

## Oxidation-enhanced annealing of implantation-induced $Z_{1/2}$ centers in 4H-SiC: Reaction kinetics and modeling

L. S. Løvlie and B. G. Svensson

University of Oslo, Department of Physics / Center for Materials Science and Nanotechnology, P.O. Box 1048 Blindern, N-0316 Oslo, Norway

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High-purity epitaxial layers of *n*-type 4H-SiC have been implanted with 4.3-MeV Si ions to a dose of  $3 \times 10^8 \text{ cm}^{-2}$  and then subjected to dry isothermal oxidation at temperatures between 1050 and 1175 °C. Analysis of the samples by depth-resolved deep level transient spectroscopy unveils a strong oxidation-enhanced annealing of the prominent  $Z_{1/2}$  center, commonly ascribed to the carbon vacancy. The integrated (total) loss of  $Z_{1/2}$  centers is proportional to the thickness of the silicon dioxide ( $\text{SiO}_2$ ) layer grown but the proportionality constant, or annihilation efficiency, decreases with decreasing oxidation temperature. At a given depth  $x$ , the annealing of  $Z_{1/2}$  obeys first-order kinetics with a rate constant  $c$  having an activation energy of  $\sim 5.3$  eV. The pre-exponential factor  $c$  decreases with increasing  $x$  and a normalized concentration-versus-depth distribution of the species injected from the surface and annihilating the  $Z_{1/2}$  centers has been deduced. This species is believed to be the carbon interstitial and is labeled  $C_1$ : numerical simulations of the reaction kinetics employing a model where (i) the generation rate of  $C_1$  at the  $\text{SiO}_2/\text{SiC}$  interface is related to the oxidation rate, (ii) the diffusion of  $C_1$  into the SiC layer is fast, and (iii) a steady-state concentration profile of  $C_1$  is rapidly established, yield good agreement with the experimental data for the evolution of both  $Z_{1/2}$  (absolute values) and  $C_1$  (relative values) with temperature, depth, and time. The activation energy obtained for the diffusivity of  $C_1$  is  $\sim 3.0$  eV, presumably reflecting the migration barrier for  $C_1$  and possibly some contribution from an extra barrier to be surmounted at the  $\text{SiO}_2/\text{SiC}$  interface.

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### I. INTRODUCTION

The most common polytypes of silicon carbide (SiC), 3C, 4H, and 6H, are gradually becoming attractive electronic materials in terms of high-quality bulk and epitaxially grown layers and also in terms of dopant and defect control. However, unlike most other semiconductors, the available methods for selective area doping of SiC are almost inherently restricted to ion implantation, due to the low diffusivity of most dopant elements.<sup>1-3</sup> This makes a genuine understanding of implantation-induced defects of paramount importance, in order to gain acceptable dopant activation and tailoring of the charge carrier lifetime in active parts of SiC devices. In particular, the prominent  $Z_{1/2}$  center, which exhibits an acceptor-like level at about  $E_C - 0.68$  eV in 4H-SiC ( $E_C$  denotes the conduction band edge),<sup>4,5</sup> has been shown to have a detrimental effect on the minority charge carrier lifetime.<sup>6</sup>  $Z_{1/2}$  is typically present with concentrations on the order of  $10^{12}$ – $10^{13} \text{ cm}^{-3}$  in as-grown material but can be reduced by high-temperature annealing, although a complete removal is challenging since  $Z_{1/2}$  remains or even reforms at temperatures approaching 2000 °C.<sup>7,8</sup> Recently, however, several reports have shown that  $[Z_{1/2}]$  (brackets denote concentration values) can be reduced below the detection limit ( $\leq 10^{10} \text{ cm}^{-3}$ ) in a surface layer by either a shallow carbon implantation followed by annealing at 1600 °C,<sup>9</sup> or, perhaps more conveniently, thermal oxidation performed on the Si-face at comparatively low temperatures ( $\sim 1100$  °C).<sup>10-12</sup> Effectively, a “defect-free” layer with an extension of several tens of micrometers in thickness can be formed. In both cases, the removal of  $Z_{1/2}$  was attributed to in-diffusion of a defect species, presumably the carbon interstitial ( $C_1$ ), which reacts with and annihilates  $Z_{1/2}$ . Hence the atomic structure of  $Z_{1/2}$  involves most likely a carbon vacancy ( $V_C$ ).<sup>13-17</sup> Indeed, convincing evidence exists,

obtained by different types of experiments, that  $Z_{1/2}$  is carbon related.<sup>10,14,17-19</sup> This is also corroborated by modeling results based on density-functional-theory (DFT) where  $V_C$  and Si-C antisite pairs have been put forward as possible candidates for  $Z_{1/2}$ .<sup>20-22</sup>

Thermal oxidation of SiC resembles that of silicon but with the additional role of carbon: carbon can be (i) released in the form of CO and  $\text{CO}_2$ , (ii) incorporated and trapped in the growing layer of  $\text{SiO}_2$ , and/or (iii) accumulated at the  $\text{SiO}_2/\text{SiC}$  interface and injected into the bulk of SiC as  $C_1$ . In addition to the removal of  $Z_{1/2}$ , thermal oxidation leads also, via process (iii), to the formation of a donorlike defect with a level in the lower half of the band gap, detected in *p*-type material.<sup>23</sup> For both low- and high-dose implantations, this center can be annealed out at 1400–1500 °C under inert ambient conditions.<sup>23</sup>

In the present work, we have investigated the physical processes governing the enhanced annealing of  $Z_{1/2}$  centers during oxidation. A nonuniform concentration-versus-depth distribution of  $Z_{1/2}$  has been formed by low-fluence implantation of mega-electron-volt Si ions and the evolution of this distribution is monitored after isothermal treatment in dry oxygen atmosphere at temperatures in the range 1050–1175 °C. The relative depth distribution of the injected species, referred to as  $C_1$ , is determined together with the kinetics and activation energy of the annihilation process of  $Z_{1/2}$ . A first-order reaction is revealed with a decreasing rate constant as a function of depth, implying an almost time-independent (steady-state) concentration profile of  $C_1$  at a given temperature. The experimental data are compared with simulations, assuming a “simple” defect reaction model, and quantitative values for the generation rate, diffusivity, and migration energy of  $C_1$  are estimated.

## II. EXPERIMENTAL

The material studied was *n*-type (0001) 4H-SiC, purchased from Cree Inc., with a 4° offcut angle and a 10 μm thick epitaxial layer grown by chemical vapor deposition on a highly *n*-doped substrate ( $\sim 10^{18}$  cm $^{-3}$ ). The epitaxial layer was doped with nitrogen to an effective carrier concentration of  $\sim 2.5 \times 10^{15}$  cm $^{-3}$  as determined by capacitance-voltage (*C-V*) measurements. The samples were implanted with 4.3 MeV Si ions to a fluence of  $3 \times 10^8$  cm $^{-2}$ . The implants were performed in a direction close to the sample normal to minimize channeling, yielding a defect distribution peaking at  $\sim 1.5$ – $1.6$  μm in depth. The concentration of  $Z_{1/2}$  centers before implantation was  $3 \times 10^{12}$  cm $^{-3}$  and uniformly distributed in the epitaxial layer, as measured by deep level transient spectroscopy (DLTS). Subsequently, the implanted samples were annealed in dry O $_2$  atmosphere at temperatures between 1050–1175 °C, and circular Schottky contacts with a diameter of 800 μm were formed by thermal evaporation of Ni after oxide removal in dilute hydrofluoric acid. In parallel, control samples were prepared under identical conditions except for annealing in dry N $_2$  (and not O $_2$ ) atmosphere. DLTS and *C-V* measurements were then employed to determine the concentration-versus-depth profiles of  $Z_{1/2}$  and the charge carriers, respectively. For the measurements, an upgraded version of a custom made setup, described in detail elsewhere,<sup>24</sup> was used. Especially, the concentration-versus-depth profiles of  $Z_{1/2}$  were obtained by selecting one rate window and holding the temperature constant at the maximum of the peak. The steady-state reverse bias voltage was kept constant, while gradually increasing the amplitude of the filling pulse (50 ms duration). The depth profiles were then extracted from the dependence of the recorded DLTS signal on the pulse amplitude, where the voltages used were converted into depth according to the conventional relations for Schottky contacts and accounting for the so-called  $\lambda$  effect.<sup>25</sup> The depth resolution is fundamentally limited by the Debye length, which equals  $\sim 0.08$  μm at 300 K in the epitaxial layers used. The absolute depth scale may suffer from systematic errors of the capacitance values recorded during the DLTS profiling measurements. However, these errors are estimated to be less than  $\sim 10\%$ , based on comparison between the peak position obtained for the  $Z_{1/2}$  center after the implantation with 4.3 MeV  $^{28}\text{Si}$  ions ( $\sim 1.55$  μm) and experimentally determined range distributions of MeV ions in 4H- and 6H-SiC<sup>26</sup> as well as simulated defect distributions using the TRIM code.<sup>27</sup>

## III. DEFECT KINETICS: SOME BASIC CONSIDERATIONS

A defect species *A*, with concentration  $[A] = [A](T, x, t)$ , anneals according to a first-order process if the decay rate is proportional to  $[A]$ ,

$$\frac{\partial [A]}{\partial t} = -c(T, x)[A], \quad (1)$$

where  $c(T, x)$  is the decay constant,  $T$  is the absolute temperature,  $x$  is the sample depth, and  $t$  is the annealing time. This gives the exponential time dependence with the solution

$$[A](T, x, t) = [A]_0 e^{-c(T, x)t}, \quad (2)$$

where  $[A]_0$  is the concentration at  $t = 0$  and  $[A]$  is assumed to vanish at  $t = \infty$ . The decay constant  $c(T, x)$  is typically represented on an Arrhenius form:

$$c(T, x) = c_0(x)e^{-E_a/kT}, \quad (3)$$

where  $c_0$  is the frequency factor and  $E_a$  is the activation energy for the decay process.

In principle, there are three kinds of physical processes giving rise to first-order kinetics (see Ref. 28 and references therein): (i) dissociation where *A* disintegrates into its constituents while back reactions (association) are negligible, (ii) a reaction between *A* and a species *B* with a much larger concentration than *A*, and (iii) a reaction between *A* and a species *B* which is continuously replenished by a source such that  $[B]$  remains constant as a function of time.

The rate of change in the concentration of defects involved in diffusion-limited reactions can be described by coupled partial differential equations,<sup>29</sup> and assuming the case (ii) or (iii) one obtains for *A*:

$$\frac{\partial [A]}{\partial t} = -4\pi R(D_A + D_B)[A][B] + D_A \frac{\partial^2 [A]}{\partial x^2}, \quad (4)$$

where  $R$  is referred to as the capture radius of the reaction with *B*, and  $D_A$  and  $D_B$  are the diffusivities of *A* and *B*, respectively. The first term on the right hand side of Eq. (4) describes the reaction rate between *A* and *B*, while the second one accounts for diffusion of *A* if a concentration gradient exists. Typically, one of the species is much more mobile than the other at a given temperature. Assuming  $D_B \gg D_A$  and that  $[B]$  remains essentially constant as a function of time, Eq. (4) becomes identical to Eq. (1) with  $c(T, x) = 4\pi R D_B [B]$ . Case (ii) ( $[A] \ll [B]$ ) holds commonly for studies of irradiation-induced point defects interacting with oxygen in Czochralski-grown silicon, where  $[O_i] \approx 10^{18}$  cm $^{-3}$ , while the defect concentrations are typically at least one order of magnitude lower.<sup>28</sup> Case (iii) is more “exotic” and seldom found, since it requires a continuous supply of *B* in order to maintain a constant concentration as a function of time ( $[B](t = 0) \approx [B](t = \infty)$  in spite of  $[A]$  being comparable to  $[B]$ ).

For case (ii), the temperature dependence of  $c(T, x)$  is given by that of  $D_B$ ,

$$D_B = D_\infty \exp(-E_d/kT), \quad (5)$$

where  $D_\infty$  is the diffusivity at infinite temperature and  $E_d$  is the activation energy for diffusion. In case (iii), also a possible variation of  $[B]$  with temperature needs to be accounted for and the deduced activation energy of  $c(T, x)$  does not necessarily equal  $E_d$ .

## IV. EXPERIMENTAL RESULTS

Figure 1 shows a representative selection of concentration-versus-depth profiles for the  $Z_{1/2}$  level at  $\sim E_C - 0.68$  eV after annealing at 1150 °C in N $_2$  and O $_2$  atmospheres. For the control samples (N $_2$  anneal), the profiles remain essentially identical and display a peak concentration of  $\sim 6 \times 10^{14}$  cm $^{-3}$  regardless of the duration (and temperature) used. In contrast, for the oxidized samples,  $[Z_{1/2}]$  decreases with increasing time. The profiles peak at a depth of  $\sim 1.55$  μm and exhibit a

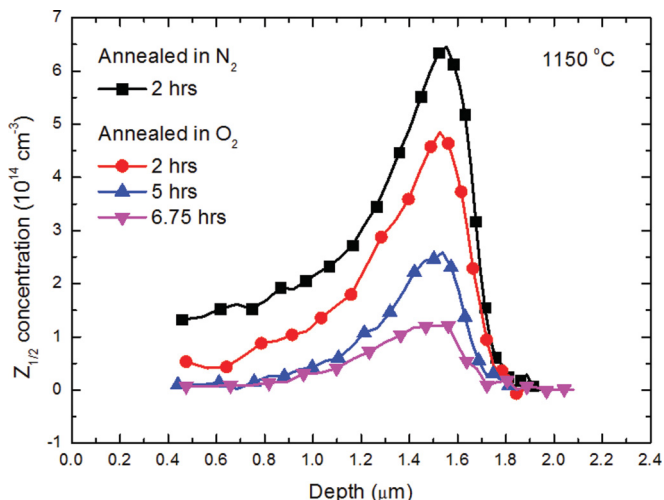
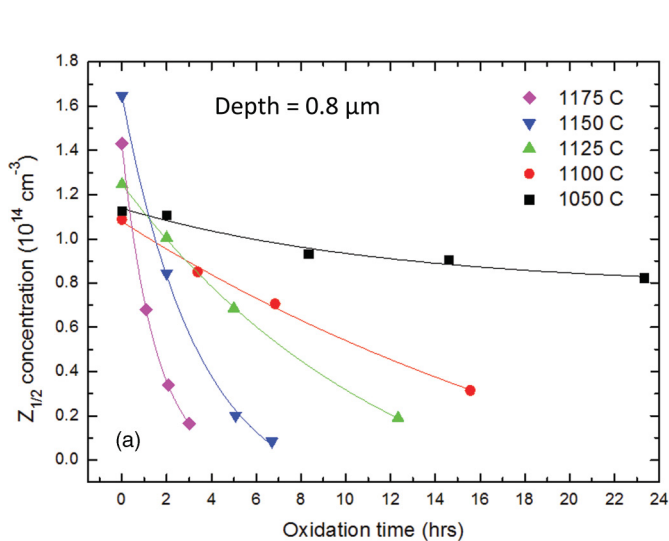


FIG. 1. (Color online) Concentration vs depth profiles of the  $Z_{1/2}$  level, after annealing in  $O_2$  and  $N_2$  atmospheres at  $1150^\circ C$ .

pronounced tail towards the surface, as anticipated after MeV ion implantation.<sup>30</sup> In addition to the decrease in absolute values also the shape of the profiles is altered during the oxidation showing a larger relative reduction in the surface tail than in the peak region.

In Fig. 2(a), the concentration of  $Z_{1/2}$  at  $x = 0.8 \mu m$  is plotted as a function of the oxidation time at 1050, 1100, 1125, 1150, and  $1175^\circ C$ . In each case, the decay of  $[Z_{1/2}]$  exhibits an exponential dependence and the rate constant  $c(T, x)$  increases strongly with temperature, cf. Eq. (2) with  $A = Z_{1/2}$ . Hence the annihilation process of  $Z_{1/2}$  obeys first-order kinetics and  $c(T, x)$  has been extracted at four different depths,  $x = 0.8, 1.0, 1.2,$  and  $1.4 \mu m$ . The results are shown in Figure 2(b) as an Arrhenius plot with  $c(T, x)$  is depicted versus the reciprocal absolute temperature; within the experimental accuracy,  $E_a$  stays constant as a function of  $x$  and a value of  $5.4 \pm 0.3 eV$  is obtained. However, the prefactor,  $c_o(x)$ , decreases with



increasing  $x$  and is reduced by a factor of two between  $x = 0.8$  and  $1.4 \mu m$ . The absolute values of  $c_o$ , i.e., the intercept with the ordinate when  $T$  approaches infinity, carry a significant uncertainty, but are in the range of  $10^{13}$  to  $10^{16} s^{-1}$ .

Without oxidation,  $Z_{1/2}$  persists up to temperatures of  $\sim 2000^\circ C$  in irradiated samples<sup>7</sup> and it may even be thermally (re)generated above  $\sim 1700^\circ C$ .<sup>8</sup> An activation energy of  $\geq 8 eV$  has been estimated for the annealing of  $Z_{1/2}$  assuming dissociation.<sup>7</sup> Thus during the oxidation  $E_a$  is lowered by  $\sim 3 eV$  and dissociation can be ruled out as the controlling process. This conclusion is also substantiated by the variation of  $c(T, x)$  with  $x$ ; for a first-order dissociation process  $c(T, x)$  depends only on  $T$  and not on  $x$ . Accordingly, the oxidation-enhanced annihilation process of  $Z_{1/2}$  is either of the type (ii) or type (iii), as discussed in Sec. III.

Figure 3 shows the total loss of  $Z_{1/2}$  centers, determined by integration of the depth profiles, as a function of thickness of the  $SiO_2$  layer grown at 1050, 1100, 1125, 1150, and  $1175^\circ C$ . The oxidation takes place in the parabolic time domain but for the temperatures and durations used the nonlinearity is weak and a linear dependence holds with a high degree of accuracy.<sup>31</sup> Figure 3 unveils a close proportionality with a slope having a tendency to increase with  $T$ , especially between 1125 and  $1150^\circ C$  where the difference is a factor  $\sim 2$ . These data demonstrate quantitatively the direct relation between the amount of oxidized Si atoms and the amount of annihilated  $Z_{1/2}$  centers but also that the annihilation efficiency depends on  $T$ , i.e., it is not sufficient to consider only the thickness of the grown  $SiO_2$  layer when estimating the amount of annihilated  $Z_{1/2}$  centers.

V. DISCUSSION

A. Defect reaction model assumed for simulations

The decreasing annihilation rate of  $Z_{1/2}$  with increasing depth (see Figs. 1 and 2) implies in-diffusion of an annihilating species from the SiC surface, in accordance with previous

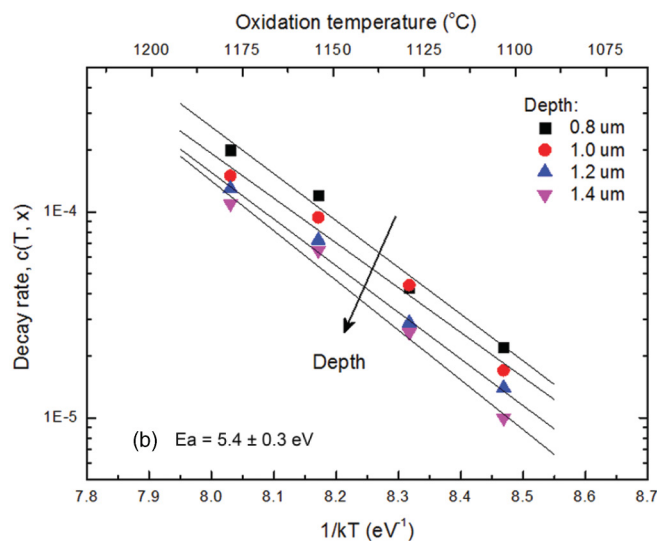


FIG. 2. (Color online) (a) The concentration of  $Z_{1/2}$  at  $x = 0.8 \mu m$  as a function of the oxidation time. The lines are exponential fits of the measured values and show a close agreement. (b) The exponential decay rate of  $[Z_{1/2}]$  at  $x = 0.8, 1.0, 1.2,$  and  $1.4 \mu m$  vs the reciprocal absolute temperature. The decay rate decreases with  $x$  but the activation energy stays constant at  $5.4 \pm 0.3 eV$ .

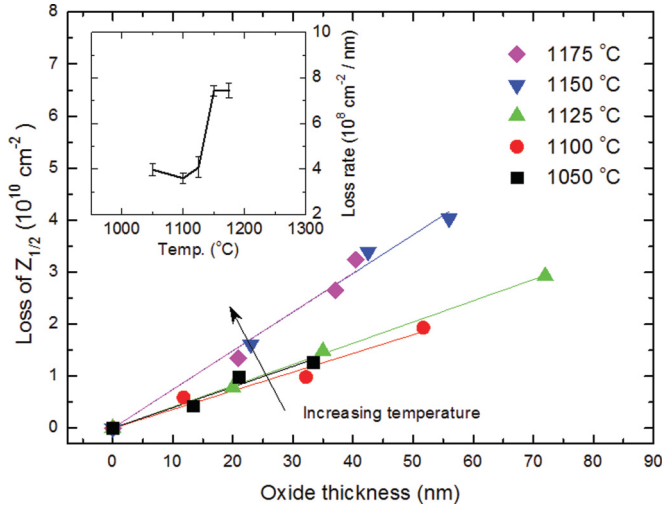


FIG. 3. (Color online) The loss of  $Z_{1/2}$  per  $\text{cm}^{-2}$  as a function of the thickness of the grown  $\text{SiO}_2$  layer. The inset shows the loss of  $Z_{1/2}$  per nm of grown  $\text{SiO}_2$  versus temperature.

findings in the literature.<sup>11,12</sup> Hereafter, this species will be referred to as  $C_1$  and it is generated during the oxidation process. However, an injection into the SiC bulk is not the only alternative for  $C_1$ ; competing reactions exist and their relative importance increases with decreasing temperature (see Fig. 3). These reactions include trapping of  $C_1$  in the  $\text{SiO}_2$  layer and at the  $\text{SiO}_2/\text{SiC}$  interface resulting in the formation of a Si-C-O interlayer and/or clusters of C.<sup>32</sup> Also out-diffusion of  $C_1$  through the  $\text{SiO}_2$  surface may be considered but it is anticipated to decrease with  $t$  and no corresponding increase in the annihilation efficiency of  $Z_{1/2}$  is observed experimentally. Hence, as a first approximation the following reaction model has been assumed,



where the latter reaction accounts for the trapping of  $C_1$  via formation of immobile carbon dimers ( $C_2$ ), primarily at the  $\text{SiO}_2/\text{SiC}$  interface but also in the  $\text{SiO}_2$  and SiC layers. Further,  $Z_{1/2}$  is regarded as immobile and applying Eq. (4), the differential rate equations for  $Z_{1/2}$  and  $C_1$  become

$$\frac{\partial [Z_{1/2}]}{\partial t} = -4\pi R D_{C_1} [Z_{1/2}] [C_1] \quad (8)$$

$$\frac{\partial [C_1]}{\partial t} = g - D_{C_1} \frac{\partial^2 [C_1]}{\partial x^2} - 4\pi R D_{C_1} [C_1] ([Z_{1/2}] + [C_1]). \quad (9)$$

$g$  is the generation rate of  $C_1$  close the interface and put as

$$g \begin{cases} > 0, & 0 < x < 10 \text{ nm}, \\ = 0, & x > 10 \text{ nm}. \end{cases}$$

The width of 10 nm reflects the extension of the Si-C-O transition layer and  $g$  has a time evolution in accordance with that of the growth rate of the  $\text{SiO}_2$  layer.<sup>31</sup>  $D_{C_1}$  is

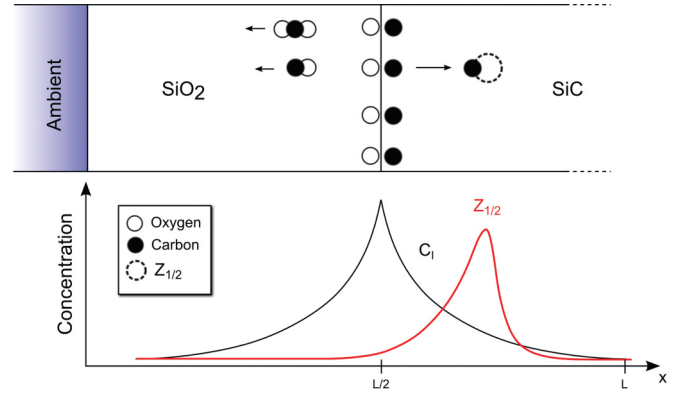


FIG. 4. (Color online) Schematic illustration of the model and sample structure assumed in the simulations.

given by

$$D_{C_1} = \begin{cases} 1.6 \times 10^{-11} \text{ cm}^2/\text{s} & (\text{in SiO}_2), \\ \text{fitting parameter} & (\text{in SiC}), \end{cases}$$

where the value in  $\text{SiO}_2$  is taken from Ref. 30. For  $[Z_{1/2}](T, x, t = 0)$  the measured concentration-versus-depth profile in the control sample is used, while  $[C_1](T, x, t = 0)$  is put equal to zero. The model is schematically illustrated in Fig. 4 for an arbitrary time  $t$ . The  $\text{SiO}_2/\text{SiC}$  interface is treated as a reference plane at  $x = L/2$  and the  $\text{SiO}_2$  layer is held constant with a sufficient thickness ( $40 \mu\text{m}$ ) to apply  $[C_1](T, x = 0, t) = 0$  as a boundary condition. Thus, as a first approximation, out-diffusion of  $C_1$  is omitted since the experimental data show minor (if any) variation of the annihilation efficiency of  $Z_{1/2}$  with the thickness of the  $\text{SiO}_2$  layer grown. Further, both  $[Z_{1/2}]$  and  $[C_1]$  are vanishing in the SiC bulk (large  $x$  values).

### B. Ultimate annihilation efficiency

In the ultimate limit of annihilation efficiency, every injected  $C_1$  contributes to the loss of  $Z_{1/2}$ , as assumed by the present authors in Ref. 12, and then the flux of  $C_1$  being emitted from the  $\text{SiO}_2/\text{SiC}$  interface can be extracted from the total loss of  $[Z_{1/2}]$  versus  $t$ , Fig. 3. Such a treatment has been applied to all the experimental data for  $[Z_{1/2}](T, x, t)$  and the extracted values of the flux were used as input to the simulations.  $D_{C_1}$  was treated as a fitting parameter and varied until an optimum agreement with the measured depth profiles of  $[Z_{1/2}]$  was obtained. The values deduced for  $D_{C_1}$  are given in Fig. 5 and similar to that found in Ref. 12, where only one temperature was studied (1150 °C), they suggest a rapid diffusivity on the order of  $10^{-8} \text{ cm}^2/\text{s}$ . The variation with  $T$  is weak and in fact, opposite to that anticipated for a thermally activated process, i.e.,  $D_{C_1}$  decreases with increasing  $T$ . This suggests strongly that the basic assumption of the ultimate annihilation efficiency is not valid and a different approach needs to be taken.

### C. Extraction of relative $C_1$ profiles and modeling of both $Z_{1/2}(T, x, t)$ and $C_1(T, x, t)$

As shown by the experimental data, the annihilation of  $Z_{1/2}$  exhibits first-order kinetics and the reaction process is either

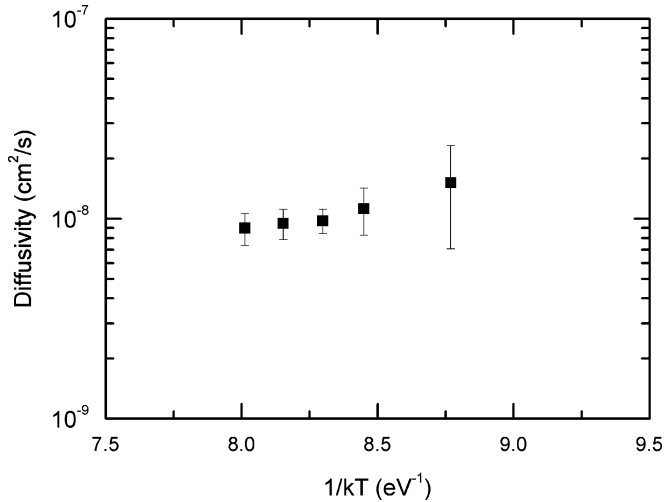


FIG. 5. The diffusivity of  $C_1$  vs the reciprocal absolute temperature deduced under the assumption that every injected  $C_1$  contributes to the loss of  $Z_{1/2}$ .

of type (ii) or (iii) (see Sec. III). Accordingly, from Eq. (8) the following relationship can be derived for  $c(x)$  at a given temperature:

$$c(x) = 4\pi R D_{C_1} [C_1](x, t), \quad (10)$$

where the time dependence of  $[C_1]$  is negligible (the explicit temperature dependence of the quantities in Eq. (10) has been omitted for ease of reading).  $C_1$  is injected from the oxidizing surface and the depth dependence of the decay rate of  $Z_{1/2}$ , i.e.,  $c(T, x)$  in Figure 2(b), is due to the variation of  $[C_1]$  with  $x$ . A large  $[C_1]$  gives fast decay of  $Z_{1/2}$ , which therefore is high at the surface and decreases towards the bulk. The relative depth profile of  $[C_1]$  ( $[C_1]'$ ), e.g., normalized to  $[C_1]$  at (or close to) the surface, can be extracted from Eq. (10) by realizing that

$$[C_1]' = \frac{[C_1](x)}{[C_1](x_{\text{surf}})} = \frac{c(x)}{c(x_{\text{surf}})}. \quad (11)$$

We have used  $x_{\text{surf}} = 0.75 \mu\text{m}$ , which is the most shallow depth where  $[Z_{1/2}]$  is sufficiently large for an accurate determination of  $c(x)$ . The extracted distributions of  $[C_1]'$  are depicted in Fig. 6 and a clear decrease with  $x$  is revealed at all the oxidation temperatures employed. The distributions extend up to  $x = 1.6 \mu\text{m}$ , i.e., just beyond the peak position of  $[Z_{1/2}]$ , whilst at larger depths, the rapid decrease of  $[Z_{1/2}]$  prevents an accurate extraction.

The profiles of  $[C_1]'$  in Fig. 6, and their negligible variation with  $t$ , imply one more criteria to be fulfilled by the simulations in addition to the evolution of  $[Z_{1/2}]$  with  $T$ ,  $x$ , and  $t$ . For each oxidation temperature and duration,  $g$  and  $D_{C_1}$  have been varied independently to fit both  $[Z_{1/2}](x)$  and  $[C_1]'(x)$  by solving Eqs. (8) and (9). The results of such a fitting procedure are illustrated in Fig. 7 for oxidation at  $1100^\circ\text{C}$ , where the squared sum of the difference between simulated and experimental data is depicted in  $D_{C_1}$ -versus- $g$  plots for  $[C_1]'$  [see Fig. 7(a)] and  $[Z_{1/2}]$  [see Fig. 7(b)]. Corresponding results have also been obtained for the other temperatures (not shown). In the fitting,  $D_{C_1}$  was held constant as a function of  $t$ , while  $g$  displayed a weak decrease during the initial

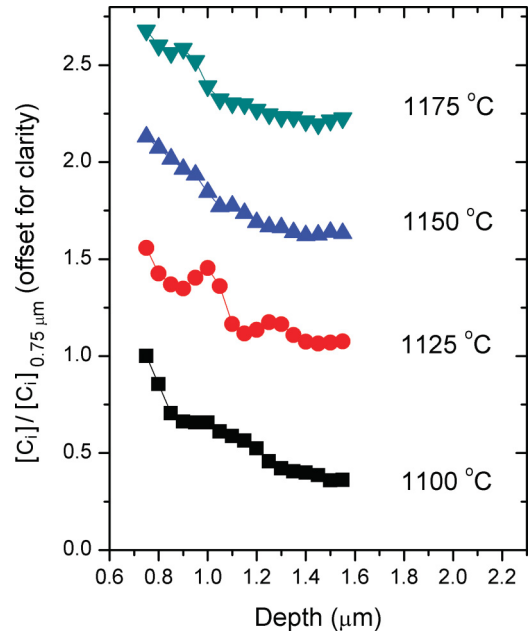


FIG. 6. (Color online) Depth profiles of  $[C_1]'$  extracted from Eq. (11) for oxidation at  $1100$ ,  $1125$ ,  $1150$ , and  $1175^\circ\text{C}$ . The profiles are displaced along the  $y$  axis to improve the readability.

stage, in accordance with a parabolic time domain of the oxidation process. Further, in the  $\text{SiO}_2$  layer,  $D_{C_1}$  has been taken from Hijikata *et al.*<sup>33</sup> and is anticipated to have low activation energy ( $\sim 0.5$ – $0.6$  eV), i.e., it stays almost constant in the temperature range studied. The absolute value of  $D_{C_1}$  in the  $\text{SiO}_2$  layer carries, however, an uncertainty by a few orders of magnitude<sup>34</sup> and, especially, higher values than that used in the simulations ( $1.6 \times 10^{-11} \text{ cm}^2/\text{s}$ ) may be anticipated, as suggested by Krafcsik *et al.*<sup>35</sup> A diffusivity of  $10^{-10} \text{ cm}^2/\text{s}$  shifts the plots in Fig. 7 by a factor of  $\sim 2$  towards higher  $g$  values but with minor effects on the topology.

As unveiled by Fig. 7(a), the solutions for  $C_1$  are rather selective with respect to  $D_{C_1}$  but not to  $g$ . However, the solutions for  $Z_{1/2}$  are selective to both  $g$  and  $D_{C_1}$ , Fig. 7(b), and combining the results for  $C_1$  and  $Z_{1/2}$  one obtains  $D_{C_1} \approx 1 \times 10^{-12} \text{ cm}^2/\text{s}$  and  $g \approx 1$ – $2 \times 10^{13} \text{ cm}^{-3}\text{s}^{-1}$  as the optimum values at  $1100^\circ\text{C}$ . These values are not fully unique but are estimated to be valid within a factor of two for  $D_{C_1}$  and less than a factor of 10 for  $g$  (albeit subject to change depending on  $D_{C_1}$  in  $\text{SiO}_2$  as discussed above). Figure 8 shows Arrhenius plots for  $g$  and  $D_{C_1}$  determined at  $1100$ ,  $1125$ ,  $1150$ , and  $1175^\circ\text{C}$ , where also the physical condition of the activation energy ( $E_a$ ) of  $g$  equal to, or above, that of the oxidation process has been imposed.  $E_a(g)$  equals  $\sim 3.3$  eV, which is slightly higher than the value of  $\sim 3.1$  eV obtained for the oxidation rate (not shown). The latter value is identical with that reported previously for oxidation of the  $\text{Si}(0001)$  face by Song *et al.*<sup>31</sup> The values in Fig. 8 give a good agreement between the simulations and the experimental data of  $[Z_{1/2}](T, x, t)$  and  $[C_1]'(T, x, t)$ , as demonstrated in Figs. 9(a) and 9(b) for  $1100$  and  $1175^\circ\text{C}$ , respectively, where the simulations are represented by solid curves and the measurements by data points (symbols). Here, it should be emphasized that only

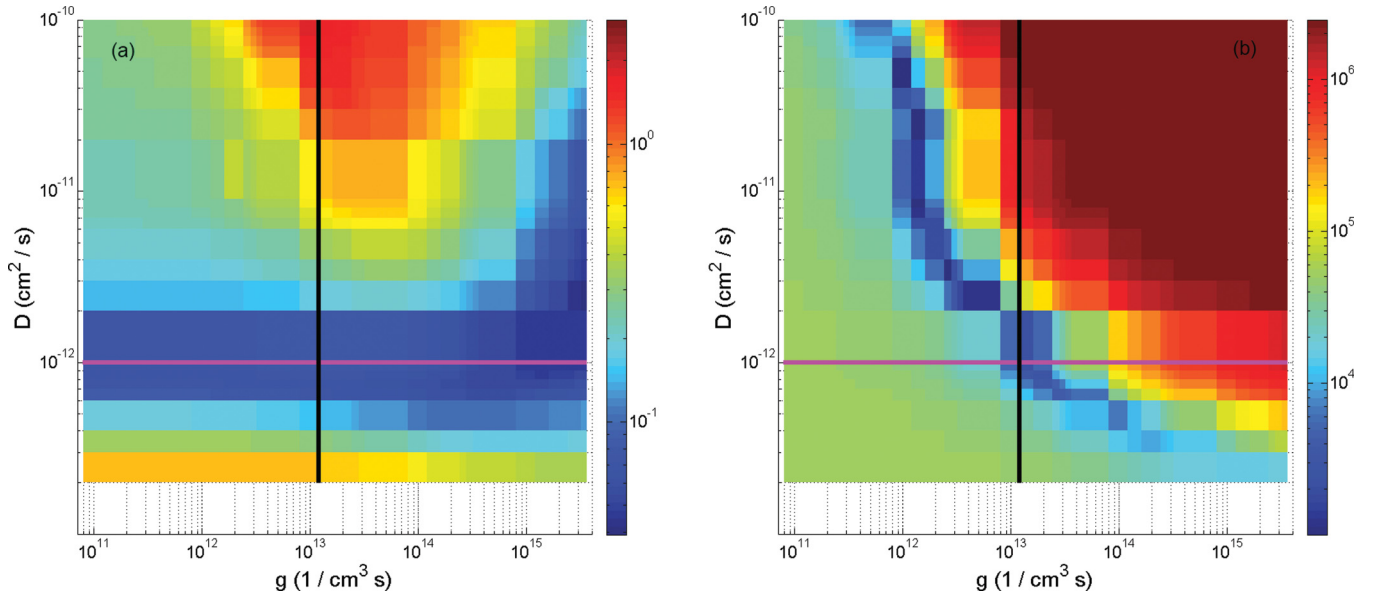


FIG. 7. (Color online) The squared deviation of the simulated data compared with the experimentally determined depth profiles of (a)  $C_1'$  and (b)  $Z_{1/2}$  after oxidation at 1100 °C. The intersection of the pink and black lines represents the optimal combination of  $D_{C_1}$  and  $g$ .

a relative comparison holds for  $C_1$  since only normalized values of  $[C_1]$  ( $[C_1]'$ ) can be deduced from the experiments [cf. Eq. (11)]. In Fig. 9,  $[C_1]'(T, x, t)$  has been multiplied by a constant factor, given by the ratio between the simulated value of  $[C_1](T, x = 0.8 \mu\text{m}, t)$  and  $[C_1]'(T, x = 0.8 \mu\text{m}, t)$ , in order to facilitate the comparison with the simulated  $[C_1](T, x, t)$  distributions.

$E_a(g) \approx 3.3 \text{ eV}$  implies a lowering by at least 4 eV for the generation of “free”  $C_1$ 's at the  $\text{SiO}_2/\text{SiC}$  interface compared to the formation energy estimated for  $C_1$  in bulk SiC under equilibrium conditions,<sup>36</sup> and it illustrates the strong catalytic effect of the oxidation process.  $E_a(D_{C_1}) \approx 3.0 \text{ eV}$  is ascribed to the migration energy of the free  $C_1$ 's injected to the SiC layer; this value is  $\sim 2.0 \text{ eV}$  higher than the migration barrier predicted by Bockstedte *et al.*<sup>36</sup> for  $C_1$  in the energetically favorable split-interstitial configuration. The calculations in Ref. 33 were performed for the 3C-polytype but are expected to

provide a first insight also into the diffusion processes in other polytypes, like 4H. The difference of  $\sim 2.0 \text{ eV}$  may indicate that the free  $C_1$ 's have to surmount an additional energy barrier at the  $\text{SiO}_2/\text{SiC}$  interface before migrating rapidly into the SiC layer. On the other hand, it can also be noted that self-diffusion experiments of  $^{12}\text{C}$  and  $^{13}\text{C}$  in intrinsic 4H-SiC yielded the activation energy for the diffusion of C, which was  $\sim 1.5\text{--}2.0 \text{ eV}$  higher than that obtained in Ref. 33 for an interstitial mechanism.

The sum of  $E_a(g)$  and  $E_a(D_{C_1})$  equals  $\sim 6.3 \text{ eV}$ , which is  $\sim 0.9 \text{ eV}$  higher than the value extracted for the decay rate,  $c$ , of  $Z_{1/2}$ , see Fig. 2(b). This shows a weaker increase of  $[C_1]$  with  $T$  (lower  $E_a$ ) than that of  $g$ , as  $c$  is directly proportional to  $[C_1]$  for a given  $D_{C_1}$  [see Eq. (10)]. Further, the shape of the simulated  $[C_1]$ -versus-depth profiles stays approximately the same for the different  $T$ 's (see Fig. 9), consistent with the  $[C_1]'$  profiles in Fig. 6. Moreover, in spite of the annihilation with  $Z_{1/2}$ ,  $[C_1](T, x, t)$  remains almost constant as a function of  $t$ , i.e., the flux of  $C_1$  from the oxidizing surface is sufficiently high to maintain nearly a steady-state concentration. In fact, the weak time dependence of  $[C_1](T, x, t)$  is a key feature for the apparent first-order annealing kinetics of  $Z_{1/2}$  at a given depth, and referring to Sec. III, the exotic case (iii) applies. The implantation-induced distribution of  $[Z_{1/2}]$  can be regarded as a trapping (or barrier) layer for  $C_1$  to penetrate before reaching the bulk and the evolution of  $[Z_{1/2}](T, x, t)$  is a monitor of the flux of  $C_1$ 's. Accordingly and consistent with Fig. 3, the integrated loss of  $[Z_{1/2}]$  for a given thickness of grown  $\text{SiO}_2$  decreases with decreasing oxidation temperature since the integrated flux of  $C_1$ 's does not only hinge on the amount of generated  $C_1$ 's but also on their diffusivity, cf. Eq. (10) where the decay rate of  $Z_{1/2}$  includes both  $[C_1]$  and  $D_{C_1}$ .

Finally, one can notice that the estimated values of  $g$  are minute relative to the rate of oxidized Si atoms at the  $\text{SiO}_2/\text{SiC}$  interface with a difference of 5–6 orders of magnitude. Hence,

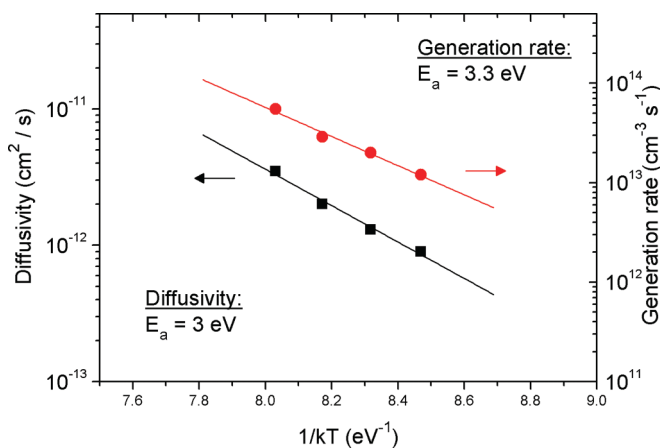


FIG. 8. (Color online) The values of  $D_{C_1}$  and  $g$  extracted from the simulations vs the reciprocal oxidation temperature.

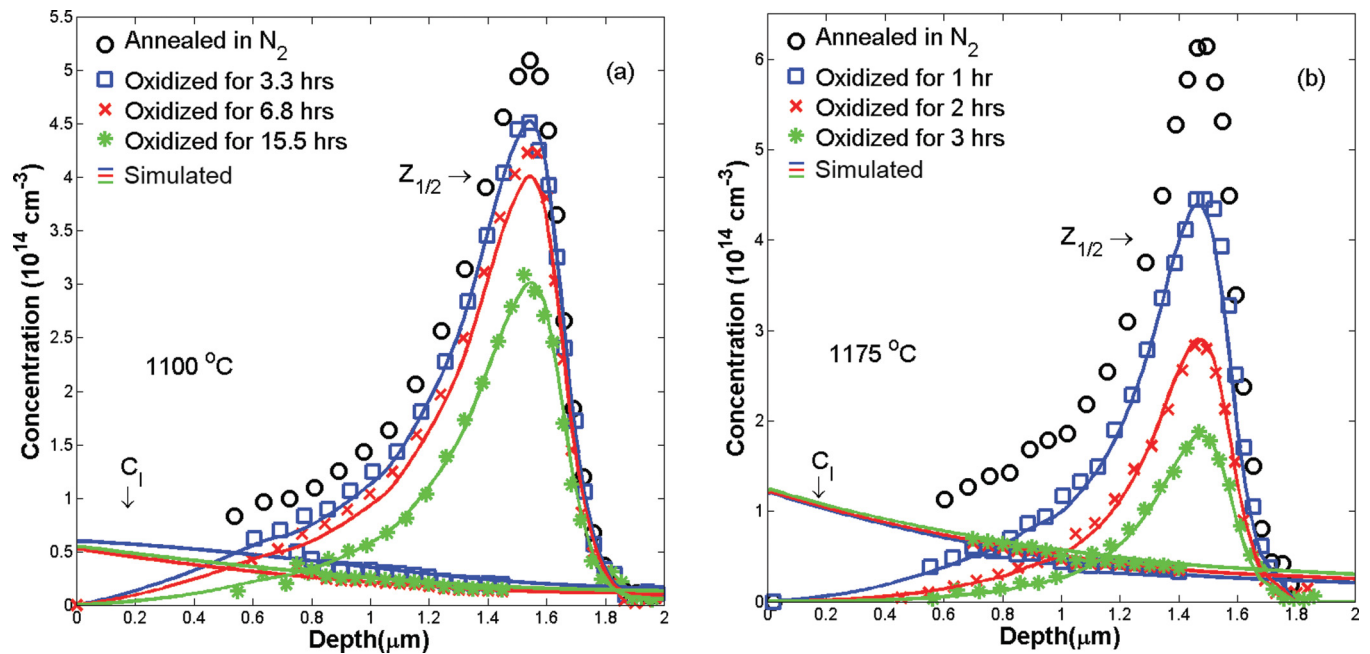


FIG. 9. (Color online) The temporal evolution of the  $Z_{1/2}$  and  $C_1$  concentration-versus-depth profiles at (a) 1100 °C and (b) 1175 °C, with activation energies of 3.0 eV for  $D_{C_1}$  and 3.3 eV for  $g$ .  $[C_1]$  stays nearly time-independent throughout the  $Z_{1/2}$  profiles, yielding first-order annealing kinetics of  $Z_{1/2}$  at a given depth. Experimental data are represented by symbols and calculated data by solid curves.

oxidation-induced injection of  $C_1$  is an important process for bulk defects but not the prevailing one at the  $\text{SiO}_2/\text{SiC}$  interface. Moreover, on the basis of the  $g$  values only a few percent of the injected  $C_1$ 's are estimated to annihilate with  $Z_{1/2}$ , which is substantially lower than the ultimate limit of 100% discussed (and ruled out) in Sec. V B.

## VI. CONCLUSIONS

At a given depth  $x$ , oxidation-induced annihilation of  $Z_{1/2}$  centers in the parabolic time regime obeys first-order kinetics with a rate constant  $c(T, x)$  having an activation energy of  $\sim 5.4$  eV. The pre-exponential factor of  $c(T, x)$  decreases with increasing  $x$ , which suggests a decreasing steady-state concentration of the annihilating species,  $C_1$ , injected from the  $\text{SiO}_2/\text{SiC}$  interface. The experimental data for  $Z_{1/2}(T, x, t)$  and  $[C_1]'(T, x, t)$  can be quantitatively described by a “simple” kinetic model (schematically illustrated in Fig. 4) where  $g$  is essentially proportional to the oxidation rate and  $D_{C_1}$  is fast, while  $Z_{1/2}$  is immobile as corroborated by data for control samples annealed in  $\text{N}_2$  atmosphere. The absolute values

extracted for  $D_{C_1}$  and  $g$  are not fully unique but are expected to be valid within a factor 2 and 10, respectively.  $D_{C_1}$  exhibits an activation energy of  $\sim 3.0$  eV, presumably reflecting the migration barrier of  $C_1$  with possibly some addition from a barrier to be surmounted at (or in the vicinity of) the  $\text{SiO}_2/\text{SiC}$  interface before reaching the SiC layer. The simulations suggest a rapid establishment of steady-state concentration-versus-depth profiles of  $C_1$  and this is a key feature in order to account for the observed first-order annealing kinetics of  $Z_{1/2}$ . Moreover, the total loss of  $Z_{1/2}$  centers is found to be proportional to the thickness of the  $\text{SiO}_2$  layer grown. However, the proportionality constant (annihilation efficiency) decreases with decreasing  $T$  and according to the modeling results, this can primarily be attributed to the decrease of  $D_{C_1}$  at low  $T$ .

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