
			F	0.18(2)	0.68(8)–0.48(5)
200	41	63	Li	3.09(1)	7.57(2)–4.93(1)
			Be	1.59(5)	4.29(12)–2.79(8)
			B	0.98(2)	2.85(6)–1.85(4)
			C	0.53(2)	1.60(6)–1.04(4)
			N	0.36(1)	1.15(3)–0.75(2)
			O	0.32(2)	1.07(6)–0.70(4)
			F	0.24(3)	0.84(9)–0.55(7)
218	42	66	Li	1.37(2)	3.28(4)–2.09(3)
			Be	1.14(1)	3.00(2)–1.90(2)
			B	0.99(1)	2.81(3)–1.79(2)
			C	0.56(2)	1.65(6)–1.05(4)
			N	0.52(1)	1.62(3)–1.03(2)
			O	0.30(2)	0.98(6)–0.62(3)
			F	0.24(1)	0.82(4)–0.52(2)

relation $E_K^{tot} = E_{c.m.} + \langle Q \rangle$. The fragment total average kinetic energies in the center of mass were obtained from the respective laboratory values assuming two-body kinematics. The variations of $\langle Q \rangle$ with the center-of-mass emission angle for the fragments ($3 \leq Z \leq 9$) obtained at different bombarding energies are displayed in Fig 4. The fragment kinetic energies were appropriately corrected for particle evaporation from the excited primary fragments assuming thermal equilibrium of the dinuclear composite system. As displayed in Fig. 4, the $\langle Q \rangle$ values for DI components for the fragments Li, Be, and B are nearly constant as a function of angle for all bombarding energies, whereas those for C to F decrease at forward angles ($\Theta_{c.m.} \lesssim 40^\circ$), and then they gradually tend to become constant; these observations imply that beyond this point, the kinetic energy damping is complete and dynamic equilibrium has been established before the scission of the dinuclear composite takes place.

D. Average velocity

The average velocities of the FF component of the fragments were computed from their respective centroid energies. The mass number A of the fragments were estimated from

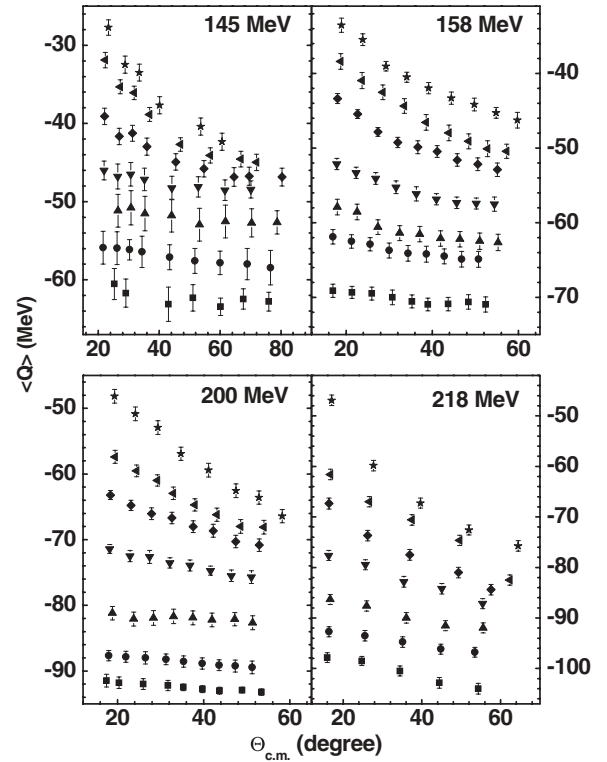


FIG. 4. Average Q values of DI component for fragments Li (square), Be (circle), B (triangle), C (inverted triangle), N (diamond), O (left triangle), and F (star) at each bombarding energy.

the respective experimentally obtained Z values using the empirical relation [38]

$$A = Z(2.08 + 0.0029Z). \tag{2}$$

The average velocities were plotted in the v_{\parallel} vs v_{\perp} plane for two representative fragments (Li and O) in Fig. 5. It is seen that the measured average velocities of the FF components (solid symbols) fall on a circle (solid curve) centered around the corresponding compound nucleus velocity v_{CN} (arrows). This means that the average velocities (as well as kinetic energies) of the fragments are independent of the c.m. emission angles at all incident energies considered here. This independence clearly indicates that these fragments are emitted from a fully equilibrated compound nucleus emission source with full momentum transfer. The magnitude of the average fragment velocities (i.e., the radii of the circles in Fig. 5) decreases with the increase of fragment mass, which is indicative of the binary nature of the emission.

TABLE II. Values of different velocity sources.

E_{lab} (MeV)	v_{CN} (v/c)	v_{DI} (v/c)
145	0.053 ± 0.001	0.061 ± 0.003
158	0.055 ± 0.001	0.067 ± 0.002
200	0.062 ± 0.001	0.074 ± 0.002
218	0.065 ± 0.001	0.085 ± 0.003

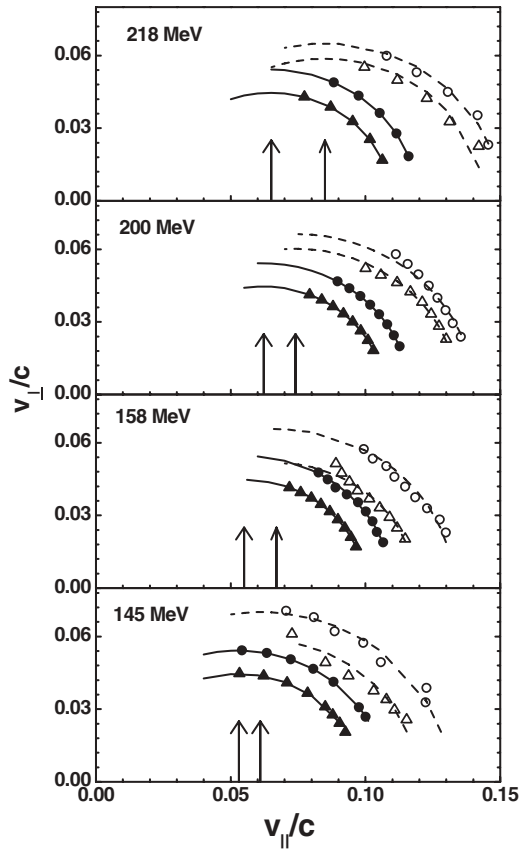


FIG. 5. Average velocities of fragments lithium (circle) and oxygen (triangle) plotted in v_{\parallel} , v_{\perp} plane at different bombarding energies for FF (solid symbol) and DI (open symbol) components. Arrows correspond to the source velocities v_{CN} (lower) and v_{DI} (higher); circles, to the most probable velocities for FF (solid) and DI (dashed) components.

The average velocities of the DI components at different bombarding energies have also been plotted in Fig. 5 (open symbols) for the same fragments Li and O. For this component, the average velocities of all fragments also fall on a circle (dashed curve), but it is centered around a higher velocity source v_{DI} . The values of v_{CN} and v_{DI} for all bombarding energies are given in Table II. It is interesting to note that at each bombarding energy, all DI fragments (only Li and O are shown in the figure) are emitted from the same source moving with velocity v_{DI} . Thus the emission of DI fragments may also be, like FF fragments, visualized in terms of emission from an equilibrated intermediate velocity source.

E. Total elemental yield

The total fusion-fission (σ_{FF}) and deep-inelastic (σ_{DI}) cross sections for different fragments were obtained by integrating the respective double differential cross section ($d^2\sigma/d\Omega dE$) over the whole energy and angular range. The cross sections thus obtained for different fragments at different bombarding energies are displayed in Fig. 6 as a function of fragment charge Z . Total uncertainties in the estimation of σ_{FF} and σ_{DI}

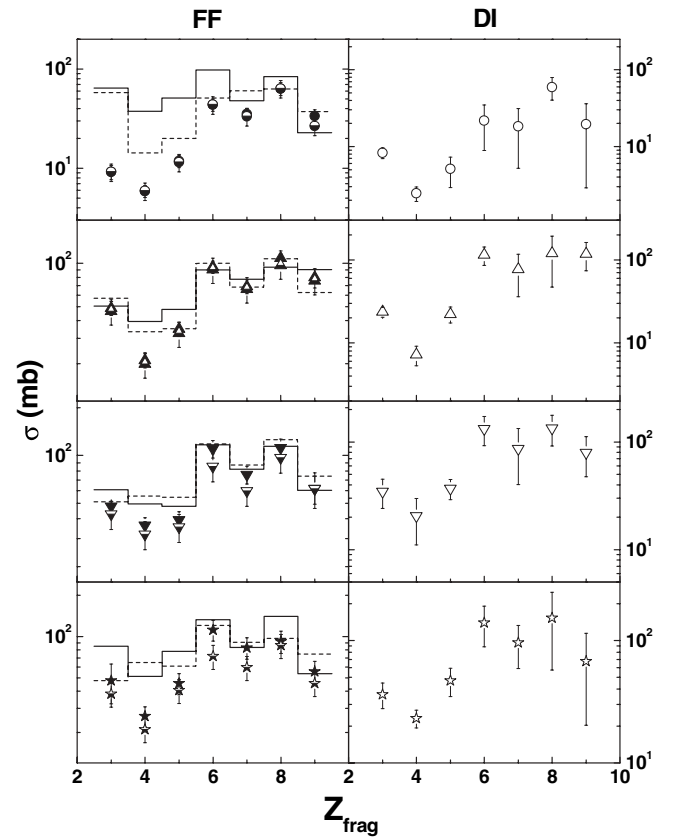


FIG. 6. Total elemental cross sections of FF (filled symbol) and DI (open symbol) components for $^{20}\text{Ne} + ^{27}\text{Al}$ reaction at bombarding energies 145 (circle), 158 (triangle), 200 (inverted triangle), and 218 MeV (star), plotted as a function of fragment charge. Histograms represent the corresponding theoretical predictions using CASCADE (solid) and EHFm (dashed). Corrected elemental yields are represented by half-filled symbols.

are due to the experimental threshold and the limited angular range of the data (error bars in Fig. 6).

The total elemental yields of the FF components (σ_{FF}) were compared with the theoretical estimates of the same obtained from the statistical model code CASCADE [39] and from the extended Hauser-Feshbach method (EHFM) [25]. The model calculations were performed by using the critical angular momentum value for the respective bombarding energy. The experimental fragment emission cross sections for FF component are shown in Fig. 6 (left) by filled symbols and the theoretical estimates of the same are represented by solid (CASCADE) and dashed (EHFM) histograms. It is seen that the theoretical predictions are in fair agreement with the experimental results except for the $Z = 4$ fragment, where the experimental values are much smaller than the respective theoretical estimates; this might be because of nondetection of unstable particle ^8Be , which decays (into two α particles) almost immediately after production and thus escapes detection.

The total elemental yields of the DI component (σ_{DI}) are shown in Fig. 6 (right) by open symbols. It has been found that a large fraction of the heavier fragment (C, N, O, F) yield is due to the DI mechanism for all bombarding energies. The FF

and DI processes are comparable in this bombarding energy range.

IV. DISCUSSION AND CONCLUSION

A. Time scale

The time scale of the DI process can be estimated from the DI angular distribution using Eq. (1), which describes the decay of a rotating dinucleus with an angular velocity $\omega = \hbar l / \mu R^2$, where μ represents the reduced mass of the system, l is the angular momentum ($l_{\text{cr}} < l \lesssim l_{\text{gr}}$; l_{cr} , l_{gr} being the critical angular momentum for fusion and the grazing angular momentum, respectively), R represents the distance between the two centers of the dinucleus, and τ is the time interval during which the two nuclei remain in solid contact in the form of the rotating dinucleus. The “life angle” Θ_o is then the product of angular velocity ω and the rotation time τ . The characteristics of a reaction process depend on the value of Θ_o . Smaller values of Θ_o are associated with faster processes for which the corresponding angular distributions are more forward peaked. Large values of Θ_o ($\geq 2\pi$) are associated with slow processes with lifetimes that are large or comparable to the dinucleus rotation period $\tau_{\text{rot}} (= 2\pi/\omega)$, the value of which lies typically in the range of $\sim (1-2) \times 10^{-21}$ s. In these cases, long-lived configurations are assumed to be formed, and the angular distributions tend to become symmetric around 90° in the c.m. ($d\sigma/d\Omega \sim 1/\sin \Theta_{\text{c.m.}}$ type distribution). The FF process is thus a limiting case of the DI process, where a very long-lived configuration is assumed to be formed and the angular distribution becomes $\propto 1/\sin \Theta_{\text{c.m.}}$. The c.m. angular distributions of the DI components have been fitted with Eq. (1), and the time scales thus obtained are given in Table I for different fragments emitted in the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction. The upper (lower) limit of τ corresponds to the estimate with $l = l_{\text{cr}}$ (l_{gr}). The values of time scales are found to vary in the range of $10^{-21} - 10^{-22}$ s, depending on the bombarding

energy and fragment mass. It has been found that the time scale decreases as the fragment charge increases. For lower mass fragments (Li to B), the time scale decreases with the bombarding energy also, and for other fragments (C to F) it is almost independent of bombarding energy. This is expected because the emission of heavier fragments (near the projectile) requires less number of nucleon transfers and therefore less time. On the other hand, the emission of lighter fragments requires more nucleon exchanges and therefore longer time.

B. Secondary decay simulation

In the case of the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction, the secondary decay of primary fragments have been studied using the statistical model codes CASCADE [39], PACE4 [40] and LILITA [41]. The binary fragments have more excitation energy than the deep-inelastic fragments. The excitation energy of deep-inelastic fragments is not enough for secondary deexcitations. Therefore, most of the contribution in secondary decay comes from the binary fragments. Typical excitation energies of the primary binary fragments emitted in the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction are given in Table III.

The elemental cross section of the fragments $Z = 3-9$ have been estimated in Sec. III E. This estimated fragment yields are those of the finally detected fragments. From Table III it is evident that the primary binary fragments having $Z > 16$ do not decay up to $Z = 9$. This evaporative deexcitation of the primary fragments may affect the estimated fragment yield to some extent. The increase in the yield of any fragment due to the evaporative secondary decay of the excited higher charged fragments may substantially be compensated by the secondary evaporative decay of the fragment itself, and the total elemental cross section may not change significantly. The decay probabilities have been calculated using the codes CASCADE and PACE4. The decay probabilities $P_Z(\Delta Z)$ of the primary fragments for ΔZ (difference of the atomic

TABLE III. Excitation energies E_{PB}^* of primary binary fragments emitted in $^{20}\text{Ne} + ^{27}\text{Al}$ reactions.

Fragment		145 MeV		158 MeV		200 MeV		218 MeV	
Mass	Charge	E_{PB}^* (MeV)	Decay up to	E_{PB}^* (MeV)	Decay up to	E_{PB}^* (MeV)	Decay up to	E_{PB}^* (MeV)	Decay up to
7	3	10.7	Li	11.8	Li	15.4	Li	16.9	Li
9	4	13.2	Be	14.5	Be	19.2	Be	21.2	Be
11	5	15.5	Li	17.1	Li	22.8	Li	25.3	t
12	6	16.3	C	18.1	C	24.3	Li	27.0	Li
14	7	18.5	C	20.6	C	27.8	Li	30.9	Be
16	8	20.6	C	23.0	C	31.3	Be	34.8	Be
19	9	24.1	B	26.6	B	36.7	Li	40.9	Li
20	10	25.0	C	28.0	C	38.3	Be	42.7	Be
23	11	28.5	N	32.0	N	43.9	B	48.9	B
24	12	29.8	O	33.4	O	45.8	C	51.1	C
27	13	33.7	F	37.7	N	51.7	B	57.7	N
28	14	35.4	Ne	39.2	O	54.1	C	60.3	C
31	15	39.9	Na	44.6	F	60.6	N	67.4	N
32	16	43.6	Ne	48.5	Ne	65.6	O	72.9	O

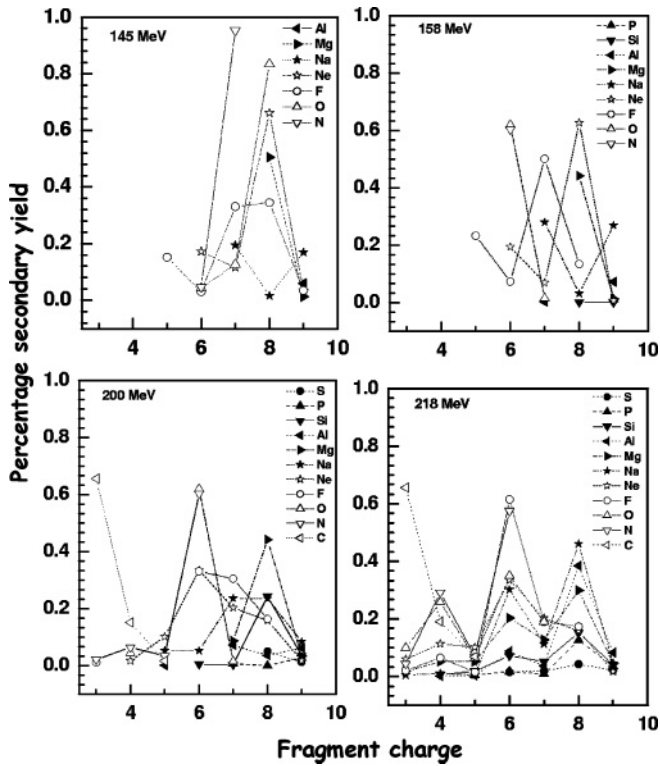


FIG. 7. Percentage secondary yield for different bombarding energies.

numbers between the primary fragment and its postevaporative daughter nucleus) decays for different bombarding energies are displayed in Fig. 7. The primary fragment yield σ_{primary} was calculated as

$$\sigma_{\text{primary}}(Z) = \sigma_{\text{final}}(Z) - \sum_{\Delta Z} \sigma_{\text{primary}}(Z + \Delta Z) P_{Z+\Delta Z} + \sum_{\Delta Z} \sigma_{\text{primary}}(Z) P_Z(\Delta Z), \quad (3)$$

where $P_Z(\Delta Z)$ is the decay probability for the excited primary fragment of charge Z in the decay mode where it loses ΔZ amount of charge through evaporation leading to the final fragment of charge $(Z - \Delta Z)$. The ratios of the final fragment yield to the primary fragment yield ($\sigma_{\text{final}}/\sigma_{\text{primary}}$) for the fragments are plotted in Fig. 8 as a function of fragment charge for all bombarding energies. For $Z < 5$, σ_{final} varies at most by 10% from σ_{primary} ; while for $Z \geq 5$, the value is $\sim 20\text{--}30\%$. Therefore, correction has to be made for the fragment yield. After the correction for secondary decay yield, the elemental yields for all the fragments changed in many cases (see Fig. 6, half-filled symbol), though the physics remains the same.

It has been observed that the elemental cross section for FF components in the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction are well predicted by the theoretical models CASCADE [39] and EHFm [25], and the DI process plays a major role in fragment emission. The energy distributions, angular distributions, and Q value distributions of the fusion-fission component of the fragments emitted in the reaction $^{20}\text{Ne} + ^{27}\text{Al}$ show the equilibrium nature of the emission process. The ratio of DI cross section to FF cross

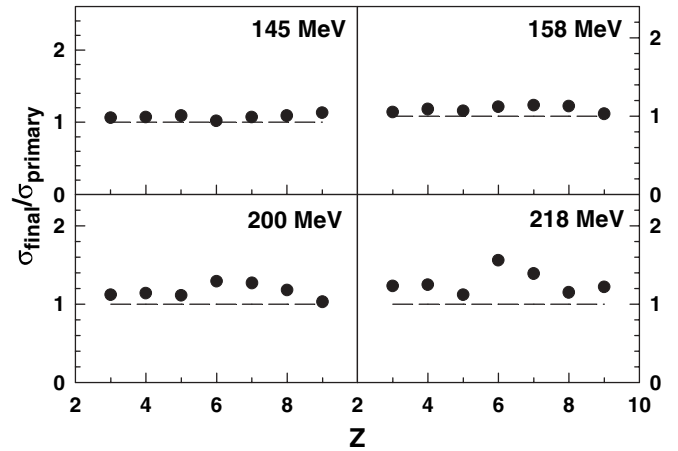


FIG. 8. $\sigma_{\text{final}}/\sigma_{\text{primary}}$ plotted as a function of fragment charge.

section, after correction, increases with bombarding energy (Fig. 9).

C. Angular momentum dissipation

In addition to kinetic energy dissipation, the dissipative heavy ion collision processes also result in significant dissipation of relative angular momentum in the entrance channel. Phenomenologically, the kinetic energy dissipation originates from the radial and tangential components of friction between the surfaces of the rotating dinuclear system; on the other hand, the angular momentum dissipation is decided solely by the tangential component of the friction, and the magnitude of dissipation is expected to lie within any of the two phenomenological limits (rolling and sticking). However, very large dissipation of relative angular momentum in excess of the sticking limit predictions has also been reported in the

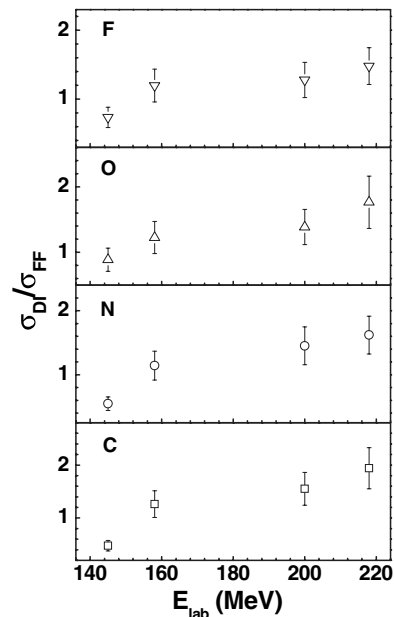


FIG. 9. Ratio of fragment yield as a function of bombarding energy.

literature [20,22]. This anomaly may be due to the ambiguity in the determination of the magnitude of angular momentum dissipation (and *vis-à-vis* the rotational contribution to the fragment kinetic energy). Moreover, the estimation of the angular momentum in the exit channel is strongly dependent on the scission configuration of the rotating dinuclear system. An independent estimation of the scission configuration is necessary to properly estimate the angular momentum transfer. Generally, it is estimated from the total kinetic energy of the rotating dinuclear system, E_K^{tot} , which is given by

$$E_K^{\text{tot}} = V_N(d) + f^2 \frac{\hbar^2 l_i (l_i + 1)}{2\mu d^2}, \quad (4)$$

where $V_N(d)$ is the contribution from Coulomb and nuclear forces at dinuclear separation distance d , μ is the reduced mass of the dinuclear configuration, l_i is the relative angular momentum in the entrance channel, and f is the numerical factor denoting the fraction of the angular momentum transferred depending on the strength of tangential friction. In the absence of any method to independently estimate the values of f and d , an earlier investigation [32,33] assumed f to be equal to its limiting value (corresponding to the sticking limit), and the whole fragment yield was assumed to be of DI origin to arrive at an extended dinuclear configuration for the $^{20}\text{Ne} + ^{27}\text{Al}$ system. However, we have demonstrated (Refs. [14,20] and present paper) that at these energies, a significant part of the fragment yield is of FF origin, and therefore this part should be subtracted from the total yield to properly estimate the DI yield. The extracted FF and DI yields can be utilized to estimate the values of d and f . A simple procedure for estimating both d and f was given in Ref. [20]. Deep-inelastic collisions are believed to occur within the angular momentum window between the critical angular momentum for fusion l_{cr} and the grazing angular momentum l_{gr} . The partially dissipative part of it (DI at forward angles) originates in near peripheral collisions ($l \sim l_{\text{gr}}$), which correspond to a small overlap and a fairly elongated dinuclear configuration; on the other hand, fully energy equilibrated dissipative components (at larger angles) correspond to more compact collisions near $l \sim l_{\text{cr}}$. Moreover, the fusion-fission yield is also most predominant in the vicinity of $l \sim l_{\text{cr}}$. It is, therefore, likely that the exit channel configurations of both processes are similar, and it appears to be reasonable to assume a compact scission shape for the fully energy damped component of the DI yield. In the present work, we estimated the scission configuration from the extracted fusion-fission component of the measured fragment energy spectra. The separation distance d between the two fragments at the scission point is calculated from the energy centroid of the FF energy spectra. The mean values of d thus estimated are 7.7 ± 1.2 fm for the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction. Assuming these scission configurations, Eq. (4) may then be used to extract the angular momentum dissipation factor f in the case of fully energy damped DI collisions. The values of f extracted for different energies for $^{20}\text{Ne} + ^{27}\text{Al}$ reaction are displayed in Fig. 11 along with the rolling (solid line) and sticking (dashed line) limit predictions for the same. During the calculation the value of initial angular momentum l_i was taken to be equal to the critical angular momentum for fusion, l_{cr} .

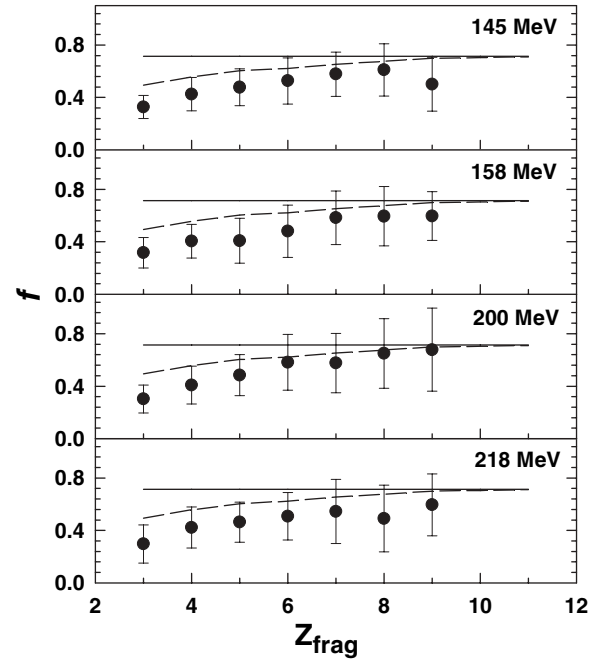


FIG. 10. Angular momentum dissipation factors extracted for different fragments (filled circles) at various incident energies. Corresponding empirical limits shown by solid (rolling) and dashed (sticking) lines, respectively.

It is apparent from Fig. 10 that for all the reactions considered, there is a discrepancy between the experimental and empirical estimates of angular momentum dissipation, so

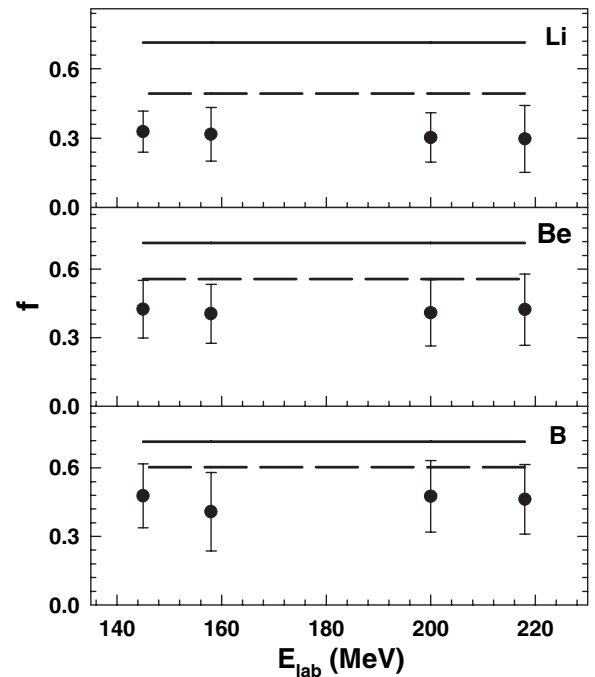


FIG. 11. Variation of angular momentum dissipation factor as a function of incident energy. Filled circles are experimental estimates; empirical rolling and sticking limits for the same are represented by solid and dashed lines, respectively.

far as the lighter fragments ($Z = 3-5$) are concerned. For these fragments, the experimental estimates of angular momentum dissipation are more than their limiting values predicted under the rolling and sticking conditions. The discrepancy is more for low mass fragments and gradually decreases for heavier fragments. This may be qualitatively understood as follows: it is known from the study of dissipative dynamics of fission [42] that strong frictional forces in the exit channel cause considerable retardation of the scission process, leading to an increase in the scission time scale. As the exit channel configurations of the fully damped DI process are taken to be similar to those for the FF process (except that the dinuclear system for the DI collision is directly formed beyond the conditional saddle point), the dynamics of the DI process may also experience stronger frictional forces. Microscopically, friction is generated by stochastic exchange of nucleons between the reacting partners through the window formed by the overlap of the density distributions of the two. Stronger friction, in this scenario, essentially means a larger degree of density overlap and more nucleon exchange. Consequently, lighter DI fragments (corresponding to more net nucleon transfer) originate from deeper collisions, for which the interaction times are larger. Therefore, the angular momentum dissipation, originating from the stochastic nucleon exchange, may also be more, which at least qualitatively explains the observed trend. The angular momentum dissipation for a particular fragment (e.g., Li, Be, and B) is found to be nearly independent of the bombarding energy. This is clearly shown in Fig. 11, where factor f is displayed as a function of bombarding energy for the $^{20}\text{Ne} + ^{27}\text{Al}$ reaction. This may be further indicative of the stochastic nucleon exchange origin of the frictional force for the fully energy damped DI process, for which the scission configuration is nearly independent of the bombarding energy.

D. Summary

We have studied the ^{20}Ne (145, 158, 200, 218 MeV) + ^{27}Al reactions and extracted the contributions to the fragment yield from fusion-fission and deep-inelastic processes. The c.m. angular distributions of the FF component were found

to have $\sim 1/\sin \Theta_{\text{c.m.}}$ dependence, whereas those of the DI component showed an exponential falloff at forward angles. The time scale of the DI process was estimated from the DI angular distribution. The lifetime of the DI process was found to decrease with increasing fragment mass as well as with increasing bombarding energy. The fusion-fission component of the emitted fragments apparently originates from the compound nucleus source (moving with velocity v_{CN}), while the deep-inelastic component of the fragments is emitted from an intermediate velocity source having velocity v_{DI} , which is higher than v_{CN} . The average Q values for DI components decrease with the increase of emission angles and saturate at higher angles, thus signifying a fully energy damped process at these angles. The elemental cross sections were obtained by integrating separately the energy distributions of the FF and DI components over the corresponding energies and over the whole angular range. The fusion-fission fragment yield σ_{FF} was fairly well explained in terms of a statistical model. The $\sigma_{\text{DI}}/\sigma_{\text{FF}}$ value increases with bombarding energies, which is expected because of the increasing contribution of DI processes at higher energies. Assuming a compact exit channel configuration (estimated from the extracted FF part of the spectra) for the fully damped part of the deep-inelastic reactions, the angular momentum dissipation was estimated and found to be more than the corresponding phenomenological limits. The deviations are greater for lighter fragments, which may be related to the microscopic (stochastic nucleon exchange) origin of nuclear friction.

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