Brief Reports

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Yields of fission products produced by thermal-neutron fission of ²⁴³Cm

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On the basis of measured yields for 72 gamma rays and known nuclear data, cumulative fissionproduct yields were deduced for 69 fission products having half-lives between 36 seconds and 65 days representing 41 mass chains created during thermal-neutron fission of ²⁴³Cm.

As part of an ongoing program¹⁻³ we have measured yields for thermal-neutron fission of the rare isotope ²⁴³Cm. The sample used contained ~75 ng of curium isotopically enriched to >99% in the ²⁴³Cm isotope by a special isotope separator.⁴ Sample preparation and irradiation by thermal neutrons, gamma-ray detection, data accumulation, and data reduction followed the same procedures as detailed previously.^{2,5} The only substantive differences were (a) use of the Oak Ridge High Flux Isotope Reactor in addition to the Oak Ridge Research Reactor as the neutron source, (b) more recent⁶⁻¹⁵ nuclear data characterizing decay of several of the fission products, and (c) corrections to the experimental yields due to fissions of ²³⁹Pu in the sample at the time of the experiment.¹⁶

Five irradiations of different durations were used. The numbers of fissions, n_f , created during each irradiation were deduced with an overall uncertainty of $\pm 7.2\%$ from



FIG. 1. Mass-yield distribution for $n_{\text{thermal}} + {}^{243}\text{Cm}$ derived from the present measurements. Also shown is a smoothed curve representing the $n_{\text{thermal}} + {}^{245}\text{Cm}$ mass distribution.

the sample mass, from measured⁴ thermal fission cross section and resonant integral values, and from the known thermal-neutron fluence.

Deduced cumulative fission-product yields (CFY) for the sample, including total absolute uncertainties, are collected in Table I. These CFY were corrected for the contributions from fission of the ²³⁹Pu in the sample; the penultimate column of the table gives the ²³⁹Pu CFY from the current U.S. ENDF/B evaluation¹⁷ used for these corrections. The ²³⁹Pu in the sample accounted for 12% of the fission events. The final column of Table I gives the deduced CFY for thermal-neutron fission of ²⁴³Cm.

Deduction of total-mass (i.e., chain) yields (MY) from individual CFY requires knowledge of fractional cumulative yields (FCY). We adopted the FCY vs ($Z - Z_{UCD}$) relationships deduced² for ²⁴⁵Cm, but, however, computing Z_{UCD} values¹⁸ for ²⁴³Cm as the independent variable to determine the FCY for each fission product in Table I. Mass yields were deduced for 38 masses, and they are exhibited in Fig. 1 compared with a curve representing MY for ²⁴⁵Cm obtained from the evaluation.¹⁷ The comparison shown in the figure indicates that the absolute normalization of the ²⁴³Cm data appears to be accurate to within $\pm 7.2\%$ uncertainty associated with n_f . One may also observe that the mass distribution for ²⁴³Cm is quite similar to that for ²⁴⁵Cm. Indeed, evaluated¹⁷ mass distributions (for thermal-neutron fission) of the pairs ²³³U-²³⁵U, ²³⁹Pu-²⁴¹Pu, and ²⁴⁹Cf-²⁵¹Cf are also quite similar, much more so than distributions for fissioning systems of different total Z.

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TABLE I. Deduced cumulative fission-product yields for thermal-neutron fission of ²⁴³Cm.

		Gamma-ray	Cumulative fission-product yield		
Fission	E_{γ}	branching ratio $(\sigma_{1})^{a}$	Sampla	(%) 239 D b	²⁴³ Cm
	(KCV)	(70)	Sample	ru	Cm
⁸⁹ Rb	1031.9	58.0 ± 5.0	1.29 ± 0.17	$1.60 {\pm} 0.27$	1.24 ± 0.32
⁹¹ Sr	1024.3	33.5 ± 0.7	1.57 ± 0.12	2.49 ± 0.05	1.45 ± 0.14
⁹¹ Y ^m	555.6	95.1 ± 0.1	0.91 ± 0.07	1.43 ± 0.05	$0.84 {\pm} 0.08$
⁹² Sr	1383.9	90.0±9.9	1.63 ± 0.23	2.98 ± 0.12	1.45 ± 0.26
⁹³ Sr	590.2	$67.4 \pm 1.2^{\circ}$	1.98 ± 0.18	3.64 ± 0.22	1.76 ± 0.20
94Sr	1428.1	95.4±0.4	2.04 ± 0.19	3.26 ± 0.20	1.88 ± 0.22
⁹⁴ Y	918.2	49.0±5.0 ^a	2.57 ± 0.35	4.33 ± 0.17	2.34 ± 0.39
³⁵ Zr	756.7	54.6±0.5	2.61 ± 0.19	4.88 ± 0.10	2.31 ± 0.22
⁹³ Nb	765.8	99.8±0.1	3.05 ± 0.22	4.88 ± 0.10	2.81 ± 0.25
97) Zr	/43.4	$92.8 \pm 0.3^{\circ}$	3.94 ± 0.28	5.26 ± 0.15	3.77 ± 0.32
⁹⁸ Nb	657.9	98.3±0.1	3.91±0.28	5.34 ± 0.11	3.70 ± 0.32
²⁰ Nb ²⁰	787.2	93.2±0.2 ¹	0.33 ± 0.03	0.03 ± 0.02	0.37 ± 0.04
⁹⁹ 1c ^m	140.5	87.2±0.7 ^g	5.20 ± 0.65	5.43 ± 0.11	5.17±0.74
³³ Mo	140.5	90.7±0.6	4.81 ± 0.35	6.20 ± 0.13	4.64 ± 0.40
¹⁰¹ Mo	192.1	$19.2 \pm 1.1^{\circ}$	5.81 ± 0.73	5.99 ± 0.18	5.79 ± 0.83
¹⁰¹ I C	306.9	88.0±4.4"	6.47 ± 0.64	6.00 ± 0.17	6.53 ± 0.72
¹⁰² 1c ^m	475.1	85.0±2.0 ⁴	0.07 ± 0.04	0.32 ± 0.02^{1}	0.04 ± 0.04
¹⁰² I C	475.1	6.3 ± 1.0	6.52 ± 1.23	$6.05 \pm 0.49^{\circ}$	$6.58 \pm 1.39^{\circ}$
¹⁰³ 1C	136.0	$16.3 \pm 2.9^{*}$	5.58 ± 1.14	6.95 ± 0.28	5.40±1.29
105 Ru	497.1	90.9±0.7	6.18 ± 0.45	6.95 ± 0.14	6.08 ± 0.51
¹⁰⁴ I C	358.0	89.0±5.0	6.90±0.52	6.01±0.36	7.02 ± 0.59
105 D	143.3	$15.7 \pm 1.0^{\circ}$	5.54 ± 0.42	5.54±0.61	5.54±0.47
105 D	/24.3	48.0±1.0	6.31 ± 0.53	5.59 ± 0.16	6.41 ± 0.60
105 D L	409.4	1.80±0.07	6.07 ± 0.55	5.59 ± 0.16	6.13 ± 0.62
106Ta	318.9	19.2±0.2	6.41 ± 0.47	5.59 ± 0.11	6.52±0.54
107 D	270.1	56.0 ± 3.0	4.93 ± 0.52	3.58 ± 0.39	5.10 ± 0.59
107 D h	194.0	14.3 ± 3.4	5.73 ± 1.52	3.25 ± 0.78	6.06 ± 1.72
108 D	302.9	05.9±4.0	$5.8/\pm1.08$	3.26 ± 0.36	6.22 ± 1.22
109 D h	105.0	28.0 ± 7.0	3.93 ± 1.03	2.03 ± 0.33	4.18 ± 1.18
112 A g	520.5 617 A	62.0 ± 7.0	4.03 ± 0.38	1.09 ± 0.19	4.34 ± 0.66
115 mm	326.2	42.0 ± 5.0	1.89 ± 0.28	0.12 ± 0.05	$2.12 \pm 0.31^{\circ}$
¹²⁷ Sb	530.2 685 7	45.9±0.1	0.52 ± 0.15 0.62 ± 0.05	0.00 ± 0.01	0.35 ± 0.17
128 S n	182.7	50.0 ± 0.5	0.02 ± 0.03	0.30 ± 0.04	0.04 ± 0.00
¹²⁸ Sh ^m	754 0	99.8 ± 0.2	0.30 ± 0.07	0.57 ± 0.03	0.34 ± 0.08
¹²⁸ Sb	754.0	99.8 ± 0.2	0.33 ± 0.07 0.19±0.02	0.05 ± 0.04	0.38 ± 0.08
¹²⁹ Sb	812.8	45.0+4.5	1.15 ± 0.15	1.35 ± 0.08	0.21 ± 0.02
¹³⁰ Sn	779.8	$59.1 + 3.9^{n}$	0.34 ± 0.08	0.91 ± 0.07	0.26 ± 0.09
¹³⁰ Sb ^{m o}	793.4	$860+50^{f}$	1.08 ± 0.13	1.28 ± 0.10	1.05 ± 0.15
¹³⁰ Sb ^m	839.5	99.8 ± 0.1	0.93 ± 0.09	1.20 ± 0.10 1 28+0 10	0.89 ± 0.10
¹³⁰ Sb ^o	330.9	$77.8 \pm 3.9^{\rm f}$	0.90 ± 0.10	0.50 ± 0.02	0.05 ± 0.10
¹³⁰ Sb	793.4	99.8 ± 0.1^{f}	0.84 ± 0.08	0.50 ± 0.02	0.99 ± 0.09
¹³⁰ Sb	839.4	99.8+0.1	0.84 ± 0.08	0.50 ± 0.02	0.89 ± 0.09
¹³¹ Sb	943.6	44.0+4.4 ^p	1.70 ± 0.23	2.53 ± 0.15	1.59 ± 0.09
¹³¹ Te ^m	852.2	21 3+0 9	1.16±0.10	1.04+0.04	1.37 ± 0.20
¹³¹ Te	149.8	$68.9\pm0.9^{\circ}$	2.28 ± 0.26	1.04 ± 0.04	1.17 ± 0.11
¹³¹ I	364.5	82.5+0.4	341 ± 0.25	2.99 ± 0.08 3.87 ± 0.04	2.19 ± 0.30 3.35 ± 0.28
¹³² Sb ^m	973.9	99.9 ± 0.1	5.11 ± 0.25	5.07 ±0.04	5.55±0.28
¹³² Sb	973.9	99.9+0.1	1.00 ± 0.11	2.91 ± 0.23	0.74 ± 0.12
¹³² Te	228.3	88.2±0.2	4.57±0.36	5.16+0.10	4.50+0.41
¹³² I	667.8	98.7±0.1	4.47 ± 0.34	5.42 ± 0.08	4.34 ± 0.38
¹³³ I	529.9	87.3±0.2	5.38 ± 0.39	6.97 ± 0.14	5.17+0.44
¹³⁴ I ^m	271.9	79.0 ± 3.0	1.82 ± 0.17	1.16 ± 0.37	1.91+0.19
¹³⁵ I	1131.5	22.8 ± 0.5	4.13 ± 0.35	6.41 ± 0.18	3.83 ± 0.40
¹³⁵ I	1260.4	29.0±0.4	4.20 ± 0.35	6.41 ± 0.18	3.90 ± 0.40
¹³⁵ Xe ^m	526.6	81.0 ± 1.0	0.84 ± 0.07	1.71 ± 0.55	0.72 ± 0.06
¹³⁵ Xe	249.9	89.9±0.3°	6.14 ± 0.68	7.60 ± 0.11	5.95±0.76
¹³⁰ I ^m	381.4	99.8±5.5	0.90 ± 0.10	1.67 ± 0.13	0.80 ± 0.11

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		Gamma-ray branching ratio	Cumulative fission-product yield		
Fission	F		(%)		
product	(keV)	(%) ^a	Sample	²³⁹ Pu ^b	²⁴³ Cm
¹³⁶ I ^m	1313.0	99.9±0.1 ^f	0.93 ± 0.21	1.67±0.13	0.83 ± 0.24
¹³⁶ I	1313.0	68.0 ± 1.0	0.80 ± 0.19	1.74 ± 0.42	0.68 ± 0.21
¹³⁶ Cs	818.5	99.7±0.1°	0.39 ± 0.04	0.09 ± 0.01	0.43 ± 0.05
¹³⁶ Cs	1048.1	79.8±0.9	0.44 ± 0.04	0.09 ± 0.01	0.48 ± 0.05
¹³⁸ Xe	258.4	31.5 ± 1.3	3.54 ± 0.42	5.17 ± 0.07	3.32 ± 0.47
¹³⁸ Xe	1748.3	16.7 ± 0.7	3.75 ± 0.36	5.17 ± 0.07	3.56 ± 0.41
¹³⁹ Xe	218.8	50.0 ± 6.0	2.09 ± 0.32	3.01 ± 0.09	1.97 ± 0.36
¹³⁹ Cs	1283.2	7.3 ± 0.6^{f}	6.20 ± 0.78	5.28 ± 0.42	6.32 ± 0.88
¹³⁹ Ba	165.8	23.8±0.3 ^q	6.69 ± 1.85	5.53 ± 0.22	6.84 ± 2.10
¹⁴⁰ Cs	602.4	55.7 ± 3.5^{1}	2.85 ± 0.36	3.92 ± 0.32	2.71 ± 0.41
¹⁴⁰ Ba	537.6	24.2 ± 0.2	4.96 ± 0.36	5.37 ± 0.11	4.91 ± 0.41
¹⁴⁰ La	487.0	45.9±0.4 ^r	5.17 ± 0.45	5.38 ± 0.11	5.14 ± 0.51
¹⁴⁰ La	1596.6	95.4±0.1	4.99 ± 0.42	5.38 ± 0.11	4.94±0.47
¹⁴¹ Ba	190.3	46.0 ± 3.0	4.88 ± 0.63	5.21 ± 0.31	4.84 ± 0.71
¹⁴² Ba	1204.0 ^s	22.6 ± 3.1^{s}	2.78 ± 0.45	4.58 ± 0.37	2.54 ± 0.50
¹⁴³ Ce	293.3	43.4±2.0	3.98 ± 0.34	4.35 ± 0.06	3.93±0.39
¹⁴⁴ La	397.4	90.0±5.0	3.19 ± 0.34	3.62 ± 0.29	3.13±0.39
¹⁴⁵ Ce	724.3	63.9 ± 3.9^{t}	3.21 ± 0.37	2.99 ± 0.06	3.24 ± 0.42
¹⁴⁶ Ce	218.3	20.5 ± 3.2	2.28 ± 0.40	2.45 ± 0.10	2.26 ± 0.45
¹⁴⁷ Nd	531.0	13.1 ± 0.8	1.95 ± 0.19	2.03 ± 0.06	1.94 ± 0.21
¹⁵¹ Pm	340.1	22.3 ± 0.5	$1.16 {\pm} 0.09$	$0.75\!\pm\!0.02$	1.21 ± 0.10

TABLE I. (Continued).

^aValues taken from our previous evaluation, Table II of Ref. 2, unless otherwise noted.

^bValues taken from current ENDF/B evaluation, Ref. 17.

^cKocher, Ref. 6.

^dGlendenin et al., Ref. 7.

^eGamma ray due to decay of ⁹⁷Nb^m; branching ratio corrected for the fraction of ⁹⁷Zr decay populating ⁹⁷Nb^m. The branching ratio given in Ref. 2 is incorrect.

^fFrom Table of Isotopes, Ref. 8.

^gDickens and Love, Ref. 9.

^hHarmatz, Ref. 10.

ⁱReversed from yields given in Ref. 17 for these isomers.

^jDeduced yield of the parent ¹⁰²Mo.

^kDeduced from data reported by Niizeki et al., Ref. 11.

¹Table VI of Ref. 2.

^mDeduced yield of the parent ¹¹²Pd.

ⁿDeduced from level diagram given in Ref. 8; there is a discrepancy between the tabulated and graphical branching ratio in this reference.

 $^{\circ}T_{1/2}(^{130}\text{Sb}^m) = 6.5 \text{ min}; T_{1/2}(^{130}\text{Sb}) = 40 \text{ min}.$

^pTable II, Ref. 3.

^qGehrke, Ref. 12.

^rDebertin et al., Ref. 13.

^sSum data for nearly degenerate doublet. Relative branching ratios from Ref. 8, combined with absolute branching ratio for $E_{\gamma} = 255$ keV from Ref. 2.

^tBranching ratio deduced by Reus and Westmeier, Ref. 14. Uncertainty deduced from data of Yamamoto et al., Ref. 15.

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