Scaling laws in 3He induced nuclear fission

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Fission excitation functions of compound nuclei in a mass region where shell effects are expected to be very strong are shown to scale exactly according to the transition state prediction once these shell effects are accounted for. Furthermore, the method applied in this paper allows for the model-independent determination of the nuclear shell effects. $[S0556-2813(96)04012-5]$

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I. INTRODUCTION

More than half a century after its discovery $\lfloor 1 \rfloor$, the study of fission is still of general interest. While the availability of relativistic heavy ions has enabled the study of several aspects of the fission process in the high energy region $[2-11]$, it has been shown recently that a new approach $\lceil 12 \rceil$ to investigate excitation functions of low energy, light particle induced fission allows for the model independent extraction of fundamental quantities of the fission process, like fission barriers, shell effects, and the much discussed fission delay time (see, e.g., Refs. $[12-14]$).

From early studies it is well known that the fission excitation functions vary dramatically from nucleus to nucleus over the periodic table $[15-17]$: Some of the differences can be understood in terms of a changing liquid-drop fission barrier with the fissility parameter, others are due to to strong shell effects which occur, e.g., in the neighborhood of the double magic numbers $Z=82$ and $N=126$. Further effects may be associated with pairing and the angular momentum dependence of the fission barrier $[18,19]$.

Fission rates have been calculated most often on the basis of the transition state method introduced by Wigner $[20]$, and applied to fission by Bohr and Wheeler $[21]$. The success of this method has prompted attempts to justify its validity in a more fundamental way, and to identify regimes in which deviations might be expected. Recent publications claim the failure of the transition state rates to account for the measured amounts of prescission neutrons or γ rays in relatively heavy fissioning systems $[13,14,22]$. This alleged failure has been attributed to the transient time necessary for the socalled slow fission mode to attain its stationary decay rate $[23-31]$. The larger this fission delay time, the more favorably neutron decay competes with the fission process. This leads to an effective fission probability smaller than predicted by the Bohr-Wheeler formula. The experimental methods of these studies, however, suffer from two difficulties: First they require a possibly large correction for postsaddle, but prescission emission; second, they are indirect methods since they do not directly determine the fission probability. The measured prescission particles can be emitted either before the system reaches the saddle point, or during the descent from saddle to scission. Only from the anomalies in the first component, would deviations of the fission rate from its transition state value be expected. The experimental separation of the two contributions, however, is fraught with difficulties which make the evidence ambiguous. It seems therefore desirable to search for transient time effects by directly measuring the fission probability and its energy dependence against the predictions of the transient state method for a large number of systems and over a broad energy range.

In the last few decades, several studies have investigated heavy ion and high energy light ion induced fission $[19]$. These reactions involve a large and variable deposition of energy, mass and, most important, of angular momentum. The latter, in particular, greatly affects the fission process and makes comparisons with liquid drop model calculations difficult $[18,19]$. In contrast, the problem of excessive angular momentum, mass and energy transfer and the associated uncertainties can be minimized by the use of light projectiles and relatively low bombarding energies; see, e.g., Ref. [15,17,32]. Becchetti *et al.* have, in particular, measured ³He induced fission excitation functions of several nuclei with masses between 159 and 232 at bombarding energies ranging from 19.1 to 44.5 MeV $\left[33\right]$. Their analysis with statistical fission theory indicates fission barriers which, in contrast to heavy ion induced fission, differ only slightly from liquid drop model predictions.

In a recent paper, a new scaling of fission excitation functions based upon the transition state prediction, collapses a large number of fission excitation functions from compound nuclei produced in α -induced reactions [17] to a single straight line, once the shell effects are accounted for $[12]$.

In this paper, we show the results of a recent experiment investigating 3He induced fission of the compound nuclei 200 Tl, 211 Po, and 212 At at excitation energies between 25 and 145 MeV. These fissioning systems bracket the closed shell region around 208Pb, and due to the strong shell effects, the analysis of these systems represents a sensitive test of the method introduced in Ref. $[12]$.

The present paper is organized as follows: In Sec. II, we present an experimental setup which allows one to measure fission excitation functions for various nuclei efficiently, and we show the results of such a measurement. In the subsequent section, we describe the analysis of the fission data and *Electronic address: TRubehn@lbl.gov our findings. Finally, our summary can be found in Sec. IV.

$E(^3\text{He})$		σ_f (mbarn)	
(MeV)	$^{200}\mathrm{Tl}$	^{211}Po	$\mathrm{^{212}At}$
21.0	0.0019 ± 0.0004	0.0004 ± 0.0002	0.0108 ± 0.0023
24.0	0.0187 ± 0.0038	0.0171 ± 0.0036	0.2176 ± 0.0441
27.1	0.0859 ± 0.0175	0.148 ± 0.030	1.25 ± 0.25
30.8	0.298 ± 0.060	0.707 ± 0.141	3.8 ± 0.8
35.0	0.765 ± 0.154	2.2 ± 0.4	10.3 ± 2.1
39.7	1.9 ± 0.4	6.1 ± 1.2	19.9 ± 4.0
44.9	3.6 ± 0.7	11.2 ± 3.9	33.6 ± 6.7
50.6	6.2 ± 1.3	19.4 ± 6.3	54.2 ± 10.9
56.8	10.6 ± 2.1	31.7 ± 9.3	78.1 ± 15.6
63.4	15.5 ± 3.1	46.6 ± 10.5	100.6 ± 20.2
67.1 ^a	18.1 ± 3.6	52.6 ± 14.5	115.1 ± 23.1
70.6	23.9 ± 4.8	72.7 ± 17.9	143.8 ± 28.8
74.4 ^a	30.7 ± 6.2	89.7 ± 19.9	160.3 ± 32.1
78.3	34.1 ± 6.8	99.7 ± 19.4	178.6 ± 35.8
82.3 ^a	33.4 ± 6.7	96.9 ± 23.6	177.9 ± 35.7
86.5	42.6 ± 8.5	117.8 ± 30.6	211.3 ± 42.3
92.5	63.0 ± 12.6	152.8 ± 31.4	243.5 ± 48.8
95.2	56.6 ± 11.3	157.0 ± 32.6	255.8 ± 51.3
99.9 ^a	59.4 ± 13.1	162.9 ± 38.1	253.7 ± 50.8
104.4	67.4 ± 14.9	190.3 ± 39.3	282.4 ± 56.6
108.5 ^a	71.2 ± 14.3	196.5 ± 45.5	285.7 ± 57.2
114.1	78.1 ± 15.6	227.3 ± 49.2	318.3 ± 63.7
119.0 ^a	88.0 ± 17.6	245.9 ± 55.6	333.0 ± 66.7
124.3	94.9 ± 19.0	277.8 ± 46.3	358.9 ± 71.9
130.0 ^a	86.7 ± 17.4	231.6 ± 53.7	305.3 ± 61.2
135.0	100.3 ± 20.1	268.6 ± 54.3	351.5 ± 70.4

TABLE I. Experimental fission cross sections.

^aThe bombarding energy was achieved by using a degrader foil as described in the text.

II. EXPERIMENT

Fission of three compound nuclei, 200 Tl, 211 Po, and ²¹²At, formed in the reactions ³He + ¹⁹⁷Au, ²⁰⁸Pb, and 209 Bi was investigated. The targets were mounted at 45 degrees with respect to the beam axis and had thicknesses between 240 and 500 μ g/cm². The Lawrence Berkeley National Laboratory's 88-Inch Cyclotron delivered ³He beams with 19 different energies between 21 MeV and 135 MeV. The number of energy points was increased to 26 (see Table I) by using a set of degraders made of aluminum foils with thicknesses between 186 and 433 μ m which were determined by weighing.

In the past, these fission reactions have been studied using small solid angle solid state counters or nuclear track detectors; see, e.g., Refs. $[15,17,32,33]$. Therefore, beamtimes on the order of weeks were necessary to measure complete excitation functions. To cover a large solid angle and, therefore, to minimize beam time, we performed an experiment using two large area parallel-plate-avalanche counters (PPAC's) with an active area of 200×240 mm² each. The detectors were mounted at 80° and 260° with respect to the beam axis, allowing for the detection of both fission fragments in coincidence. The PPAC's were placed at a distances of 150 mm from the target to the center of each detector. As the beam energy increases the velocity of the compound nucleus in the laboratory's frame increases, resulting in a decreasing folding angle. Since we require the detection of both fission fragments in coincidence, and our detectors are mounted at a fixed relative angle, the acceptance has a weak dependence on the bombarding energy of the projectile: For our detector setup, we have determined a geometric angular coverage between 18 and 20% for bombarding energies between 135 and 21 MeV, respectively.

The PPAC's detector volume is divided by a cathode foil made of 2 μ m thick mylar foil which is set at a voltage of 450–550 V during operation. The readout of the cathode gives a position independent amplitude and time signal. On both sides of the cathode, signal wireplanes are mounted at a distance of 3 mm, one with horizontal and the other one with vertical oriented wires. The wires have a thickness of 20 μ m, the distance between the individual wires is 1 mm. Five wires are combined to a group which is read out by a delay line to reconstruct the position of the particle. An intrinsic resolution of 1.0 mm (FWHM) has been achieved in both horizontal and vertical position which allows for the measurement of the folding angle precisely. Each detector has an entrance window made of mylar foil which separates the gas atmosphere in the detector from the chamber vacuum. In the present experiment, the counters were operated by flowing isobutane gas at a constant pressure of 4 mbar.

In Fig. 1, we show a typical experimental amplitude spectrum for coincidence events. It shows that the fission peak is clearly visible and the background is negligible. Cross sections were determined for these fission events using

FIG. 1. Typical amplitude spectrum for coincidence events as measured with the PPAC's in the reaction 3 He+ 197 Au at 86.5 MeV.

$$
\sigma_f = \frac{n_f A}{n_{\text{beam}} N_A m} \eta(\theta, \phi), \tag{1}
$$

where n_f and n_{beam} are the number of fission events and the number of beam particles, respectively. *A* represents the mass number of the target, N_A Avogadro's constant, and m the thickness of the target. Due to the incomplete angular coverage, the quantity $\eta(\theta,\phi)$ which accounts for the geometrical acceptance and for the nonisotropic emission of the fission fragments has be be taken into account. The anisotropic angular distribution $(d\sigma/d\Omega)_{\theta}/(d\sigma/d\Omega)_{90^{\circ}}$ of the fission fragments has been shown to be reasonably described by the function $\sin^{-1}\theta$ [18]. We have used this dependence for the determination of our acceptance. The beam normalization was done using a Faraday cup. The systematic uncertainty of this method can be estimated to $\pm 15\%$.

In Fig. 2, we show the experimental fission cross sections for the three compound nuclei 200 Tl, 211 Po, and 212 At as a function of excitation energy. The error bars denote both the

FIG. 2. Excitation function for fission of several compound nuclei formed in 3 He induced reactions. The different symbols correspond to the experimental data points. The solid line shows the results of a fit to the data using a level density parameter $a_n = A/8$. The error bars denote the statistical and systematic errors combined in quadrature.

statistical and the systematic errors. While the statistical errors dominates at the lowest energy points, the systematic uncertainties are the main contribution at higher excitation energies. The excitation energy was calculated assuming a full momentum and mass transfer of the helium ions to the compound nucleus (CN) . The binding energies of ³He, the target isotopes, and the compound nuclei were taken from $Ref. [34]$.

III. ANALYSIS AND RESULTS

We will analyze our data according to a method introduced in Ref. $[12]$ that allows us to investigate deviations from the transition state rates and enables us to extract effective fission barriers and values for the shell effects which are independent of those obtained from the ground state masses. The transition state expression for the fission decay width $[20,21]$

$$
\Gamma_f \approx \frac{T_s}{2\pi} \frac{\rho_s (E - B_f - E_r^s)}{\rho_n (E - E_r^{g.s.})}
$$
\n(2)

allows one to write the fission cross section as follows:

$$
\sigma_f = \sigma_0 \frac{\Gamma_f}{\Gamma_{\text{total}}} \approx \sigma_0 \frac{1}{\Gamma_{\text{total}}} \frac{T_s \rho_s (E - B_f - E_r^s)}{2 \pi \rho_n (E - E_r^{gs})},\tag{3}
$$

where σ_0 is the compound nucleus formation cross section, Γ_f is the decay width for fission, and T_s is the energy dependent temperature at the saddle; ρ_s and ρ_n are the saddle and ground state level densities, B_f is the fission barrier, and *E* the excitation energy. Finally, E_r^s and $E_r^{gs.}$ represent the saddle and ground state rotational energies. This equation can be rewritten as

$$
\frac{\sigma_f}{\sigma_0} \Gamma_{\text{total}} \frac{2 \pi \rho_n (E - E_r^{\text{g.s.}})}{T_s} = \rho_s (E - B_f - E_r^s). \tag{4}
$$

To further evaluate this expression, we use the form $\rho(E)$ \propto exp(2 \sqrt{aE}) for the level density. This leads to:

$$
\ln\left(\frac{\sigma_f}{\sigma_0}\Gamma_{\text{total}}\frac{2\,\pi\rho_n(E - E_r^{\text{g.s.}})}{T_s}\right) = 2\,\sqrt{a_f(E - B_f - E_r^s)}.\tag{5}
$$

If the transition state null hypothesis holds, plotting the left hand side of the equation versus $\sqrt{E-B_f-E_r^s}$ should result in a straight line. This equation has already been used in Ref. [35] to demonstrate the scaling of over 80 excitation functions obtained by the study of the emission of complex fragments from compound nuclei like ^{75}Br , $^{90,94}Mo$, and $110,112$ In.

Since the neutron width Γ_n dominates the total decay width in our mass and excitation energy regime, we can write

$$
\Gamma_{\text{total}} \approx \Gamma_n \approx K T_n^2 \frac{\rho_n (E - B_n - E_r^{\text{g.s.}})}{2 \pi \rho_n (E - E_r^{\text{s}})}
$$
(6)

where B_n represents the binding energy of the last neutron, *Tn* is the temperature after neutron emission, and $K=2m_nR^2g'/\hbar^2$ with the spin degeneracy $g'=2$.

TABLE II. Values of the effective fission barriers, a_f/a_n , and shell effects. For comparison, we give the values of the isotope 211 Po obtained from the analysis of 4 He induced fission [12] and the calculated shell effects Δ_{calc} taken from Ref. [37].

CN	Proj.	B_f^* (MeV)	a_f/a_n	Δ_{shell} (MeV)	Δ_{calc} (MeV)
212 At	3 He	19.5 ± 1.0	1.008 ± 0.020	10.7 ± 1.5	9.6
^{211}Po	3 He	23.0 ± 1.0	1.009 ± 0.030	13.7 ± 1.5	10.8
^{211}Po	4 He	$23.1 + 1.5$	1.028 ± 0.050	13.4 ± 1.5	10.8
200 Tl	3He	25.1 ± 1.0	0.995 ± 0.046	12.1 ± 1.5	6.6

The study of the fission process in the lead region forces us to take strong shell effects into account. For the fission excitation functions discussed in this paper, the lowest excitation energies for the residual nucleus after neutron emission are of the order of 15–20 MeV and therefore high enough to assume the asymptotic form for the level density $\lceil 36 \rceil$ which is given below:

$$
\rho_n (E - B_n - E_r^{\text{g.s.}}) \propto \exp[2\sqrt{a_n (E - B_n - E_r^{\text{g.s.}} - \Delta_{\text{shell}})}]
$$
(7)

where Δ_{shell} is the ground state shell effect of the daughter nucleus $(Z, N-1)$. For the level density at a few MeV above the saddle point, we can use

$$
\rho_s (E - B_f - E_r^s) \propto \exp[2\sqrt{a_f (E - B_f^* - E_r^s)}]
$$
 (8)

since the large saddle deformation implies small shell effects. Deviations due to pairing, however, may be expected at very low excitation energies. In Eq. (8) , we introduced the quantity B_f^* which represents an effective fission barrier, or, in other words, the unpaired saddle energy, i.e., $B_f^* = B_f + 1/2g\Delta_0^2$ in the case of an even-even nucleus and $B_f^* = B_f + 1/2g\Delta_0^2 - \Delta_0$ for nuclei with odd mass numbers. Here, Δ_0 is the saddle gap parameter and *g* the density of doubly degenerate single particle levels at the saddle.

Finally, the use of Eqs. (7) and (8) for the level densities allows us to study the scaling of the fission probability as introduced in Eq. (5) :

$$
\frac{1}{2\sqrt{a_n}} \ln\left(\frac{\sigma_f}{\sigma_0} \Gamma_{\text{total}} \frac{2\pi \rho_n (E - E_r^{\text{g.s.}})}{T_s}\right)
$$

$$
= \frac{\ln R_f}{2\sqrt{a_n}} = \sqrt{(a_f/a_n)(E - B_f^* - E_r^*)}.
$$
(9)

The values for B_f^* , Δ_{shell} , and a_f/a_n using $a_n = A/8$ can be obtained by a three parameter fit of the experimental fission excitation functions; the best results of the fits are shown in Fig. 2 and listed in Table II. For this procedure, the formation cross sections σ_0 , which is approximated by the reaction cross section, and the corresponding values for the maximum angular momentum *l*max were taken from an optical model calculation [38]. A simple parametrization, σ_0 $= \sigma_{\text{geom}}(1-V/E_{\text{c.m.}})$, where σ_{geom} is the geometrical cross section, *V* the Coulomb barrier, and $E_{\text{c.m.}}$ the energy in the center of mass, was used to interpolate the results of the optical model calculations. Here, we used the expressions $V = (Z_1 Z_2 e^2)/R$ for the Coulomb barrier, $R = r_0 (A_1^{1/3})$

 $+A_1^{1/3} + \delta$, and $\sigma_{\text{geom}} = \pi R^2$ for the geometrical cross section. The parameters r_0 and δ were locally fitted so that the resulting cross sections were in agreement with the optical model calculations. The overall uncertainty of the calculated formation cross sections can be estimated to 5%. Finally, we computed the rotational energy at the saddle assuming a configuration of two nearly touching spheres separated by 2 fm.

In a previous paper, it has been shown that the employed method allows one to extract values for the shell effect directly from the data in contrast to the standard procedure where shell effects are determined by the difference of the ground state mass and the corresponding liquid drop value [12]. Furthermore, it has been pointed out that the determination of the shell effects is completely local since it only depends on the properties of the considered nucleus.

In Fig. 3, we now plot the left hand side of Eq. (9) versus the square root of the effective excitation energy above the barrier, $\sqrt{E-B_f^*}-E_r^s$, including the results of the fits described above. We should note that we *do not* make use of the fitted value of a_f/a_n . A remarkable straight line can be observed for the three investigated compound nuclei. This scaling extends over six orders of magnitude in the fission probability, although the shell effects are very strong in this regime. Furthermore, a linear fit to the data results in a straight line that goes through the origin and has a slope which represents the ratio a_f/a_n , consistent with unity. The observed scaling and the lack of deviations over the entire range of excitation energy indicates that the transition state null hypothesis and the above discussed equations for the

FIG. 3. The quantity $\ln R_f/2\sqrt{a_n}$ vs the square root of the intrinsic excitation energy over the saddle for fission of several compound nuclei as described in the text. The straight line represents a fit to the entire data set.

level density hold very well. The result of this work is in complete agreement with the findings of a similar analysis investigating 14 α -induced fission excitation functions $[12,39]$.

Since the experimental fission rates are well described by the transition state rates, it seems likely that any excess prescission emission occurs during the descent from saddle to scission. If this is the case, then the present fission results are not in contradiction with recent measurements of prescission neutrons and γ rays [13,14,22]. More conclusive investigations are still needed to extract reliable values of a possible transient time.

IV. SUMMARY

Experimentally, we have investigated 3 He induced fission excitation functions of three different compound nuclei, ²⁰⁰Tl, ²¹¹Po, and ²¹²At between 25 and 140 MeV excitation energy.

The data have been analyzed and discussed according to a method which allows one to check the validity of the transition state null hypothesis over a large range of excitation energy and a regime of compound nuclei masses which is characterized by strong shell effects. The shell effects can be determined directly from the experimental data by using the above described procedure. Once these shell effects are accounted for, no deviation from the transition state rate is observed.

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