Non-Hermitian acoustic metamaterials: Role of exceptional points in sound absorption

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Effective non-Hermitian Hamiltonians are obtained to describe coherent perfect absorbing and lasing boundary conditions. \mathcal{PT} symmetry of the Hamiltonians enables us to design configurations which perfectly absorb at multiple frequencies. Broadened and flat perfect absorption is predicted at the exceptional point of \mathcal{PT} -symmetry breaking while, for a particular case, absorption is enhanced with the use of gain. The aforementioned phenomena are illustrated for acoustic scattering through Helmholtz resonators revealing how tailoring the non-Hermiticity of acoustic metamaterials leads to novel mechanisms for enhanced absorption.

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I. INTRODUCTION

In both classical and quantum physics, non-Hermitian Hamiltonians are being used to describe open systems [\[1\]](#page-7-0) and systems featuring energy dissipation and/or gain [\[2,3\]](#page-7-0). Most of the interesting phenomena in non-Hermitian systems manifest close to the exceptional points (EPs) which are spectral singularities appearing when two eigenmodes coalesce [\[2–4\]](#page-7-0). A particular class of non-Hermitian systems, featuring balanced gain and loss, are called $\mathcal{P}\mathcal{T}$ -symmetric [\[5\]](#page-7-0), and have attracted considerable attention. Such systems suggest possible generalization of quantum mechanics and are extensively studied in diverse areas of physics including Bose-Einstein condensates [\[6,7\]](#page-7-0), optomechanics [\[8\]](#page-7-0), acoustics [\[9,10\]](#page-7-0), and mostly in optics $[11–19]$. Operating around the EPs of \mathcal{PT} symmetric scattering systems has lead to the observation of extraordinary wave effects such as unidirectional invisibility [\[12,20,21\]](#page-7-0), optical isolation [\[16,22\]](#page-7-0), unidirectional perfect absorption [\[23\]](#page-8-0), the simultaneous appearance of coherent perfect absorption (CPA) and lasing [\[24–28\]](#page-8-0), nonreciprocal light propagation [\[14\]](#page-7-0), or asymmetric wave transport [\[29\]](#page-8-0).

Beyond PT -symmetric systems, non-Hermitian configurations featuring unequal amount of loss and gain (or only losses) also exhibit interesting phenomena, closely related with the existence of EPs. These include CPA [\[24\]](#page-8-0), unidirectional near total light absorption [\[30\]](#page-8-0), chiral modes and directional lasing [\[31\]](#page-8-0), and mode switching [\[32\]](#page-8-0). In this context, effective non-Hermitian Hamiltonians associated with the scattering matrix have been obtained to describe CPA, both in microwave [\[33\]](#page-8-0) and polaritonic [\[34,35\]](#page-8-0) systems.

Especially in acoustics, the phenomenon of perfect absorption has attracted great attention the last years due to its direct applications to numerous noise reduction problems. Many solutions have been proposed in the low frequency regime based on subwavelength metamaterial designs, by critically coupling [\[36\]](#page-8-0) resonant scatterers to the waveguide, i.e., by balancing the energy leakage and the internal losses of the resonances. Such studies include the use of membranes [\[37–41\]](#page-8-0), the concept of slow sound [\[42,43\]](#page-8-0), and Helmholtz resonators both in the linear [\[44–47\]](#page-8-0) and nonlinear [\[48\]](#page-8-0) regimes.

Here, we show that by properly tuning the non-Hermiticity of acoustic metamaterials and exploiting the appearance of EPs is a novel way to control sound absorption. The non-Hermiticity of acoustic metamaterials has only been exploited very recently. Specifically, in Ref. [\[49\]](#page-8-0) a closed system of resonant cavities was used to study higher order EPs, in Ref. [\[50\]](#page-8-0) an open lossy acoustic system is used to achieve high quality acoustic hologram, and in Ref. [\[51\]](#page-8-0) the mode coupling around EPs is studied for a lined waveguide. In this work we derive, directly from the acoustic equations, a coupled mode theory (CMT) for the scattering of low frequency waves, in a waveguide side loaded by *N* Helmholtz resonators (HR) at the same position. In Sec. II, we employ the CMT and obtain two different effective Hamiltonians corresponding to different boundary conditions of the scattering problem: no outgoing waves (for CPA) and no incident waves (for laser). For no outgoing waves, the eigenvalues of the effective Hamiltonian yield the particular frequencies where CPA is obtained, which are generally complex since the matrix is non-Hermitian. For the case of two HRs we show how the avoided crossings around an EP lead to the appearance of CPA for real frequencies. In Sec. [III,](#page-2-0) PT symmetry of the effective Hamiltonian is found to provide the necessary condition for multiple CPAs. For the case of two resonators the conditions for \mathcal{PT} symmetry coincide with the critical coupling (CC) of each resonator with the waveguide. Surprisingly, in the case of three HRs, critical coupling of each resonator does not lead to multiple CPAs. PT symmetry however can be established for three resonators, leading to three perfectly absorbed frequencies obtained by the aid of acoustic gain. At the EPs separating the $\mathcal{P}\mathcal{T}$ -unbroken and broken phases, we observe flattened absorption, which is analytically approximated and is found to be stronger for higher order EPs.

II. NON-HERMITIAN EFFECTIVE HAMILTONIANS

A. Coupled mode theory for *N* **resonators**

We consider the scattering of plane waves by *N* Helmholtz resonators, side loaded to an acoustic waveguide at x_0 [see Fig. [\(1\)\]](#page-1-0), which without loss of generality we assume to be $x_0 = 0$. The HRs can be considered as point scatterers and are characterized by a resonance frequency ω_i , internal losses R_i , and external coupling strengths Γ_i ($i = 1, 2, \ldots N$). The conventional way to study the system is by using the scattering matrix **S** which relates the incident acoustic pressure p_1^+ and p_2^- (see Fig. [1\)](#page-1-0) with the outgoing ones p_1^- and p_2^+ , given by

$$
\begin{pmatrix} p_2^+ \\ p_1^- \end{pmatrix} = \mathbf{S}(\omega) \begin{pmatrix} p_1^+ \\ p_2^- \end{pmatrix} \equiv \begin{pmatrix} t & r_R \\ r_L & t \end{pmatrix} \begin{pmatrix} p_1^+ \\ p_2^- \end{pmatrix} . \tag{1}
$$

FIG. 1. A schematic illustration of the configurations under consideration, using two (dimer) and three (trimer) point resonant scatterers side loaded to a waveguide. $\omega_{1,2,3}$ are the resonant frequencies, $r_{1,2,3}$ the intrinsic losses, and $\gamma_{1,2,3}$ the coupling strengths. Arrows depict the incoming and outgoing waves in the waveguide.

 r_L and r_R are the complex reflection coefficients for left and right incidence, and *t* is the complex transmission coefficient of the reciprocal system. For the point symmetric scatterers considered here, $r_L = r_R = r$ and $t = 1 + r$ [\[44\]](#page-8-0). Using these relations, one can show that the determinant of the scattering matrix is given by

$$
\det(\mathbf{S}) = t + r. \tag{2}
$$

Following a different approach which we find convenient, the scattering properties can also be obtained using the continuity of pressure and the conservation of acoustic flux in the waveguide, along with the evolution of the acoustic field *pci* in the *i*th HR. The corresponding CMT is derived in Appendix [A,](#page-5-0) and the resulting equations are

$$
p_1^+(t) + p_1^-(t) = p_2^+(t) + p_2^-(t),
$$
\n(3)

$$
p_1^+(t) - p_1^-(t) = p_2^+(t) - p_2^-(t) + \sum_i 2 \frac{\gamma_i}{\Omega_i^2} \dot{p}_{ci}, \qquad (4)
$$

$$
\ddot{\vec{P}} + \mathbf{R}\dot{\vec{P}} + \mathbf{K}\vec{P} = \vec{F},\tag{5}
$$

where () denotes differentiation with respect to the normalized time $t \to \omega_1 t$. In Eq. (5), $\vec{P} = [p_{c1}, \dots, p_{cN}]^T$ is the field amplitude in the *N* resonators, and $\vec{F} = [\Omega_1^2(p_1^+ +$ p_2^- , , Ω_N^2 (p_1^+ + p_2^-)] is the external driving force due to the incoming waves from the waveguide. The matrix **K** is diagonal and its elements are the normalized resonant frequencies Ω_i^2 . The matrix **R** includes the internal losses (r_i) and the leakage of the resonators to the waveguide (γ_i) . Below using Eqs. (3)–(5), we derive effective Hamiltonians to describe specific boundary conditions of the scattering problem.

1. Perfect absorption

This boundary condition of special interest is the one of *no outgoing waves* $p_1^- = p_2^+ = 0$, which when used in Eq. (3) leads to

$$
p_1^+ = p_2^-.
$$
 (6)

Equation (6) shows that, in a two port system with point scatterers side loaded at the same position, perfect absorption occurs only when the incoming waves have equal amplitudes *and* phase. Under these conditions, we may re-write Eq. (5) in the usual Hamiltonian matrix form

$$
i\ddot{\Psi} = \mathbf{L}\ddot{\Psi},\tag{7}
$$

where $\vec{\Psi} = [p_{c1}, \dots, p_{cN}, \dot{p}_{c1}, \dots, \dot{p}_{cN}]^T$. Assuming harmonic solutions of Eq. (7) in the form $\vec{\Psi}(t) = e^{-i\omega t} \vec{\Psi}_0$, we obtain the following eigenvalue problem

$$
(\mathbf{L} - \omega \mathbf{I}) \vec{\Psi}_0 = 0. \tag{8}
$$

In general the eigenvalues of the non-Hermitian matrix **L** are *complex*. When an eigenvalue becomes real, at that particular frequency the in-phase incoming acoustic waves will be completely absorbed and this corresponds to a CPA [\[24,35,38,39,41,44,48\]](#page-8-0).

2. Laser

Another boundary condition of interest is the one of *no incoming waves*, $p_1^+ = p_2^- = 0$ leading to $\vec{F} = 0$. For this boundary condition, we can also write the corresponding system of equations and the eigenvalue problem as

$$
i\overline{\Psi} = \mathbf{H}\overline{\Psi}, \quad (\mathbf{H} - \omega \mathbf{I})\overline{\Psi}_0 = 0. \tag{9}
$$

The non-Hermitian matrix **H** can be obtained from **L** using the relation

$$
\mathbf{H}(r_i, \gamma_i, \Omega_i) = \mathbf{L}(r_i, -\gamma_i, \Omega_i). \tag{10}
$$

The complex eigenvalues of matrix **H** correspond to the *quasibound* states of the system. Their real part corresponds to the resonance frequency and their imaginary part describes the width of the resonance. When an eigenvalue of **H** becomes real, the system appears to have a finite output without any input (since we have chosen the boundary $p_1^+ = p_2^- = 0$ for **H**), and this is a *lasing* frequency of the system. Equation (10) describes in a compact way the connection between the two sets of boundary conditions: Laser frequencies described by **H** have a CPA partner which corresponds to changing the boundary conditions and the sign of the leakage.

A direct connection between the scattering matrix and the effective Hamiltonians can be established [\[35\]](#page-8-0) by noting that the determinant of **S** can be written as:

$$
\det(\mathbf{S}) = -\frac{\det(\mathbf{L} - \omega \mathbf{I})}{\det(\mathbf{H} - \omega \mathbf{I})}.
$$
 (11)

Equation (11) shows that the eigenvalues of **L** are the *zeros* of the determinant of the scattering matrix, and the eigenvalues of **H** are its *poles*.

B. Exceptional points of the effective Hamiltonians

In this work, we focus on the scattering through an acoustic waveguide sideloaded with two (dimer) and three (trimer) HRs as shown in panels (a) and (b) of Fig. 1, respectively. The exact form of the effective Hamiltonians **L** for both the dimer and trimer are given by Eq. $(B1)$ and Eq. $(B2)$ in the appendix, respectively. The eigenvalues *ω* of the matrices **L** can be found from the corresponding secular equations

$$
f_{L2} = \omega^4 - i\alpha\omega^3 + \beta\omega^2 + i\mu\omega + \nu = 0, \qquad (12)
$$

$$
f_{L3} = \omega^6 - i\lambda' \omega^5 + y' \omega^4 + i\alpha' \omega^3 + \beta' \omega^2 + i\mu' \omega + \nu' = 0,
$$
\n(13)

for the dimer and trimer, respectively. The polynomials $f_{L2}(\omega, r_i, \gamma_i, \Omega_i)$ and $f_{L3}(\omega, r_i, \gamma_i, \Omega_i)$ are functions of ω and

FIG. 2. (a) A sketch of a realistic setup composed by an acoustical waveguide of cross-section area *S* side loaded with two HRs. (b) The geometrical characteristics of a single HR.

depend on the $3N - 1$ parameters r_i , γ_i , and Ω_i (since $\Omega_1 = 1$). The corresponding equations for the matrices **H** are given by

$$
f_{H2} = f_{L2}(\omega, r_i, -\gamma_i, \Omega_i), \qquad (14)
$$

$$
f_{H3} = f_{L3}(\omega, r_i, -\gamma_i, \Omega_i), \qquad (15)
$$

due to Eq. [\(10\)](#page-1-0). Note that the polynomials also satisfy the relation $f_H(\omega^*, -r_i, \gamma_i, \Omega) = f_L(\omega, r_i, \gamma_i, \Omega)$. For the lossless case $(r_i = 0)$ the latter relation recovers the well known fact that the zeros and poles of the scattering matrix are complex conjugates due to time reversal symmetry.

An appealing property of non-Hermitian matrices is the existence of EPs and the associated wave phenomena around them. Here, we investigate the wave scattering around the EPs of the non-Hermitian matrix **L** and their connection with the emergence of CPA. To start with, we consider the case of a dimer, as the one shown in Fig. $2(a)$. The parametric space of the relevant matrix **L** is five dimensional $(r_{1,2}, \gamma_{1,2}, \Omega_2)$, and we simplify the problem by reducing it to the two-dimensional space of Ω_2 and r_2 . The coupling coefficients $\gamma_{1,2}$ are fixed to the moderate values of $\gamma_1 = 0.15$ and $\gamma_2 = 0.1$, and the losses of one of the HRs $r_1 = 0.138$.

The aforementioned parameter values, as well as the ones use in the rest of this work, are relevant to the experiments of Refs. [\[44,48\]](#page-8-0). Namely, a waveguide of cross section $S = 20 \times$ 10^{-4} m² loaded by HRs of fixed neck surface $S_n = 10^{-4}$ m² and length $l_n = 0.04$ m (see Fig. 2). The section and length of the HR cavities are of the order of $S_c \sim 10^{-3}$ m² and *lc* ∼ 0*.*05 m, respectively but are considered tunable. For this setup the HRs have a resonance frequency around 700 Hz, the values of $\gamma_i \sim 0.1$ which can be modified by changing the geometry of the HR, and finally losses r_i are usually of the order of $\sim 10^{-2}$ but are easily tuned to higher values by adding absorbing materials in the cavity.

As is shown in Appendix C , we locate two EPs in the two-dimensional parameter space (Ω_2, r_2) . These are found at $\omega_{\text{EP1}} \approx 0.9367 + i0.005$ and $\omega_{\text{EP2}} \approx 1.0595 + i0.006$. For parameter values close to the EPs, the complex eigenvalues are enforced to repel each other through an avoided crossing. An example is shown in Fig. $3(a)$, where the trajectories of the two complex eigenvalues of **L** are plotted with the solid lines for $\Omega_2 \in [0.8, 1.2]$ and $r_2 = 0.086$. The two eigenvalues, initially located at points A and B for $\Omega = 0.8$, repel as they approach the leftmost EP [leftmost (red) circle in panel (a)], and one crosses the real axis. Exactly at the point where this eigenvalue becomes real a CPA emerges. By further increasing

FIG. 3. (a) Solid (dashed) lines show the eigenvalues of **L** (**H**) for the dimer at parameter values $\gamma_1 = 0.15$, $\gamma_2 = 0.1$, $r_1 = 0.1386$, and $r_2 = 0.085$ while the running parameter is $\Omega \in [0.8, 1.2]$. Triangles indicate the eigenvalues corresponding to CPA1. (b) Determinant of **S** in the complex frequency plane for parameters corresponding to the CPA1 of panel (a). The inset depicts the geometry of a HR.

 Ω_2 , the eigenvalue crosses the real axis around the rightmost EP, signaling a second CPA, and ends at point B' when $\Omega =$ 1.2. The dashed lines in Fig. $3(a)$, depict the corresponding complex eigenvalues of **H** (solutions of f_{H2}). Note that the eigenvalues do not coalesce rather than their trajectories meet at some point.

Figure $3(b)$ is presented to visualize the relation between the eigenvalues of **L** and **H** and the zeros and poles of det(**S**). In particular we show $det(S)$ in the complex frequency plane for the parameters corresponding to CPA1 of panel (a). The (green) triangles indicate the respective eigenvalues from panel (a).

III. *PT* **-SYMMETRIC EFFECTIVE HAMILTONIANS**

In the previous section it was shown that a CPA frequency appears when an eigenvalue of**L**, around an EP, is driven across the real axis and becomes real. It is known however, that when a non-Hermitian matrix is \mathcal{PT} symmetric, it is possible to obtain regions where *all* eigenvalues are real. It is very interesting then that PT symmetry provides a condition to obtain multiple CPA frequencies. Also, it ensures the emergence of EPs on the real axis, which as we will show below, leads to interesting results regarding broadened flat perfect absorption.

It appears that \mathcal{PT} symmetry is enforced quite easily: We simply require the corresponding secular equations of the non-Hermitian matrix **L** to be real [\[52\]](#page-8-0). Then, the eigenvalues are either real or complex conjugates.

A. Dimer

From Eq. [\(12\)](#page-1-0) we immediately obtain that \mathcal{PT} symmetry requires $\alpha = \mu = 0$ leading to the following equations

$$
r_1 - \gamma_1 + r_2 - \gamma_2 = 0,\t(16)
$$

$$
\Omega_2^2(r_1 - \gamma_1) + r_2 - \gamma_2 = 0. \tag{17}
$$

According to Eqs. [\(16\)](#page-2-0) and [\(17\)](#page-2-0), two different \mathcal{PT} configurations are possible: (i) $\Omega_2 = 1$ with the rest of the parameters satisfying Eq. [\(16\)](#page-2-0), and (ii) each of the resonators is critically coupled (i.e., $r_i = \gamma_i$) and the frequency Ω_2 is freely chosen. In the former case, the system is always found to be in the PT -broken phase and the eigenvalues of **L** are always complex conjugates exhibiting no CPA. We thus focus our study in case (ii) where each resonator is critically coupled. This is an intriguing generalization of the trivial case with one resonance. It is known that the CPA condition for a single resonator is satisfied for a critically coupled resonance with $r_1 = \gamma_1$ [\[38,41,44–46,48\]](#page-8-0). Here we have found that by adding another critically coupled resonator we can obtain two CPA frequencies. However as we will show below, this pattern is not valid for more resonators since the interactions between the eigenvalues become more complex.

Choosing $r_1 = \gamma_1$ and $r_2 = \gamma_2$, we can rewrite the secular equation (12) as

$$
f_L = (\omega - \tilde{\omega}_1)(\omega + \tilde{\omega}_1)(\omega - \tilde{\omega}_2)(\omega + \tilde{\omega}_2), \qquad (18)
$$

where, $\tilde{\omega}_{1,2}$ are the eigenvalues of **L** given by

$$
\tilde{\omega}_{1,2} = \frac{1}{\sqrt{2}} \sqrt{\delta \pm \sqrt{\delta^2 - 4\Omega_2^2}},\tag{19}
$$

with $\delta = 1 + \Omega_2^2 + \gamma_1 \gamma_2$. In Fig. 4(a) we show a phase diagram, indicating the broken and unbroken PT -symmetric phases. In the unbroken phase [outside the parabola (yellow)] where $\delta > 2\Omega_2$, the eigenvalues $\tilde{\omega}_{1,2}$ are real and correspond

FIG. 4. (a) The phase plane indicating the \mathcal{PT} -broken and unbroken phases when both resonators are critically coupled. The solid line parabola indicates the EPs separating the two phases. (b) A trajectory of the eigenvalues of matrix **L** corresponding to the dashed horizontal line of panel (a) with $\gamma_1 = r_1 = 0.15$, $\gamma_2 = r_2 = 0.1$, and $\Omega_2 \in [0.8, 1.2]$. Arrows indicate the direction of the eigenvalues as Ω_2 increases. EPs points are at $\Omega_2 = 1 \pm \sqrt{\gamma_1 \gamma_2}$.

to two different simple CPA frequencies of a particular configuration. On the contrary, in the broken phase [inside the parabola (blue)], when δ < 2 Ω ₂, the eigenvalues $\tilde{\omega}_{1,2}$ are complex conjugates and the system features no CPA. The solid black line of Fig. 4 corresponds to $\delta = 2\Omega_2$ and indicates the family of EPs separating the two phases, with real eigenvalues $\tilde{\omega}_1 = \tilde{\omega}_2 \equiv \omega_{EP}$. The EPs correspond to the coalescence of two CPA frequencies which we, further on, call *double* CPA.

In Fig. 4(b), we plot the eigenvalues of **L** for the trajectory indicated by the horizontal dashed line of panel (a). Initially the system is in the unbroken phase with two different real eigenvalues corresponding to two CPA frequencies (points A and B). As Ω_2 is increased, they approach each other along the real axis and collide at an EP. Note that in contrast with the non PT -symmetric case shown in Fig. [3\(a\),](#page-2-0) the EP is now on the real axis. Beyond this EP the \mathcal{PT} symmetry is broken and the system does not have a CPA. As Ω_2 increases, a second EP appears where the two eigenvalues coalesce and become real again re-entering the unbroken phase. Note the differences of Fig. $4(b)$ with the solid lines in Fig. $3(a)$ and especially the fact that the two EPs have been shifted onto the real axis.

The next step is to illustrate what is the influence of the proposed *PT* -symmetric configurations in the scattering properties of the acoustic system. We first note that the occurrence of CPA and laser frequencies can both be captured using the ratio between outgoing and incoming field intensity Θ defined as

$$
\Theta = \frac{|p_1^-|^2 + |p_2^+|^2}{|p_1^+|^2 + |p_2^-|^2},\tag{20}
$$

where $\Theta \rightarrow 0$ at a CPA frequency while $\Theta > 1$ signals the amplification of incoming waves. Note that in a conservative system $\Theta = 1$. To achieve CPA we are obliged to satisfy Eq. [\(6\)](#page-1-0) by considering scattering with incoming waves of equal amplitude and phase. In that case Eq. (20) can be written as

$$
\Theta = \frac{|p_1^-|^2 + |p_2^+|^2}{2|p_1^+|^2} = |t + r|^2,\tag{21}
$$

which using Eqs. (2) and (11) is explicitly written as

$$
\Theta = \frac{|f_L(\omega, r_i, \gamma_i, \Omega_i)|^2}{|f_H(\omega, r_i, \gamma_i, \Omega_i)|^2}.
$$
\n(22)

In Fig. [5,](#page-4-0) we plot Θ as a function of frequency when matrix **L** is $\mathcal{P}\mathcal{T}$ symmetric. We show three different cases when **L** is in the PT-broken phase [dashed-dotted (black) line], in the PT-unbroken phase [dashed (black) line], and at an EP [solid (red) line]. In the broken phase the parameter Θ is nonzero for all frequencies (no CPA). In the unbroken phase, $\Theta = 0$ at the two real eigenvalues of **L** showing two simple CPA. According to Eq. (18) and Eq. (22), around each CPA frequency the parameter Θ is analogous to $\Theta \sim |(\omega - \tilde{\omega}_{1,2})^2|$ which is quadratic in frequency. For the case of an EP, the coalescence of the two eigenvalues of **L** gives rise to a double CPA point around $\omega = \omega_{EP}$ (solid red line of Fig. [5\)](#page-4-0).

Around the EP, Eq. (22) can be approximated by

$$
\Theta \approx \frac{|(\omega - \omega_{\rm EP})^4 (\omega + \omega_{\rm EP})^4|}{|f_H(\omega_{\rm EP})|^2},\tag{23}
$$

FIG. 5. The parameter Θ as a function of frequency for the same parameters as in Fig. $4(b)$. The solid (red) line corresponds to the leftmost EP, the dashed (black) in the \mathcal{PT} -unbroken (Ω ₂ = 1.2), and the dashed-dotted (black) line in \mathcal{PT} -broken ($\Omega_2 = 1$) regions. The inset shows a close up of Θ to illustrate the difference between a standard CPA and the CPA at the exceptional point. The blue dotted line indicates the analytical approximation of Eq. [\(23\)](#page-3-0).

which is plotted in the inset of Fig. 5 by the dotted (blue) line. The consequence of Eq. [\(23\)](#page-3-0), which exhibits a *quartic* dependence of Θ with frequency, is that perfect absorption is flattened, in comparison with the simple CPA [\[35,38,44\]](#page-8-0). On the other hand the denominator which depends on the polynomial f_H controls how broadband is the perfect absorption.

B. Trimer

We now proceed with the case of the trimer which can display not only three CPAs but also higher order EPs. First we identify the parameter space where the relevant matrix **L** is PT symmetric. The corresponding secular equation for the trimer is given by Eq. [\(13\)](#page-1-0) and \mathcal{PT} symmetry is enforced when $\lambda' = \alpha' = \mu' = 0$, leading to the following conditions

$$
r_1 - \gamma_1 + r_2 - \gamma_2 + r_3 - \gamma_3 = 0, \tag{24}
$$

$$
\Omega_2^2(r_3 - \gamma_3) + \Omega_3^2(r_2 - \gamma_2) + \Omega_2^2 \Omega_3^2(r_1 - \gamma_1) = 0, \quad (25)
$$

$$
r_2 - \gamma_2 + r_3 - \gamma_3 + \Omega_2^2 (r_1 - \gamma_1 + r_3 - \gamma_3)
$$

+
$$
\Omega_3^2 (r_1 - \gamma_1 + r_2 - \gamma_1) + r_2 r_3 (r_1 - \gamma_1)
$$

-
$$
r_1 (r_2 \gamma_3 + r_3 \gamma_2) = 0.
$$
 (26)

A surprising result of Eqs. (24) – (26) is the following: By critically coupling each of the three HRs (i.e., $r_i =$ *γi*) we *do not* obtain a PT -symmetric configuration and cannot have three CPA frequencies. Indeed, choosing $r_i = \gamma_i$, Eqs. (24) and (25) are satisfied while Eq. (26) is not, due to a nonvanishing term $\sim r_1(r_2\gamma_3 + r_3\gamma_2)$. This is a rather counterintuitive result, since this term does not vanish even when the resonant frequencies are far away from each other.

Configurations which support three CPAs and also feature higher order EPs, can be obtained when Eqs. (24) – (26) are satisfied, and **L** is \mathcal{PT} symmetric. In this case, the eightdimensional parameter space of the trimer is reduced to a fivedimensional one, which exhibits a plethora of regions either in the broken or unbroken phase. We choose to study a particular parametric region in order to illustrate both the transition from the broken to the unbroken phase and also show the existence of

FIG. 6. Trajectories of the eigenvalues of **L** given by Eq. [\(13\)](#page-1-0) with varying parameter $\Omega \in [0.7, 0.9]$. The rest parameters chosen are $\gamma_1 = r_1 = 0.2$, $\gamma_2 = 0.2$, and $\gamma_3 = 0.01$. The losses r_2 and r_3 are then given by Eqs. (24)–(26) as a function of Ω . Shaded region depicts the PT -unbroken regime. The dashed line shows the eigenvalues for the same parameters but with $\gamma_3 = 0.0157$, when the system exhibits a triple EP.

a triple EP. In particular, we chose $\Omega_2 = \Omega_3 \equiv \Omega$ as a varying parameter and fix $\gamma_{1,2,3}$ and r_1 . The rest of the parameters (r_2) and r_3) are given by Eqs. (24) – (26) . Note that this choice of parameters leads to negative values for r_3 namely the inclusion of acoustic gain. Mechanisms for gain in acoustics have been realized experimentally for example in Ref. [\[9\]](#page-7-0) by the use of loudspeakers with tailored electrical circuits.

A PT -symmetric trajectory of the eigenvalues of **L** is shown in Fig. 6. At the beginning of the trajectory at $\Omega = 0.7$, **L** is in the \mathcal{PT} -broken phase where there is one real eigenvalue (denoted by triangles) and a complex conjugate pair (denoted by stars). Thus the corresponding curve of Θ as a function of frequency, shown with the solid line in Fig. $7(a)$, exhibits one single CPA frequency at $\omega \approx 0.95$. The additional dip around $\omega \approx 0.72$ corresponds to the complex conjugate pair indicated by the stars in Fig. 6 and the inset of Fig. $7(a)$. The peak appearing in Fig. $7(a)$ emerges due to one of the solutions of *fH*³ (i.e., a pole) which is very close to the real axis. At $\Omega = 0.781$, two complex conjugate eigenvalues coalesce and become real. Beyond this EP, **L** is in the \mathcal{PT} -unbroken phase indicated by the shaded area in Fig. 6. In the unbroken region there are three real eigenvalues and the system exhibits three single CPA. An example of Θ in the unbroken region is shown in Figs. [7\(a\)](#page-5-0) and [7\(b\)](#page-5-0) with the dashed line for $\Omega = 0.79$. By further increase of Ω , two eigenvalues coalesce at another EP and the system returns to the PT -broken phase. At the two transition points separating the broken and unbroken phases, shown by the vertical lines in Fig. 6, the system acquires one EPs and one real eigenvalue. This corresponds to a double CPA and one single CPA, which are shown in Fig. [7\(b\)](#page-5-0) with the blue dotted curve. Furthermore, an example featuring a higher order EP is shown in Fig. 6 by the dashed lines, and it is found for the same parameters as for the solid lines, but with $\gamma_3 = 0.0157$. The parameter Θ at the triple EP is plotted

FIG. 7. Panel (a): same as in Fig. [5](#page-4-0) for the trimer. Solid line depicts the PT -broken phase for $\Omega = 0.7$. The dashed line corresponds to a $\mathcal{P}\mathcal{T}$ -unbroken case for $\Omega = 0.78$. The inset depicts the eigenvalues of **L** (triangle and stars) and of **H** (squares). Panel (b): Dashed line is the same as in panel (a). A zoom at the frequencies between $\omega = 0.8$ and $\omega = 1$. The dotted (blue) line depicts the case of $\Omega = 0.803$ corresponding to a simple EP (rightmost vertical line of Fig. [\(6\)](#page-4-0)]. Solid (red) line corresponds to the triple EP with $\Omega = 0.803$ and $\gamma_3 = 0.0157$.

with the solid (red) line in Fig. $7(b)$. Around the triple EP the parameter Θ can be approximated as

$$
\Theta \approx \frac{|(\omega - \omega_{EP})^6 (\omega + \omega_{EP})^6|}{|f_H(\omega_{EP})|^2},\tag{27}
$$

revealing the fact that the higher order EP displays flattened absorption with respect to the simple EP.

The significance of Eqs. (23) and (27) and the quintessence of this section is that broadband flat perfect absorption can be achieved, by the fine tuning of the system parameters such as to obtain an EP and a large value of $|f_H|$ at the EP.

IV. CONCLUSIONS

Our results display how harnessing the non-Hermiticity of acoustic metamaterials provides a promising pathway towards improved acoustic absorbers. Operating around the EPs of non-Hermitian matrices, associated with the scattering process, can lead to CPA through the avoided crossing of the corresponding eigenvalues. Enforcing $\mathcal{P}\mathcal{T}$ symmetry on the non-Hermitian matrices leads to multiple CPAs, the number of which depends on the number of subwavelength resonators. At the EP separating the PT -unbroken and broken phases, we find a flattened perfect absorption, which is even enhanced when the EP is of higher order.

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APPENDIX A: COUPLED MODE EQUATIONS

Here we derive the coupled mode equations describing the scattering of acoustic waves, in a cylindrical waveguide side loaded by subwavelength Helmholtz resonators. For frequencies below the first cutoff frequency of the waveguide, the propagation is considered one dimensional (namely *x* direction). The linearized mass and momentum conservation laws can be written as:

$$
\frac{\partial p}{\partial t} + c^2 \rho_0 \frac{\partial u}{\partial x} = 0,
$$
 (A1)

$$
\rho_0 \frac{\partial u}{\partial t} + \frac{\partial p'}{\partial x} = 0, \tag{A2}
$$

where *p* and *u* are the pressure and velocity fluctuations in the waveguide. Above, we have used the constitutive equation $p =$ $c^2 \rho$ with ρ being the density of air and *c* the speed of sound. In the low frequency regime the resonators can be considered as point scatterers located at $x = 0$, and we decompose the pressure field in the waveguide as follows

$$
p(x,t) = \begin{cases} p_1^+(\xi_+) + p_1^-(\xi_-) & x \le 0, \\ p_2^+(\xi_+) + p_2^-(\xi_-) & x \ge 0, \end{cases}
$$
 (A3)

where $\xi_{\pm} = t \mp x/c_0$, while ⁺ and ⁻ denote right- and leftgoing waves, respectively.

The continuity of pressure at $x = 0$ for both configurations is the following

$$
p_1^+(t) + p_1^-(t) = p_2^+(t) + p_2^-(t) \equiv p_0.
$$
 (A4)

FIG. 8. Panels (a) and (b) depict a sketch of the configurations considered in this work consisting of a cylindrical waveguide side loaded with two (a) or three (b) Helmholtz resonators. Panels (c) and (d): schematic of the continuity of acoustic flux as the waves pass through the point scatterers.

The conservation of flux at $x = 0$ [illustrated in panels (c) and (d) of Fig. [8\]](#page-5-0) can be written as

$$
S\rho_0 u\Big|_{x=0^-} = S\rho_0 u\Big|_{x=0^+} + \sum_i S_{ni}\rho_0 u_{ni}, \qquad (A5)
$$

where *i* takes values from 1*,...,*N for a total number of N resonators. *S* and S_{ni} are the cross sections of the tube and the neck of the *i*th resonator, respectively, while u_{ni} is the particle velocity in the neck of each Helmholtz resonator. The velocities at the resonators neck are given by

$$
u_{ni} = -\frac{V_i}{c^2 \rho_0 S_{ni}} \frac{\partial p_{ci}}{\partial t}.
$$
 (A6)

where V_i is the volume of the cavity of the *i*th resonator. Finally it can be shown that the conservation of mass can be written as

$$
p_1^+(t) - p_1^-(t) = p_2^+(t) - p_2^-(t) + \sum_i \frac{V_i}{Sc_0} \frac{\partial \dot{p}_{ci}}{\partial t}.
$$
 (A7)

For sufficiently low frequencies, the dynamics of the pressure in each cavity of the resonators $p_{ci}(t)$, can be described by the following approximate equations (see for example Refs. [\[53–55\]](#page-8-0)):

$$
\frac{\partial^2 p_{ci}}{\partial t^2} + \omega_i^2 p_{ci} + R_i \frac{\partial p_{ci}}{\partial t} = \omega_i^2 p_0,
$$
 (A8)

where p_0 is the pressure at the entrance of the resonator, and $\omega_i^2 = c_0^2 S_n / l_{n_i} V_i$ is the resonance frequency of each HR. The resistance factor R_i is a parameter which quantifies the linear viscothermal losses in the resonator [\[54\]](#page-8-0). Furthermore, using both Eqs. $(A4)$ – $(A7)$ we replace the pressure at the neck of the resonator connected with the waveguide with the following:

$$
p_0 = p_1^+ + p_2^- - \sum_i \frac{\Gamma_i}{\omega_i^2} \dot{p}_i,
$$
 (A9)

where $\Gamma_i = c S_{ni} / 2 l_{ni} S$ quantifies the coupling with the waveguide. We use a normalized time coordinate $t \to \omega_1 t$, and the normalized parameters become $r_i = R_i/\omega_i$, $\gamma_i = \Gamma_i/\omega_i$ and $\Omega_i = \omega_i/\omega_1$.

The coupled mode theory is then described by the following normalized set of equations used in the main text

$$
p_1^+(t) + p_1^-(t) = p_2^+(t) + p_2^-(t), \tag{A10}
$$

$$
p_1^+(t) - p_1^-(t) = p_2^+(t) - p_2^-(t) + \sum_i 2 \frac{\gamma_i}{\Omega_i^2} \dot{p}_{ci}, \quad \text{(A11)}
$$

$$
\ddot{\vec{P}} + \mathbf{R}\dot{\vec{P}} + \mathbf{K}\vec{P} = \vec{F},
$$
 (A12)

where () denotes differentiation with respect to the normalized time, $\vec{P} = [p_{c1}, ..., p_{cN}]^T$ and $\vec{F} = [\Omega_1^2(p_1^+ +$ p_2^-), ..., $\Omega_N^2(p_1^+ + p_2^-)$]. The matrix *R* has elements

$$
R_{ii} = r_i + \gamma_i, \quad R_{ij} = \gamma_j \frac{\Omega_i^2}{\Omega_j^2}
$$
 (A13)

while **K** is diagonal with elements $K_{ii} = \Omega_i^2$. Note that the above derived CMT is valid for any number of *N* resonators, as long as the evanescent coupling between the resonators is negligible.

APPENDIX B: EFFECTIVE MATRICES END SECULAR EQUATIONS FOR THE DIMER AND TRIMER

The non-Hermitian matrix **L** for the dimer has the following form

$$
\mathbf{L} = \begin{pmatrix} 0 & 0 & i & 0 \\ 0 & 0 & 0 & i \\ -i & 0 & -i(r_1 - \gamma_1) & -i\gamma_2/\Omega_2^2 \\ 0 & -i\Omega_2^2 & -i\gamma_1\Omega_2^2 & -i(r_2 - \gamma_2) \end{pmatrix}.
$$
 (B1)

On the other hand, for the trimer it takes the form

$$
\mathbf{L} = \begin{pmatrix} 0 & i\mathbf{I}_3 \\ L_{31} & L_{32} \end{pmatrix},\tag{B2}
$$

where I_3 is the 3 \times 3 identity matrix, while L_{31} and L_{32} are given by the following expressions

$$
\mathbf{L}_{31} = \begin{pmatrix} -i & 0 & 0 \\ 0 & -i\Omega_2^2 & 0 \\ 0 & 0 & -i\Omega_3^2 \end{pmatrix}, \n\mathbf{L}_{32} = \begin{pmatrix} -i(r_1 - \gamma_1) & -i\gamma_2/\Omega_2^2 & -i\gamma_3/\Omega_3^2 \\ -i\gamma_1\Omega_2^2 & -i(r_2 - \gamma_2) & -i\gamma_3\Omega_2^2/\Omega_3^2 \\ -i\gamma_1\Omega_3^2 & -i\gamma_2\Omega_3^2/\Omega_2^2 & -i(r_3 - \gamma_3) \end{pmatrix}.
$$
\n(B3)

The corresponding characteristic polynomials are

$$
f_{L2} = \omega^4 - i\alpha\omega^3 + \beta\omega^2 + i\mu\omega + \nu = 0, \qquad (B4)
$$

$$
f_{L3} = \omega^6 - i\lambda'\omega^5 + y'\omega^4 - i\alpha'\omega^3 + \beta'\omega^2 + i\mu'\omega + \nu' = 0.
$$
\n(B5)

The coefficients for the dimer are the following

$$
\alpha = r_1 - \gamma 1 + r_2 - \gamma 2, \tag{B6}
$$

$$
\beta = \gamma_1 \gamma_2 \Omega_2^2 - \Omega_2^2 - 1 + (r_1 - \gamma_1)(r_2 - \gamma_2), \tag{B7}
$$

$$
\mu = \Omega_2^2 (r_2 - \gamma_2) + r_1 - \gamma_1, \tag{B8}
$$

$$
\nu = \Omega_2^2,\tag{B9}
$$

and for the trimer

$$
\lambda' = r_1 - \gamma 1 + r_2 - \gamma_2 r_3 - \gamma_3, \qquad \text{(B10)}
$$

\n
$$
y' = -\left(1 + \Omega_2^2 + \Omega_3^2 + r_1(r_2 + r_3 - \gamma_2 \gamma_3)\right) + r_2(r_3 - \gamma_1 - \gamma_3) - r_3(\gamma_1 + \gamma_2),
$$

\n
$$
\alpha' = r_2 - \gamma_2 + r_3 - \gamma_3 + \Omega_2^2(r_1 - \gamma_1 + r_3 - \gamma_3) + \Omega_3^2(r_1 - \gamma_1 + r_2 - \gamma_1) + r_2r_3(r_1 - \gamma_1) - r_1(r_2\gamma_3 + r_3\gamma_2), \qquad \text{(B11)}
$$

$$
\mu' = \Omega_2^2(r_2 - \gamma_2) + r_1 - \gamma 1, \tag{B12}
$$

$$
\nu' = \Omega_2^2. \tag{B13}
$$

APPENDIX C: EXCEPTIONAL POINTS FOR THE DIMER

To locate the exceptional points of matrix **L** given by Eq. $(B3)$ we solve the corresponding eigenvalue problem numerically. Since the matrix is non-Hermitian, the left and right eigenvectors $|\phi^r\rangle$ and $|\phi^l\rangle$ are generally different and satisfy the following equations

$$
\mathbf{L}|\phi^r\rangle = \omega|\phi^r\rangle, \quad \langle \phi^l|\mathbf{L} = \langle \phi^l|\omega. \tag{C1}
$$

These two vectors are biorthogonal satisfying the relation

$$
\langle \phi_i^l | \phi_j^r \rangle = \delta_{ij},\tag{C2}
$$

and the phase rigidity σ_i for the *i*th eigenvector is defined as

$$
\sigma = \frac{1}{\langle \phi^r | \phi^r \rangle}.
$$
 (C3)

When the matrix is away from an exceptional point, the eigenvectors are almost orthonormal with $\sigma_i \rightarrow 1$. On the other hand, approaching the exceptional point the eigenvectors coalesce and $\sigma \to 0$. The quantity $|\sigma - 1|$ is then an appropriate indicator to identify EPs when it becomes unity. In our case, we fix the parameters to $\gamma_1 = 0.15$, $\gamma_2 = 0.1$, and $r_1 = 0.138$ and scan the two parameter space of Ω_2 and r_2 to find the EPs. For each point in this surface we calculate the quantity $|\sigma - 1|$ and we plot the results in Fig. 9. As is shown, two EPs are found, EP1 = {0*.*8775*,*0*.*09} and EP2 = {1*.*123*,*0*.*0872}. Furthermore in Figs. 9(b) and 9(c) we plot the eigenvalues of**L**(solid lines) and **H** which pass through the two EPs.

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FIG. 9. Panel (a): A contour plot showing the parameter $|\sigma - 1|$ in the Ω , r_2 plane. The arrows indicate the position of the two EPs. Panels (b) and (c): The eigenvalues of the matrices **L** (solid lines) and **H** (dashed lines) for a trajectory with $\Omega_2 \in [0.8, 1.2]$ and $r_2 = 0.0872$ for panel (b) and $r_2 = 0.09$ for panel (c). The rest of the parameters are $\gamma_1 = 0.15$, $\gamma_2 = 0.1$, and $r_1 = 0.138$.

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