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Minimum reflection channel in amplifying random media

Seng Fatt Liew and Hui Cao*

Applied Physics Department, Yale University, New Haven, Connecticut 06520, USA (Received 19 August 2015; revised manuscript received 4 December 2015; published 29 December 2015)

We present a numerical study on the minimum reflection channel of a disordered waveguide and its modification by coherent amplification of light. The minimum reflection channel is formed by destructive interference of quasinormal modes at the front surface of a random medium. While the lowest reflection eigenvalue increases with optical gain in most random realizations, the minimum reflection channel can adjust its modal composition to enhance destructive interference and slow down the growth of reflectance with gain. Some of the random realizations display a further reduction of the minimum reflectance by adding optical gain. The differential amplification of the modes can make their destructive interference so effective that it dominates the amplitude growth of the modes, causing the reflectance to drop with gain in these cases. Therefore, the interplay between interference and amplification can further minimize light reflection from a strong scattering medium; indicating optical gain may provide an additional degree of freedom for coherent control of mesoscopic transport.

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I. INTRODUCTION

Due to multiple scattering of light, disordered media such as paper, paint, or biological tissue have high reflectivity and are opaque. However, wave interference effects may diminish the reflectance by creating highly transmitting open channels [1-4]. Recent developments of wavefront shaping and phase recording techniques in optics have enabled the coupling of incident light to these open channels [5-19]. The open channels can greatly enhance light transmission through scattering media, having a profound impact in a wide range of applications from deep tissue imaging and laser surgery to spectroscopy [20-30] and optogenetics [31]. So far, most experimental studies of high transmission channels rely on optical access to both sides of a scattering media, which is not practical in realistic situations. However, there is a one-to-one correspondence between the transmission eigenchannels and reflection eigenchannels in turbid media without absorption. Thus information about the transmission channels may be obtained from reflection measurements, which are conducted on the input side of samples, and thus noninvasive [32]. For example, by reducing reflection, one can couple light into the minimum reflection channel, which corresponds to the maximum transmission channel.

The correspondence between transmission and reflection holds only in the absence of absorption. Absorption exists in many material systems and is known to have a significant impact on the mesoscopic transport of light [18,33–44]. Our recent studies show that when significant absorption is introduced uniformly across a diffusive system, the maximum transmission channel becomes quasiballistic [18]. In the case that the absorption is distributed nonuniformly in space, a high transmission channel may redirect the energy flow to circumvent the strong absorbing regions [44]. Because light absorption can also reduce reflection, the minimum reflection channel no longer corresponds to the maximum transmission channel [18]. Usually optical gain has the opposite effects of absorption, and there have been extensive studies on the effects of coherent amplification on light propagation through random media [35–37,39,45–61]. However, it is unclear how optical amplification modifies transmission and reflection channels. Intuitively, one expects both transmittance and reflectance to increase with gain due to light amplification. However, such an expectation does not take into account the interference of multiply scattered light, which plays a dominant role in enhancing transmission and suppressing reflection [62]. As illustrated in the previous studies on random lasers, coherent amplification can enhance interference effects in random media [63,64]. Moreover, minimizing the reflectivity of the pump light could lower the lasing threshold as more pump light is absorbed instead of reflected.

In this paper, we present a numerical study to address the following questions: what is the impact of light amplification on a minimum reflection channel? Is it possible to further reduce reflectance of a strong scattering medium by adding optical gain? How will the interference effect that underlies the formation of the minimum reflection channel be modified by coherent amplification? To answer these questions, we numerically calculate the minimum reflection channels in disordered waveguides with optical gain. We find that the minimum reflection channel is formed by destructive interference of quasinormal modes at the front surface of the random system. In most of the disordered waveguide configurations, adding gain to the system causes the reflectance to increase, but the increment can be reduced by adjusting the input wavefront to enhance the destructive interference effect. In some disordered waveguides, the enhancement of the destructive interference is so strong that the reflectance drops with increasing gain. This result illustrates that in a random medium with gain, coherent phenomena (due to interference of excited modes) may dominate over incoherent phenomena (due to mode amplifications). Thus optical gain provides an additional degree of freedom for coherent control of mesoscopic transport of light.

This paper is organized as follows. Section II presents our numerical model of a two-dimensional (2D) disordered waveguide with gain. In Sec. III we demonstrate the modification of the minimum reflection eigenvalue by gain. In Sec. IV we conduct a modal analysis of the reflected light. In Sec. V,

^{*}hui.cao@yale.edu

the interference effects among the quasinormal modes that constitute the minimum reflection channels are investigated. Section VI illustrates how the modal interference can further reduce the minimum reflection in the presence of gain. Section VII presents the concluding remarks.

II. DISORDERED WAVEGUIDE WITH GAIN

Our numerical model consists of a 2D disordered waveguide, shown schematically in Fig. 1(a). Dielectric cylinders with refractive index $n_s = 2.5$ and radius $r_c = 0.1\lambda$ are randomly positioned inside the waveguide with perfectly reflecting sidewalls. The average distance between adjacent cylinders is $a = 0.87\lambda$, giving an area filling fraction of 0.04 for the dielectric in air. The wavelength of the input light is chosen to be away from the Mie resonances of individual cylinders, so that the scattering properties of the random system do not vary strongly with frequency. The incident light enters the waveguide from an open end and is scattered by the cylinders in the *x*-*y* plane. The light transmitted through, or reflected from the random array is absorbed by the perfectly matched layers located at both ends of the waveguide.

The probe light is transverse-magnetic (TM) polarized, with the electric field parallel to the cylinder axis (*z* axis). The width of the waveguide is $W = 10.3\lambda$, and the number of guided modes in the empty waveguide is $N = 2W/\lambda = 20$. The length of the random array of cylinders is $L = 20.2\lambda$. The transport mean free path is $l_t = 0.07L$ and the localization length is $\xi = (\pi/2)Nl_t = 2.3L$. The system is in the diffusion regime but not far from the localization threshold. Thus the transport



FIG. 1. (Color online) (a) Schematic of a 2D disordered waveguide simulated. Dielectric cylinders are placed randomly in a waveguide with perfectly reflecting sidewalls. An electric field $E_{in}^{(j)}$ is launched from the left end of the waveguide, and scattered by the cylinders. The reflected electric field $E_r^{(j)}$ is probed at the left end, and the transmitted electric field $E_t^{(j)}$ at the right end. Perfectly matched layers are placed at both open ends to absorb the transmitted and reflected waves. (b) The ensemble-averaged reflectance $\langle R_0 \rangle$ for the input wavefront corresponding to the minimum reflection channel without gain (dashed line) and the minimum reflection eigenvalue ρ_1 at each gain level (solid line) as a function of optical gain l_t/l_g . (c) The minimum reflection eigenvalue ρ_1 drops with increasing gain l_t/l_g in two of the disordered waveguides in the ensemble.

displays a large fluctuation from one random configuration to another. Within the same statistical ensemble there are random realizations that are closer to or further away from the localization transition. This allows us to study the diverse behavior in the same ensemble.

Usually optical gain exists either inside scattering particles or in the background material that hosts the particles. Contrast in the imaginary part of the refractive index causes additional scattering [65], which is avoided by introducing gain to both the scatterers and the host material. More specifically, the optical gain is introduced uniformly across the scattering region [highlighted in Fig. 1(a)] by adding a constant imaginary part $-\gamma$ to the refractive index $n = n_0 - i\gamma$, where n_0 is the real part of refractive index without gain. The gain length is $l_g = 1/(2k\gamma)$, where the wave vector $k = 2\pi/\lambda$. When the gain length l_g reaches the average path length of light in a 2D diffusive waveguide of length L, $2L^2/l_t$, the diffusive amplification length $l_{amp} = \sqrt{l_t l_g/2}$ becomes equal to L. $L = l_{amp}$ corresponds to the lasing threshold of a diffusive random laser [63], above which nonlinear gain saturation must be taken into account. To stay in the linear gain regime, we make sure the amount of gain is below the lasing threshold $L < l_{amp}$. We check individual configuration and verify that all of the random systems stay below the lasing threshold even in the presence of fluctuation. Spontaneous emission and its amplification are ignored in the calculation below.

To construct the reflection matrix r of the disordered waveguide, we use the guided modes in the empty waveguide (without scatterers) as a basis. The electromagnetic field inside the disordered waveguide was calculated using the finite-difference frequency-domain method [66]. We launch a guided mode $E_{in}^{(j)}(y)$ from the input end (x = 0), calculate the reflected wave and decompose it by the empty waveguide modes at x = 0, $E_r^{(j)}(y) = \sum_{i=1}^N r_{ij} E_{in}^{(j)}(y)$. The coefficient r_{ij} relates the field incident into the waveguide mode j to the field reflected to the waveguide mode i. After repeating this procedure for j = 1, 2, ..., N, we obtain all the elements r_{ij} for the reflection matrix r. Similarly, the transmission matrix t is constructed by computing the transmitted waves $E_t^{(j)}(y)$ at the output end x = L.

III. MODIFICATION OF MINIMUM REFLECTION BY GAIN

A singular value decomposition of the reflection matrix r gives

$$r = U \Sigma V^{\dagger} , \qquad (1)$$

where Σ is a diagonal matrix with nonnegative real numbers $\sqrt{\rho_n}$, ρ_n is the eigenvalue of $r^{\dagger}r$, and $\rho_1 < \rho_2 < \rho_3 < \cdots < \rho_N$. *U* and *V* are $N \times N$ unitary matrices, *V* maps input waveguide modes to eigenchannels of the disordered waveguide, and *U* maps eigenchannels to output waveguide modes. The column vectors in *V* (*U*) are orthonormal and are called input (output) singular vectors. The input singular vector with the lowest reflection eigenvalue ρ_1 couples to the minimum reflection eigenchannel; its elements represent the complex coefficients of the waveguide modes that combine to achieve minimum reflection from the random medium.

Similarly, the transmission eigenvalues τ_n where $\tau_1 > \tau_2 > \tau_3 > \cdots > \tau_N$ are obtained from singular value decomposition of the field transmission matrix *t*.

In a passive system without gain or loss, there is a one-toone correspondence between the transmission and reflection eigenchannels, $\tau_n + \rho_n = 1$. The minimum reflection channel has the same input wavefront as the maximum transmission channel. Since our system is close to the localization threshold, some of the random configurations have the maximum transmission eigenvalue τ_1 smaller than 1. Therefore, the ensembleaveraged maximum transmission eigenvalue $\langle \tau_1 \rangle = 0.7$ and the minimum reflection eigenvalue $\langle \rho_1 \rangle = 0.3$.

We fix the input wavefront to be the minimum reflection channel and then introduce optical gain into the system. The ensemble-averaged reflectance $\langle R_0 \rangle$ increases due to light amplification [dashed line in Fig. 1(b)]. We also compute the reflection matrix at each gain level, and from the singular value decomposition we obtain the ensemble-averaged minimum reflection eigenvalue $\langle \rho_1 \rangle$, which is plotted as a function of l_t/l_g [solid line in Fig. 1(b)]. The increase of $\langle \rho_1 \rangle$ is slower than $\langle R_0 \rangle$, indicating that the minimum reflection channel with gain deviates from that without gain.

Surprisingly, we observe that in about 10% of the disordered waveguides in our ensemble, the minimum reflection eigenvalue ρ_1 is further reduced by adding gain to the system. Figure 1(c) shows two of these disordered waveguides, where ρ_1 drops with increasing gain l_t/l_g .

IV. MODAL ANALYSIS OF REFLECTED LIGHT

To interpret the formation of minimum reflection channels, we resort to the quasinormal modes, which represent the resonances of an open system. More specifically, they are eigenstates of Maxwell's equations in an open system, whose coupling with the environment results in complex eigenfrequencies. The interference between quasinormal modes has been investigated previously to explain coherent transport of light in random media [18,62,67,68]. Below we will consider the contribution of quasinormal modes to the light reflected from the disordered waveguide. There are two types of quasinormal modes: (i) the outgoing modes u_m which are the eigenfunctions of Maxwell's equations which satisfy the boundary conditions that there are only outgoing waves to infinity; (ii) the incoming modes v_m which are the eigenfunctions for the boundary conditions of only incoming waves from infinity. In a passive system (without gain or loss), the two types of eigenfunctions are related by $u_m = v_m^*$. We use the commercial program COMSOL [66] to compute the quasinormal modes in the disordered waveguide. The spatial field distributions of the modes remain the same when gain is introduced uniformly across the system.

With light incident onto the random waveguide, both types of the quasinormal modes are excited, and the electric field distribution inside the disordered medium is decomposed (see Appendix):

$$E(x,y) = \sum_{m} a_{m} u_{m}(x,y) + \sum_{m} b_{m} v_{m}(x,y).$$
(2)

The reflected field at the front surface (x = 0) of the disordered waveguide can be expressed by the outgoing modes as

$$E_r(y) = \sum_m a_m u_m(0, y).$$
(3)

The contribution of the *m*th mode to the reflectance $R = \int |E_r(y)|^2 dy$ depends on its overlap with the reflected field E_r , namely,

$$\sqrt{R} = \sum_{m} a_m \int E_w^*(y) u_m(0, y) dy = \sum_m \alpha_m, \qquad (4)$$

where $E_w(y) \equiv E_r(y)/\sqrt{R}$ is the normalized reflected field, and α_m represents the contribution from the *m*th mode. α_m is a complex number $\alpha_m = |\alpha_m|e^{i\theta_m}$, where the phase $\theta_m \in$ $[-180^\circ, 180^\circ]$ determines its interference with other modes. The reflectance can be written as

$$R = \left| \sum_{m} \alpha_{m} \right|^{2}$$
$$= \sum_{m} |\alpha_{m}|^{2} + \sum_{i,j,j \neq i} |\alpha_{i}| |\alpha_{j}| \cos(\theta_{i} - \theta_{j})$$
$$= R_{i} + R_{c},$$

where $R_i \equiv \sum_m |\alpha_m|^2$ is the incoherent sum of the modal contributions to the reflectance R, and $R_c \equiv \sum_{i,j,j \neq i} |\alpha_i| |\alpha_j| \cos(\theta_i - \theta_j)$ is the interference term that depends on the relative phases of the modes, i.e, $\cos(\theta_i - \theta_j) > 0$ gives constructive interference, and $\cos(\theta_i - \theta_j) < 0$ the destructive interference. The ratio $C \equiv R/R_i = 1 + R_c/R_i$ quantifies the effect of modal interference on the reflection. For a random input wavefront, the phase difference between α_m are randomly distributed in $[-180^\circ, 180^\circ]$; thus $R_c \approx 0$ and $C \approx 1$.

V. DESTRUCTIVE INTERFERENCE OF MODES TO MINIMIZE REFLECTION

Next we apply the modal analysis to the minimum reflection channel. As an example, let us consider a typical disordered waveguide, whose minimum reflection eigenvalue ρ_1 is close to the ensemble average and it increases with gain. We fix the input wavefront to that of the minimum reflection channel in the absence of gain, and calculate the reflectance R_0 as a function of gain. As shown by the solid line in Fig. 2(a), R_0 increases from 0.37 at $l_t/l_g = 0$ (labeled A1) to 0.59 at $l_t/l_g = 0.0025$ (labeled A2). The top panel in Fig. 2(b) plots the amplitude $|\alpha_m|$ of different modes' contribution to the reflection as a function of the difference between the mode center frequency k_m and the incident light frequency $k, \delta k_m L = (k_m - k)L$. The minimum reflection channel consists mainly of three modes, labeled i–iii, in the vicinity of k, with mode i being the most dominant one.

To illustrate the modal interference at the front surface of the disordered waveguide, we plot α_m in the complex plane in Fig. 2(c) for the reflected light with and without gain. At $l_t/l_g = 0$, the top panel of Fig. 2(c) shows that mode i interferes destructively with modes ii and iii, as their phase differences fall in 90°–180°, leading to $R_c = -0.71 < 0$ and C = 0.34 < 1 (Table I). Thus destructive interference



FIG. 2. (Color online) Formation of the minimum reflection channel by destructive interference of quasinormal modes. (a) Solid (dashed) line shows the evolution of reflectance R_0 (R_g) with gain l_t/l_g when the input wavefront is set to that of the minimum reflection channel at $l_t/l_g = 0$ ($l_t/l_g = 0.0025$). The crossing of the curves reveals that the optimal wavefront for the minimum reflection channel changes with gain. (b) Amplitudes of the contributions of quasinormal modes to the reflectance $|\alpha_m|$ at $l_t/l_g = 0$ (A1, B1) and $l_t/l_g = 0.0025$ (A2, B2) with the input wavefront equal to that of the minimum reflection channel at $l_t/l_g = 0$ (A1, A2) and that of $l_t/l_g = 0.0025$ (B1, B2), respectively. The horizontal axis $\delta k_m = k_m - k$ is the difference between the *m*th mode frequency k_m to the input light frequency k. Three modes in the vicinity of k, labeled i-iii, have major contributions to the reflected light, and their amplitudes grow with gain at a different rate. (c and d) Individual quasinormal modes' contributions α_m are plotted in the complex plane to show their relative phases in four cases of A1, A2, B1, and B2. The degree of destructive interference of the modes is characterized by the value of C given in each panel. The three major modes, i-iii, in A1 and A2 interfere destructively to minimize the reflection. The destructive interference effect, which is weaker in B1, is enhanced by gain in B2.

minimizes the reflected light intensity. When gain is added to the system, the amplitudes $|\alpha_m|$ for modes i–iii increase due to light amplification [A2 in the top panel of Fig. 2(b)], but they continue to interfere destructively with C = 0.32 at $l_t/l_g = 0.0025$ [bottom panel of Fig. 2(c)]. Both the incoherent

TABLE I. Values of reflectance R, the incoherent sum of modal contributions R_i , and the interference term R_c in the cases of A1, A2, B1, and B2 in Fig. 2(a), as well as their ratios.

	R	R_i	R_c
Al	0.37	1.07	-0.71
A2	0.59	1.83	-1.24
A2/A1	1.59	1.71	1.75
B1	0.40	0.46	-0.05
B2	0.53	0.71	-0.19
B2/B1	1.33	1.54	3.80

sum R_i and the interference term R_c have a similar amplitude growth with gain, leading to an increase of the reflectance R_0 (Table I).

In the above analysis, the input wavefront is set to that of the minimum reflection channel without gain, which may not be optimal when there is gain. We calculate the minimum reflection channel from the reflection matrix in the presence of gain, and find the minimum reflection eigenvalue ρ_1 increases slower with gain than R_0 . For example, at $l_t/l_g = 0.0025$, $\rho_1 = 0.53$ [B2 in Fig. 2(a)], while $R_0 = 0.59$ (A2), indicating the input wavefront can be further optimized in the presence of gain to minimize reflection. For comparison, we fix the input wavefront to that of the minimum reflection channel at $l_t/l_g = 0.0025$, and calculate the reflectance R_g when gradually reducing the gain to 0. As plotted by the dashed curve in Fig. 2(a), R_g is higher than R_0 at $l_t/l_g = 0$ (labeled B1), but it grows at a lower rate with gain than R_0 . The modal analysis [bottom panel of Fig. 2(b)] reveals that the minimum reflection channel evolves with gain to impede the growth of reflection due to amplification. Compared to R_0 [top panel of Fig. 2(b)], more modes are excited and contribute to the reflectance R_g . Without gain, the destructive interference of modes in R_g is less efficient, the interference term $R_c = -0.05$ is very small, and the ratio C = 0.88 is closer to 1 [top panel of Fig. 2(d)]. With the introduction of optical gain, the modal interference becomes more destructive, $R_c = -0.19$ and C = 0.79 at $l_t / l_g = 0.0025$ [bottom panel of Fig. 2(d)]. As listed in Table I, the magnitude of the interference term $|R_c| = -R_c$ increases by a factor of 3.8, while the incoherent sum, $|R_i| = R_i$, only by a factor of 1.54. The enhancement of the destructive interference effect makes the growth of R_g slower than R_0 .

VI. REDUCTION OF MINIMUM REFLECTION BY GAIN

The above section shows that the minimum reflection channel adjusts its modal composition to enhance the destructive interference effect in the presence of gain. This slows down the increase of the minimum reflection eigenvalue with gain, which is a typical behavior for most of the disordered configurations. However, in some of the disordered waveguides, e.g, the two shown in Fig. 1(c), the minimum reflection eigenvalue is further reduced with the addition of gain. Below we explain this behavior by the interference of the constituent modes at the front surface of the disordered waveguide.

First we study the random waveguide with the minimum reflection eigenvalue labeled $\rho_1^{(1)}$ in Fig. 1(c). Figure 3(a) shows that the input wavefront for the minimum reflection channel with gain is highly correlated to that without gain. This means the minimum reflection channel is barely modified in the presence of gain. Nevertheless, the reflectance drops with increasing gain, even when the input wavefront is fixed to that of the minimum reflection channel in the absence of gain. The modal decomposition reveals that the minimum reflection channel without gain is dominated by one mode, labeled mode i in Fig. 3(b), which is slightly detuned from the frequency of input light. Another mode, labeled mode ii, has the frequency closest to the input light but its contribution to the reflected light is much less significant. Such differences can be understood from the mode's spatial field profile $|E_z(x, y)|$ and



FIG. 3. (Color online) Further reduction of the minimum reflection by gain. (a) The correlation C_R between the input wavefront for the minimum reflection channel with gain to that without gain, showing they are highly correlated. The reflectance R_0 with the input wavefront equal to that of the minimum reflection channel at $l_t/l_g = 0$ almost coincides with R_g with the input wavefront set to that of the minimum reflection channel at $l_t/l_g = 0.0025$. Both drop with increasing gain l_t/l_g . (b) Amplitudes of modes' contributions $|\alpha_m|$ to the reflection without gain [C1 in (a)] and with gain [C2 in (a)], showing the major contributions from four modes labeled i–iv. (c) Spatial distribution of the electric field amplitude $|E_z(x,y)|$ for modes i and ii in (b). (d) Without gain $l_t/l_g = 0$, the modes interfere destructively to form the minimum reflection channel, C = 0.11 (top panel). With gain $l_t/l_g = 0.0025$, the destructive interference of modes is further enhanced; *C* is reduced to 0.05 (bottom panel).

spectral width k_i (the imaginary part of the eigenfrequency). As shown in the top panel of Fig. 3(c), mode i is spatially concentrated close to the front surface of the disordered waveguide, resulting in a large leakage rate. Consequently, mode i has a broad spectral width that exceeds the detuning of its center frequency from the input frequency, $k_i > \delta k_m$. The spectral overlap of mode i with the input light leads to an efficient excitation of mode i by the input light, and mode i's proximity to the front surface of the waveguide enhances its contribution to the reflected light. In contrast, mode ii penetrates deeper into the waveguide and has a smaller leakage rate; thus its contribution to the reflected light is much less [bottom panel of Fig. 3(c)].

With the introduction of gain, mode ii experiences stronger amplification than mode i due to its lower leakage rate, and its contribution to the reflection grows faster than mode i [Fig. 3(b)]. As shown in top panel of Fig. 3(d), modes i and ii have a phase difference of $\sim 180^{\circ}$, so they interfere destructively. When there is no gain, the relatively large difference in their amplitudes makes their interference insignificant. In the presence of gain, the imbalance of their amplitudes is reduced, as a result of the faster growth of mode ii, and their destructive interference becomes more significant. This means

TABLE II. Values of reflectance R, the incoherent sum of modal contributions R_i , and the interference term R_c in the cases of C1 and C2 in Fig. 3(a), as well as their difference.

	R	R_i	R_c
C1	0.067	0.60	-0.54
C2	0.035	0.68	-0.65
C2-C1	-0.032	0.08	-0.11

the differential amplification of individual modes can enhance the degree of destructive interference, as confirmed by the reduction of *C* from 0.11 at $l_t/l_g = 0$ to 0.05 at $l_t/l_g = 0.0025$ [Fig. 3(d)]. More quantitatively, the interference term R_c decreases from -0.54 at $l_t/l_g = 0$ to -0.65 at $l_t/l_g = 0.0025$, while the incoherent sum R_i increases from 0.60 to 0.68 (Table II). The increase of R_i is not sufficient to compensate for the reduction of R_c ; thus the reflectance *R* decreases with gain.

Next we investigate the second disordered waveguide configuration shown in Fig. 1(c). Similar to the first one, the input wavefront for the minimum reflection channel with gain is nearly identical to that without gain [Fig. 4(a)] (Table III). The reflectance with the input wavefront fixed to that of the minimum reflection channel without gain R_0 is almost the same as the reflectance with the input wavefront set to that



FIG. 4. (Color online) Another example showing the minimum reflection eigenvalue decreases with gain. (a) The correlation C_R between the input wavefront for the minimum reflection channel with gain to that without, showing they are highly correlated. The reflectance R_0 for the input wavefront fixed to that of the minimum reflection channel without gain and the reflectance R_g for the input wavefront fixed to that of the minimum reflection channel without gain and the reflectance R_g for the input wavefront fixed to that of the minimum reflection channel with decrease with increasing gain. (b) Amplitudes of modes' contributions $|\alpha_m|$ to the reflection without gain [D1 in (a)] and with gain [D2 in (a)], showing the major contributions from five modes labeled i–v. (c) Without gain $(l_t/l_g = 0)$, the modes interfere destructively to form the minimum reflection channel, C = 0.49. (d) With gain $l_t/l_g = 0.0025$, the destructive interference effect is further enhanced and *C* is reduced to 0.31.

TABLE III. Values of reflectance R, the incoherent sum of modal contributions R_i , and the interference term R_c in the cases of D1 and D2 in Fig. 4(a), as well as their difference.

	R	R_i	R_c
D1	0.10	0.21	-0.11
D2	0.08	0.27	-0.19
D2-D1	-0.02	0.06	-0.08

of the minimum reflection channel with gain R_g ; they both decrease as gain increases. The modal decomposition reveals that there are more modes contributing to the reflected light [Fig. 4(b)], compared to the previous two cases [Figs. 2 and 3]. These modes interfere destructively to form the minimum reflection channel when there is no gain [Fig. 4(c)], and the destructive interference effect is further enhanced by adding gain to the system [Fig. 4(d)]. Hence, the reduction of the reflectance due to enhanced destructive interference effect dominates over the increment due to the growth of the modes' amplitudes with gain, leading to a further reduction of the minimum reflectance.

VII. CONCLUSION

In summary, we present a numerical study on the minimum reflection channels in disordered waveguides and their modification as a result of the introduction of optical gain. A modal analysis reveals that the minimum reflection channel is formed by destructive interference of quasinormal modes at the front surface of the random media. In most of the disordered configurations, the minimum reflection eigenvalue increases with gain; however, the minimum reflection channel can adjust its input wavefront to enhance the destructive interference of modes and impede the growth of reflectance with gain. In some of the disordered waveguides, the differential amplification of the modes makes their destructive interference effective enough that it dominates the amplitude growth of the modes, causing the reflectance to decrease with gain. Therefore, it is possible to further reduce light reflection from a strong scattering medium by adding optical gain to it. This counterintuitive behavior illustrates the interplay between interference and amplification in a disordered system. For practical applications it would be useful to find a way of predicting a priori the disordered configurations that lead to a further reduction of the reflectance by adding gain, and also the probability of such configurations. This is beyond the scope of the current work and will be studied in the future.

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APPENDIX: FIELD DECOMPOSITION BY QUASINORMAL MODES

To decompose the electric field distribution inside the random system by the quasinormal modes, we use the



FIG. 5. (Color online) Field decomposition by quasinormal modes. (a) The spatial distribution of the electric field amplitude $|E_s(x,y)|$ inside the random waveguide with an input wavefront corresponding to the minimum reflection channel without gain in Fig. 2(a). (b) The reconstructed field distribution by modal decomposition $|E_c(x,y)|$. The cross-section integrated intensity $I(x) = \int |E(x,y)|^2 dy$ and the phase of the electric field E(x,y = 0) between the original and reconstructed fields are shown in (c) and (d), respectively. The relative difference between the two field profiles is measured by $\int \int |E_c(x,y) - E_s(x,y)|^2 dx dy / \int \int |E_s(x,y)|^2 dx dy = 2.14 \times 10^{-5}$.

finite-difference-frequency-domain (FDFD) method [66] to calculate the modes with incoming and outgoing wave boundary conditions. In particular, we use the "Eigenfrequency" solver provided by a commercial software COMSOL [66] to compute the eigensolutions to the wave equation, after inputting the spatial distribution of the dielectric constant. Figure 5(a) shows the spatial distribution of the electric field amplitude $|E_S(x, y)|$ inside the disordered waveguide for the minimum reflection channel without gain in Fig. 2(a). The electric field inside the random system is decomposed by the quasinormal modes of the passive system:

$$E_C(x,y) = \sum_m a_m u_m(x,y) + \sum_m b_m v_m(x,y),$$

where u_m (v_m) is the *m*th resonant mode with a purely outgoing (incoming) wave boundary condition. The decomposition involves finding the coefficients a_m and b_m by fitting $E_C(x, y)$ to $E_S(x, y)$ using the nonlinear curve-fitting function lsqcurvefit in MATLAB. After the decomposition, the reconstructed field profile in Fig. 5(b) matches well the original one in Fig. 5(a). The good agreement is further shown in the cross-section integrated intensity $I(x) = \int |E(x,y)|^2 dy$ and the phase of the electric field E(x, y = 0) in Figs. 5(c) and 5(d). The error of the fitting, characterized by the relative difference between $E_S(x, y)$ and $E_C(x, y)$, is calculated by $\int \int |E_C(x, y) - E_S(x, y)|^2 dx dy / \int \int |E_S(x, y)|^2 dx dy =$ 2.14×10^{-5} . MINIMUM REFLECTION CHANNEL IN AMPLIFYING ...

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