

Quasiperfect absorption by subwavelength acoustic panels in transmission using accumulation of resonances due to slow sound

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We theoretically and experimentally report subwavelength resonant panels for low-frequency quasiperfect sound absorption including transmission by using the accumulation of cavity resonances due to the slow sound phenomenon. The subwavelength panel is composed of periodic horizontal slits loaded by identical Helmholtz resonators (HRs). Due to the presence of the HRs, the propagation inside each slit is strongly dispersive, with near-zero phase velocity close to the resonance of the HRs. In this slow sound regime, the frequencies of the cavity modes inside the slit are down-shifted and the slit behaves as a subwavelength resonator. Moreover, due to strong dispersion, the cavity resonances accumulate at the limit of the band gap below the resonance frequency of the HRs. Near this accumulation frequency, simultaneously symmetric and antisymmetric quasicritical coupling can be achieved. In this way, using only monopolar resonators quasiperfect absorption can be obtained in a material including transmission.

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I. INTRODUCTION

Two main types of audible acoustic panels are desired in practical engineering applications: first, nonreflecting treatments and, second, zero-transmission materials. The first group requires that the reflection coefficient of a rigidly backed material vanishes. This is typically achieved by using porous or fibrous materials, that are mainly efficient in the inertial regime and for frequencies higher than the so-called quarter wavelength resonance of the backed layer, i.e., $f = c_0/4L$, the sound speed in current porous materials being nearly similar to that in the air, c_0 . On the other hand, zero transmission is commonly obtained by using highly reflecting materials together with an interior frame made of a porous absorber. These structures are efficient for frequencies higher than the first Fabry-Pérot resonance of the slab of equivalent material, i.e., $f = c/2L$. Concerning low frequency sound, both groups of structures result in practical limitations due to the excessive thickness, L , and weight of the treatments.

Designing materials with both zero reflection and zero transmission simultaneously, i.e., perfect absorbers including transmission, is of special interest. Perfect absorption is of particular interest for many applications such as energy conversion [1], time reversal technology [2], coherent perfect absorbers [3], or soundproofing [4] among others. In the case of rigidly backed materials, acoustic metamaterials are efficient solutions to design sound absorbing materials which can present simultaneously subwavelength dimensions and strong or perfect acoustic absorption. These include double porosity materials [5], metaporous materials [6–9], dead-end porosity materials [10,11], metamaterials composed by membrane-type resonators [4,12–14], Helmholtz resonators (HRs) [14–16], and quarter-wavelength resonators (QWRs) [11,17–19]. These last types of metamaterials [11,16–18] make use of strong dispersion giving rise to slow-sound propagation inside the material. Using slow sound results in a decrease of the cavity resonance frequency and, hence, the structure thickness can be drastically reduced to the deep-subwavelength regime [18].

In transmission problems, where both reflection and transmission are possible, acoustic metamaterials for perfect absorption have also been presented recently using decorated membrane resonators based on degenerate resonances [20]. In this case, monopolar and dipolar resonators are used to critically couple the symmetric and antisymmetric problem respectively and, therefore, to get perfect absorption of the full problem with transmission [21]. Perfect absorption has also been observed in metamaterials composed only by monopolar resonators, e.g., by using two unsymmetrical HRs [22]. In these structures, the transmission vanishes at the resonance of one HR, behaving effectively as a hard wall. By tuning a second HR the reflection problem can be critically coupled and, therefore, perfect absorption is obtained. The propagation of acoustic waves in waveguides loaded by arrays of monopolar resonators have been also considered previously, e.g., as in arrays of QWRs [23], arrays of HRs [24] producing Bragg interference and local resonances, and arrays of two concentrically placed QWRs producing Fano resonance [25]. In this work, we present quasiperfect absorption in a subwavelength metamaterial panel for transmission problems using identical monopolar resonators. The current design is based on the accumulation of resonances due to slow sound. The system works as follows: first, strong dispersion inside the slits is generated below the resonance frequency of the HR, while around the resonance frequency a band gap is generated and transmission vanishes. Second, in the propagation band the cavity resonances of each slit are stretched in frequency and accumulate below the resonance frequency of the HR. Due to this accumulation of resonances, the absorption using only monopolar resonators can exceed 50%. Then, by tuning the geometry of the system it can be almost critically coupled with the exterior medium, therefore achieving quasiperfect absorption.

II. DESCRIPTION OF THE SYSTEM AND THEORETICAL MODELS

The system consists in a panel perforated with a periodic arrangement of open slits, of thickness h and length L , with periodicity d in the x_1 direction, as shown in Fig. 1. The

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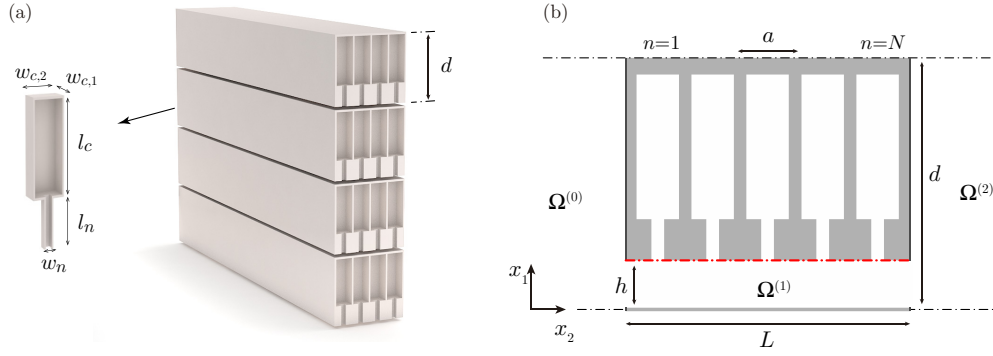


FIG. 1. (a) Conceptual view of the thin panel placed on a rigid wall with $N = 4$ layers of square cross-section Helmholtz resonators. (b) Scheme of the unit cell of the panel composed of a set of N Helmholtz resonators. Symmetry boundary conditions are applied at boundaries $\Gamma_{x_1=d}$ and $\Gamma_{x_1=0}$.

upper wall of the slit is loaded by N identical HRs in a square array of side a , in such a way that the length of the system is $L = Na$. To maximize the volume of the cavity of the resonators and hence to minimize the resonance frequency, HRs with rectangular cross section are used, characterized by a square neck with side w_n , a rectangular cavity with sides $w_{c,1}$ and $w_{c,2}$, and length l_n and l_c respectively. The viscothermal losses in the system are considered in both the resonators and in the slit by using effective complex and frequency dependent physical parameters [26]. Therefore, by changing the geometry, the intrinsic losses of the system can be tuned.

In order to have a deeper understanding of the physics involved in the system described above, several theoretical models with different hypotheses have been applied to analyze the scattering of the system. In this section, we briefly present each one, more details being given in the Appendixes.

A. Modal expansion method (MEM)

The first model is a modal expansion method (MEM) [18]. The acoustic field is expanded in the modal basis for each domain, and then each domain is assembled by applying the boundary conditions (continuity of pressure and velocity are considered at the entrance and exit of the slit). The effect of the resonators is included by an impedance condition at $x_1 = h$ in the slit, by considering $Z = Z_{HR}/\phi$, with Z_{HR} the impedance of the HRs and $\phi = w_n^2/a^2$ the slit surface porosity. The impedance of the HR including the radiation correction of the neck is presented in the Appendixes. Eventually, a mode-matching linear system is obtained, allowing us to calculate the reflection and transmission coefficients [18].

One of the interesting points of this method is that, considering the first order terms in the expansion, the low frequency approximation of the mode-matching system gives the effective parameters, i.e., the complex and frequency dependent effective bulk modulus, κ_e , and effective density, ρ_e , as

$$\kappa_e = \frac{\kappa_s}{\phi_t} \left[1 + \frac{\kappa_s \phi (V_c \kappa_n + V_n \kappa_c)}{\kappa_n h (S_n \kappa_c - V_c \rho_n l_n \omega^2)} \right]^{-1}, \quad (1)$$

$$\rho_e = \frac{\rho_s}{\phi_t}, \quad (2)$$

where $\phi_t = h/d$ is the total porosity of the metamaterial, ρ_s and ρ_n are the effective densities of the slit and neck, κ_s, κ_n , and κ_c are the effective bulk modulus of the slit, neck, and cavity, respectively, V_n and V_c are the volumes of the neck and cavity of the HRs, respectively, and ω is the angular frequency. From Eqs. (1) and (2) it is clear that this metamaterial allows only for negative compressibility for frequencies around the resonance frequency of the HRs. The reflection and transmission coefficients are linked to the effective parameters by

$$R_t = \frac{i(\bar{Z}_e^2 - 1) \sin(k_e L)}{2\bar{Z}_e \cos(k_e L) - i(\bar{Z}_e^2 + 1) \sin(k_e L)}, \quad (3)$$

$$T_t = \frac{2\bar{Z}_e}{2\bar{Z}_e \cos(k_e L) - i(\bar{Z}_e^2 + 1) \sin(k_e L)}, \quad (4)$$

with normalized effective impedance $\bar{Z}_e = \rho_e \kappa_e / \rho_0 \kappa_0$ and effective wave number $k_e = \omega \sqrt{\rho_e / \kappa_e}$. Finally, the absorption of the system is defined as $\alpha = 1 - |T_t|^2 - |R_t|^2$. Another interesting point of the MEM is that if high order terms are included in the expansion, no end corrections are required both at the entrance and exit of the slit.

B. Transfer matrix method (TMM)

The second model is based on the transfer matrix method (TMM), in which the N resonators are included as 1D point scatterers. N matrices are assembled for a system made of N unit cells, giving the transfer matrix, from which the reflection, transmission, and absorption coefficients can be obtained. Using the transfer matrix of a single unit cell with the Floquet-Bloch periodic boundary conditions, the dispersion relations in the periodic system can be obtained. This model accounts for the finite and discrete arrangement of HR while the MEM model, being based on an average impedance at the wall, does not consider the effect of discreteness, i.e., the finite number of HR. Moreover, contrary to the MEM, in which we can obtain the effect of the higher order modes in the system, the TMM directly considers the plane wave approximation, which is valid for the low frequency regime. The radiation corrections are included in the impedances of the resonators and in the slits in order to mimic the effect of the higher order modes. Importantly, the TMM gives a direct information of the effect of the finite number of resonators.

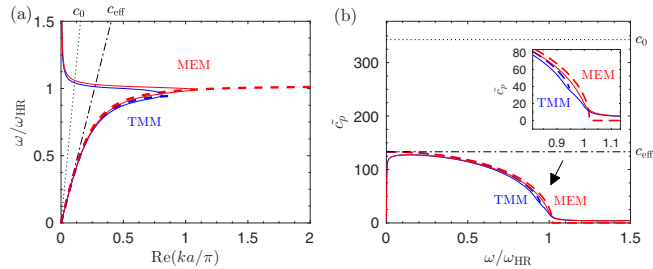


FIG. 2. (a) Dispersion relation in the slit calculated using (red) modal expansion method (MEM), (blue) transfer matrix method (TMM) in the lossless (dashed line), and lossy case (continuous line). Wave number in the air $k_0 = \omega/c_0$ (dotted line) and the low frequency asymptotic limit ω/c_{eff} (dashed-dotted line). (b) Representation of $\tilde{c}_p = \text{Re}(\omega/k)$, which is closely related to the phase speed. The inset shows the slow sound regime.

C. Finite element method (FEM)

In order to validate the previous analytical models and to show the limits of validity of each of them, we have used a finite element method (FEM) algorithm (COMSOL Multiphysics) to solve the scattering problem, where the effects of the finite number of resonators, the higher order modes, and the losses are taken into account numerically. The viscothermal losses are introduced as effective parameters in the slit and the resonator elements [26]. A plane wave impinges the system and the complete geometry is considered using the radiation conditions that simulate the Sommerfeld conditions in the limits of the numerical domains.

III. DISPERSION RELATION AND SLOW SOUND CONDITIONS IN THE SLIT

Figure 2(a) shows the real part of the complex wave number in the slit using MEM and TMM for a metamaterial with parameters $h = 1.2$ mm, $a = 4.95$ cm, $w_n = 7.1$ mm, $w_c = 4.9$, $d = 5$ cm, $l_n = 7.3$ mm, and $l_c = d - h - l_n$. A band gap is observed above the resonance frequency of the HRs, ω_{HR} . Inside the slit a dispersive propagation band is generated below the band-gap frequency, where the wave number in the slit is remarkably increased and, therefore, as Fig. 2(b) shows, slow sound conditions are achieved in this range of frequencies. It can be observed that the effective low-frequency sound speed in the lossless case, calculated from Eqs. (1) and (2), $c_{\text{eff}} = c_0/\sqrt{1 + V_{\text{tot}}\phi_n/hS_n}$, is accurately described by both models, with V_{tot} the total volume of the resonator.

In the lossless case, zero phase velocity can be observed for frequencies just below ω_{HR} . It is worth noting here that the maximum wave number using TMM is limited to $k_{\text{max}} = \pi/a$ due to the fact that this model accounts for the periodicity of the system, while using MEM the wave number can be infinite in the lossless case, due to the fact that the MEM does not account for the periodicity of the system. This limitation of the MEM will be discussed in more detail later in Sec. IV B.

Once thermoviscous losses are introduced, the dispersion relation inside the slit is modified. As Theocharis *et al.* showed [27], the minimum value of speed of sound is limited by the thermoviscous losses. Figure 2(b) shows the slow sound

region below ω_{HR} . We can clearly see that, although the quantity $\tilde{c}_p = \text{Re}(\omega/k)$, closely related to the phase velocity, is anymore zero in the lossy case, slow sound conditions are still observed in this range of frequencies: the mean phase speed in the low frequency range is much lower than the speed of sound in air, c_0 , and the phase speed near the resonance frequency of the HR is extremely low. This makes possible the shortening of the ratio λ/L and, therefore, the slit behaves as a subwavelength resonator. The dispersion relation in the slit and the sound speed predicted by the different theoretical models agree in the low frequency regime, while only small differences can be observed near the band gap between the TMM and MEM calculations due to the different hypothesis used in each model.

IV. REFLECTION AND TRANSMISSION PROBLEMS

In this work we deal with a symmetric and reciprocal system. In the low frequency regime the problem can be considered as 1D because only plane waves propagate. In this situation, the two eigenvalues of the scattering matrix (with T_t on the diagonal), which relates the amplitudes of the input with the output waves, are given by $T_t - R_t$ and $T_t + R_t$. Therefore, the absorption of the system can be described by decomposing the full problem in its symmetric and antisymmetric equivalent problems in reflection [22], as shown schematically in Fig. 3(a). In fact, the two eigenvalues of the scattering matrix give the reflection coefficients for the symmetric and antisymmetric subproblems in reflection, respectively. Thus, by setting rigid, $\partial p/\partial x = 0$ (symmetric), and soft, $p = 0$ (antisymmetric), boundary conditions at the symmetry plane of the system, the reflection coefficients of each subproblem can be obtained as

$$R_{\text{sym}} = T_t - R_t = \frac{\bar{Z}_e \sin k_e L/2 - i \cos k_e L/2}{\bar{Z}_e \sin k_e L/2 + i \cos k_e L/2}, \quad (5)$$

$$R_{\text{asym}} = T_t + R_t = \frac{\bar{Z}_e \cos k_e L/2 + i \sin k_e L/2}{i \sin k_e L/2 - \bar{Z}_e \cos k_e L/2}, \quad (6)$$

for the symmetric and antisymmetric problems, respectively. Then, the absorption coefficient of the full problem can be obtained from the absorption of each subproblem as $\alpha = (\alpha_{\text{sym}} + \alpha_{\text{asym}})/2$, where $\alpha_{\text{sym(asym)}} = 1 - |R_{\text{sym(asym)}}|^2$ [22].

A. Asymptotic behavior, large number of resonators

Let us first consider N sufficiently large to accurately describe the system as a slab of material with the effective parameters. Figures 3(b) and 3(c) show the corresponding reflection coefficient in the complex frequency plane. It is obtained with the TMM, of the symmetric and antisymmetric problems for $N = 30$ resonators considering a complex frequency $\omega = \omega_r + i\omega_i$, with ω_r and ω_i the real and imaginary frequencies. First, it can be observed that a series of zero-pole pairs appears in the frequency complex plane [15]. The poles correspond to the cavity modes inside the slab of effective material [28]. Due to dispersion, these cavity modes accumulate below the resonance frequency of the HRs. On

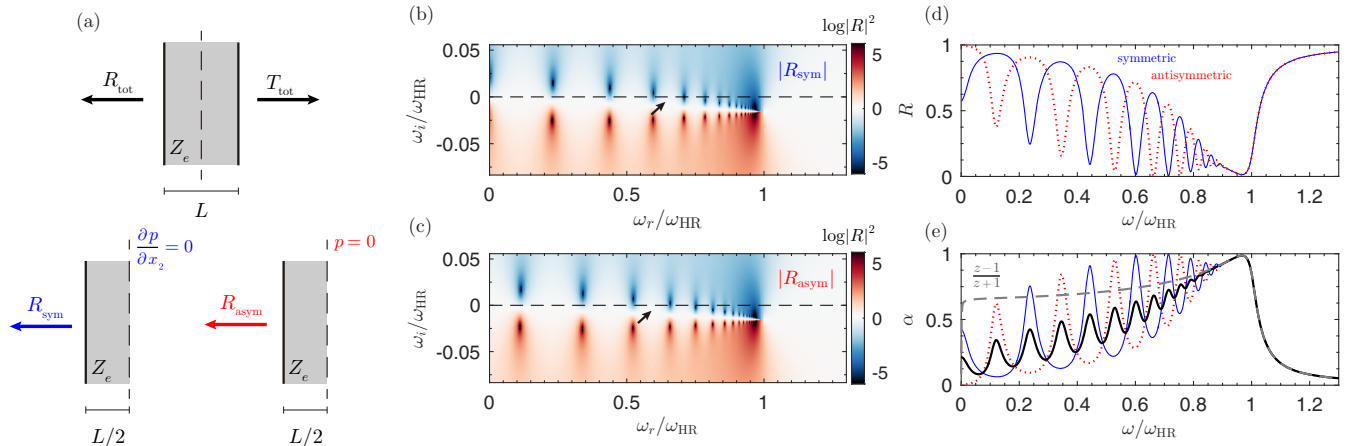


FIG. 3. (a) Symmetric and antisymmetric problem decomposition for a homogeneous layer of material with effective parameters. (b),(c) Complex frequency representation of the reflection coefficient for the symmetric and antisymmetric problem, respectively. (d) Reflection coefficient at the real axis for symmetric (blue) and antisymmetric (dotted red). (e) Absorption for symmetric (blue), antisymmetric (dotted red), total (thick black), and impedance matching condition (dashed gray).

the other hand, it can be seen that the cavity modes of the symmetric problem (see R_{sym}) appear at frequencies different from the frequencies of the antisymmetric one (see R_{asym}). This effect is clearly seen in Fig. 3(d), where the reflection coefficients for each problem are plotted at the real axis of frequencies.

In addition, it can be seen that for some particular frequencies, as those marked with the arrows in Figs. 3(b) and 3(c), the zeros of the reflection coefficient are located on the real axis of frequencies. At these frequencies, the reflection coefficient of the (anti)symmetric vanishes and the structure is critically coupled. This condition is enough to achieve perfect absorption for, e.g., the symmetric problem, as was demonstrated in rigid-backed materials [14,16,18]. However, to obtain perfect absorption of the full problem including transmission, both symmetric and antisymmetric reflection coefficients must simultaneously vanish [21,22], as the following relations hold: $R_t = (R_{\text{sym}} + R_{\text{asym}})/2$ and $T_t = (R_{\text{sym}} - R_{\text{asym}})/2$.

In general, for a homogeneous slab of material the cavity resonances of the symmetric and antisymmetric problems, i.e., its Fabry-Pérot modes, are staggered in frequency and perfect absorption is not possible. However, in our system the cavity modes are accumulated below the limit of the band gap because of the strong dispersion introduced by the presence of the resonators. Then, the zeros of the reflection coefficient for the symmetric and antisymmetric problems can be close to one another in frequency and quasiperfect absorption can be obtained at the edge of the band gap. Figure 3(e) shows the corresponding absorption of the full problem (black line), where the absorption due to accumulation of resonances around ω_{HR} is observed. It is interesting to show that, in the limit of a semi-infinite panel, both the reflection coefficient of the symmetric and antisymmetric problems collapse to the impedance matching condition, $\lim_{L \rightarrow \infty} R_{\text{sym}} = \lim_{L \rightarrow \infty} R_{\text{asym}} = (\bar{Z}_e - 1)/(\bar{Z}_e + 1)$, and then, only in this limit, perfect absorption can be achieved, as shown in Fig. 3(e). However, for a finite layer $R_{\text{sym}} \neq R_{\text{asym}}$ and only quasiperfect absorption can be reached with a single homogenized slab of

material. Moreover, \bar{Z}_e is generally complex and no perfect matching can be achieved.

B. Finite number of resonators

Figure 4 shows the scattering of the system in the lossless case for $N = 3$ resonators with the same parameters as in Sec. IV A. Figures 4(a) and 4(b) show the complex frequency representation of the reflection coefficient obtained by using the MEM, while Figs. 4(d) and 4(e) show the corresponding one obtained by using the TMM. It is worth noting here that if we solve the problem using the MEM (with an effective-impedance boundary condition to represent the effect of the HRs), it presents a zero-pole structure with an infinite collection of resonances that accumulate around the band-gap frequency. Note for a finite number of resonators there should be a finite number of resonances. The TMM correctly accounts for the finite number of resonances, in this case $N = 3$, in agreement with FEM simulations as shown in Fig. 4(g). It is also worth noting here that these cavity resonances are in fact the collective modes of the HRs and there exist only N different collective modes. Figure 4(f) shows the total reflection and transmission in the real axis calculated with TMM and FEM. The agreement between the two methods is very good, showing that the hypothesis of the TMM are correct for the considered frequency range. It can also be noticed that, by including the discreteness of the system, the band-gap frequency is shifted down from ω_{HR} , as it was previously noticed from the dispersion relations. However, the finite number of HRs limits the accumulation of resonances near the band gap: as N decreases the condition to have symmetric and antisymmetric resonances close to one another in frequency will become more difficult to achieve. Therefore, the number of (identical) HRs is a critical parameter to obtain quasiperfect absorption in metamaterials with transmission by means of the accumulation of resonances.

Once losses are introduced in the system, the zero-pole structure is down-shifted in the complex frequency plane and

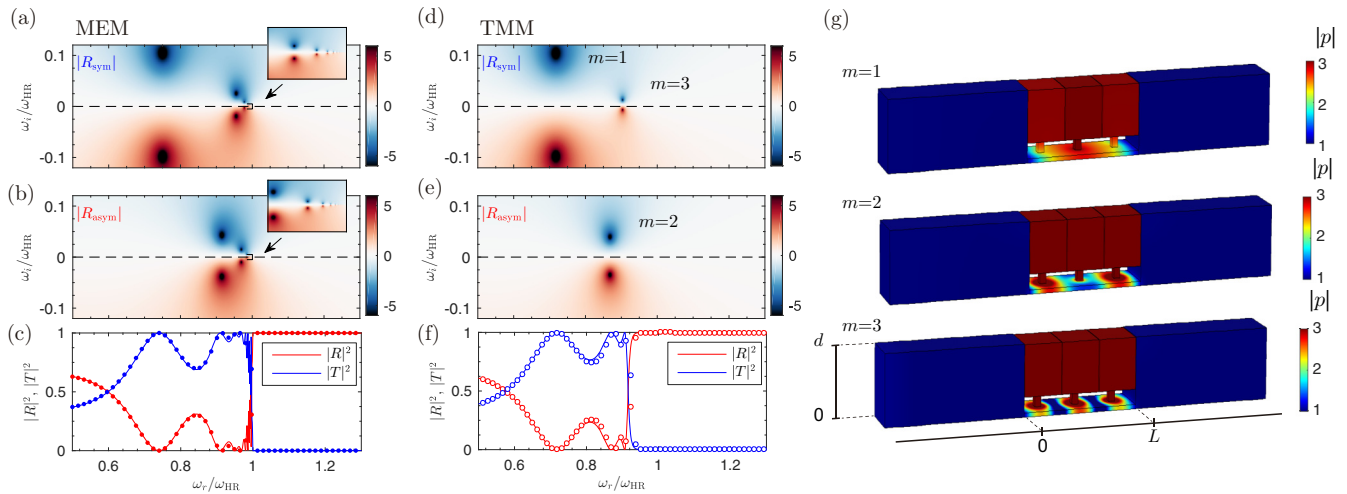


FIG. 4. Complex frequency plane representation of the reflection coefficient for a panel of $N = 3$ resonators. (a) Symmetric and (b) asymmetric reflection obtained using the modal expansion method (MEM). Color bar in $\log |R|^2$ units. (c) Total transmission (blue) and reflection (red) using MEM (continuous lines) and its effective parameters (dots). (d) Symmetric and (e) asymmetric reflection using the transfer matrix method (TMM). (f) Total transmission (blue) and reflection (red) using TMM. (g) Acoustic field obtained using finite element method (FEM) at frequencies corresponding to the resonances $m = 1, 2, 3$, color bar in normalized pressure units.

the system starts to absorb energy [15]. Figure 5(a) presents the absorption of a panel as a function of the number of resonators, N , and frequency. First, it can be observed that for a relatively large number of resonators quasiperfect absorption can be achieved even when the discreteness is retained, e.g., for $N = 50$ resonators as shown in Fig. 5(b). The material is almost impedance matched with the exterior medium and both MEM and TMM agree: the system can be described as a homogenized slab of locally reactive material. Only small differences between MEM and TMM solutions exist near the band gap due to the infinite number of resonances of the MEM.

For most sound absorption applications it is desirable to use panels with reduced thickness, and of special interest is the design of panels with subwavelength dimensions. Then, when reducing the panel thickness the number of resonators must also be reduced and, therefore, the accumulation of

resonances becomes limited. Figure 5(c) shows the absorption of a panel with $N = 15$ ($L \approx \lambda_{\alpha_{\max}}/2$), while Fig. 5(d) shows the absorption of a panel with $N = 5$ ($L = \lambda_{\alpha_{\max}}/6.6$). In both cases, a peak of absorption is still observed, but its amplitude falls to $\alpha_{\max} = 0.96$ and $\alpha_{\max} = 0.92$, respectively, for each case. The corresponding reflection coefficient in complex frequency plane for $N = 5$ is shown in Fig. 5(f) for the symmetric and antisymmetric problems. Again, the zeros of the symmetric problem appear staggered in frequency with respect to the antisymmetric one and, as a consequence, the accumulation of resonances is limited by the small number of resonators. However, by tuning the geometry of the system, high acoustic absorption can be achieved by locating one zero of the reflection coefficient of the symmetric problem on the real frequency axis and, simultaneously, locate another zero of the antisymmetric problem as close as possible to the real axis

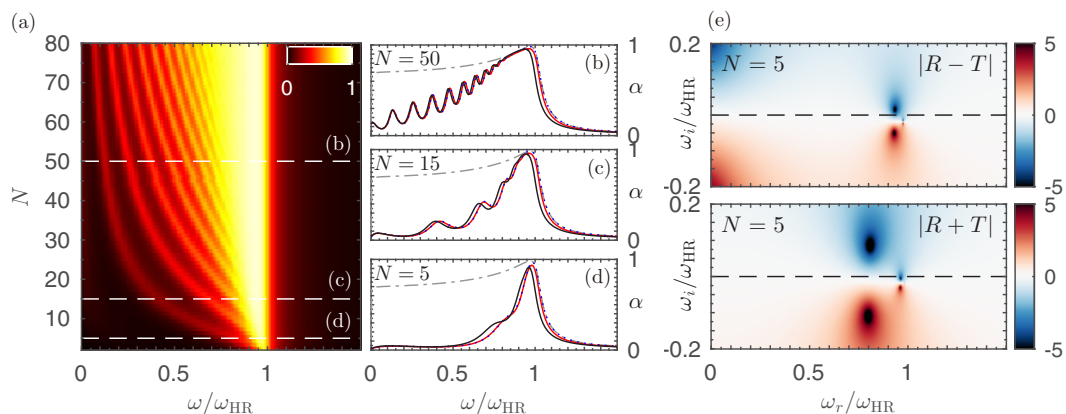


FIG. 5. (a) Absorption of the material as a function of the number of resonators and frequency. (b)–(d) Absorption for $N = 50, 15,$ and 5 resonators, obtained using MEM (red), effective parameters (dotted blue), and TMM (black). Dashed-dotted gray line shows the impedance matching condition. (e) Complex frequency representation of the reflection coefficient for $N = 5$ resonators. Color map in $\log |R|^2$ units.

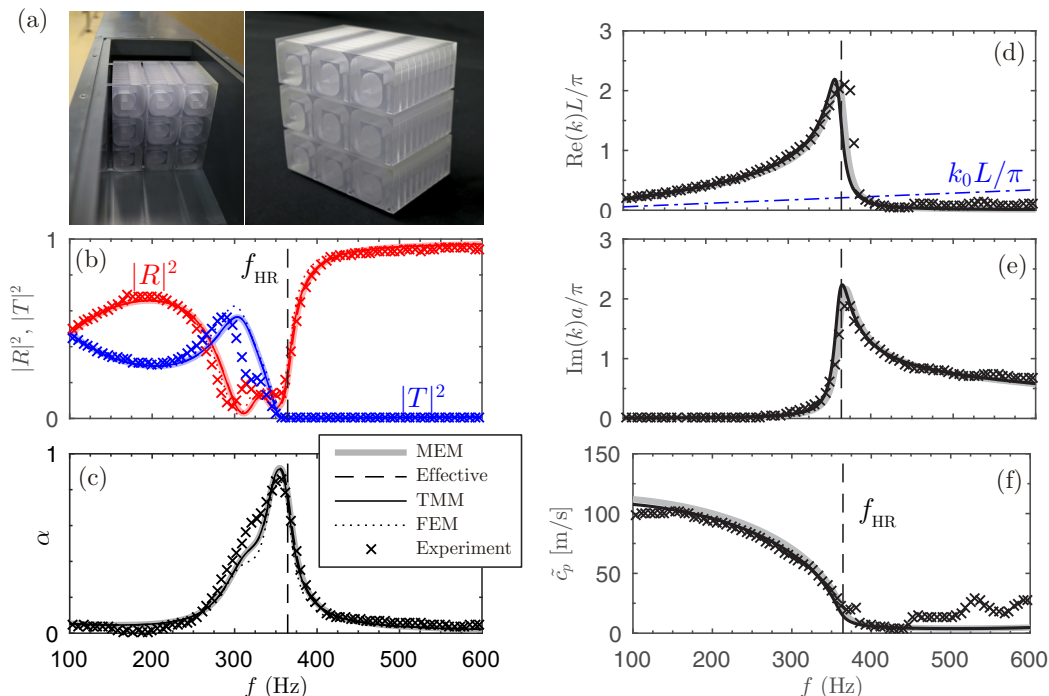


FIG. 6. (a) Photographs of the experimental setup, where the semitransparent resin allows one to see the coiled Helmholtz resonators inside the material. (b) Corresponding reflection (red) and transmission (blue) coefficients of the sample measured experimentally (markers), calculated using the MEM (thick lines), by using the effective parameters (dashed), TMM (continuous), and finite element simulation (dotted). The vertical dashed line marks the resonance of the HRs. (c) Corresponding absorption. (d) Real part of the wave number (thick gray), and its reconstruction using the experimental data (markers) and analytic data (continuous line). (e) Corresponding imaginary part. (f) Quantity $\tilde{c}_p = \text{Re}(\omega/k)$, closely related to the speed of sound.

at a different but near frequency. Therefore, the maximum value of absorption is directly dependent on the number of HRs and inversely dependent on the panel thickness. Using an array of identical resonators the design of the panel is a compromise between the peak acoustic absorption and the parameter λ_{max}/L .

V. EXPERIMENTAL RESULTS

A subwavelength thickness sample with $N = 10$ resonators was built using stereolithography techniques using a photosensitive epoxy polymer (Accura 60[®], 3D Systems Corporation, Rock Hill, SC 29730, USA), where the acoustic properties of the solid phase are $\rho_0 = 1210 \text{ kg/m}^3$ and $c_0 = 1630 \pm 60 \text{ m/s}$. The geometry of the structure was tuned using an optimization method [sequential quadratic programming (SQP) method [29]] in order to maximize the absorption at a given frequency (350 Hz), while the panel thickness was constrained to $L = \lambda/10$. The resulting parameters were $h = 4.3 \text{ mm}$, $a = 9.8 \text{ mm}$, $w_n = 5.3 \text{ mm}$, $w_{c,1} = 11.4 \text{ mm}$, $w_{c,2} = 9.3 \text{ mm}$, $d = \text{cm}$, $l_n = 25.2 \text{ mm}$, and $l_c = 139.6 \text{ mm}$. It is worth noting here that we use the coiling of the HRs in order to save space. The amplitude of the acoustic source was low enough to consider negligible the contribution of the nonlinearity of the HRs. Figure 6 summarizes the experimental results. First, Fig. 6(a) shows a photograph of the panel, composed by three unit cells with $N = 10$ for each one, allowing the measurement of reflection and transmission coefficients at normal incidence, which are shown in Fig. 6(b). A good agreement between

the experimental results, theoretical predictions, and FEM simulations is observed. The results show the band gap generated by the resonance of the HRs, where the low-cutoff frequency of the band gap is just below the resonance frequency of the HRs, $f_{\text{HR}} = 364 \text{ Hz}$. In this frequency range, transmission almost vanishes and the total reflection does not, as shown in Fig. 6(b), as a consequence of the staggered structure of zero-pole structure. The corresponding absorption is plotted in Fig. 6(c), where again good agreement can be observed between theory and experiments. Here, at 350 Hz the absorption peak obtained from the experiments was $\alpha = 0.87$, while $\alpha = 0.91$ was obtained from TMM predictions. In addition, small differences can be observed around 300 Hz. These small discrepancies can be associated to imperfections on the fitting of the structure to the impedance tube and due to the coiling of the HRs.

On the other hand, the effective wave number inside the slits was reconstructed using an inversion method [30]. Figures 6(d) and 6(e) show the experimental and theoretical reconstruction of the real and imaginary part of the wave number, respectively. It can be observed that the experimental reconstruction agrees with the theoretical prediction. Here, at $f = 350 \text{ Hz}$ where the peak absorption is observed, the real part of the wave number is greatly increased compared to the wave number in air, k_0 . Moreover, the imaginary part of the wave number is also increased, leading to the damping of the acoustic waves inside the material. Finally, the quantity $\tilde{c}_p = \text{Re}(\omega/k)$ is shown in Fig. 6(f). It can be seen that slow sound conditions are achieved by the experiment and the speed of sound inside the

material is reduced to $\tilde{c}_p = 34$ m/s at the peak absorption frequency, $f = 350$ Hz. Finally, it is important to note that the effect of the evanescent coupling between adjacent resonators is negligible. This coupling is implicitly included in FEM simulations and inherently present in the experiments. The good agreement between FEM simulations and experiments, and theoretical models shows the evanescent coupling can be considered negligible.

VI. CONCLUSIONS

The absorption of panels in transmission with periodic arrays of slits loaded by monopolar resonant inclusions made of HRs has been studied. We have shown that by using an array of identical monopolar resonators the symmetric and antisymmetric resonances of the system exist at staggered frequencies and, therefore, simultaneous critical coupling of the symmetric and antisymmetric modes is not possible. However, due to the loading HRs, strong dispersion is observed in the interior of each slit and the cavity resonances accumulate below the band-gap frequency, being the symmetrical and antisymmetrical modes staggered but very close in frequency. In this frequency range and by tuning the geometry, the system can be quasically coupled with the exterior medium and therefore quasiperfect absorption can be obtained.

The limits of acoustic absorption in symmetric and reciprocal panels with transmission were explored experimentally, and quasiperfect absorption for a subwavelength panel with thickness $L = \lambda/10$ was demonstrated. These results underline the necessity of breaking the symmetry of the system to achieve perfect absorption in transmission or the use of degenerate resonators with symmetric (monopolar) and antisymmetric (dipolar) resonances. Strategies for breaking the symmetry include the use of, e.g., different sized HRs [22]. Strategies to use degenerate resonances have been also studied [20,21].

On the other hand, the extension of the results shown in this work to other analogous physical systems is also possible, with special interest for those where the number of resonators in the cavity can be remarkably increased, e.g., by using deep-subwavelength resonators as arrays of identical membranes with added mass or by using gas microbubbles for underwater acoustic applications.

The proposed configuration presents interesting and remarkable features as the open slits allow the air to flow through the panel, e.g., being able to use these subwavelength metamaterials for low-frequency noise control in industrial applications where simultaneously chromatic noise absorption and machinery refrigeration or air flow are required. These promising results open the possibilities to study different configurations based on these metamaterials and to extend the results to broadband and omnidirectional perfect absorption with deep subwavelength structures, which remains a great scientific challenge.

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APPENDIX A: VISCOTHERMAL LOSSES MODEL

The viscothermal losses in the system are considered both in the resonators and in the slit by using its effective complex and frequency dependent parameters [26].

Slits. The effective parameters in the slit, considering only plane waves propagate inside, are expressed as

$$\rho_s = \rho_0 \left[1 - \frac{\tanh\left(\frac{h}{2}G_\rho\right)}{\frac{h}{2}G_\rho} \right]^{-1}, \quad (\text{A1})$$

$$\kappa_s = \kappa_0 \left[1 + (\gamma - 1) \frac{\tanh\left(\frac{h}{2}G_\kappa\right)}{\frac{h}{2}G_\kappa} \right]^{-1}, \quad (\text{A2})$$

with $G_\rho = \sqrt{i\omega\rho_0/\eta}$ and $G_\kappa = \sqrt{i\omega\text{Pr}\rho_0/\eta}$, and where γ is the specific heat ratio of air, P_0 is the atmospheric pressure, Pr is the Prandtl number, η the dynamic viscosity, ρ_0 the air density, and $\kappa_0 = \gamma P_0$ the air bulk modulus.

Ducts. The propagation in a rectangular cross-section tube can be described by its complex and frequency dependent density and bulk modulus, and considering that plane waves propagate inside, can be expressed as [26]

$$\rho_t = - \frac{\rho_0 a^2 b^2}{4G_\rho^2 \sum_{k \in \mathbb{N}} \sum_{m \in \mathbb{N}} [\alpha_k^2 \beta_m^2 (\alpha_k^2 + \beta_m^2 - G_\rho^2)]^{-1}}, \quad (\text{A3})$$

$$\kappa_t = \frac{\kappa_0}{\gamma + \frac{4(\gamma-1)G_\kappa^2}{a^2 b^2} \sum_{k \in \mathbb{N}} \sum_{m \in \mathbb{N}} [\alpha_k^2 \beta_m^2 (\alpha_k^2 + \beta_m^2 - G_\kappa^2)]^{-1}}, \quad (\text{A4})$$

with the constants $\alpha_k = 2(k + 1/2)\pi/a$ and $\beta_m = 2(m + 1/2)\pi/b$, and the dimensions of the duct a and b being either the neck, $a = b = w_n$, or the cavity, $a = w_{c,1}$ and $b = w_{c,2}$, of the Helmholtz resonators.

APPENDIX B: MODAL EXPANSION METHOD (MEM)

1. Mode matching system

As sketched in Fig. 1, the full space is divided into three subdomains: the forward exterior medium, $\Omega^{[0]}$, the interior of the slit, $\Omega^{[1]}$, and the backward exterior air, $\Omega^{[2]}$. The field can be represented on each $\Omega^{[i]}$ domain as

$$p^{[0]} = \sum_q (A^i \delta_q e^{-ik_{2q}^{[0]}(x_2-L)} + R_q e^{ik_{2q}^{[0]}(x_2-L)}) e^{ik_{1q} x_1}, \quad (\text{B1})$$

$$p^{[1]} = \sum_n (B_n e^{-ik_{2n}^{[1]} x_2} + C_n e^{ik_{2n}^{[1]} x_2}) \sin k_{1n} (x_1 - L), \quad (\text{B2})$$

$$p^{[2]} = \sum_q T_q e^{ik_{1q} x_1 - ik_{2q}^{[0]} x_2}, \quad (\text{B3})$$

where A^i is the amplitude of the incident wave, R_q and T_q are the reflection and transmission coefficients of the q th Bloch mode, respectively, and δ_n^0 is the Kronecker delta. Here and beyond the superscript $[i]$ indicates the domain according to Fig. 1. Periodic boundary conditions are assumed at $x_1 = 0$ and $x_1 = d$. It is worth noting here that for normal incidence periodic boundary conditions reduce to symmetric (rigid) boundary conditions. Inside the slit, at $x_1 = h$, the effect of the resonators is included by a wall impedance condition given

by $Z_{\text{wall}} = Z_{\text{HR}}/\phi$, with Z_{HR} the impedance of the HRs and $\phi = w_n^2/a^2$ the surface porosity of the slit. The application of these boundary conditions and continuity between domains leads to the following mode matching system:

$$\begin{aligned} R_q - \sum_{q'} \sum_n \frac{\eta_n^{[1]}}{\eta_{nq}^{[0]}} \frac{h}{d N_n} \left(\frac{-i R_{q'}}{\tan k_{2n}^{[1]} L} \right) I_{nq'}^+ I_{nq}^- \\ - \sum_{q''} \frac{\eta_n^{[1]}}{\eta_q^{[0]}} \frac{h}{d N_n} \sum_n \left(\frac{i T_{q''}}{\sin k_{2n}^{[1]} L} \right) I_{nq''}^+ I_{nq}^- \\ = A^i + \sum_n \frac{\eta_n^{[1]}}{\eta_q^{[0]}} \frac{h}{d} \frac{-i A^i}{\tan k_{2n}^{[1]} L N_n} I_{n0}^+ I_{nq}^- \end{aligned} \quad (\text{B4})$$

and

$$\begin{aligned} T_q + \sum_{q'} \sum_n \frac{\eta_n^{[1]}}{\eta_{nq}^{[0]}} \frac{h}{d} \left(\frac{-i R_q}{N_n \sin k_{2n}^{[1]} L} \right) I_{nq'}^+ I_{nq}^- \\ + \sum_{q''} \sum_n \frac{\eta_n^{[1]}}{\eta_{nq}^{[0]}} \frac{h}{d N_n} \frac{i T_{q''}}{\tan k_{2n}^{[1]} L} I_{nq''}^+ I_{nq}^- \\ = \sum_n \frac{\eta_n^{[1]}}{\eta_{nq}^{[0]}} \frac{h}{d} \frac{i A^i}{\sin(k_{2n}^{[1]} L) N_n} I_{n0}^+ I_{nq}^-, \end{aligned} \quad (\text{B5})$$

where $\eta_q^{[j]} = k_{2q}^{[j]}/\rho^{[j]}$. Thus the reflection and transmission coefficients can be calculated by solving the linear system of Eqs. (B4) and (B5), where the integrals I_{nq}^{\pm} are written in analogy with Refs. [16–18].

2. Low frequency approximation: Effective parameters

In the low frequency regime, the system (B4) and (B5) leads to the reflection and transmission coefficients as

$$R_0 + \frac{i \bar{Z}_e R_0}{\tan k_2^{[1]} L} - \frac{i \bar{Z}_e T_0}{\sin k_2^{[0]} L} = \left(1 - \frac{i \bar{Z}_e}{\tan k_2^{[1]} L} \right), \quad (\text{B6})$$

$$T_0 - \frac{i \bar{Z}_e R_0}{\sin k_2^{[1]} L} + \frac{i \bar{Z}_e T_0}{\tan k_2^{[1]} L} = \frac{i \bar{Z}_e}{\sin k_2^{[1]} L}, \quad (\text{B7})$$

where the normalized effective impedance is defined as $\bar{Z}_e = \eta^{[1]} h / \eta^{[0]} d = Z^{[1]} / Z^{[0]} \phi_t$, with the total porosity $\phi_t = h/d$, and $A^i = 1$. We clearly identify the effective wave number inside the panel as

$$k_2^{[1]} = \sqrt{(k_1^{[1]})^2 - (k_{10})^2}. \quad (\text{B8})$$

The transversal component of the wave number is given by [31]

$$k_{10} = \frac{1}{h} \sqrt{\frac{-i \omega \rho_s h}{Z_{\text{wall}}}}, \quad (\text{B9})$$

and using the Helmholtz resonator impedance in the low frequency regime it becomes

$$k_{10} = \frac{1}{h} \sqrt{\frac{-\omega \rho_s h (V_c Z_n k_c + S_n Z_c k_n l_n) \phi}{Z_n (S_n Z_c - V_c Z_n k_c k_n l_n)}}. \quad (\text{B10})$$

Using Eq. (B8) the effective wave number reads

$$k_e = k_2^{[1]} = \frac{\omega^2}{c_0^2} \left[1 + \frac{\kappa_s (V_c \kappa_n + V_n \kappa_c) \phi}{\kappa_n (S_n \kappa_c - V_c l_n \omega^2 \rho_n) h} \right]. \quad (\text{B11})$$

The effective parameters, i.e., the complex and frequency dependent bulk modulus and density are given by

$$\kappa_e = \frac{\kappa_s}{\phi_t} \left[1 + \frac{\kappa_s \phi (V_c \kappa_n + V_n \kappa_c)}{\kappa_n h (S_n \kappa_c - V_c l_n \omega^2 \rho_n)} \right]^{-1}, \quad (\text{B12})$$

$$\rho_e = \frac{\rho_s}{\phi_t}. \quad (\text{B13})$$

Using these parameters, the reflection and transmission coefficients can be calculated according to Eqs. (B6) and (B7) as

$$R_0 = \frac{i (\bar{Z}_e^2 - 1) \sin(k_e L)}{2 \bar{Z}_e \cos(k_e L) - i (\bar{Z}_e^2 + 1) \sin(k_e L)}, \quad (\text{B14})$$

$$T_0 = \frac{2 \bar{Z}_e}{2 \bar{Z}_e \cos(k_e L) - i (\bar{Z}_e^2 + 1) \sin(k_e L)}. \quad (\text{B15})$$

APPENDIX C: TRANSFER MATRIX METHOD

A discrete model is developed accounting for the finite number of resonators using the transfer matrix method (TMM). Thus, for identical resonators, the transfer matrix is written as

$$\begin{pmatrix} P_i \\ U_i \end{pmatrix} = \mathbf{T} \begin{pmatrix} P_o \\ U_o \end{pmatrix}, \quad (\text{C1})$$

where the transmission matrix \mathbf{T} is written as

$$\mathbf{T} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} = \mathbf{M}_{\Delta l_{\text{slit}}} (\mathbf{M}_s \mathbf{M}_{\text{HR}} \mathbf{M}_s)^N \mathbf{M}_{\Delta l_{\text{slit}}}.$$

Here, the transmission matrix for each lattice step in the slit, \mathbf{M}_s , is written as

$$\mathbf{M}_s = \begin{pmatrix} \cos(k_s \frac{a}{2}) & i Z_s \sin(k_s \frac{a}{2}) \\ \frac{i}{Z_s} \sin(k_s \frac{a}{2}) & \cos(k_s \frac{a}{2}) \end{pmatrix}, \quad (\text{C2})$$

where the slit characteristic impedance is written as $Z_s = \sqrt{\kappa_s \rho_s} / S_s$ and $S_s = h a$. The resonators are introduced as punctual scatters by a transmission matrix \mathbf{M}_{HR} as

$$\mathbf{M}_{\text{HR}} = \begin{pmatrix} 1 & 0 \\ 1/Z_{\text{HR}} & 1 \end{pmatrix}, \quad (\text{C3})$$

and the radiation correction of the slit to the free space as

$$\mathbf{M}_{\Delta l_{\text{slit}}} = \begin{pmatrix} 1 & Z_{\Delta l_{\text{slit}}} \\ 0 & 1 \end{pmatrix}, \quad (\text{C4})$$

with the characteristic radiation impedance of the slit $Z_{\Delta l_{\text{slit}}} = -i \omega \Delta l_{\text{slit}} \rho_0 / \phi_t S_0$, where $S_0 = d a$, ρ_0 is the air density, and Δl_{slit} is the proper end correction that will be described later.

The reflection and transmission coefficients of the system can be directly calculated from the elements of the matrix \mathbf{T} as

$$T_{\text{TMM}} = \frac{2e^{ikL}}{T_{11} + T_{12}/Z_0 + Z_0T_{21} + T_{22}}, \quad (\text{C5})$$

$$R_{\text{TMM}} = \frac{T_{11} + T_{12}/Z_0 - Z_0T_{21} - T_{22}}{T_{11} + T_{12}/Z_0 + Z_0T_{21} + T_{22}}, \quad (\text{C6})$$

with $Z_0 = \rho_0 c_0 / S_0$, and the effective parameters can be obtained from the transfer matrix elements as follows:

$$k_{\text{TMM}} = \frac{1}{L} \cos^{-1} \left(\frac{T_{11} + T_{22}}{2} \right), \quad (\text{C7})$$

$$Z_{\text{TMM}} = \frac{1}{Z_0} \sqrt{\frac{T_{12}}{T_{21}}}. \quad (\text{C8})$$

APPENDIX D: RESONATOR IMPEDANCE AND END CORRECTIONS

Using the effective parameters for the neck and cavity elements given by Eqs. (A3) and (A4), the impedance of a Helmholtz resonator can be written as

$$Z_{\text{HR}} = iZ_n \frac{A - \tan k_n l_n \tan k_c l_c}{A \tan k_n l_n + \tan k_c l_c}, \quad (\text{D1})$$

with $A = Z_c / Z_n$, l_n and l_c are the neck and cavity lengths, $S_n = w_n^2$ and $S_c = w_{c,1} w_{c,2}$ are the neck and cavity surfaces, and k_n and k_c , and Z_n and Z_c are the effective wave numbers and effective characteristic impedance in the neck and cavity, respectively.

It is worth noting here that this expression is not exact as long as correction due to the radiation should be included. The characteristic impedance accounting for the neck radiation can be expressed as [27]

$$Z_{\text{HR}} = -i \frac{\cos(k_n l_n) \cos(k_c l_c) - Z_n k_n \Delta l \cos(k_n l_n) \sin(k_c l_c) / Z_c - Z_n \sin(k_n l_n) \sin(k_c l_c) / Z_c}{\sin(k_n l_n) \cos(k_c l_c) / Z_n - k_n \Delta l \sin(k_n l_n) \sin(k_c l_c) / Z_c + \cos(k_n l_n) \sin(k_c l_c) / Z_c}, \quad (\text{D2})$$

where the correction length is deduced from the addition of two correction lengths $\Delta l = \Delta l_1 + \Delta l_2$ as

$$\Delta l_1 = 0.82 \left[1 - 1.35 \frac{r_n}{r_c} + 0.31 \left(\frac{r_n}{r_c} \right)^3 \right] r_n, \quad (\text{D3})$$

$$\Delta l_2 = 0.82 \left[1 - 0.235 \frac{r_n}{r_s} - 1.32 \left(\frac{r_n}{r_t} \right)^2 \right. \quad (\text{D4})$$

$$\left. + 1.54 \left(\frac{r_n}{r_t} \right)^3 - 0.86 \left(\frac{r_n}{r_t} \right)^4 \right] r_n. \quad (\text{D5})$$

The first length correction, Δl_1 , is due to pressure radiation at the discontinuity from the neck duct to the cavity of the Helmholtz resonator [32], while the second Δl_2 comes from the radiation at the discontinuity from the neck to the principal waveguide [33]. This correction only depends on the radius of the waveguides, so it becomes important when the duct length is comparable to the radius, i.e., for small neck lengths and for frequencies where $kr_n \ll 1$.

Another important end correction comes from the radiation from the slits to the free air. The radiation correction for a periodic distribution of slits can be expressed as [34]

$$\Delta l_{\text{slit}} = h \phi_t \sum_{n=1}^{\infty} \frac{\sin^2(n\pi \phi_t)}{(n\pi \phi_t)^3}. \quad (\text{D6})$$

Note for $0.1 \leq \phi_t \leq 0.7$ this expression reduces to $\Delta l_{\text{slit}} \approx -\sqrt{2} \ln[\sin(\pi \phi_t / 2)] / \pi$. Although Eq. (D6) is appropriate for a periodic array of slits, it is not exact for slits loading HRs; therefore, we can evaluate a more realistic value for the end correction by reconstructing an equivalent impedance, \tilde{Z} , from the reflection coefficient of the zeroth order Bloch mode calculated with the MEM and comparing it to $\tilde{Z}_e = \rho_e \kappa_e / \rho_0 \kappa_0$

in analogy with Ref. [18]:

$$\tilde{Z} - \tilde{Z}_e = -i\omega \frac{\rho_0}{\phi_t} \Delta l_{\text{slit}}. \quad (\text{D7})$$

The slit end correction using this last approach gives a value that depends on the geometry of the HRs and for the present structures is around 1.5 times the one using Eq. (D6).

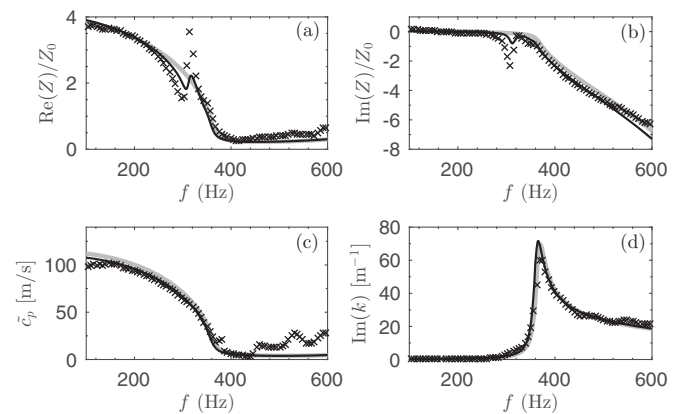


FIG. 7. Effective parameters computed by (thick gray lines) the low frequency approximation of the MEM, Eqs. (1) and (2), (markers) reconstructed from the experimental data and (continuous lines) reconstructed from the MEM analytical reflection and transmission coefficients. (a) Real and (b) imaginary part of the complex density normalized by the ambient density and total porosity. (c) Real and (d) imaginary part of the complex compressibility normalized by the ambient bulk modulus and total porosity. The dashed line marks the resonance frequency of the Helmholtz resonators, $f_{\text{HR}} = 364$.

APPENDIX E: RECONSTRUCTION OF EFFECTIVE PARAMETERS

The effective parameters of the metamaterial, i.e., the complex and frequency dependent density and bulk modulus, can be reconstructed from its effective wave number and impedance. Figure 7 shows the reconstruction using the experimental data (markers), the effective parameters given by Eqs. (1) and (2) (gray line), and the reconstruction method using the MEM analytical reflection and transmission coefficients as the input (black line). It can be seen that the inversion method, even with the analytical transmission and reflection data, fails to reconstruct the effective parameters at the frequencies corresponding to $\text{Re}(k)L/\pi = (1, 2, \dots)$.

This is caused by the poor reconstruction of the effective impedance at the Fabry-Pérot resonances of a slab of effective material. However, the main features of the effective parameters are captured by the reconstruction. First, the effective density of the metamaterial is almost the density of air normalized by the total porosity, ϕ_t , it being almost constant in frequency. Second, the real part of the effective bulk modulus is reduced up to 15% of the bulk modulus of the air at 350 Hz, it vanishes at the resonance frequency of the HRs ($f_{\text{HR}} = 364$ Hz, vertical dashed line), and it is negative for frequencies above f_{HR} . Therefore, the effective compressibility of the material is greatly increased, allowing the structure to resonate in the subwavelength regime.

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