# Effect of the $\alpha$ -transfer reaction on the elastic scattering of ${}^{12}C + {}^{24}Mg$

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Angular distribution of the elastic scattering <sup>24</sup>Mg(<sup>12</sup>C, <sup>12</sup>C)<sup>24</sup>Mg and of the <sup>24</sup>Mg(<sup>12</sup>C, <sup>16</sup>O)<sup>20</sup>Ne transfer reaction have been measured at 40 MeV incident energy, respectively, in the 20°  $\leq \theta_{c.m.} \leq 115^{\circ}$  and 20°  $\leq \theta_{c.m.} \leq 60^{\circ}$  angular regions. The elastic scattering and transfer reactions were analyzed with Frahn's closed formalism as well as with optical model calculations. The influence of the two-step  $\alpha$ -transfer channel (<sup>12</sup>C + <sup>24</sup>Mg  $\rightarrow$  <sup>16</sup>O + <sup>20</sup>Ne  $\rightarrow$  <sup>12</sup>C + <sup>24</sup>Mg) on the elastic scattering was calculated explicitly using the coupled channel extension of the closed formalism. This calculation shows that the coupling between the  $\alpha$  transfer and elastic channel can account for the intermediate angle oscillations observed in the elastic scattering angular distributions.

NUCLEAR REACTIONS <sup>24</sup>Mg(<sup>12</sup>C,<sup>12</sup>C)<sup>24</sup>Mg, <sup>24</sup>Mg(<sup>12</sup>C,<sup>16</sup>O)<sup>20</sup>Ne (g.s.) measured  $\sigma(\theta)$ ,  $E_{lab} = 40$  MeV. Deduced optical model and closed-formalism parameters. Calculated effect of  $\alpha$ -transfer on elastic scatter-ing.

## I. INTRODUCTION

A great amount of experimental data was collected since the first observation<sup>1</sup> of unexpectedly large cross sections near  $\theta_{c.m.} = 180^{\circ}$  for the elastic and inelastic scattering of <sup>16</sup>O + <sup>28</sup>Si at  $E_{c.m.} = 35$  MeV. Elastic and inelastic scattering excitation function measurements at 180° for <sup>16</sup>O + <sup>28</sup>Si,<sup>2</sup> <sup>12</sup>C + <sup>28</sup>Si,<sup>2</sup> and <sup>12</sup>C + <sup>24</sup>Mg (Ref. 3) exhibit strong and regular structures with widths of about 1-2 MeV and large peak-to-valley ratios. Similar structures have been seen in the forward<sup>4</sup> as well as backward-angle<sup>5</sup> excitation functions of the  $\alpha$ -transfer reaction <sup>24</sup>Mg(<sup>16</sup>O, <sup>12</sup>C)<sup>28</sup>Si and in the backward angle excitation function<sup>6</sup> of the reaction <sup>28</sup>Si(<sup>16</sup>O, <sup>12</sup>C)<sup>32</sup>S and in the forward angle excitation function of the reaction <sup>20</sup>Ne(<sup>16</sup>O, <sup>12</sup>C)<sup>24</sup>Mg.<sup>7</sup>

Angular distributions of the elastic scattering of  ${}^{16}\text{O} + {}^{28}\text{Si}, {}^{8}$   ${}^{12}\text{C} + {}^{28}\text{Si}, {}^{9,10}$   ${}^{12}\text{C} + {}^{24}\text{Mg}, {}^{11}$  and  ${}^{16}\text{O} + {}^{24}\text{Mg}, {}^{12}$  as well as the above-mentioned  $\alpha$ -transfer reactions,  ${}^{6,13}$  exhibit strong oscillatory patterns and a rise of some orders of magnitude in the cross section at  $\theta_{\text{c.m.}} = 180^{\circ}$ . The entrance and exit channel elastic scattering excitation functions, corresponding to the  $\alpha$ -transfer reactions  ${}^{24}\text{Mg}({}^{16}\text{O}, {}^{12}\text{C}){}^{28}\text{Si}$  and  ${}^{28}\text{Si}({}^{16}\text{O}, {}^{12}\text{C}){}^{32}\text{S}$ , have also been measured at  $\theta_{\text{c.m.}} = 180^{\circ}$ , and there seems to be no clear correlation between the structures in different channels or at different angles.

It has been observed that these phenomena are most significant when the target and projectile have  $n \times \alpha$  structure, and the addition of one or a few nucleons<sup>10,14,15</sup> to the target or projectile reduces greatly or eliminates the observed effects. Recent data<sup>8</sup> on the elastic scattering of <sup>16</sup>O on <sup>29</sup>Si and <sup>30</sup>Si constitute an exception to the above rule, the backward angle excitation function exhibiting regular structures of the same width as  ${}^{16}O + {}^{28}Si$ , with a moderate reduction (from a factor of 5 for <sup>29</sup>Si, to a factor of 50 for <sup>30</sup>Si) in the 180° cross section. The physical origin of these phenomena is not fully understood yet. However, several explanations have been proposed, ranging from surface transparent<sup>16</sup> and parity dependent<sup>17,18</sup> optical potentials, Smatrix descriptions explicitly including the interference<sup>8</sup> between the barrier wave and the internal wave, introduction of an *l*-window in the S matrix<sup>19</sup> or isolated resonances<sup>8,13</sup> in the composite system superposed, to direct reaction background.

There is a clear indication that the overall picture one obtains may be summarized as follows<sup>19,20</sup>: The elastic scattering amplitude of these  $\alpha$  nuclei is composed of three terms; an "E-18" type of contribution arising from the global "optical" properties of the interacting pair, which is common to all heavy-ion systems; a parity-independent anomalous window; and finally a parity-dependent window that contributes mostly in the back-angle region.

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It was clearly shown in Ref. 19 that such a picture reproduces rather well both the 180° excitation function and the full angular distribution. A similar interpretation was invoked in Ref. 21 in connection with the 90° excitation function.

A possible mechanism that may give rise to these anomalous windows, which was suggested in Refs. 19 and 20, is based on a multistep  $\alpha$ -transfer contribution to the elastic amplitude. These authors relate the parity-independent anomalous window to the polarization in the elastic channel due to its coupling to a single- $\alpha$  transfer channel. The parity-dependent window, which was found to be much smaller in magnitude, is then related to a higher-order process involving the elastic transfer of three  $\alpha$  particles.

In order to test this hypothesis one would necessarily have to deal with a complicated multicoupled channel description. One may, though, simplify the description by exploiting the fact that the contribution to the elastic amplitude arising from the parity-dependent window is concentrated mostly in the back-angle region. Therefore, one should be able to test the dynamical origin of the parityindependent window, referred to above, by analyzing the angular distribution in the intermediate angle region.

For this reason we measured the angular distributions of the elastic scattering  ${}^{24}Mg({}^{12}C, {}^{12}C){}^{24}Mg$  in the forward and intermediate angle region, and the  $\alpha$ -transfer reaction  ${}^{24}Mg({}^{12}C, {}^{16}O){}^{20}Ne$  in the forward angle region at 40-MeV incident energy. The calculation which includes the effect of the two-step  $\alpha$  transfer on the elastic scattering was performed in the frame of Frahn's closed formalism,<sup>22</sup> and it shows that the coupling can account for the intermediate angle oscillations observed in the elastic scattering angular distribution.

### **II. EXPERIMENTAL METHOD AND RESULTS**

The angular distributions of the reactions  $^{24}Mg(^{12}C,^{12}C)^{24}Mg$  and  $^{24}Mg(^{12}C,^{16}O)^{20}Ne$  were measured using a  $^{12}C$  beam accelerated to 40 MeV by the São Paulo Pelletron Accelerator. Targets of isotopically enriched  $^{24}Mg$ , evaporated in  $^{12}C$  backing, were used. Three sets of  $\Delta E$ -E telescopes were used, the E detectors being standard Si surface barrier detectors, the  $\Delta E$  detectors proportional counters for the forward angles, and surface barrier detectors for the backward angle data. At backward angles the  $^{16}O$  provenient from the transfer re-

action were stopped in the  $\Delta E$  detectors. The reason for the use of telescopes was the necessity of identification for the transfer reaction at forward angles, and the presence of light particles, provenient from the fusion of  ${}^{12}C + {}^{12}C$  and  ${}^{12}C + {}^{16}O$ , at backward angles. For normalization purposes, a  $(1 \ \mu g/cm^2)$ -thick gold layer was evaporated on the targets. A monitor detector placed at 15° with respect to the beam permitted us to calculate the ratio of  ${}^{24}Mg$  to gold target thicknesses. The absolute cross sections were obtained by normalizing to Rutherford scattering on gold and using the ratio of target thicknesses. The energy resolution at all angles was sufficient to separate the elastic peak from inelastic peaks.

At some angles the <sup>16</sup>O ions recoiling elastically from the target have the same energy as the <sup>16</sup>O ions provenient from the  $\alpha$ -transfer reaction. The thickness of the <sup>16</sup>O layer in target was determined by two independent methods: The elastic scattering of <sup>12</sup>C on <sup>16</sup>O was measured from  $\theta_{lab} = 20^{\circ}$  to 30° at  $E_{lab} = 24$  MeV and compared to absolute cross sections measured by Kuehner et al.,23 and the 40-MeV elastic scattering of <sup>12</sup>C on <sup>16</sup>O was compared to absolute cross sections measured by Charles et al.<sup>24</sup> These two methods yielded target thicknesses which were within 10% in accord. The recoil cross section was obtained for all measured angles from the complete elastic scattering angular distribution measured by Charles et al.<sup>24</sup> These recoil counts were subtracted from the total counts



FIG. 1. A typical spectrum of <sup>12</sup>C ions elastically scattered to  $\theta_{lab} = 40^{\circ}$ .



FIG. 2. Spectra of <sup>16</sup>O ions provenient from the  ${}^{24}Mg({}^{12}C, {}^{16}O){}^{20}Ne$  g.s. transfer reaction and from the elastic recoil of  ${}^{16}O + {}^{12}C$ .

at all angles where the kinematic overlap of peak energies was verified. This procedure introduced an additional error in the measured transfer cross sections.

The typical spectrum of <sup>12</sup>C ions elastically scattered to 40° is presented in Fig. 1. The spectra of <sup>16</sup>O ions provenient from the transfer reaction and from the recoil are shown in Fig. 2. The angular distributions of elastic scattering and transfer reactions are presented, respectively, in Figs. 3 and 4. The absolute errors in the elastic cross sections are 5% for the forward angles and 10-20% for intermediate angles. The elastic angular distribution presents pronounced oscillations at intermediate angles, which are characteristics of the  $\alpha$ -structure nuclei in this energy region. The period of oscillations is  $\sim 10^\circ$ , in accord with the prevision obtainable from the grazing angular momentum lg = 18. The transfer angular distribution is also oscillatory and the period is the same as in the elastic scattering, depicting the contribution of grazing surface partial waves to the transfer cross section.



FIG. 3. Angular distribution of the elastic scattering  ${}^{24}Mg({}^{12}C, {}^{12}C){}^{24}Mg$  measured at  $E_{lab} = 40$  MeV.



FIG. 4. Angular distribution for the transfer reaction  ${}^{24}Mg({}^{12}C, {}^{16}O){}^{20}Ne$  (g.s.) measured at  $E_{lab} = 40$  MeV.

## **III. ANALYSIS OF THE DATA**

## A. Frahn-Hussein formalism

In a recent work Frahn and Hussein<sup>22</sup> developed an extension of the closed formalism for elastic heavy-ion collisions to account for channel coupling effects on this process. The specific transfer channel that will be taken into account is the double  $\alpha$ transfer presented schematically in Fig. 5.

The contribution of other transfer channels, involving the excited states of  $^{20}$ Ne or other intermediate systems, such as  $^{8}$ Be +  $^{28}$ Si, could also be taken into account in a straightforward way. One



FIG. 5. Coupling scheme used in the calculations described in the text.

begins the procedure<sup>22</sup> from the set of coupledchannels equations and, using the radial Gellmann-Goldberger relation, writes the total nuclear S matrix as the sum of the uncoupled elastic S matrix and a correction term that describes the coupling to the  $\alpha$  transfer channel. The use of the on-shell approximation, which was invoked in Ref. 22, implies that the intermediate system is taken out to infinity and is brought back again:

$$S_{l_n}^N(k_n) = \mathring{S}_{l_n}^N(k_n) + S_{l_n}^N(k_n)$$
  
=  $\mathring{S}_{l_n}^N(k_n) [1 - t_{l_n}(k_n k_m)],$  (1)

where  $t_{l_n}$  is written in terms of distorted wave Born approximation (DWBA) radial integrals  $R_{l_n l_m}$  and  $R_{l_m l_n}$ :

$$t_{l_{n}}(k_{n}k_{m}) = \frac{\mu_{n}^{2}k_{n}k_{m}}{2\pi^{2}\hbar^{4}} a_{l_{m}l_{n}}a_{l_{n}l_{m}} \times \frac{R_{l_{n}l_{m}}(k_{n}k_{m})R_{l_{m}l_{n}}(k_{m}k_{n})}{\mathring{S}_{l_{n}}^{N}(k_{n})\mathring{S}_{l_{m}}^{N}(k_{m})}, \quad (2)$$

where  $a_{l_n l_m}$  is the strength of the coupling interaction

$$V_{l_n l_m}(r) = a_{l_n l_m} F(r) \equiv a_T(k_n k_m) F(r)$$
 (3)

and contains the spectroscopic factors and geometric factors. The DWBA radial integrals are factorized in terms of Coulomb radial integrals and the unperturbed nuclear S matrix; with the use of the Sopkovitch approximation<sup>25</sup>

$$R_{l_{n}l_{m}}^{L}(k_{n}k_{m}) = \frac{2\pi}{\xi_{n}k_{n}k_{m}K_{n}} [\mathring{S}_{l_{n}}^{N}(k_{n})]^{1/2} \times I_{L-K}(\theta,\xi) [\mathring{S}_{l_{m}}^{N}(k_{m})]^{1/2} .$$
 (4)

The Coulomb radial integrals  $I_{L-K}$  are calculated in the Wentzel-Kramers-Brillouin (WKB) approximation.<sup>25</sup> Supposing that the channel spin  $I_n = I_m = 0, L = 0, K = 0$ , and the total S matrix can be written as a continuous function of the variable  $\lambda = l + \frac{1}{2}$  as

$$S^{N}(\lambda) = \mathring{S}(\lambda) [1 - t(\lambda)] = \mathring{S}(\lambda) \left[ 1 - \frac{2\mu^{2}}{\hbar^{4}} \frac{a_{T}(K_{n}K_{m})a_{T}(K_{m}K_{n})I_{00}^{(K_{n})}I_{00}^{(K_{m})}}{\xi nk_{n}K_{n}\xi_{m}k_{m}K_{m}} \right].$$
(5)

 $K_n$ ,  $K_m$  are the imaginary wave numbers of the bound states *n* and *m*,  $k_n$ ,  $k_m$  are wave numbers in the channels *n* and *m*, and  $\xi_n$ ,  $\xi_m$  are scale factors that partly account for recoil effects. The profile of the correction term in the *S* matrix is bell shaped and centered around  $\Lambda_T = \Lambda + \delta_T$ , where  $\delta_T$  is determined by characteristics of the unperturbed nuclear *S* matrix and by the wave numbers and Sommerfeld parameters of the channels *n* and *m*.

We note that the contribution to the elastic S matrix due to transfer channel coupling is completely determined by the characteristics of the transfer process. The elastic scattering amplitude can be calculated from the S matrix by the sum of partial waves. We have

$$f(\theta) = \frac{i}{k} \sum_{l} (l + \frac{1}{2}) [1 - S_{l}(k)] P_{l}(\cos\theta) .$$
 (6)

The scattering amplitude also can be written as a

sum of two terms:

$$f(\theta) = \tilde{f}(\theta) + \tilde{f}(\theta) , \qquad (7)$$

where

$$\mathring{f}(\theta) = \frac{i}{k} \sum_{l} (l + \frac{1}{2}) [1 - \mathring{S}_{l}(k)] P_{l}(\cos\theta)$$
(8)

and

$$\widetilde{f}(\theta) = -\frac{i}{k} \sum_{l} (l + \frac{1}{2}) \widetilde{S}_{l}(k) P_{l}(\cos\theta) .$$
(9)

Analytic expressions for  $f(\theta)$  representing the leading terms in an asymptotic expansion for large Sommerfeld parameters and large grazing angular momenta have been derived by Frahn.<sup>26</sup> Similar methods are used to evaluate the amplitude  $\tilde{f}(\theta)$ .<sup>22</sup>

The analytic expression derived for  $\tilde{f}(\theta)$  and valid in the angular range  $1/\Lambda_T \le \theta \le \pi$  is

$$\widetilde{f}(\theta) = \frac{i\Lambda_T}{2k_n} \exp[2i\sigma(\Lambda_T)] \left[ \frac{\pi - \theta}{\sin\theta} \right]^{1/2} t(\Lambda_T) \{H_T^+(\theta)[J_0(\Lambda_T(\pi - \theta)) + iJ_1(\Lambda_T(\pi - \theta))] + H_T^-(\theta)[J_0(\Lambda_T(\pi - \theta)) - iJ_1(\Lambda_T(\pi - \theta))] \},$$
(10)

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V (MeV)	<i>r<sub>R</sub></i> (fm)	<i>a<sub>R</sub></i> (fm)	W (MeV)	<i>r<sub>I</sub></i> (fm)	<i>a<sub>I</sub></i> (fm)	<i>r<sub>C</sub></i> (fm)
10.00	1.350	0.618	23.400	1.277	0.435	1.20
10.16	1.460	0.470	4.210	1.530	0.200	1.46
	V (MeV) 10.00 10.16	$ \begin{array}{c cccc} V & r_R \\ (MeV) & (fm) \\ \hline 10.00 & 1.350 \\ 10.16 & 1.460 \end{array} $	V $r_R$ $a_R$ (MeV)         (fm)         (fm)           10.00         1.350         0.618           10.16         1.460         0.470	$V$ $r_R$ $a_R$ $W$ (MeV)         (fm)         (fm)         (MeV)           10.00         1.350         0.618         23.400           10.16         1.460         0.470         4.210	$V$ $r_R$ $a_R$ $W$ $r_I$ (MeV)(fm)(fm)(MeV)(fm)10.001.3500.61823.4001.27710.161.4600.4704.2101.530	$V$ $r_R$ $a_R$ $W$ $r_I$ $a_I$ (MeV)(fm)(fm)(MeV)(fm)(fm)10.001.3500.61823.4001.2770.43510.161.4600.4704.2101.5300.200

TABLE I. Optical potential parameters used for the calculation of the angular distributions presented in Figs. 6 and 7.

where  $J_0(x)$  and  $J_1(x)$  are cylindrical Bessel functions,  $H^{\pm}(\theta)$  are functions depending on the particular parametrization used for the unperturbed S matrix, the normalization of the amplitude  $\tilde{f}(\theta)$  is contained in the term  $t(\Lambda_T)$ :

$$t(\Lambda_T) = \frac{1}{2} \frac{\mu_n \mu_m}{\hbar^4 k_n k_m^*} a_T(K_n K_m) a_T(K_m K_n) I_{00}^{(k_n)}(\theta_R^+ \xi) I_{00}^{(k_m)}(\theta_R^+ \xi) , \qquad (11)$$

$$a_{T}(K_{n}K_{m}) = N_{1}N_{2}(-1)^{l_{1}}\frac{\hbar^{2}}{2\mu_{T}}K_{n}^{-l_{1}}K_{m}^{l_{1}-1},$$
(12)

where  $N_1N_2$  is the product of the spectroscopic factors of the target and projectile, and  $l_1$  is the orbital angular momentum of the transferred  $\alpha$  particle in <sup>24</sup>Mg.

#### B. Numerical results

In order to calculate the elastic cross section

$$\left| \frac{d\sigma}{d\Omega} \right|_{\text{elastic}} = |\mathring{f}(\theta) + \widetilde{f}(\theta)|^2$$
(13)

taking into account the influence of the double  $\alpha$  transfer on the elastic channel, we must calculate  $f(\theta)$  and  $\tilde{f}(\theta)$ .

# 1. Unperturbed amplitude $f(\theta)$

In order to calculate the unperturbed amplitude  $\mathring{f}(\theta)$  we need the unperturbed S matrix  $\mathring{S}(\lambda)$  which describes the interaction of  ${}^{12}\text{C} + {}^{24}\text{Mg}$  at 40 MeV. As we claim that the intermediate and backward angle oscillations are due to the double  $\alpha$ -transfer channel, we determine  $\mathring{S}(\lambda)$  from an optical potential that fits all forward angle elastic scattering data of  ${}^{12}\text{C} + {}^{24}\text{Mg}$  at energies from  $E_{\text{lab}} = 19$  to 40 MeV. Unpublished data<sup>27</sup> at  $E_{\text{lab}} = 19$ , 21, and 23 MeV, data at  $E_{\text{lab}} = 24.8$ , 31.20, and 34.80 MeV from Mermaz,<sup>3</sup> and data at  $E_{\text{lab}} = 21$  and 24 MeV from Carter<sup>28</sup> were analyzed together with our 40-MeV data. Two potentials were successful in fitting the forward angle region at all energies; they are

presented in Table I. The real and imaginary potentials have the usual Woods-Saxon form, and the radii are defined as

$$R_{R,I} = r_{R,I} (A_T^{1/3} + A_P^{1/3})$$

and

$$R_C = r_C (A_T^{1/3} + A_P^{1/3})$$

The potential X3 is derived from E 18 just changing the imaginary radius and diffuseness, and potential I was obtained by Kono and Mittig<sup>27</sup> for the lower energy data. Carter's potential<sup>28</sup> was not adequate for other energies.



FIG. 6. Elastic scattering angular distributions (Ref. 27) and optical potential calculations performed with potentials X3 and I (see Table I) to fit the forward angle data.



FIG. 7. Elastic scattering angular distributions of Mermaz (Ref. 3) and our data, with optical model calculations that fit the forward angle data.

The fits obtained with these two potentials are shown in Figs. 6 and 7. The reflection functions  $\eta_l$  calculated from these two potentials are presented in Fig. 8. In our closed formalism calculations we used the Ericson's parametrization for the unperturbed S matrix:



FIG. 8. The reflection functions of the potentials X 3 and I (see Table I) together with the dotted-dashed line adopted as the unperturbed reflection function  $|\mathring{S}(\lambda)|$ , with parameters  $\Lambda = 18.7$ ,  $\Delta = 1.3$ ,  $\alpha = 0.5$ .

$$\dot{S}(\lambda) = \frac{1}{1 + \exp\left[\frac{\Lambda - \lambda}{\Delta} - i\alpha\right]} .$$
(14)

The  $\mathring{S}(\lambda)$  adopted in our calculation has a reflection function  $|\mathring{S}(\lambda)|$ , which reproduces the optical potential reflection functions well; it is represented by the dotted-dashed curve in Fig. 8.

The parameters  $\Lambda$ ,  $\Delta$ , and  $\alpha$  are found to be  $\Lambda = 18.7$ ,  $\Delta = 1.3$ , and  $\alpha = 0.5$ . The fit obtained to the elastic scattering data at 40 MeV from  $d\sigma/d\Omega = |\mathring{f}(\theta)|^2$ , using these parameters in  $\mathring{S}(\lambda)$  and calculating  $\mathring{f}(\theta)$  by the explicit summation of partial waves, is presented in Fig. 9 as the dashed line. It reproduces the forward angle data well, but deviates from data at intermediate angles and presents no oscillations there.

# 2. The amplitude $\tilde{f}(\theta)$

As we have seen before, the amplitude  $\tilde{f}(\theta)$  depends only on the characteristics of the transfer process. In order to determine the relevant charac-



FIG. 9. The experimental angular distribution of the elastic scattering, together with the elastic scattering cross section calculated from  $f(\theta)$  (unperturbed elastic scattering amplitude) as the dashed line, and the cross section calculated taking into account the coupling to the  $\alpha$ -transfer channel, with a phase  $\phi = 2.0$  between the amplitudes  $f(\theta)$  and  $\tilde{f}(\theta)$  as the continuous line.

teristics of the  $\alpha$  transfer  ${}^{12}C + {}^{24}Mg \rightarrow {}^{16}O + {}^{20}Ne$ , we analyzed these transfer data in the frame of Frahn's closed formalism for transfer.<sup>25</sup> Beginning

with the DWBA transition amplitude and using the approximations already mentioned previously, one obtains, for L = 0, K = 0, M = 0,

$$\left[\frac{d\sigma}{d\Omega}\right]_{\text{transfer}} = |f_T(\theta)|^2$$

$$= \frac{A\mu_n\mu_m}{(2\pi\hbar^2)^2} \frac{k_n}{k_m} \frac{\pi}{(k_nk'_mK)^2} \frac{\theta}{\sin\theta}$$

$$\times \left| (d_{00}^0)^2 \Lambda_T I_{00}^K(\theta_R^T,\xi) e^{\gamma \delta_T} \exp[i 2\delta_k(\Lambda_T)] \pi \Delta$$

$$\times \{H^+(\theta)[J_0(\Lambda_T\theta) + iJ_1(\Lambda_T\theta)] + H^-(\theta)[J_0(\Lambda_T\theta) - iJ_1(\Lambda_T\theta)]\} \right|^2.$$
(15)

In the actual calculation of  $f_T(\theta)$  we used an asymptotic expansion for the cylindrical Bessel functions  $J_0$  and  $J_1$ , valid in forward and intermediate angles. The quantity A, which is a normalization factor related to the strength of the interaction  $V_{l_n l_m}$  responsible for the  $n \rightarrow m$  transfer, contains the spectroscopic, geometric, and spin factors. The derivation of  $f_T(\theta)$  is based on zero range and no-recoil assumptions. We know that these dynamic effects are important and the absolute transfer cross section calculated without taking into account these dynamic effects can be underestimated by orders of magnitude. For practical purposes we define the normalization factor

$$A = \frac{\left(\frac{d\sigma}{d\Omega}\right)_{exp}}{\left(\frac{d\sigma}{d\Omega}\right)_{theor}}$$

and it will contain the usual geometric, spectroscopic, and spin factors, together with a dynamic factor determined empirically.

The comparison of the experimental transfer cross section and the theoretical calculations, which gives a good fit to the data using the above formula, permits one to obtain the relevant parameters of the transfer amplitude:  $\Lambda_T = 18.27$ ,  $\Delta_T = 0.3$ ,  $\alpha_T = 1.57$ . The results of the above transfer calculation are presented in Fig. 10.

If we compare the expressions of the double  $\alpha$  transfer amplitude  $\tilde{f}(\theta)$  and the single  $\alpha$  transfer amplitude  $f_T(\theta)$ , we can verify that they have the same angular dependence and that  $\tilde{f}(\theta)$  is proportional to the square of  $f_T(\theta)$ , showing in a certain

manner that  $\tilde{f}(\theta)$  describes the round trip of an  $\alpha$  particle from <sup>24</sup>Mg to <sup>12</sup>C and back again. The normalization of  $\tilde{f}(\theta)$  is known except for the empirical dynamic factor due to the zero range and norecoil nature of the calculation. The way we introduce this dynamic factor into  $\tilde{f}(\theta)$  is to assume that the strength  $a_T(K_nK_m)$  of the coupling interaction is the same both in the derivation of  $f_T(\theta)$  and that of  $\tilde{f}(\theta)$ . This assumption leads to the following relation between the normalization factors:



FIG. 10. The  $\alpha$ -transfer reaction <sup>24</sup>Mg(<sup>12</sup>C, <sup>16</sup>O)<sup>20</sup>Ne (g.s.) together with the calculation in Frahn's formalism.

$$N^{2} = N_{1}N_{2} = \frac{2\mu_{T}}{\xi \hbar} \left[ \frac{2J_{i} + 1}{2J_{f} + 1} AK_{n}K_{m} \right]^{1/2}.$$
(16)

The normalization factor obtained from A, empirically determined by adjusting the transfer cross section, is N = 1300.

The complete calculation, adding to the elastic amplitude  $\mathring{f}(\theta)$  the amplitude  $\widetilde{f}(\theta)$  (calculated with the parameters  $\Lambda_T$ ,  $\Delta_T$ ,  $\alpha_T$  and N conveniently determined from the transfer reaction), gives an angular distribution where the amplitudes of oscillations are of the same order of magnitude as the experimental ones; the period is also correct, but the oscillations are somewhat out of phase. We performed calculations introducing an arbitrary phase  $\phi$  between  $\mathring{f}(\theta)$  and  $\widetilde{f}(\theta)$ ,

$$\left|\frac{d\sigma}{d\Omega}\right|_{\text{elastic}} = |\mathring{f}(\theta) + e^{i\phi}\widetilde{f}(\theta)|^2, \qquad (17)$$

and determined  $\phi = 2.0$  rad. The result of the calculation with phase  $\phi$  is presented in Fig. 9 as the continuous line. It reproduces the forward angle and intermediate angle oscillations well. One possible origin of  $\phi$  may be traced to the off-shell effects, which were completely neglected in Ref. 22.

## **IV. CONCLUSIONS**

The aim of this study was to test the hypothesis that the oscillations seen in the angular distributions at intermediate angles are related to the polarization in the elastic channel due to its coupling to a single- $\alpha$  transfer channel. Using the picture discussed in Sec. III, we found a good accord with the data; the period and amplitude of the oscillations are comparable at intermediate angles. The only adjusted parameter to fit the elastic data is the relative phase between the amplitudes  $\hat{f}(\theta)$  and  $\tilde{f}(\theta)$ . The other parameters were fixed by the transfer data or by a large amount of elastic data at other energies.

From our calculations we can conclude that the channel coupling to the  $\alpha$ -transfer process could have an important effect at intermediate angles and at energies above the Coulomb barrier. At backward angles, the elastic transfer, which produces a parity dependent term in the nuclear S matrix, should come into play. As the spectroscopic factor for the elastic transfer of a <sup>12</sup>C must be very small, the successive transfer of three  $\alpha$  particles can be also responsible for the very backward rise in the cross section. The main advantage of doing the kind of calculation reported here within the framework of the closed formalism is the mathematical simplicity, which permits a better physical insight into the processes.

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