

Thickness dependence of spin-orbit torques generated by WTe₂David MacNeill,¹ Gregory M. Stiehl,¹ Marcos H. D. Guimarães,^{1,2} Neal D. Reynolds,¹
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We study current-induced torques in WTe₂/permalloy bilayers as a function of WTe₂ thickness. We measure the torques using both second-harmonic Hall and spin-torque ferromagnetic resonance techniques for samples with WTe₂ thicknesses that span from 16 nm down to a single monolayer. We confirm the existence of an out-of-plane antidamping torque, and we show directly that the sign of this torque component is reversed across a monolayer step in the WTe₂. The magnitude of the out-of-plane antidamping torque depends only weakly on WTe₂ thickness, such that even a single-monolayer WTe₂ device provides a strong torque that is comparable to much thicker samples. In contrast, the out-of-plane fieldlike torque has a significant dependence on the WTe₂ thickness. We demonstrate that this fieldlike component originates predominantly from the Oersted field, thereby correcting a previous inference drawn by our group based on a more limited set of samples.

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Current-induced torques in materials with strong spin-orbit coupling provide an attractive approach for efficiently manipulating nanomagnets [1]. Spin-orbit torques are most commonly studied in polycrystalline ferromagnet/heavy-metal bilayers [2–9], but several groups have also investigated crystalline spin-orbit materials [10–17]. Using noncentrosymmetric crystals, researchers have demonstrated spin-orbit torques within a single ferromagnetic layer [10,11,13,16] and electrical switching of an antiferromagnet [14]. For some low-symmetry crystal structures, it is possible to generate out-of-plane polarized spin injection in response to an in-plane applied current [17]. This is an important capability for applications. Out-of-plane spin injection could enable efficient antidamping switching of high-density magnetic memory devices with perpendicular magnetic anisotropy that is not possible with conventional spin-orbit torques [17].

Recently, our group has measured current-induced torques acting on a ferromagnetic layer (permalloy, Py = Ni₈₀Fe₂₀) deposited on single crystals of the layered material WTe₂ [17]. WTe₂ is an intriguing choice of spin-source material, due to its strong spin-orbit coupling [18,19], surface states [20,21], high mobility [22–24], and low-symmetry crystal structure [25,26]. The crystal structure of WTe₂ is such that when current is applied along the WTe₂ *a* axis, a spin-orbit torque consistent with transfer of spins oriented partially along the *z* axis (out of the sample plane) is observed in the permalloy. The geometry is illustrated in Fig. 1. We refer to this torque as the out-of-plane antidamping torque, τ_B . As discussed in our previous work, the dependence of τ_B on the current flow direction reflects the symmetries of the WTe₂ surface in a detailed way.

While the existence of τ_B is consistent with symmetry constraints, its microscopic origin is not understood. Even the conventional current-induced torques in the WTe₂/Py system (an in-plane antidamping torque, τ_S , and an out-of-plane fieldlike torque, τ_A) have not yet been assigned concrete mechanisms. Known mechanisms such as the Rashba-Edelstein effect (REE) [10,27] and the spin Hall effect (SHE) [28,29] have distinct thickness dependencies once the layer thickness is comparable to the spin diffusion length. For this reason,

varying the spin-source thickness can provide clues as to the origin of current-induced torques [5,30–33].

Here, we report measurements of current-induced torques in WTe₂/Py bilayers for a wide range of WTe₂ thicknesses, down to the previously unexplored monolayer limit. We employ second-harmonic Hall [3,34] and spin-torque ferromagnetic resonance (ST-FMR) [5,12] measurements as complementary techniques for studying current-induced torques, and we report good agreement between the two. We find that the magnitude of the out-of-plane antidamping torque component $|\tau_B|$ depends only weakly on the WTe₂ thickness *t* for *t* > 4 nm, and it remains significant even for thinner samples all the way to the monolayer (0.7 nm) limit for WTe₂. We also demonstrate by direct measurements that the sign of τ_B reverses across a monolayer step. In contrast to a conclusion we made previously based on a much smaller data set [17], we find that the out-of-plane fieldlike torque varies as a function of WTe₂ thickness with a form in quantitative agreement with a dominant contribution from the current-induced Oersted field.

Our WTe₂/Py stack is shown in Fig. 1(a). To prepare the stack, we take a commercially available WTe₂ crystal (from HQgraphene), and we exfoliate it onto a high-resistivity Si/SiO₂ wafer using Scotch tape. The final step of exfoliation, where the tape is removed from the substrate to cleave the WTe₂ crystals, is carried out in the load-lock chamber of our sputter system. The pressure at this step is well below 1×10^{-5} Torr. This preparation differs from our previous work (Ref. [17]), in which the samples were exfoliated in flowing nitrogen after purging the load-lock. The samples are then moved to the process chamber without breaking vacuum, where we deposit 6 nm of Py by glancing angle ($\sim 5^\circ$) sputtering and 2 nm of Al to prevent oxidation of the ferromagnet. The Py moment lies in the sample plane. Before further processing, the topography and thickness of the chosen flakes are characterized by atomic force microscopy (AFM). We are careful to position devices only in regions that are atomically smooth (less than 200 pm roughness) and contain no steps in the WTe₂ layer, except for devices in which steps are positioned intentionally between different sets of Hall contacts

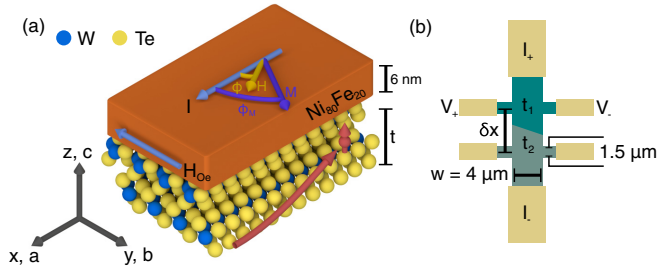


FIG. 1. (a) Illustration of our WTe_2/Py bilayers. The Py thickness is 6 nm, and the WTe_2 thickness, t , varies between devices. For all devices we study, the WTe_2 c axis is normal to the sample plane, and the current flow direction is chosen to be approximately aligned to the WTe_2 a axis. We carry out our measurements with the magnetic field applied at a variable angle, ϕ , from the current flow direction. The red arrow depicts injection of out-of-plane spins into the permalloy, which can account for an out-of-plane antidamping torque. (b) Illustration of the device geometry and electrical connections. For some devices, we used WTe_2 with mono- or bilayer steps in the channel, allowing for multiple thickness data points from a single device. To eliminate cross-talk, we keep $\delta x > 4 \mu\text{m}$.

(see below). The films are then patterned into Hall bars using e-beam lithography and argon ion-milling (where we use SiO_2 as the etch mask). The current-flow direction is chosen to lie along the direction of long straight edges in the cleaved WTe_2 flakes, which typically corresponds to the WTe_2 a axis. The angle between the current flow direction and the a axis is later checked using planar Hall effect measurements on the completed devices (see below). This angle was always less than 20° and typically less than 5° . Contact pads of 5 nm Ti/75 nm Pt are also defined using e-beam lithography and sputtering.

We will first discuss second-harmonic Hall measurements of the spin-orbit torques. Second-harmonic Hall measurements allow for a precise calibration of the current flowing in the device (more easily than, e.g., ST-FMR) and therefore provide a convenient method for making an accurate comparison between devices. When the equilibrium magnetization is in the sample plane, this technique is most easily used for measuring out-of-plane torques because in this geometry the signals for in-plane torques must be disentangled from an artifact due to the anomalous Nernst effect [35]. Our Hall bar design is shown in Fig. 1(b). We keep the width of the channel ($w = 4 \mu\text{m}$) and the voltage probes ($1.5 \mu\text{m}$) consistent across all devices. This helps prevent artifacts in the thickness series due to changes in the current distribution. For the second-harmonic Hall measurements, we apply a voltage of 400 mV root mean square (rms) at 1.317 kHz to the device and a series resistor, and we measure the first- and second-harmonic Hall voltages simultaneously. We calibrate the current flowing through the device by measuring the voltage across the series resistor. For some of our devices, we placed multiple Hall contact pairs (up to three) on the same device, with each pair sensing regions of different WTe_2 thickness. Since the transverse voltages are expected to decay as $e^{-\pi\delta x/w}$ [see Fig. 1(b)] [36], we placed the contacts at least $4 \mu\text{m}$ apart to avoid cross-talk. This allows for direct thickness comparisons within the same device.

The Hall resistance of a WTe_2/Py bilayer can be modeled as $R_H = R_{\text{PHE}} \sin(2\phi_M) \sin^2(\theta_M) + R_{\text{AHE}} \cos(\theta_M)$, where ϕ_M is the angle between the Py moment and the current flow direction, θ_M is the angle of the Py moment from the z axis, R_{PHE} is the planar Hall resistance, and R_{AHE} is the anomalous Hall resistance. When a current $I(t) = I_0 \sin(\omega t)$ is applied to the bilayer, any out-of-plane current-induced torques will rotate the moment in-plane, $\phi_M \rightarrow \phi_M + \delta\phi_M \sin(\omega t)$. In-plane torques will rotate the moment out-of-plane: $\theta_M \rightarrow \theta_M + \delta\theta_M \sin(\omega t)$. The Hall voltage is therefore $V_H(t) = I(t)R_H(t) = I_0 R_H \sin(\omega t) + I_0 \frac{dR_H}{d\phi_M} \delta\phi_M \sin^2(\omega t) + I_0 \frac{dR_H}{d\theta_M} \delta\theta_M \sin^2(\omega t)$, where the last two terms represent the response from current-induced torques. Calculating $\delta\phi_M$ and $\delta\theta_M$ as a function of the in-plane and out-of-plane torques, τ_ϕ and τ_z , gives the second-harmonic (2ω) voltage component (see Appendix B):

$$V_H^{2\omega} \approx I_0 R_{\text{PHE}} \cos(2\phi_M) \frac{\tau_z/\gamma}{H + H_A \cos(2\phi_M - 2\phi_E)} - \frac{1}{2} I_0 R_{\text{AHE}} \frac{\tau_\phi/\gamma}{H + M_s + H_A \cos^2(\phi_M - \phi_E)}, \quad (1)$$

where H is the applied field magnitude, M_s is the effective magnetization, H_A is the in-plane uniaxial anisotropy field, and ϕ_E is the angle of the anisotropy axis relative to the current flow direction. We have previously shown that the in-plane easy axis always lies along the WTe_2 b axis in WTe_2/Py bilayers (so that $\phi_E \approx 90^\circ$). We determine H_A and ϕ_E for each sample by analyzing the dependence of the first-harmonic planar Hall voltage on the angle of an applied magnetic field (see Appendix C). The results of this determination are given in Table I in Appendix A. We find that the current-flow direction was always aligned with the WTe_2 a axis to within better than 20° , and H_A has values in the range 48–96 Oe.

To complete our model, we note that torques from the Oersted field and ordinary SHE will be proportional to $\hat{m} \times \hat{y}$ and $\hat{m} \times (\hat{m} \times \hat{y})$, respectively. Then $\tau_{z,\text{Oe}}(\phi_M) = \tau_A \cos(\phi_M)$ and $\tau_{\phi,\text{SHE}}(\phi_M) = \tau_S \cos(\phi_M)$. When a magnet absorbs out-of-plane spins, the resulting torque is $\propto \hat{m} \times (\hat{m} \times \hat{z})$ [37], so that the out-of-plane antidamping torque gives an angle-independent contribution, $\tau_z(\phi_M) = \tau_B$, for an in-plane magnetic moment. For our fits, we also add an angle-independent voltage offset, C , and a term $\propto \cos(\phi_M)$ to account for the anomalous Nernst effect resulting from an out-of-plane thermal gradient [35]. The resulting model for the field and angle dependence of our second-harmonic Hall data is

$$V_H^{2\omega} = I_0 R_{\text{PHE}} \cos(2\phi_M) \frac{[\tau_A \cos(\phi_M) + \tau_B]/\gamma}{H + H_A \cos(2\phi_M - 2\phi_E)} - \frac{1}{2} I_0 R_{\text{AHE}} \frac{\tau_S \cos(\phi_M)/\gamma}{H + M_s + H_A \cos^2(\phi_M - \phi_E)} + V_{\text{ANE}} \cos(\phi_M) + C, \quad (2)$$

where V_{ANE} is the anomalous Nernst voltage. In our system, $H_A \ll M_s$, which means the anomalous Nernst effect and the in-plane torques give second-harmonic Hall voltages with indistinguishable ϕ dependence. We fit them with a single term $\propto \cos(\phi_M)$. There are six other fit parameters: $I_0 R_{\text{PHE}} \tau_A$, $I_0 R_{\text{PHE}} \tau_B$, H_A , ϕ_E , C , and an overall angular offset not shown

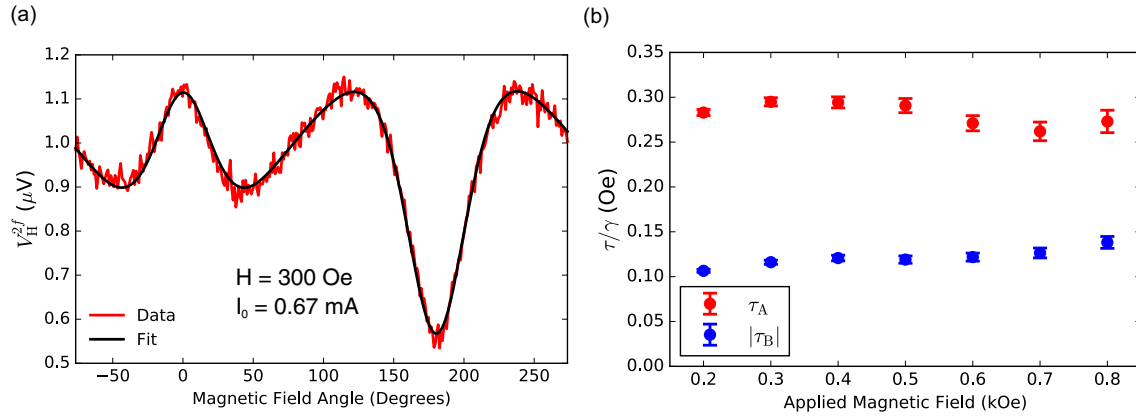


FIG. 2. (a) Second-harmonic Hall voltage for a WTe₂ (5.6 nm)/Py (6 nm) bilayer as a function of the in-plane angle of the applied magnetic field (the magnitude of the applied field is 300 Oe). The red curve represents measured data, and the black line is a fit to Eq. (2). The lack of odd symmetry under $\phi \rightarrow \phi + 180^\circ$ indicates the presence of an out-of-plane antidamping torque, τ_B . (b) Dependence of the measured out-of-plane fieldlike (τ_A , red circles) and out-of-plane antidamping torque (τ_B , blue circles) on the magnitude of applied magnetic field. The negligible field dependence is evidence that the signals arise from current-induced torques.

here, which accounts for any misalignment of the device from the axes of the measurement apparatus. $I_0 R_{\text{PHE}}$ is determined independently using the ϕ dependence of the first-harmonic Hall voltage, allowing measurements of τ_A and τ_B from data for $V_H^{2\omega}$ as a function of ϕ .

Figure 2(a) shows $V_H^{2\omega}(\phi)$ data from one of our WTe₂/Py bilayers. The WTe₂ is 5.6 nm thick and the current flows along the WTe₂ a axis ($\phi_E \approx 90^\circ$). The red line shows measured data, and the black line is a fit to Eq. (2). The existence of a nonzero value of τ_B is apparent from the lack of $\phi \rightarrow \phi + 180^\circ$ symmetry; in particular, the different-sized peaks at $\phi = 0^\circ$ and 180° relate to the cooperation $\tau_z = \tau_B + \tau_A$ or competition $\tau_z = \tau_B - \tau_A$ of the different out-of-plane torques. This asymmetry reflects the absence of rotational symmetry at the WTe₂ surface. Figure 2(b) shows τ_A and τ_B [from fits to Eq. (2)] as a function of the applied magnetic field. The extracted torques are to a good approximation independent of the magnitude of the applied field, confirming that they originate from current-induced torques.

A key prediction of our symmetry arguments in Ref. [17] is that the sign of τ_B should change across a monolayer step in WTe₂ thickness if this step occurs at the Py/WTe₂ interface. This is because adjacent WTe₂ layers are related by a 180° rotation around the c axis (see Fig. 3), and τ_B is not twofold symmetric— τ_B changes sign with a 180° rotation about the c axis. In Ref. [17] we presented indirect evidence for this conclusion, in which a sample whose device area spanned across a single-monolayer step in the WTe₂ layer exhibited a suppressed value of τ_B due to partial cancellations of the contributions from the two crystal faces. Here we provide a direct test by fabricating devices containing multiple Hall contacts so that we can separately measure the values of τ_B produced by different regions of the same sample separated by steps of known height (see Fig. 1). We have fabricated six devices with Hall contacts on either side of a monolayer step, as determined by AFM measurements showing a step height 0.7 ± 0.3 nm. Figure 3 shows second-harmonic Hall data for a device where the WTe₂ thickness increases from a monolayer to a bilayer in the middle of the channel. For the monolayer

side we found $\tau_B/\gamma = -0.093 \pm 0.002$ Oe, whereas for the bilayer side $\tau_B/\gamma = 0.049 \pm 0.002$ Oe. The out-of-plane fieldlike component τ_A has the same sign on both sides of the step ($\tau_A/\gamma = 0.103 \pm 0.004$ and 0.123 ± 0.003 Oe for the monolayer and bilayer, respectively). In five out of six devices with Hall contacts on opposite sides of a monolayer step, we found that τ_B changes sign between contacts (see Appendix A). In principle, the monolayer step we observe by AFM could be on either the top (Py/WTe₂) or bottom (WTe₂/SiO₂) interface of the WTe₂, and we do not expect that a step at the WTe₂/SiO₂

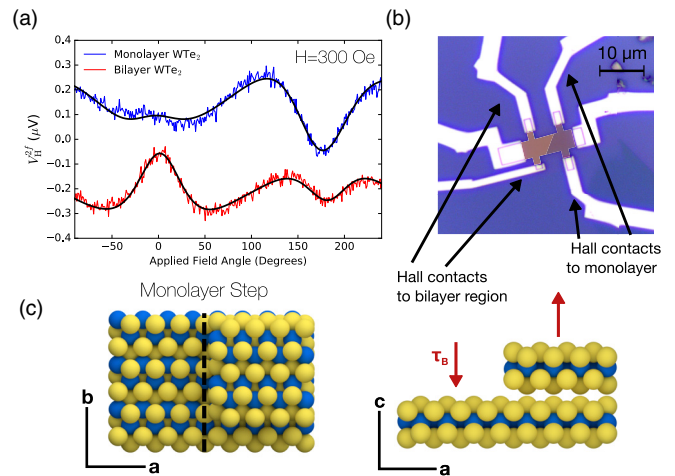


FIG. 3. (a) Second-harmonic Hall data for a WTe₂/Py device for a region of the sample with a monolayer-thick WTe₂ layer (top curve, blue) and for a different region of the same sample with bilayer WTe₂ (bottom curve, red), as a function of the angle of the applied magnetic field (defined relative to the current flow direction). The lines are fits to Eq. (2). The sign reversal of τ_B is reflected in the different angles at which the peak signals are found. A vertical offset is added to the data for ease of viewing. (b) Optical micrograph of the device measured for panel (a), showing the monolayer and bilayer WTe₂ regions in false color. (c) Schematic of the crystal structure of WTe₂, showing that the surface structure is rotated by 180° across a monolayer step.

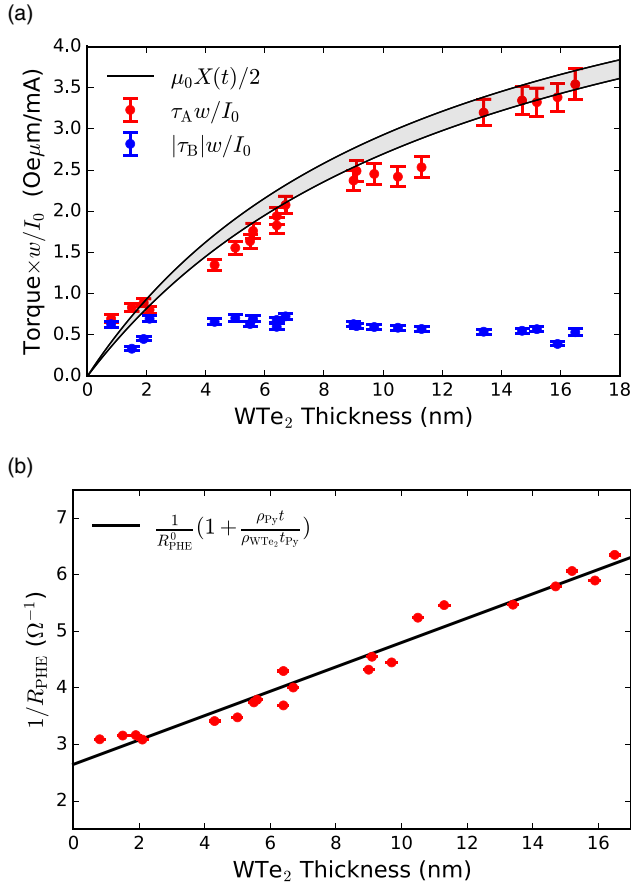


FIG. 4. (a) Torques normalized per unit I_0/w for (red circles) the out-of-plane fieldlike component $\tau_A w/I_0$ and (blue circles) the out-of-plane antidamping component $|\tau_B|w/I_0$, as a function of WTe₂ thickness, for all devices measured. The shaded region shows a $\pm 1\sigma$ estimate for the torque from the magnetic field generated by the current flowing in the WTe₂. (b) (red circles) Dependence of the inverse of the first-harmonic planar Hall resistance on the WTe₂ thickness. Current shunting through the WTe₂ leads to a linear increase in $1/R_{\text{PHE}}$ as t is increased. The black line is a linear fit, which gives an estimate of the shunt factor $X(t)$ as a function of WTe₂ thickness.

interface would affect the sign of τ_B . Therefore, it is somewhat surprising that we observe sign changes in more than 50% of samples. It may be that the mechanics of exfoliation causes steps in the WTe₂ to be more likely on the top surface of the flake than the bottom. In devices with a bilayer step dividing two sets of Hall contacts, τ_B never changes sign (three out of three devices).

We now turn to our thickness series over multiple devices. In total, we measured torques from 12 distinct devices, some with multiple Hall contacts per device. The resulting data are shown in Fig. 4(a), where we plot $|\tau_B|w/I_0$ (blue points) and $\tau_A w/I_0$ (red points) as a function of WTe₂ thickness. The complete data set is given in Appendix A. We normalize the torques by the current density I_0/w since we can measure the current flowing in the channel more easily than the electric field. We observe in Fig. 4(a) that the out-of-plane fieldlike torque τ_A/I_0 has a significant dependence on the WTe₂ thickness, increasing by

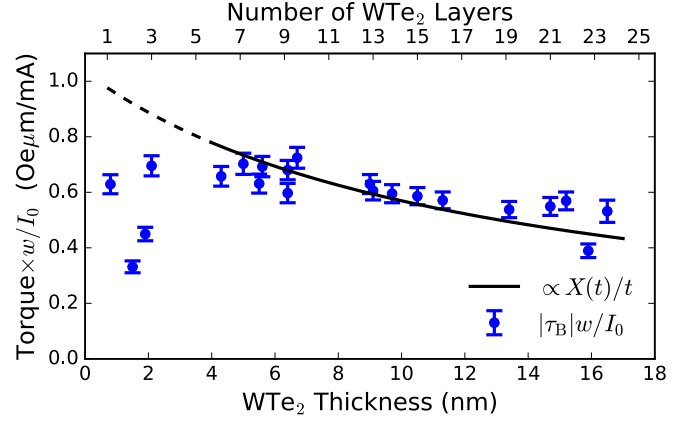


FIG. 5. $|\tau_B|w/I_0$ as a function of WTe₂ thickness (blue circles) along with a curve proportional to $X(t)/t$ as estimated from our planar Hall effect data (black solid and dashed lines). The proportionality constant is chosen to fit the data above 4 nm of WTe₂ thickness.

a factor of over 4.8 between the monolayer sample and 16 nm, while the out-of-plane antidamping torque has a much weaker dependence.

In many spin-orbit torque systems (but not all [12,15,16,38]), the out-of-plane fieldlike torque τ_A is dominated by a contribution from the Oersted field. The Oersted torque is related to the fraction of current flowing in the nonmagnetic underlayer, $X(t) \equiv I_{\text{WTe}_2}/I_0$, by $\tau_{\text{Oe}} = \mu_0 X(t) I_0 / 2w$, where $I_0 = I_{\text{Py}} + I_{\text{WTe}_2}$. To determine the factor $X(t)$ for our devices, we examine the planar Hall resistance extracted from the first-harmonic Hall voltage as a function of t [shown in Fig. 4(b)]. The observed linear dependence on WTe₂ thickness is consistent with a reduction in the planar Hall resistance due to shunting through the WTe₂, and an approximately constant WTe₂ resistivity:

$$\frac{1}{R_{\text{PHE}}} = \frac{I_{\text{Py}} + I_{\text{WTe}_2}}{V_{\text{PHE}}} = \frac{1}{R_{\text{PHE}}^0} \left[1 + \frac{\rho_{\text{Py}} t}{\rho_{\text{WTe}_2} t_{\text{Py}}} \right], \quad (3)$$

where $1/R_{\text{PHE}}^0 \equiv I_{\text{Py}}/V_{\text{PHE}}$ when $I_{\text{Py}} = I_0$. The fit yields a normalized WTe₂ conductivity of $\rho_{\text{Py}}/(\rho_{\text{WTe}_2} t_{\text{Py}}) = 0.081 \pm 0.006 \text{ nm}^{-1}$ and a planar Hall coefficient of $R_{\text{PHE}}^0 = 0.38 \pm 0.1 \Omega$ for the Py. The normalized WTe₂ conductivity can be used to estimate

$$X(t) \approx \frac{1}{1 + \frac{\rho_{\text{WTe}_2} t_{\text{Py}}}{\rho_{\text{Py}} t}}. \quad (4)$$

The shaded black area of Fig. 4(a) shows the range of the expected Oersted torque (times w/I_0) within one standard deviation of the best-fit value for $\rho_{\text{Py}}/(\rho_{\text{WTe}_2} t_{\text{Py}})$. The measured points for $\tau_A w/I_0$ all fall close to this area, indicating that τ_A is dominated by the current-generated Oersted field. This result differs from a conclusion we drew based on a more limited data set of devices with $\phi_{a-1} < 20^\circ$ in Ref. [17]. Of course, our data cannot rule out additional spin-orbit contributions, which may be detected by more precise calibration of the Oersted field.

As noted above, compared to $\tau_A w/I_0$, the out-of-plane antidamping torque $|\tau_B|w/I_0$ displays a much weaker dependence on WTe₂ thickness. The form of this weaker dependence is displayed in Fig. 5, which shows a zoomed-in plot of the

same data as in Fig. 4(a) (blue points). For WTe_2 thicknesses greater than 4 nm, $|\tau_B|w/I_0$ decreases slightly as the WTe_2 thickness is increased. This slight decrease is consistent with current shunting if one assumes that $|\tau_B|$ is proportional to the applied electric field within the device. In this case, $|\tau_B|w/I_0$ should be proportional to $X(t)/t$. This proportionality occurs because for a given applied current I_0 the total electric field will decrease with increasing WTe_2 thickness due a decreased overall device resistance. The black line in Fig. 5 shows $X(t)/t$ estimated from the PHE data of Fig. 4(b), rescaled to fit the $|\tau_B|w/I_0$ data for WTe_2 thicknesses above 4 nm. This good agreement, however, tells us little about the origin of τ_B , since the total electric field in the device, the charge current density in the WTe_2 , and the charge current density in the Py are all proportional to this factor.

For $t < 4$ nm, the measurements of $|\tau_B|$ exhibit significantly increased scatter, but even in this regime $|\tau_B|$ can remain large. For the one sample with a single-monolayer WTe_2 that we have been able to study, we find $|\tau_B|w/I_0 = 0.63 \pm 0.03$ Oe $\mu\text{m}/\text{mA}$, very comparable to the values measured for much thicker WTe_2 layers, and fully 65% of the value expected simply by scaling the results from the thicker layers by the factor $X(t)/t$ (see Fig. 5). Our observation that the torque for monolayer WTe_2 samples is not suppressed close to zero suggests that either the spin diffusion length in WTe_2 is very short, comparable to the layer spacing, or else the out-of-plane antidamping torque results from a spin current generated in the Py layer that reflects off of the WTe_2 surface [39–41]. Our data for very thin WTe_2 layers also provide a hint that there might be an even-odd effect in the number of WTe_2 layers in that $|\tau_B|$ for a bilayer sample is the smallest for any of our devices, and in particular it is smaller than for either the monolayer sample or trilayer samples.

To confirm the results of Fig. 4(a) using an independent measurement technique, we also performed ST-FMR measurements using two-terminal devices fabricated from our vacuum-exfoliated WTe_2/Py bilayers. The ST-FMR technique has the advantage that it can provide reliable measurements of both out-of-plane and in-plane current-induced torques, although the current calibration has greater uncertainty because this calibration must be performed using network-analyzer reflectance measurements [38]. For this reason, we will present our ST-FMR results in terms of ratios for the different torque components, in which case the current calibration does not enter.

For the ST-FMR samples, the WTe_2/Py bilayers were etched into bars and contacted in a ground-signal-ground geometry compatible with microwave probes. The device geometry and protocol for our ST-FMR measurements are detailed in Ref. [17]; for the data shown here, the applied frequency was 9 GHz. Figure 6(a) compares the torque ratios $|\tau_B/\tau_A|$ measured with ST-FMR to those from second-harmonic Hall measurements as a function of WTe_2 thickness. The ratio $|\tau_B/\tau_A|$ shows good agreement with the second-harmonic Hall measurements.

Figure 6(b) displays the in-plane torques measured with ST-FMR. Consistent with the results in Ref. [17], we measure a significant in-plane antidamping torque of the form $\tau_S \hat{m} \times (\hat{m} \times \hat{y})$. We find that $|\tau_S/\tau_B| > 1$ and that $|\tau_S/\tau_B|$ does not depend strongly on thickness. As in Ref. [17], we again

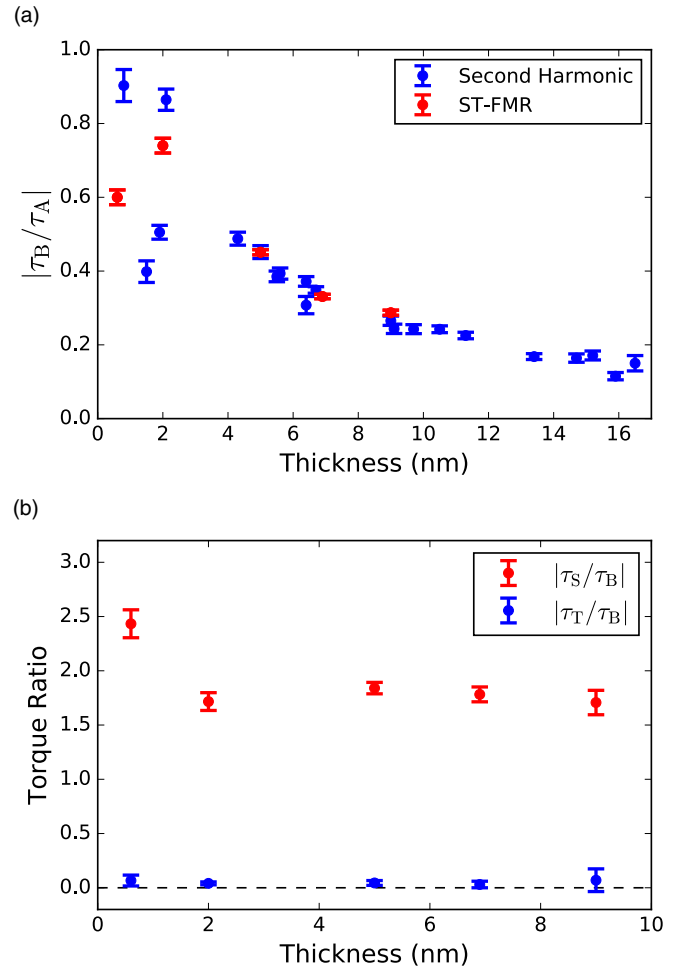


FIG. 6. (a) Comparison of the torque ratios $|\tau_B/\tau_A|$ from ST-FMR and second-harmonic Hall measurements for WTe_2/Py bilayers, as a function of thickness. The blue circles give $|\tau_B/\tau_A|$ from the second-harmonic Hall measurements, and the red circles are the values from ST-FMR. For all ST-FMR measurements, the applied frequency was 9 GHz, and for the second-harmonic measurements, the applied magnetic field was 300 Oe. (b) (red circles) Ratios of the in-plane antidamping torque τ_S to the out-of-plane antidamping torque τ_B as a function of WTe_2 thickness. (blue circles) Ratios of the in-plane fieldlike torque τ_T to the out-of-plane antidamping torque τ_B as a function of WTe_2 thickness. The latter ratio is zero within our measurement uncertainty.

note that although symmetry allows for an in-plane fieldlike torque of the form $\tau_T \hat{m} \times \hat{z}$, we find that $\tau_T = 0$ within our measurement uncertainty.

In summary, we measure current-induced torques in WTe_2/Py bilayers as a function of WTe_2 thickness. We provide direct confirmation that the out-of-plane antidamping torque τ_B changes sign across a monolayer step in the WTe_2 , consistent with the nonsymmorphic symmetries in bulk WTe_2 . For WTe_2 thicknesses t greater than 4 nm, $|\tau_B|$ decreases slowly with increasing thickness consistent with simple current shunting within the bilayer. For t less than 4 nm, $|\tau_B|$ exhibits significant device-to-device variations, which might be associated with finite-size effects, interfacial charge transfer, or electronic structure changes. Nevertheless, τ_B remains

large even for a single-monolayer of WTe_2 . The out-of-plane fieldlike torque τ_A displays a much stronger dependence on WTe_2 thickness, which is quantitatively consistent with the effect of the Oersted field produced by current flowing within the WTe_2 layer. This conclusion regarding the dependence of the fieldlike torque component on WTe_2 thickness represents a correction of our previous report based on a more limited data set of devices with $\phi_{a-1} < 20^\circ$ [17].

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APPENDIX A: TORQUES AND MAGNETIC ANISOTROPY PARAMETERS FOR ALL SECOND-HARMONIC HALL MEASUREMENTS

Table I contains torques and magnetic anisotropy parameters for all second-harmonic Hall measurements.

TABLE I. Device parameters, torques measured by the second-harmonic Hall technique (for the values of applied current I_0 listed in the last column), and measured magnetic anisotropy parameters for the WTe_2/Py bilayers analyzed in the main text. Here ϕ_E is the angle of the magnetic easy axis with respect to the current flow direction, and H_A is the anisotropy field. The number after ‘‘S’’ in each device name indexes the sets of contacts on the same device.

Device name	t (nm) ± 0.3 nm	L (μm) ± 0.2 μm	τ_A (Oe)	τ_B (Oe)	H_A (Oe)	$\phi_E - 90^\circ$ (deg)	I_0 (μA) ± 0.1 μA
SH4D10S1	5.6	13	0.295(4)	-0.116(2)	57.6(4)	2.9(2)	670.0
SH4D10S2	6.4	13	0.325(7)	0.100(3)	61.8(5)	2.7(2)	670.0
SH4D7S1	0.8	12.5	0.103(4)	-0.093(2)	48(4)	-2.6(2)	591.3
SH4D7S2	1.5	12.5	0.123(3)	0.049(2)	54.4(5)	-1.9(3)	591.3
SH4D6S1	16.5	23.5	0.473(9)	-0.071(4)	60.9(5)	1.7(2)	534.3
SH4D6S2	15.9	23.5	0.452(4)	0.052(2)	54.3(5)	2.0(2)	534.3
SH4D6S3	15.2	23.5	0.444(5)	-0.076(2)	58.9(5)	2.9(2)	534.3
SH5D12S1	6.7	9.5	0.410(3)	0.143(2)	64.7(9)	-1.7(4)	789.7
SH5D18S1	2.1	8.5	0.155(4)	-0.134(2)	57.7(5)	18.8(2)	770.8
SH5D26S1	5.5	14.5	0.249(3)	0.096(2)	63.1(8)	4.2(4)	608.3
SH5D26S2	4.3	14.5	0.205(3)	0.100(2)	60.6(2)	4.6(4)	608.3
SH5D25S1	11.3	10.0	0.506(4)	0.114(2)	57.5(7)	2.6(3)	798.6
SH5D25S2	10.5	10.0	0.483(4)	0.117(2)	56.9(7)	1.8(3)	798.6
SH5D29S1	6.4	17.1	0.242(3)	0.090(1)	61.1(8)	2.7(4)	529.4
SH5D29S2	5.0	17.1	0.206(3)	0.093(2)	64.6(8)	2.3(3)	529.4
SH5D28S1	9.7	17.5	0.367(4)	-0.089(2)	68.1(6)	2.1(2)	598.4
SH5D28S2	9.0	17.5	0.355(4)	0.094(2)	69.3(9)	2.4(4)	598.4
SH5D32S1	1.7	7.0	0.192(3)	0.097(2)	77.4(9)	-2.4(3)	862.9
SH5D33S1	13.4	14.0	0.565(4)	-0.095(2)	72(1)	0.5(4)	706.7
SH5D33S2	14.7	14.0	0.591(6)	-0.097(3)	67.9(7)	0.3(3)	706.7
SH5D36S1	9.1	8.5	0.530(6)	0.129(3)	96(2)	-16.1(4)	851.8

APPENDIX B: DERIVATION OF EQ. (1) FROM THE LANDAU-LIFSHITZ-GILBERT-SLONCZEWSKI EQUATION

Our derivation of Eq. (1) in the main text is an adaptation of the analysis in Ref. [34]. To calculate the displacement of the permalloy magnetic moment in response to the current-induced torque, $\boldsymbol{\tau}$, we solve the Landau-Lifshitz-Gilbert-Slonczewski (LLGS) equation in the static limit, i.e., with $d\hat{m}/dt = 0$, where \hat{m} is a unit vector pointing along the macrospin magnetization direction. This reduces to the condition that the net torque (current-induced torque plus the torques from the magnetic anisotropy and applied field) on the magnet vanishes:

$$0 = -\gamma\hat{m} \times [H\hat{h} - M_s(\hat{m} \cdot \hat{z})\hat{z} + H_A(\hat{m} \cdot \hat{b})\hat{b}] + \boldsymbol{\tau}, \quad (\text{B1})$$

where \hat{b} points along the WTe_2 b axis (the magnetic easy axis), and \hat{z} points out of the sample plane. We also introduce vectors for the direction of the in-plane applied field (\hat{h}) and the total current induced torque ($\boldsymbol{\tau}$). To solve Eq. (B1) for the current-induced reorientation of the magnetization, we linearize the equation around the equilibrium (zero-current) magnetization direction \hat{r} , setting $\hat{m} \approx \hat{r} + m_z\hat{z} + m_\phi\hat{z} \times \hat{r}$. Here $\hat{z} \times \hat{r}$ gives an in-plane unit vector orthogonal to the equilibrium magnetization. In equilibrium, the magnetization will point along the total anisotropy field, leading to a self-consistency condition:

$$\hat{r} = [H\hat{h} + H_A(\hat{r} \cdot \hat{b})\hat{b}]/H_{\text{eq}}, \quad (\text{B2})$$

where we have introduced H_{eq} , which is the total anisotropy field evaluated at the equilibrium position of the magnetization

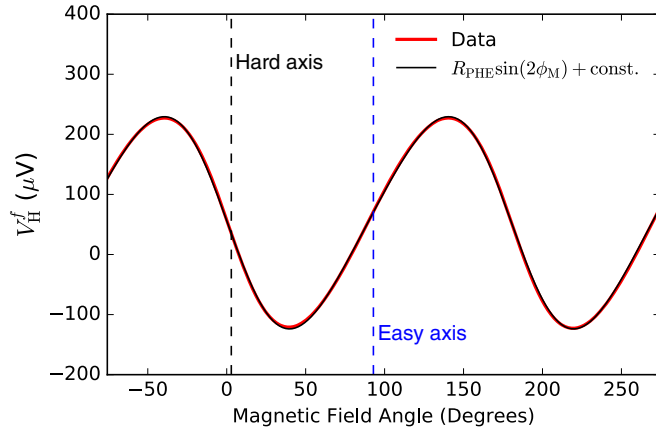


FIG. 7. V_H^f vs ϕ for a WTe_2/Py bilayer with a 5.6 nm WTe_2 underlayer (red). The applied field is 300 Oe. The presence of in-plane magnetic anisotropy is apparent from the lack of symmetry around $\phi = 45^\circ$. The solid black line is a fit assuming an in-plane uniaxial field of magnitude H_A with an easy axis at ϕ_E from the current-flow direction. The values for ϕ_E and H_A determined from the fit are recorded in the “SH4D10S1” row of Table I. The dotted black and blue lines give the estimated angles of the magnetic hard and easy axes, respectively. These are equivalent to the WTe_2 crystal a and b axes.

and so equals $|H\hat{h} + H_A \cos \phi_{M-E}\hat{b}|$. ϕ_{M-E} is the angle between the magnetic moment and the magnetic easy axis in equilibrium.

We can conveniently regroup the terms in the anisotropy field using the consistency condition and $\hat{m} \cdot \hat{b} = \hat{r} \cdot \hat{b} + m_\phi(\hat{z} \times \hat{r}) \cdot \hat{b}$:

$$\tau/\gamma = \hat{m} \times [H_{\text{eq}}\hat{r} - M_s m_z \hat{z} - H_A m_\phi \sin \phi_{M-E} \hat{b}], \quad (\text{B3})$$

where we use $\hat{b} = \cos \phi_{M-E} \hat{r} - \sin \phi_{M-E} \hat{z} \times \hat{r}$ to evaluate $(\hat{z} \times \hat{r}) \cdot \hat{b}$. Substituting in the approximation for \hat{m} and expanding the cross-product gives

$$\begin{aligned} \tau/\gamma = & (M_s + H_{\text{eq}})m_z \hat{z} \times \hat{r} \\ & - (H_{\text{eq}} - H_A \sin^2 \phi_{M-E})m_\phi \hat{z}, \end{aligned} \quad (\text{B4})$$

where we have dropped all terms at second order in the small deviations m_ϕ and m_z . This equation is decoupled in m_ϕ and m_z and so it can trivially be solved to find $\delta\phi_M = m_\phi$ and $\delta\theta_M = -m_z$ required for Eq. (1) of the main text.

The final ingredient is an approximation for H_{eq} , which proceeds from Eq. (B2),

$$\begin{aligned} H_{\text{eq}}^2 = & |H\hat{h} + H_A \cos \phi_{M-E}\hat{b}|^2, \\ H_{\text{eq}} \approx & H + H_A \cos^2 \phi_{M-E}, \end{aligned} \quad (\text{B5})$$

where we assume $H_A \ll H$ and keep terms to first order in H_A/H . This approximation together with Eq. (B4) yields the denominators of Eq. (1).

APPENDIX C: DETERMINATION OF THE MAGNETIC EASY-AXIS FROM FIRST-HARMONIC HALL MEASUREMENTS

To confirm the alignment of the current flow direction to the WTe_2 a axis, we use first-harmonic Hall measurements.

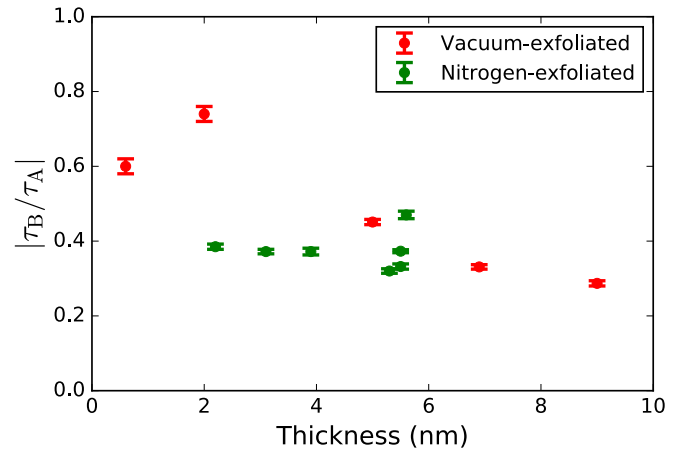


FIG. 8. $|\tau_B/\tau_A|$ extracted from ST-FMR measurements on (green points) devices from Ref. [17] exfoliated in flowing nitrogen and (red points) devices from this paper exfoliated in vacuum.

This is possible since the WTe_2 a axis is always along the hard direction of the in-plane uniaxial magnetic anisotropy. We previously established this fact through comparison of ST-FMR, second-harmonic Hall, and polarized Raman scattering measurements [17]. Because of the in-plane uniaxial anisotropy, the magnetization angle of the permalloy, ϕ_M , will deviate slightly from the applied field angle, ϕ . The equilibrium magnetization angle satisfies the condition

$$\sin(\phi_M - \phi) = -\frac{H_A}{2H} \sin(2\phi_M - 2\phi_E). \quad (\text{C1})$$

Assuming that $H_A \ll H$, we can solve this equation up to first order in H_A/H giving

$$\phi_M = \phi - \frac{H_A}{2H} \sin(2\phi - 2\phi_E). \quad (\text{C2})$$

Fitting the first-harmonic Hall data to $R_H = R_{\text{PHE}} \sin(2\phi_M)$ (and a constant offset) then allows a measurement of ϕ_E and H_A . Data for V_H^f versus ϕ , along with a fit, are given in Fig. 7.

APPENDIX D: COMPARISON BETWEEN ST-FMR DATA FROM THIS PAPER AND FROM REF. [17]

As discussed in the main text, for the ST-FMR data in Ref. [17] we exfoliated WTe_2 flakes in flowing nitrogen in the load-lock chamber of our sputter system. For both the second-harmonic Hall and ST-FMR data in this paper, we exfoliated the WTe_2 flakes in the load-lock under vacuum better than 1×10^{-5} Torr. The ratio $|\tau_B/\tau_A|$ extracted via ST-FMR on the two device types is compared in Fig. 8. For WTe_2 films around 4 nm, the vacuum-exfoliated (red) and nitrogen-exfoliated (green) devices are in good agreement, whereas there is apparent disagreement for thinner flakes. We are not certain whether this apparent disagreement arises from low statistics, or from reaction of the WTe_2 during the nitrogen exfoliation. The effects of oxygen/water exposure on the WTe_2 surface merit further study.

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