## Giant field enhancement in electromagnetic Helmholtz nanoantenna

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Inspired by the acoustic Helmholtz resonator, we propose a slit-box electromagnetic nanoantenna able to concentrate the energy of an incident beam into surfaces a thousand times smaller than with a classical lens. This design produces a giant electric field enhancement throughout the slit. The intensity enhancement reaches  $10^4$  in the visible range up to  $10^8$  in the THz range even with focused beams, thanks to an omnidirectional reception. These properties could target applications requiring extreme light concentration, such as surface-enhanced infrared absorption, nonlinear optics, and biophotonics.

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### I. INTRODUCTION

Optical antennas are very useful to funnel light from free space into deep-subwavelength volumes resulting in large electric field enhancements [1-8]. They have a wide range of applications, including surface-enhanced Raman scattering (SERS) [9], photovoltaics and photodetection [10], nonlinear optics [11], biosensing [12], surface-enhanced infrared absorption (SEIRA) [13–15], and thermal emission [16]. The important properties of an antenna are its cross section that determines its coupling to the external field, its angular acceptance that allows further enhancement of the field with a focused beam, and the volume in which the field is enhanced, which is critical for light-matter-interaction-based applications. Intensity enhancement up to  $10^3$  was observed using subwavelength particles [17] and an enhancement of  $10^8$  has been demonstrated in atomic thin gaps in metal for millimeter waves [18]. Inspired by radio-frequency designs, various nanoantennas have been engineered to improve the field enhancement in larger volumes. For instance, Yagi-Uda antenna have been adapted to optics, but are limited by their directionality [19–21]. Bow-tie antenna are less directional, but only enhance the field in hot spots [22,23]. Eventually, quarter-wave antennas such as slits or metal-insulator-metal patches have been shown to efficiently collect light, thanks to a funneling effect with a near- $\lambda$  cross section and a large angular acceptance [24–27]. Nonetheless, the enhancement of the field is mainly limited by the aperture size of these quarter-wave antenna, and is not homogeneous within their length. Recently, inspired by acoustic design [28], an optical Helmholtz resonator made of a metallic slit box has been demonstrated [29]. The resonance wavelength  $\lambda$  of the optical Helmholtz resonator is tuned independently by the slit (width w, height h) and the cavity.

In this paper, we show that the slit-box Helmholtz resonator is able to omnidirectionally funnel all the light through its aperture regardless of its width, leading to a millionfold electric field intensity enhancement in a hot volume. Based on a quasistatic model, we demonstrate on a wide spectral range

 $(1-100 \ \mu m)$  that the giant enhancement factor is obtained within the volume of the slit driven by the ratio  $\lambda^2/(hw)$ . This enhancement factor only depends slightly on the angle of incidence, which permits one to use this antenna at the focal spot of a classical lens to further strongly enhance the electric field intensity. This giant field intensity enhancement should be instrumental for devices based on SEIRA or nonlinear optics which use a focused beam.

## **II. OPTICAL HELMHOLTZ RESONATOR**

The optical Helmholtz resonator is presented in Fig. 1(a). It consists of a box (height  $h_b$ , width  $w_b$ ) and a slit (height  $h_s$ , width  $w_s$ ) and is long enough along the y direction to be considered as infinite. The structure is made of gold whose dielectric function is computed from a Drude model,  $\varepsilon_{\rm Au}(\lambda) = 1 - [(\lambda_p/\lambda + i\gamma)\lambda_p/\lambda]^{-1}$ , which fits well with the experimental data in the infrared domain for  $\lambda_p = 159$  nm and  $\gamma = 0.0077$  [30].

Exact Maxwell computations [31] of this slit-box resonator are performed for a first structure such that  $w_b = 49$  nm,  $h_b =$ 49 nm,  $w_s = 2.5$  nm, and  $h_s = 12$  nm periodically repeated with a period d = 800 nm. Its reflectivity spectrum is plotted in Fig. 1(b) between 1 and 2.4  $\mu$ m. It exhibits a nearly total absorption resonance at  $\lambda_r = 1.7 \ \mu m$ .

#### **III. FIELD ENHANCEMENT FROM NEAR IR TO THZ**

# A. Examples of giant field enhancement

The distribution of the electric intensity  $(|\mathbf{E}|^2)$  normalized by the incident intensity  $(|\mathbf{E}_0|^2)$  in the structure is presented in Figs. 2(a) and 2(b) at different zoom levels and shows that a field intensity enhancement of  $10^5$  is reached with this structure. In Fig. 2(c), it is shown that this enhancement is confined to the slit volume: the field intensity enhancement stays uniform along the height of the slit, but outside its volume the electric field intensity quickly drops by losing four orders of magnitude over about 50 nm. It is noteworthy that this profile of the electric field departs from the behavior of a Fabry-Perot slit, and it adds to the fact that the slit-box resonator does not exhibit harmonics features [32]. The quality

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FIG. 1. (Color online) (a) Two-dimensional Helmholtz resonator infinite in the **y** direction, with a slit of height  $h_s$  and width  $w_s$  and a box of width  $w_b$  and height  $h_b$ . (b) Reflectivity spectrum of a grating of the Helmholtz slit-box resonator with a period  $d = 0.8 \ \mu\text{m}$  for a normally incident plane wave. The Helmholtz resonator has the following parameters:  $w_b = 49 \ \text{nm}$ ,  $h_b = 49 \ \text{nm}$ ,  $w_s = 2.5 \ \text{nm}$ , and  $h_s = 12 \ \text{nm}$ , and exhibits an almost total absorption for  $\lambda_r = 1.7 \ \mu\text{m}$ .

factor is  $Q \simeq 10$  for a resonance wavelength of  $\lambda_R = 1.7 \ \mu m$ , as shown in Fig. 2(d).

Very strong field intensity enhancements can be reached not only in the infrared range, but in the whole spectrum from visible to THz domain. To illustrate this, two other structures have been designed to exhibit a strong field enhancement at the wavelengths of 15 and 200  $\mu$ m. The second structure is made of a square box where  $w_b = h_b = 485$  nm and  $w_s =$ 2 nm,  $h_s = 30$  nm is simulated on a periodic grating (period  $d = 3 \mu$ m) and exhibits a total absorption at a resonance wavelength of 15  $\mu$ m, where a 10<sup>6</sup> intensity enhancement is observed. Another structure with a box such that  $w_b = h_b =$ 5.7  $\mu$ m,  $w_s = 4$  nm,  $h_s = 80$  nm, and  $d = 50 \mu$ m shows a  $10^8$ -fold intensity enhancement at a resonance wavelength of 200  $\mu$ m.

Theses enhancement factors for the Helmholtz structures can be compared to the literature showing theoretical predictions of high field enhancement in large volumes as we do not compare to enhancement soccurring in hot spots. In the near infrared, an enhancement factor of  $10^5$  is observed, whereas the literature usually shows a  $10^3$  enhancement factor for the near-IR or visible wavelengths [8,13,15,17]. In the far IR, we demonstrate a  $10^6$  enhancement factor compared to  $10^4$  in the literature [33] and, finally, we observe  $10^8$  vs  $10^6$  in the THz domain [34].

As a matter of fact, these record values are obtained thanks to exact electromagnetic computations, using a realistic permittivity of gold [30]. However, the geometry of the structure exhibits high aspect ratios with nanometric slits. A real structure might thus yield lower enhancement values due to technological imperfections.

#### B. Model for the field intensity enhancement

It has been shown that the slit-box structure is fairly well described by a quasistatic model: the slit behaves as a capacitor and the box behaves as an inductance [29]. Thus, for an arbitrary length T of the structure in the y direction, the capacitance of the slit can be written as  $C_{\text{slit}} = \varepsilon_0 \varepsilon_s \frac{h_s T}{w_s}$ and the inductance of the cavity can be written as  $L_{\text{box}} = \mu_0 \frac{w_b h_b}{T}$ . The resonance wavelength is eventually expressed as  $\lambda_r \simeq 2\pi \sqrt{\varepsilon_s w_b h_b (h_s + w_s)/w_s}$ , where  $\varepsilon_s$  is the permittivity of the dielectric material filling the slit. However, when using



FIG. 2. (Color online) The electric field intensity enhancement is shown at different scales for a normally incident plane wave. (a) Field intensity enhancement in the Helmholtz resonator at  $\lambda = 1.7 \ \mu m$ . (b) Close view in the vicinity of the slit. (c) Field intensity enhancement along the *z* axis, at the center of the structure (x = 0). A rather homogeneous enhancement of 10<sup>5</sup> is found in the whole slit volume. (d) The field intensity enhancement in the center of the slit is plotted at different wavelengths. We see that  $\lambda = 1.7 \ \mu m$  is a resonance wavelength that provides a maximal enhancement. The quality factor of this resonance is about 10.

Helmholtz structures made of real metal at near-infrared frequencies, the previous model should be corrected as

$$\lambda_r = 2\pi A \sqrt{\varepsilon_s w_b h_b \frac{h_s + K w_s}{w_s} + B \lambda_p}.$$

The coefficients have been fitted on the spectral range between 1.5 and 15  $\mu$ m as A = 1.16, B = 4.4, and K = 1.1.

We now derive the enhancement factor of the resonator. Let us first introduce the quality factor of the resonator which links the energy dissipated during one period to the energy stored in the resonator:

$$\frac{Q_{nr}}{2\pi} = \frac{U_{\text{stored}}}{U_{\text{dissipated per period}}}.$$
 (1)

We now give an explicit form of the energy stored in the resonator by evaluating the maximum energy stored in the capacitor. Given the link between the electric field  $|\mathbf{E}|$ amplitude and the maximum difference of electric potential V in the capacitor,  $|V| \simeq |\mathbf{E}|w_s$ , the stored energy in the resonator for one spatial period along the x direction and a length T along the y direction is

$$U_{\text{stored}} = \frac{1}{2} C_{\text{slit}} |\mathbf{E}|^2 w_s^2 = \frac{\varepsilon_0 \varepsilon_s |\mathbf{E}|^2 h_s w_s T}{2}.$$
 (2)

We now express the energy dissipated during one cycle. In the stationary regime, the power dissipated in a spatial period of area dT is equal to the incident power given by

$$P_{\text{incident}} = \frac{|\mathbf{E}_0|^2 dT}{2Z_0},\tag{3}$$

where  $Z_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}}$  is the characteristic impedance of vacuum and **E**<sub>0</sub> is the amplitude of the incoming plane wave.

In the stationary regime, the incident power is equal to the dissipated power. It follows that the dissipated energy during one temporal period is given by

$$U_{\text{dissipated per period}} = \frac{\varepsilon_0 A |\mathbf{E}_0|^2 \lambda dT}{2},$$
 (4)

where A is the absorption coefficient of the structure.

This allows one to express the field intensity enhancement G thanks to Eqs. (1), (2), and (4):

$$G = \frac{|\mathbf{E}|^2}{|\mathbf{E}_0|^2} = \frac{Q_{nr}}{2\pi} \frac{A\lambda d}{\varepsilon_s h_s w_s}.$$
 (5)

In the optimal situation where a perfectly impedancematched structure is designed (A = 1) and for which the cross section is maximum  $(d = \lambda)$ , the maximum field intensity enhancement  $G_{\text{max}}$  in the slit at the resonance can be expressed as

$$G_{\max} = \frac{|\mathbf{E}_{\max}|^2}{|\mathbf{E}_0|^2} = \frac{Q_{nr}}{2\pi} \frac{\lambda^2}{\varepsilon_s h_s w_s}.$$
 (6)

In Fig. 3, the enhancement factor has been plotted for variously shaped structures ( $\varepsilon_s = 1$ ) exhibiting resonances from the near infrared to the far infrared and is plotted as a function of *G*. This figure shows the good agreement between this analytic model and the values obtained through numerical simulations in the different domains of frequencies.



FIG. 3. (Color online) Simulations for different sizes of structure have been realized with  $\varepsilon_s = 1$ . For each structure, the enhancement factor  $G_{\text{simulations}}$  for a plane incident wave is computed and compared to the analytic model  $G_{\text{analytic}}$  expressed in Eq. (5) as a function of the geometry. We see a strong correlation between the simulation results and the formula provided in the paper for the different domains of frequency. Three sets of simulations have been made, i.e., the first in the near-IR domain ( $\lambda$  between 2 and 8  $\mu$ m), the second in the medium-IR domain ( $\lambda$  between 10 and 25  $\mu$ m), and the last in the far-IR domain ( $\lambda$  between 30 and 80  $\mu$ m).

It must be emphasized that at a given wavelength, the field enhancement is set by the area of the slit. Higher enhancement factors are obtained at larger wavelength and for smaller slits. The quality factor of the resonance for simulated structures was between 5 and 15. With the resonance wavelength being set by other geometric parameters [29], this model gives the rules to design a Helmholtz structure exhibiting a given field enhancement at a given wavelength within the simulated range.

### IV. POLARIZATION-INDEPENDENT DESIGN OF THE GIANT FIELD ENHANCEMENT

A potential drawback of the two-dimensional (2D) resonator with a single slit, introduced in Ref. [29], is its polarization dependence. To make the Helmholtz structure independent of the light polarization on a normal incidence, one Helmholtz structure along the x axis can be crossed with one structure along the y axis, as can be seen in Fig. 4(a). For this structure with geometric dimensions similar to the structures presented above (in Figs. 1 and 2), the electromagnetic computations made with COMSOL multiphysics show that the resonance wavelength is redshifted from 1.7  $\mu$ m for the 2D resonator to 1.8  $\mu$ m for the 3D resonator.

At the resonance wavelength, the field intensity enhancement for a linearly polarized wave equally distributed between the x axis and the y axis is plotted in Figs. 4(b) and 4(c). In this situation, the electric intensity is enhanced by at least 35 000 (between two slit intersections) and up to  $10^5$  at the intersection between the two slits.

When the light is normally incident and polarized along the x axis, the field enhancement is of the same magnitude as in the 2D structure and is localized in the slit along the y direction. For a normally incident plane wave equally distributed along the two axes, one-half of the energy corresponds to the x



FIG. 4. (Color online) (a) Polarization-independent structure which is a combination of two crossed Helmholtz structures. For a polarization-independent structure, having similar dimension as the structure studied above, the resonance wavelength is slightly shifted to 1.8  $\mu$ m. (b) The field intensity enhancement is plotted at the middle of the slit height and near the intersection of the two structures, for the incident field **E**<sub>0</sub> specified on the figure (equally distributed between the *x* and *y* axis). (c) The intensity enhancement along the *x* axis and average along the *y* axis is plotted for one period. It shows that the field enhancement is maximal at the intersection where a hot spot appears. Elsewhere inside the slit, the field intensity enhancement is above 35 000 and increases up to 70 000.

component of the electric field, and the other half corresponds to its y component. In this case, each component produces a slightly smaller intensity enhancement at the extremity of the slit compared to the half of the intensity enhancement provided by the 2D structure; however, the two contributions are summed at the intersection of the slits, showing that this design could still be used for strong intensity enhancement with fields with any polarization.

### V. ANGULAR ACCEPTANCE AND LIGHT FOCUSING

The angular dependence of the enhancement is studied in Fig. 5. The general configuration of conical incidence is described in Fig. 5(a); the light is impinging on the antenna with an angle  $\vartheta$  in the plane defined by the azimuthal angle  $\varphi$ and is polarized so that the magnetic field is in the y-z plane. The enhancement G as a function of both angles is plotted in Fig. 5(b). It remains above  $5 \times 10^4$  for angle of incidence



FIG. 5. (Color online) The electric field intensity enhancement is computed for an incident plane wave (polarized parallel to the slits) with different angles of incidence and different planes of incidence. The structure is the same as described in the paper. (a) The plane of incidence is rotated by an angle  $\varphi$ ; the angle of incidence is  $\vartheta$ . (b) The results of the field intensity enhancement are represented with polar coordinates on the right. The field intensity enhancement remains above  $5 \times 10^4$  for angles of incidence below  $40^\circ$ ; it is above  $10^4$  for angle of incidence below  $65^\circ$ .

below  $35^\circ$ , which demonstrates the broad acceptance of the resonator.

Due to the high angular tolerance of the structure, the enhancement *G* would only be slightly reduced when the structure is placed at the focal spot of a lens. In this case, the electric field intensity  $|\mathbf{E}|^2$  would be similar to the one obtained if, beyond the limits of diffractive optics, a beam of given power was focused in a spot of area  $\lambda^2/G$  instead of  $\lambda^2$ . It is noteworthy that this intensity is uniformly obtained in a "hot volume" of height  $h_s$  and area  $\lambda w_s \gg \lambda^2/G$ .

The behavior of the slit-box structure under a focused beam has been simulated [32]. The streamlines of the Poynting vector plotted at a large scale in Fig. 6(b) show that the incident energy is focused into a beam limited by diffraction [see Fig. 6(c)], where 90% of the energy is concentrated in a  $\lambda$ -wide spot (here the wavelength is  $\lambda = 1.7 \mu$ m). Next, in the near field [z < 500 nm; see Fig. 6(d)], all of the focused energy is funneled towards the opening of the resonators where it is absorbed on the metallic sidewalls. In fact, given the size of the focal spot, 60% of the total energy is absorbed by the central resonator, while the remaining energy is equally absorbed by the two surrounding resonators. Since the incoming energy goes through the slit of the resonator, the electric field intensity is still strongly enhanced in the whole slit volume.

Focusing light onto the structure produces a stronger incident field that is further enhanced into the tiny slit by the mechanism described above; the giant enhancement factor is also unchanged with focused beams. Thus, the resulting



FIG. 6. (Color online) (a) A beam is focused on the Helmholtz structure with  $w_s = 2.5$  nm,  $h_s = 12$  nm,  $w_b = h_b = 49$  nm, and  $d = 800 \ \mu$ m. (b) Streamlines of the beam focused into the structure; the beam waist is about  $\lambda = 1.7 \ \mu$ m wide. (c) The beam is focused on one individual structure that collects about 60% of the incoming energy. The remaining energy is fully collected by the neighboring slits. (d) Streamlines of the Poynting vector in the vicinity of the structure, showing that the magnetoelectric interference redirects the incident energy inside the resonator [24].

electric field intensity after focusing light onto one slit would be stronger than the one obtained for a plane incident wave carrying the same energy.

## VI. CONCLUSION

The 2D optical Helmholtz resonator allows one to funnel nearly all of the incident energy through the arbitrarily narrow aperture of the slit, leading to giant enhancement of the electric field in the whole slit volume, typically two orders of magnitude higher than previously demonstrated in the literature. It is well described by a quasistatic model where the slit behaves as a capacitor and the cavity behaves as an inductance, and is only coupled to the free space through the capacitor. This model permits one to derive the enhancement factor within the volume of the slit, as a function of the slit area and the quality factor. This enhancement factor only slightly depends on the angle of incidence, which permits one to use this antenna at the focal spot of a classical lens to further strongly enhance the electric field intensity. These appealing properties are very promising for light-matter interactions such as in photodetection, SERS, SEIRA, and nonlinear optics.

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