

**Nonthermal and purely electronic resistive switching in a Mott memory**

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Mott insulator to metal transitions under an electric field are currently the subject of numerous fundamental and applied studies. This puzzling effect, which involves nontrivial out-of-equilibrium effects in correlated systems, is indeed at play in the operation of a new class of electronic memories, the “Mott memories.” However, the combined electronic and thermal effects are difficult to disentangle in Mott insulators undergoing such transitions. We report here a comparison between the properties under an electric field of a canonical Mott insulator and a model built on a realistic two-dimensional resistor network able to capture both thermal effects and electronic transitions. This comparison made specifically on the family of narrow gap Mott insulators  $AM_4Q_8$  ( $A = \text{Ga}$  or  $\text{Ge}$ ;  $M = \text{V}$ ,  $\text{Nb}$  or  $\text{Ta}$ ; and  $Q = \text{S}$  or  $\text{Se}$ ) unambiguously establishes that the resistive transition experimentally observed under an electric field arises from a purely electronic mechanism.

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The possibility of inducing an insulator to metal transition (IMT) in correlated compounds by application of electrical fields  $E$  [1–4] is currently receiving considerable attention due to the potentially new physics involved as well as for the possible applications in electronics [5,6]. On the fundamental side, an  $E$ -controlled IMT may result from emerging out-of-equilibrium mechanisms [7,8] going beyond the well established bandwidth- and filling-controlled IMT in Mott insulators [9]. On the applicative side, the new class of “Mott memories” based on this  $E$ -controlled IMT property, also referred to as resistive switching, [10], is a promising candidate for the next generation of electronic memories [11–13].

A central issue in this field is the identification of basic mechanisms leading to resistive transition in correlated insulators. Recent research has shown that they can be sorted into three groups: thermal effects, electric-field-assisted ionic migration, and electronic effects. In the first group, Joule heating can trigger a sharp resistive transition in materials undergoing an IMT driven by temperature. Archetypical examples are the celebrated Mott insulators  $\text{VO}_2$  [9,14–23] and  $\text{NbO}_2$  [24]. In these compounds, the strong drop of electrical resistivity at the IMT temperature is accompanied by a change in lattice symmetry. In a second group, migration of ions (for example, oxygen atoms) in a correlated material can lead to a local nonstoichiometry and therefore to a local filling-controlled IMT that destabilizes the Mott insulating (MI) state [6,25]. In such systems, an electric-field-assisted displacement of ions occurs at the interfaces [26] and leads to bipolar resistive transition. The third group comprises purely electronic mechanisms, such as the theoretically predicted destabilization

of the correlated state in strong electric field [7], also referred to as Zener dielectric breakdown of Mott insulators [8]. In such a mechanism, the IMT occurs without changes in the lattice symmetry [27]. Recently, an additional purely electronic mechanism of resistive transition has emerged [2] from studies of the prototypical family of Mott insulators  $AM_4Q_8$  ( $A = \text{Ga}$ ,  $\text{Ge}$ ;  $M = \text{V}$ ,  $\text{Nb}$ ,  $\text{Ta}$ ;  $Q = \text{S}$ ,  $\text{Se}$ ,  $\text{Te}$ ) [28]. In these compounds, a resistive transition occurs above a moderate threshold electric field  $E_{\text{th}}$  in the 1–10 kV/cm range. The observation of an  $E_{\text{th}}$  vs  $E_{\text{gap}}$  dependence, very similar to the classical semiconductors, leads us to propose that an electronic avalanche is the driving force of the resistive transition in these Mott insulators [2]. The other mechanisms of resistive transition thus far identified seem indeed unsuitable for the  $AM_4Q_8$  compounds. The unipolar and noninterfacial character of the resistive transition easily excludes mechanisms related to ionic migration. Conversely, thermal effects are trickier to rule out. On one hand,  $AM_4Q_8$  compounds do not display any IMT driven by temperature as observed in  $\text{VO}_2$ . On the other hand,  $AM_4Q_8$  compounds display a strong temperature-dependent resistivity associated with a Mott-Hubbard gap of 0.1–0.3 eV. In this context, the possibility that the observed resistive transition results from the sudden formation of a hot and highly conductive filament induced by Joule heating [29] cannot be dismissed out of hand.

In this paper, we show that the resistive transition cannot arise from Joule heating effects in  $AM_4Q_8$  compounds and that these narrow gap Mott insulators are a prototypical system for the study of purely electronic resistive switching in correlated systems. We compare key experimental observations with calculations performed for both the hot filament and an electric-field-driven collapse of the Mott state scenarios. The experimental results are in clear disagreement with the thermal model characteristics, whereas they present all the features

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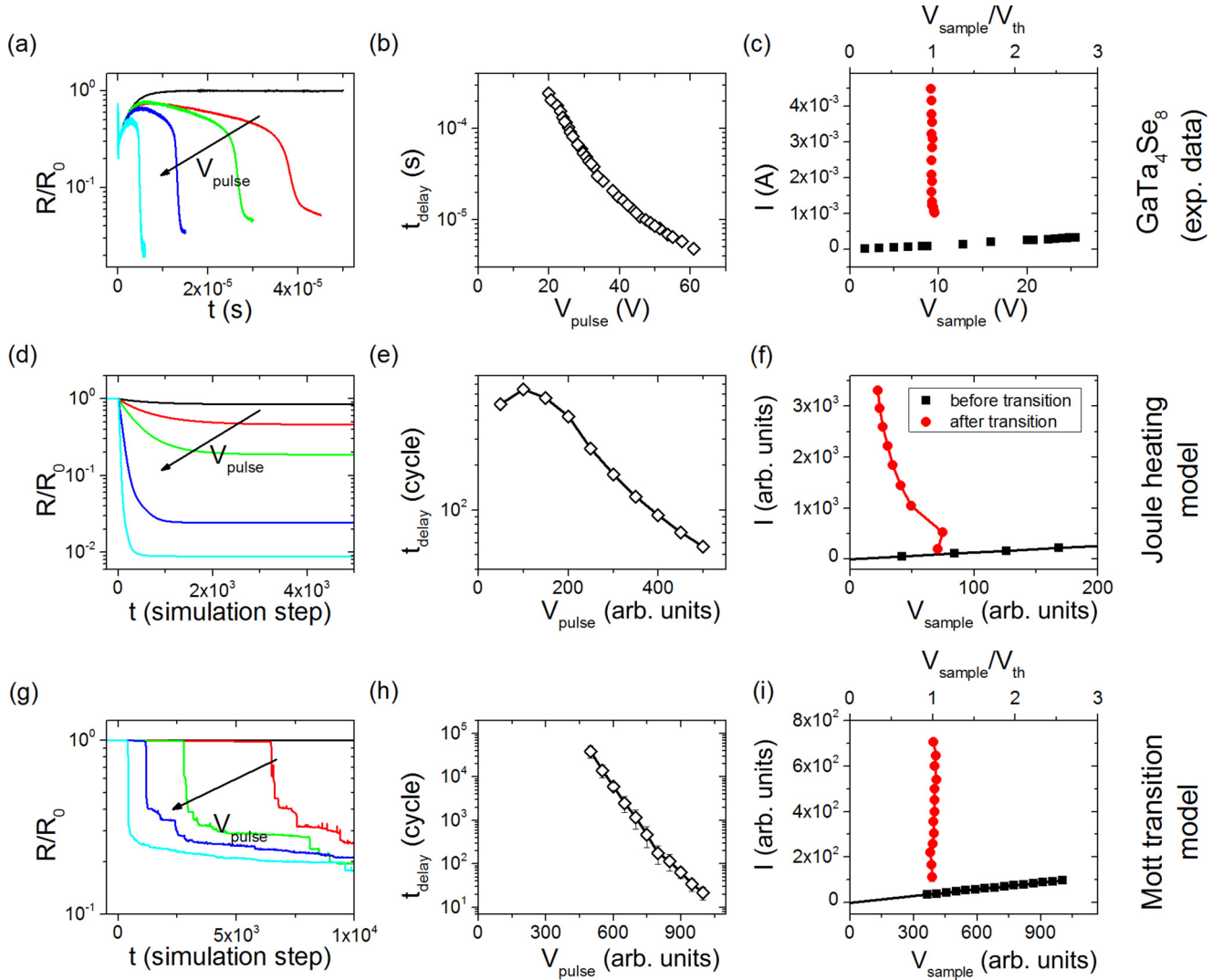


FIG. 1. (Color online) Comparison between the experimental data (a)–(c) and the two studied models, the Joule heating model (d)–(f), and the Mott transition model (g)–(i) [37]. The measurements were conducted in a GaTa<sub>4</sub>Se<sub>8</sub>-based device at 77 K. For each case we present the variation of the resistance of the device in time for increasing  $V_{\text{pulse}}$ , the delay elapsed between the application of  $V_{\text{pulse}}$ , and the switching (if it occurs) and the I–V characteristic before and after the switching. The curves presented in (a) correspond to  $V_{\text{pulse}}$  values of 6, 40, 44, 56, and 86 V. The duration of pulses was limited to 50, 30, 15, and 6  $\mu\text{s}$  to avoid overheating of the sample. For the thermal model, the  $t_{\text{delay}}$  (e) is considered when the decrease of resistance is half of the final value, and (f) plots the current and the voltage at the beginning of the simulations and after  $10^5$  cycles, where the system was always in stationary regime. The curves in (d) correspond to  $V_{\text{pulse}}$  values of 50, 100, 150, 300, and 500 arb. units and the curves presented in (g) to  $V_{\text{pulse}}$  values of 400, 600, 650, 700, and 750 arb. units.

predicted by a purely electronic model. This strongly suggests that the resistive switching in these systems is primarily driven by electronic rather than thermal effects.

The phenomenology of the resistive switching in the  $AM_4Q_8$  compounds was comprehensively reported in previous publications [30–32]. The typical experiments relevant to this study are performed on  $AM_4Q_8$  single crystals with two metal contacts on opposite faces. Initially the system is in an MI state, with a resistance  $R_0$ . A voltage pulse  $V_{\text{pulse}}$  is applied to the sample through a series limiting resistor  $R_L \approx R_0/10$ . Above a threshold field of a few kilovolts per centimeter, the sample undergoes a sharp decrease of its resistance during the pulse (the electric field is defined as the voltage on the sample,  $V_{\text{sample}}$ , divided by the distance

between the electrodes,  $d$ ). This effect is called *volatile* resistive switching because the resistance of the sample returns to its initial value after the pulse. For even higher electric fields (about three to five times the threshold field), the resistive switching becomes *nonvolatile*, meaning that the sample remains in a low resistance state after the electric pulse. In the rest of this work, we focus only on the volatile transition of the  $AM_4Q_8$ -based devices as both the volatile and the nonvolatile resistive switching derive from the same initial physical mechanism [31].

Figure 1(a) displays the change in resistance of the GaTa<sub>4</sub>Se<sub>8</sub> crystal ( $R/R_0$ ) during the application of voltage pulses [33]. Resistive switching is observed for voltages that exceed the threshold voltage  $V_{\text{th}} \approx 10$  V, corresponding to

a threshold field  $E_{th} \approx 2.5$  kV/cm ( $E_{th} = V_{th}/d$ ). The time  $t_{delay}$ , at which the sharp resistive switching occurs, decreases when the voltage pulse increases [see Fig. 1(b)]. The sample voltage  $V_{sample}$  after the resistive switching is always the same and is equal to  $V_{th} \approx 10$  V whatever the voltage applied to the sample before the resistive switching. Consequently, the current flowing through the sample  $I$  after the switching varies in a large extent. Figure 1(c) shows the current-voltage characteristic, which is highly non-Ohmic and appears as an almost vertical line in the “transited” state. As we shall see, this voltage stabilization is a key feature in our study.

To address the question of whether the creation of a hot filament by Joule heating could account for the resistive switching in  $AM_4Q_8$  compounds, an experimental approach could be envisioned. For example, a “tour de force” experiment was recently performed by using the fluorescence spectra of rare-earth doped micron sized particles as local temperature sensors at the surface of a  $VO_2$  thin layers [16]. However, addressing the question of a hot filament is much more demanding in our case, since it also requires both a submicron spatial resolution in the bulk of the  $AM_4Q_8$  single crystals and also a microsecond time resolution. As such experimental approaches are, to our knowledge, out of reach, we have thus adopted a strategy based on thermal modeling. We have first tested the hypothesis of the formation of hot conductive filaments within a thermal model based on the activated dependence of the resistivity in these compounds. We thus adopted the two-dimensional (2D) resistor network model shown in Fig. 2(a) to simulate the resistance and local thermal variations of our sample. Each cell (grayed box in the figure) is named  $C_{y,x}$ ;  $x = 1 \dots 64$ ,  $y = 1 \dots 25$ , i.e., we have 25 lines of cells between the electrodes. Each cell consists of four resistors connected to a single node in cross shape. In addition, for the present thermal model calculation, the cell has four thermal conductances  $\kappa$  and a heat capacity  $c$ . Periodic boundary conditions are assumed in the  $x$  direction. The four resistors of a given cell have the same value, which depend on the temperature of the cell,  $T(x, y)$ , following the activated law

$$r(x, y) = r_0 \exp\left(\frac{E_A}{k_B T(x, y)}\right), \quad (1)$$

where  $E_A$  is the activation energy for the electrical transport,  $k_B$  the Boltzmann constant, and  $r_0$  an arbitrary prefactor [34,35]. We chose  $E_A$  and  $r_0$  so that  $r(x, y)$  fits accurately the temperature dependence of the experimental resistivity. The simulation time is discretized in time steps. At each time step, the 2D resistor network is solved for the applied external voltage by standard nodal analysis. A temperature  $T_A$  is initially set for all the sites. To account for defects present in the bulk material and the imperfections of the electrodes, we set the resistance of a few cells (<1%) with a fixed  $r_{defect}$ ,  $10^4$  times lower than  $r(x, y)$  at  $T_A$ . From the calculated local currents, the change in temperature of each site is computed and updated. This is done using the heat equation, expanding  $\nabla^2 T(x, y)$  by means of the discrete Laplace approximation:

$$\frac{\partial T(x, y)}{\partial t} c = p(x, y) - \kappa \cdot \left( 4T(x, y) - \sum_i^{1st\ neighbors} T_i \right), \quad (2)$$

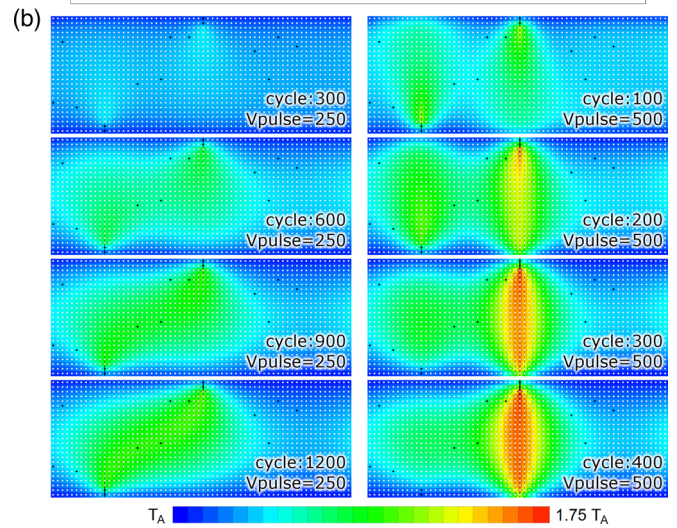
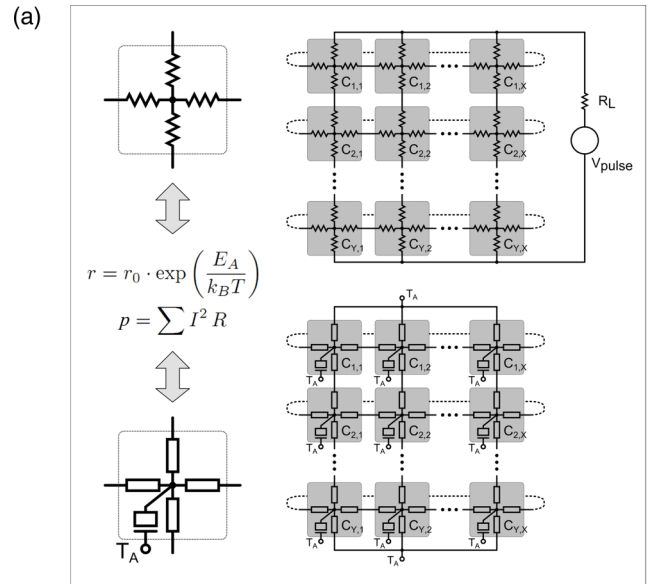


FIG. 2. (Color online) Concept of the Joule heating model (a) and simulated evolution of the temperature profile inside the device (b). The color scale represents local increase of the temperature above the initial  $T_A$ . The cells with black dots are considered as highly conductive defects. In the figures throughout this work, voltage is applied between the electrodes located at the top and at the bottom of the resistor network.

where  $c$  is the heat capacity of each cell,  $p(x, y)$  the electric power generated in the cell, and  $\kappa$  the thermal conductance between neighboring sites (same for all the networks). As a boundary condition, the cells at the top and at the bottom exchange heat with the three neighbors and a virtual cell with a fixed temperature  $T_A$ , which represents the electrodes. Based on this new temperature profile, the matrix  $r(x, y)$  is updated, and then the simulation moves on to the next time step [36].

Typical results of the simulation are presented in Figs. 1(d)–1(f). A gradual decrease of the resistance is observed for all applied voltages due to Joule heating, eventually arriving at a stable low resistance condition. Also, sequences showing the evolution of the temperature profile at a different simulation

time are presented in Fig. 2(b). We observe the formation of a hot percolative path bridging the electrodes. Due to the activated temperature dependence, the resistivity of this hot filamentary path decreases, leading to a reduction of the sample resistance. This resistance drop can reach several orders of magnitude for a large  $V_{\text{pulse}}$ . As observed in the experiments,  $t_{\text{delay}}$  decreases as  $V_{\text{pulse}}$  increases. However, a quick comparison with the experimental data reveals that the Joule heating model fails to reproduce the  $R_{\text{sample}}(t)$  curve and the I-V characteristics. Unlike the experiments, simulations never present a sharp drop of the resistance at a ( $V_{\text{pulse}}$ -dependent) delay time measured from the beginning of the application of the pulse. Moreover, further key discrepancies with experiments are that the model fails to predict the existence of a defined threshold voltage and the voltage regulation effect that is observed after the transition. In fact, all applied  $V_{\text{sample}}$  do produce similar transients, but the asymptotic  $V_{\text{sample}}$  does not reach the same final value after switching. Instead the final  $V_{\text{sample}}$  value decreases with increasing  $V_{\text{pulse}}$ . As a consequence, the I-V characteristic in the stationary regime [red circles in Fig. 1(f)] displays a typical negative differential resistance (NDR [29]), which is in strong contrast with the experiments. This NDR regime is a clear indication of the generation of the high-current/low-resistivity filaments shown in Fig. 2(b). The almost vertical I-V characteristic found in the  $AM_4Q_8$ -based devices reflects a zero differential resistance that evidences a mechanism of a different nature [see red circles in Fig. 1(c)].

At this step it is clear that the resistive switching observed in the  $AM_4Q_8$ -based devices does not arise from a purely Joule heating process. We have therefore implemented a purely electronic model as introduced in Ref. [37]. This model, illustrated in Fig. 3(a), assumes that the active layer is composed of cells that may be in either one of only two states; a low-resistivity correlated metal (CM) state and a high-resistivity MI state. For each cell, an energy barrier  $E_B$  must be overcome to switch from the MI to the CM state. The cells are modeled by four resistors with value  $r_{\text{MI}}$  when it is in the MI state or  $r_{\text{CM}}$  when it is in the CM state, with  $r_{\text{CM}} < r_{\text{MI}}$ . The electronic configuration of the MI state is more stable (the experimental system is, in fact, a single-crystal Mott insulator), so that in thermal equilibrium the device is initially assumed to be in a high resistance state (HRS). Each cell should represent a small portion of the sample, such that the local resistivity may have a well-defined value, that is, of at least a few tenths of nanometers.

We assume that the electronic configuration of a cell in the MI state can be destabilized by the effect of a local electric field  $\varepsilon$ . It effectively reduces the  $E_B$  barrier, resulting in a probability

$$P_{\text{CM}}(x, y) = \exp\left(-\frac{E_B - q|\varepsilon(x, y)|}{k_B T(x, y)}\right) \quad (3)$$

for the local ‘‘collapse’’ of the MI state toward the CM one. We initially keep  $T(x, y)$  at a fixed uniform and constant value during the simulations (we shall later relax this constraint). When a cell commutes to the highly conductive CM state, its internal electric field becomes negligible ( $\varepsilon \approx 0$  inside a metallic region), so that the cell will have a

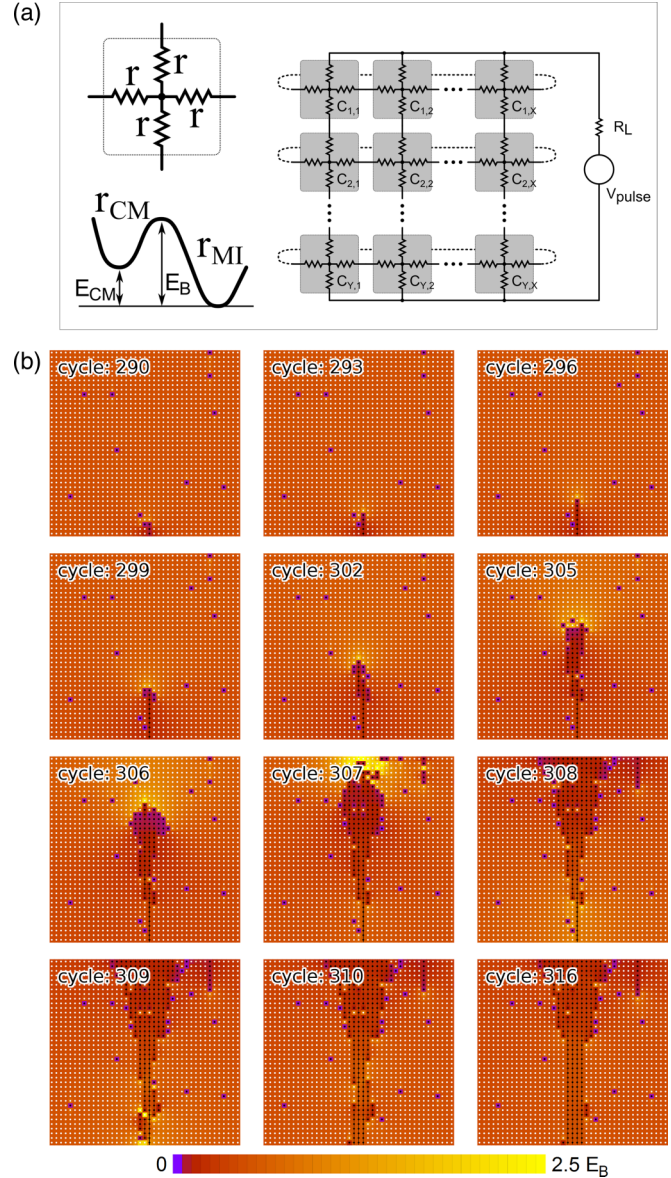


FIG. 3. (Color online) Concept of the Mott transition model (a) and evolution of the electric field profile in a region of the device (b). The color scale represents the local electric field  $q\varepsilon$ . The state of each cell is represented by a white or black dot, corresponding to insulating and metallic cells, respectively.

probability

$$P_{\text{MI}}(x, y) = \exp\left(-\frac{E_B - E_M}{k_B T(x, y)}\right) \quad (4)$$

for switching back to the MI state.

Figure 3(a) presents the array of cells connected to the pulse source  $V$  through the limiting resistor  $R_L$ . We simulated the time evolution of this system similarly as before. The sole difference is that from the computed voltage drops at each cell and by means of Eq. (3) and Eq. (4), we evaluate whether a cell must change its state or not, and the value of the resistors of the network are updated accordingly [38].

Figures 1(g)–1(i) show the typical results of the model simulations. In this case, the computed curves qualitatively reproduce the experiment; that is, the delayed sudden drop of

the resistance above a voltage threshold [Fig. 1(g)], the scaling of  $t_{\text{delay}}$  with the voltage [Fig. 1(h)], and the voltage regulation effect after switching [Fig. 1(i)].

The simulations with this purely electronic model predict two different regimes depending on the applied voltage: a low voltage regime where it remains in the HRS and a high voltage regime where it undergoes a transition to a low resistance state. In the low voltage regime, the stationary state corresponds to a diluted condition, i.e., with the system largely in a homogeneous MI state, and just a few isolated CM cells. There, equilibrium is reached when the rate of MI cells switching to the CM state equals the rate of CM cells switching back to the MI state (cf. Eqs. (3) and (4)). In this situation, the electric field remains essentially homogeneous across the system. Instead, in the high voltage regime, the density of CM cells steadily increases in time. At this higher voltage, there is a significant probability for the formation of metallic clusters, which create spatial inhomogeneities in the electric field. Eventually, a high local field region will be the seed of a “runaway” event, which results in the sudden formation of a metallic filament that connects the electrodes, as illustrated in Fig. 3(b). The two regimes that we just described characterize the existence of a threshold voltage, as observed in the experiments.

While it is now clear that the electronic model captures the key features of the resistive switching, it is also an experimental fact that the resistivity of these narrow-band insulators is very sensitive to local changes in temperature. Therefore, we shall finally combine the electronic (Fig. 3) and the thermal models to study the interplay between the IMT and the Joule heating. Now, the temperature at each cell is calculated as described before, and the switching probabilities  $P_{\text{CM}}$  and  $P_{\text{MI}}$  [Eq. (3) and Eq. (4)] depend on the computed local temperature. Additionally, the resistances in the MI state are now considered temperature dependent, following Eq. (1).

Figure 4 presents the results of this combined model. We observe that the increase in temperature before switching is minimal. The switching behavior is set off by the mechanism associated with the electronic model, i.e., it is dominated by the electric-field-driven IMT. After switching, the temperature of the filament first rapidly increases and, after a voltage dependent time-scale, reaches a stable state with a higher conductance. Therefore, both behaviors are present but operate at different time scales. At short times we observe voltage regulation after switching. At longer times this stabilization is lost due to filament Joule heating that might ultimately lead to sample destruction.

In conclusion, we compared resistive switching experimental results in  $AM_4Q_8$  compounds to the predictions of two models that incorporate different physical mechanisms that have been suggested in the literature as likely candidates to capture the IMT in correlated Mott insulators under strong electric pulsing: a purely thermal and a purely electronic model. Our results showed that the former might capture the lowering of the resistance by the formation of a highly conductive hot filament but misses key experimental observations such as the sharpness of the resistive transition and the precise voltage regulation after switching. On the other hand, our results demonstrate that the latter model, based on the electric collapse of the Mott state, successfully reproduces all the qualitative experimental features. Finally,

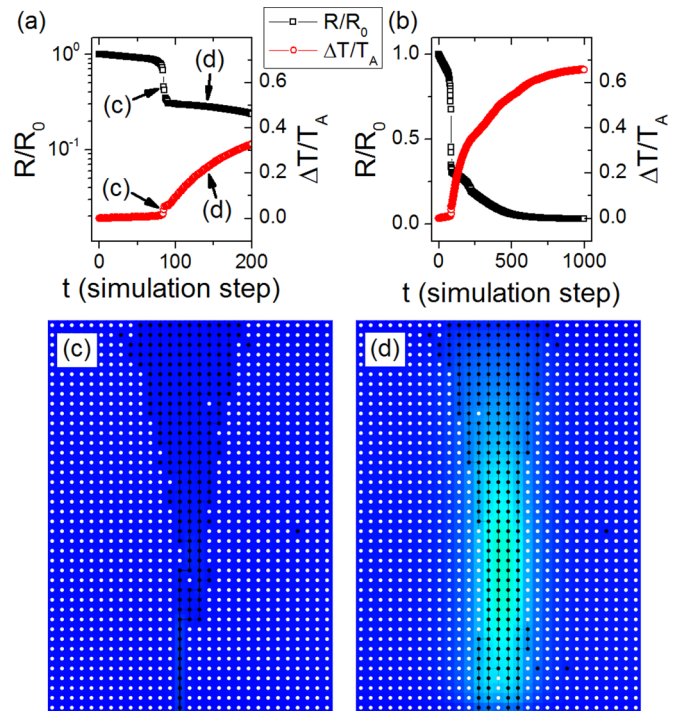


FIG. 4. (Color online) Output of the combined (electronic + thermal) model. (a) and (b) present the time evolution of the resistance  $R$  and the increase of the temperature in the hottest point  $\Delta T$  at different time scales. At short time scale (a) the electronic switch is evident, whereas the progressive increase of the temperature is observed at longer times (b). The temperature profiles (c) and (d), with the same color scale as Fig. 2, show that the relevant Joule heating starts after the electronic switch.

taking into account thermal effects in the electronic model leaves this main conclusion unchanged: the driving force of the resistive transition in  $AM_4Q_8$  is an electronic effect. We note that the “switched” state in  $AM_4Q_8$ , consisting basically in percolating conducting filaments embedded in a MI matrix, strongly differs from the one in “Mott compounds” exhibiting a temperature-driven IMT. In compounds such as  $VO_2$ , the entire sample can switch to a bulk and homogeneous metallic state for large enough Joule heating. More generally, our results and conclusions are likely of a broader reach. In fact, they may be relevant also to other narrow gap Mott insulators, including the canonical system Cr-doped  $V_2O_3$  and  $Ni(S,Se)_2$  where similar effects were recently uncovered [37]. Important theoretical challenges remain ahead, in particular a full many-body out-of-equilibrium treatment of the Mott transition, which remains a formidable problem. Therefore, numerical studies, such as the present one, are urgently needed to provide useful insights and guidance to the current fast progress of the emergent field of correlated electronics.

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- [23] VO<sub>2</sub> is a typical example of Mott insulator for which the mechanism of resistive switching is under debate. This compound undergoes an IMT just above room temperature, which was ascribed by some authors to the Mott physics [9,14,15]. Application of a DC voltage of enough amplitude on a VO<sub>2</sub> sample, at a temperature lower than the IMT, lead to a volatile resistive switching that was recently ascribed to the crossing of the IMT transition due to self-Joule heating [16]. Nonvolatile resistive switching may be also observed in this compound resulting from the hysteretic character of the first-order temperature-driven IMT. In this case, after an electric pulse, the persistence of metallic nanodomains within the insulating matrix explains the lowered value of the resistance [17–19]. Most works performed thus far in dc mode on VO<sub>2</sub> suggest that temperature-driven IMT and thermal Joule heating are key ingredients of the mechanism of this resistive switching [16,17]. But voltage pulse experiments [20] or delay time measurements [21] as well as recent modeling [22] indicate that an electric-field-driven electronic transition rather than Joule heating could trigger the resistive switching in VO<sub>2</sub>. Some questions remain, therefore, open concerning this resistive switching as it is not always easy to disentangle the electric field and thermal effects especially in Mott insulators with *T*-driven IMT like VO<sub>2</sub>.
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