

# Controlling the frequency-temperature sensitivity of a cryogenic sapphire maser frequency standard by manipulating Fe<sup>3+</sup> spins in the sapphire lattice

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To create a stable signal from a cryogenic sapphire maser frequency standard, the frequency-temperature dependence of the supporting whispering gallery mode must be annulled. We report the ability to control this dependence by manipulating the paramagnetic susceptibility of Fe<sup>3+</sup> ions in the sapphire lattice. We show that the maser signal depends on other whispering gallery modes tuned to the pump signal near 31 GHz, and the annulment point can be controlled to exist between 5 and 10 K, depending on the Fe<sup>3+</sup> ion concentration and the frequency of the pump. This level of control has not been achieved previously and will allow improvements in the stability of such devices.

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## I. INTRODUCTION

The whispering gallery mode sapphire maser is a stable microwave oscillator which makes use of paramagnetic Fe<sup>3+</sup> ions in ultra-low-loss HEMEX (the highest purity sapphire grown using the Heat Exchange Method by Crystal Systems, USA) cylindrical sapphire crystal at low temperature and has been described in detail previously.<sup>1–5</sup> The fractional frequency instability has been demonstrated to be as low as  $\sigma_y(1s < \tau < 100s) = 10^{-14}$ . This instability is normally measured at the frequency-temperature turnover point (or annulment temperature) of a high  $Q$ -factor ( $>10^9$ ) whispering gallery mode (WGM) excited in the sapphire, where the effects of temperature fluctuations on frequency are nullified to first order by the magnetic susceptibility of residual paramagnetic impurities.<sup>6,7</sup> Many publications describe the application of this self-compensation technique,<sup>6–13</sup> and all show that the annulment temperature is dependent on the presence and relative concentrations of paramagnetic ions such as Cr<sup>3+</sup> with an electron spin resonance (ESR) at 11.4 GHz, Mo<sup>3+</sup> (100 GHz) and Ti<sup>3+</sup> (1 THz). The ions are substitutionally included in the crystal lattice during the crystal growing process and occur unintentionally.

In this work we show that the frequency-temperature annulment for the maser depends predominately on the Fe<sup>3+</sup> ions and can be controlled by manipulating the number of ions involved in the maser process. We compare the behavior of two crystals—C1 (concentration of active Fe<sup>3+</sup> ions = 10 ppb) and C2 (100 ppb). We also report the observation of an upper limit in temperature of 30 K for operation of the maser. This limit is explained using a Boltzmann distribution for the active ion, and we show that the populations of the energy levels are so close at this temperature that the effect of the pump at 31 GHz used to excite the maser at 12 GHz is negligible.

Controlling spins in such high- $Q$  cavities could also have other potential applications. For example, it has recently been suggested that HEMEX sapphire with paramagnetic impurities could have applications for quantum measurement

at millikelvin temperatures,<sup>14,15</sup> such as qubits or quantum memory applications.<sup>16–22</sup>

## II. MASER DESCRIPTION

The maser scheme is based on the three energy levels of Fe<sup>3+</sup> ions at zero applied dc magnetic field in the sapphire lattice of a WGM resonator (Fig. 1). The concentration of active ions used to create the effect is about 10–100 ppb, whereas the total concentration is on the order of 1 ppm. The bandwidth of the ESR is  $\Delta\nu_{\text{Fe}^{3+}} \approx 27$  MHz, where the whispering gallery (WG) mode width is only  $\Delta\nu_{\text{WG}} \approx 10$  Hz at 4.2 K.

The maser signal frequency  $\nu_{\text{op}}$  is fixed at the frequency  $\nu_{\text{WG}}$  of the WG mode involved in the process. It is well known that the frequency  $\nu_{\text{WG}}$  is strongly sensitive to temperature variations and needs to be precisely controlled. In this kind of resonator,  $\nu_{\text{WG}}$  possesses a frequency-temperature turnover point (also referred to as the annulment or annulment temperature) above 4.2 K, although annulment temperatures as low as 90 mK have been recently measured.<sup>15</sup> The frequency variations can be described by<sup>6</sup>

$$\frac{\nu_{\text{WG}} - \nu_0}{\nu_0} = AT^4 + C(T, \nu), \quad (1)$$

where  $\nu_0$  is the mode frequency at 0 K without ions, and  $AT^4$  is the thermal sensitivity due to the sapphire dilation ( $A \approx 10^{-12}$  K<sup>-4</sup> for our modes). The other term  $C(T, \nu)$  is thermal sensitivity due to the paramagnetic ions and is defined by

$$C(T, \nu) = \frac{1}{2} \sum_i \eta_i(\nu) \chi_0^{(i)} \frac{(2\pi\tau_2^{(i)})^2 \nu_i(\nu_i - \nu)}{1 + (2\pi\tau_2^{(i)})^2 (\nu_i - \nu)^2}. \quad (2)$$

This term depends in reality on both temperature and operational frequency. The annulment temperature is then calculated by considering the maxima of Eq. (2), where the index  $i$  labels the different paramagnetic species present in the lattice. The

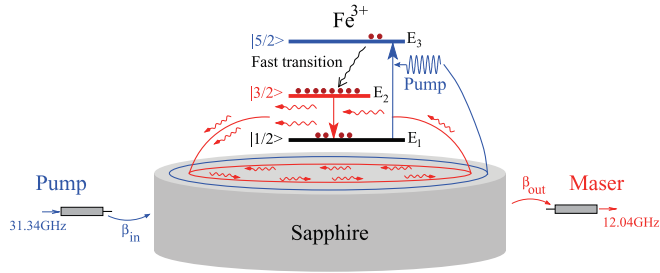


FIG. 1. (Color online) Principle of operation: We apply a signal at 31.34 GHz, coinciding with a WG mode, to pump the ions from the lowest energy level  $|1/2\rangle$  to the third  $|5/2\rangle$ . The ions then (nonradiatively) relax to the second energy level  $|3/2\rangle$ . A population inversion is obtained between the two lowest energy levels, and stimulated emission can be achieved at 12.04 GHz, which is enhanced by another WG mode coincident in frequency.

magnetic filling factor  $\eta_i$  of the mode describes its magnetic field distribution in relation to the  $i$ th species of paramagnetic ion, and  $\chi_0^{(i)}$  is the dc magnetic susceptibility of that ion. As the operating frequency is fixed at around 12.04 GHz, only the effect of the  $\text{Fe}^{3+}$  is considered [i.e., the summation in Eq. (2) is only performed over a single ion  $i = \text{Fe}^{3+}$ ], and the annulment temperature ( $T_{\text{inv}}$ ) can then be expressed as follows:<sup>6,23</sup>

$$T_{\text{inv}} = \left( \frac{(g\mu_B)^2 \mu_0 \pi \tau_2 v_{12} \sigma_{12}^2 N_{\text{int}}}{48k_B A} \right)^{1/5}, \quad (3)$$

where the Bohr magneton  $\mu_B = 9.274 \times 10^{-24} \text{ J T}^{-1}$ , the Boltzmann constant  $k_B = 1.38 \times 10^{-23} \text{ J K}^{-1}$ , the Landé  $g$  factor  $g \approx 2$ ,  $\sigma_{12}^2 \approx 2$  is a characteristic constant of the absorption rate of the ions at 12.04 GHz (calculated from the  $\text{Fe}^{3+}$  sapphire spin Hamiltonian parameters),<sup>23–25</sup> and the spin-spin relaxation time  $\tau_2$  is related to the width at half resonance of the ESR ( $\Delta v_{12} = \frac{1}{\pi \tau_2}$ ). If two spins are in phase and one absorbs a photon causing a phase shift,  $\tau_2$  is the necessary time for the spins to be in phase again.

Figure 2 shows the bandwidth for active maser operation in crystal C2, which is more than 186 MHz for the 12-GHz and 31-GHz ESR levels. We can note from Fig. 2 that the maser can operate in a multimode configuration. For example, when the pump frequency is in the range 31.350–31.375 GHz, two signals can operate at once at 12.037 and 12.149 GHz. In the rest of the paper, the characterization of the turnover temperature has been investigated for single-mode maser operation. We consider then in this paper  $\Delta v_{12} = 27 \text{ MHz}$ , the width measured by Bogle and Symmons.<sup>26</sup>  $N_{\text{int}}$  is the concentration of the active ions involved in the annulment temperature in units of ion/ $\text{m}^3$ . However, it is convenient to express it as a fraction of the  $\text{Al}_2\text{O}_3$  in the crystal, i.e.,  $2.35 \times 10^{22} \text{ ion/m}^3 \equiv 1 \text{ ppm}$ . This concentration is related to the total ion concentration in the lattice as follows:

$$N_{\text{int}} = \zeta \times N_{\text{total}}, \quad (4)$$

where  $\zeta$  is the fraction of the ion concentration involved in the process ( $0 \leq \zeta \leq 1$ ), and  $N_{\text{total}}$  the total ion concentration in the lattice. When  $\zeta = 0$ , no frequency-temperature annulment is observed, and when  $\zeta = 1$  all the ions in the lattice participate in the annulment process. Figure 3 shows that the

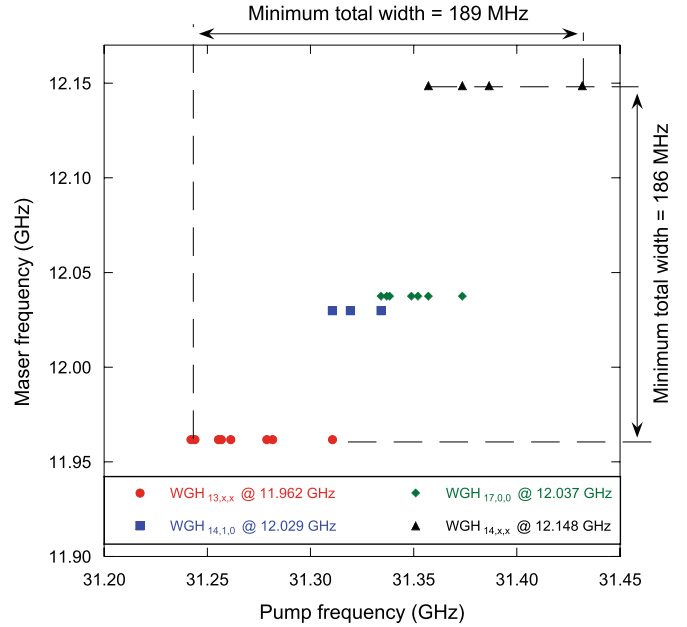


FIG. 2. (Color online) The active maser bandwidth over which we can generate a signal is of order 180–190 MHz for crystal C2. Masing occurs at discrete frequencies where WGMs exist between 11.95 and 12.15 GHz, which is in turn pumped at discrete frequencies between 31.24 and 31.44 GHz where higher frequency WGMs exist.

annulment temperature  $T_{\text{inv}}$  increases with the total number of ions  $N_{\text{total}}$ .

### III. MEASUREMENTS

To characterize the maser signal, we amplify it by 30 dB and then compare it to a signal from a synthesizer referenced to a hydrogen maser. The beat note is then amplified and bandpass filtered before being counted (Fig. 4). The accuracy of the temperature control at the resonator cavity is about 2 mK.

#### A. Behavior of C1 with low concentration of $\text{Fe}^{3+}$

The maser characterized in this section oscillates at the  $\text{WGH}_{17,0,0}$  (the 17th azimuthal order fundamental Whispering Gallery quasi-Transverse Electric) mode frequency

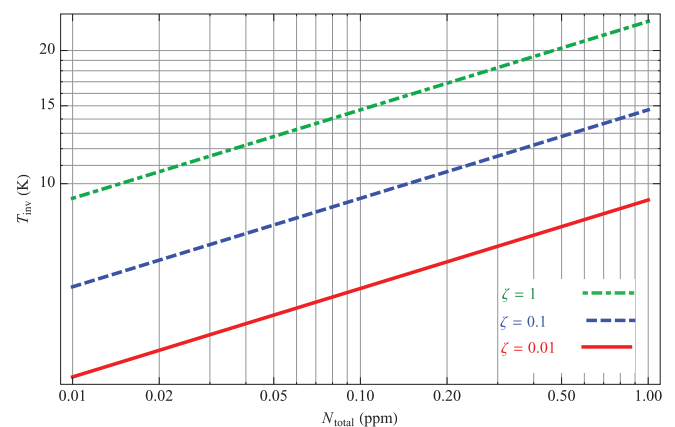


FIG. 3. (Color online) Evolution of the annulment temperature with the total  $\text{Fe}^{3+}$  concentration for different values of the fraction  $\zeta$ .

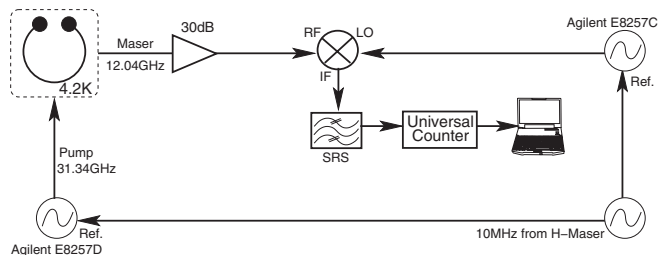


FIG. 4. Experimental setup: The crystal is a cylindrical HEMEX sapphire, 30 mm height and 50 mm diameter, placed in a cylindrical cavity and cooled to 4.2 K using a cryocooler.

(12.038 GHz) of crystal C1 and can be excited using a pump signal corresponding to any of several WG modes around 31.34 GHz. The frequency of the WG mode that enhances the maser signal shows a turnover temperature  $T_{inv}$  around 7.8 K, with no dependence on the input power applied to the crystal. The evolution of the maser frequency with temperature is shown in Fig. 5.

The excitation frequency of each pump WG mode was varied, and the evolution of the maser frequency with temperature was observed at various levels of pump power. The frequency was changed in steps of 250 Hz at various levels of pump power. As Fig. 6 shows,  $T_{inv}$  is independent of the pump power and pump frequency for each pump mode. For example, the 31.339-GHz pump mode has an annulment temperature which stays constant at 8.25 K.

Despite the fact that  $T_{inv}$  is independent of the input power and frequency of the pump signal (for a particular choice of pump mode), its value does change when a different pump WG mode is selected, as shown in Fig. 7. The  $T_{inv}$  point is measured for the pump frequency range 31.320–31.339 GHz. No turnover point is observed at higher frequencies, due to the annulment temperature residing outside the measurable

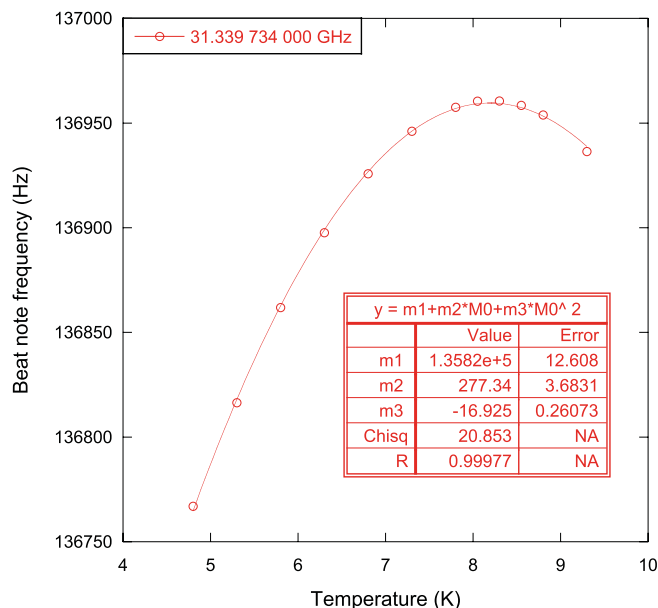


FIG. 5. (Color online) Evolution of the maser frequency (for C1) at 12.038 GHz with temperature for a fixed pump at 31.339 734 GHz. From the fit, the annulment temperature is 8.193 K.

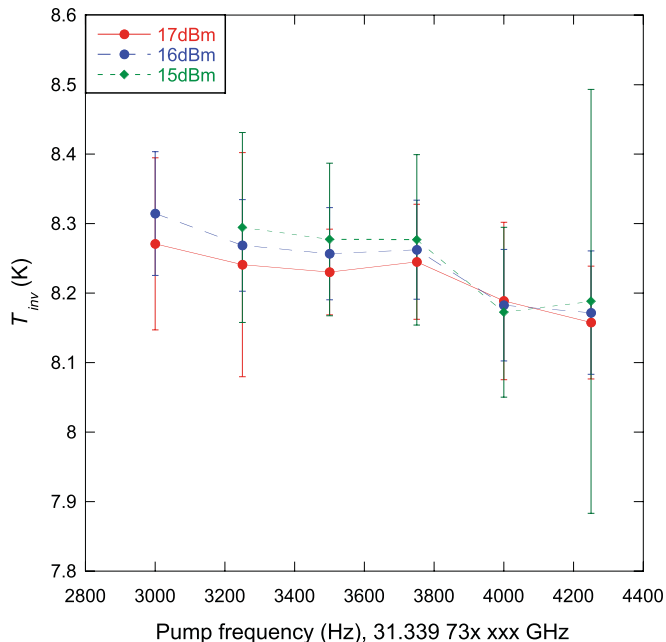


FIG. 6. (Color online) Evolution of the annulment temperature for different values of pump power and frequency. The pump mode chosen was at 31.339 GHz.

temperature range (below 4 K).  $T_{inv}$  can be calculated for each pump by a simple second-order polynomial equation, as shown in Fig. 5.

For each pump at 31 GHz, the population of active ions  $N_{maser}$  used to create the maser signal is different from that fraction of ions that determine  $T_{inv}$  for the mode. The active ion concentration was deduced for each  $T_{inv}$  from the maser

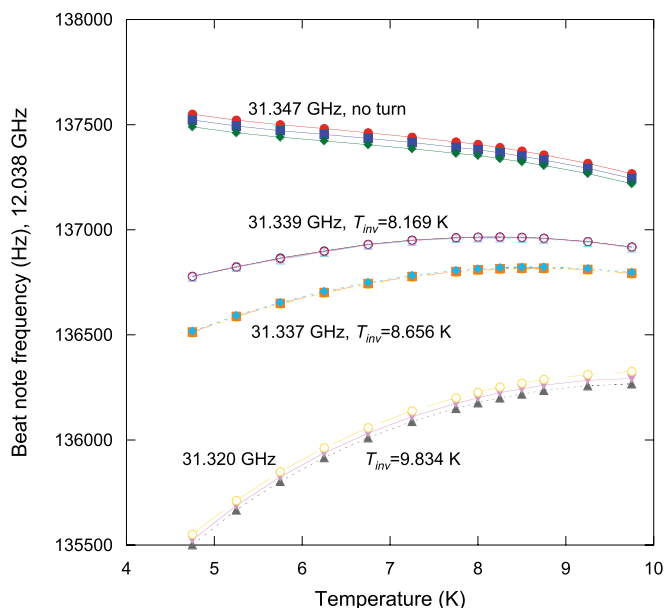


FIG. 7. (Color online) Evolution of the maser signal frequency with temperature for different pumps near 31.3 GHz. For each pump  $T_{inv}$  is independent from its frequency and the power.

TABLE I. Measured parameters for the WGH<sub>17,0,0</sub> mode at 8 K. The maser signal was operating on the lower doublet of the mode.

Mode	$T_{\text{inv}}$ (K)	$\nu_{\text{WG}}$ (GHz)	$\beta_{\text{out}}$	$Q_0 \times 10^6$	$V_{\text{eff}}$ (m <sup>3</sup> )	$\eta$
WGH <sub>17,0,0</sub>	7.8	12.038 136	0.200	600	$10^{-5}$	0.992 68
		12.038 137	0.009	–		

output power calculated by Benmessai *et al.*,<sup>27</sup> as shown by Eq. (5):

$$N_{\text{maser}} = \frac{1 + \beta_{\text{out}}}{\beta_{\text{out}}} \left[ \frac{\beta_{\text{out}}}{Q_0} \frac{3k_B T \Delta \nu_{12}}{2\eta(g\mu_B)^2} \mu_0 \sigma_{12}^2 I_{\text{ratio}} \nu_{12} + \frac{2\tau_1}{3h\nu_{12} V_{\text{eff}}} \frac{2\Delta N_{23} + 5\Delta N_{13}}{\Delta N_{13}(\Delta N_{23} - \Delta N_{12})} \frac{\text{Power}}{\xi} \right]. \quad (5)$$

The concentrations  $N_{\text{maser}}$  and  $N_{\text{int}}$  are the same only if the ESR is saturated.  $N_{\text{maser}}$  is calculated from the rate equations and the Boltzmann law at saturation, and  $N_{\text{int}}$  is calculated from WG mode behavior. The ion inversion ratio  $I_{\text{ratio}}$  is defined as follows:

$$I_{\text{ratio}} = \frac{(\Delta N_{23} - \Delta N_{12})(\Delta N_{13} + \Delta N_{23})}{\Delta N_{12}(5\Delta N_{13} + 2\Delta N_{23})}, \quad (6)$$

where the different  $\Delta N_{ij}$  are the normalized population difference between the energy levels  $i$  and  $j$  and are calculated as shown by Benmessai *et al.*<sup>27</sup> The relaxation time  $\tau_1 \approx 10$  ms at 8 K is the spin-lattice relaxation time. This time is considered as constant around  $T_{\text{inv}}$ . In reality, it undergoes a direct relaxation process and follows  $T^{-1}$  when  $T \leq 15$  K.<sup>28–30</sup> Here,  $\beta_{\text{out}}$  is the coupling of the mode at 12.04 GHz,  $Q_0$  is its unloaded  $Q$  factor,  $V_{\text{eff}}$  is the effective mode volume, and  $\eta$  is the filling factor. The mode parameters are constant over the temperature range in which we characterize the signal and are summarized in Table I.

By definition,  $\xi$  is the ratio between the power in the unsaturated regime and saturation ( $0 < \xi \leq 1$ ). Note that for the pump at 31.337 GHz, where the maser is at saturation,  $\xi$  should be equal to unity. From the results shown in Fig. 7, where  $T_{\text{inv}}$  is different from one pump to another, it is possible to calculate the corresponding concentration for each  $T_{\text{inv}}$  from Eq. (2). It is also possible to calculate the same concentration from Eq. (5). Knowing the maser output power, the results are shown in Table II.

Equation (5) is evaluated when the maser signal is maximum (i.e., at saturation). As the maser signal is oscillating at one mode (WGH<sub>17,0,0</sub>) for all the pumps, it is clear that

for each pump the amount of active ions is different, leading to a calculation of different concentrations. Each pump has a different configuration of coupling and field distribution in the crystal, so each pump will interact with a different quantity of ions; whether saturation is reached is determined by the coupling.

### B. Behavior of C2 with high concentration of Fe<sup>3+</sup>

It has been shown previously<sup>5</sup> that the concentration of Fe<sup>3+</sup> ions in sapphire can be increased significantly by annealing in air, causing conversion of Fe<sup>2+</sup> impurities to Fe<sup>3+</sup>. Originally the two crystals C1 and C2 exhibited similar properties of very low concentration of Fe<sup>3+</sup> impurities. However, C2 went through a series of additional annealing and was thus transformed from the low-concentration regime (as reported here for C1) to the high-concentration regime. The improvement in ion concentration is permanent, and once in the high-concentration regime the resonator will exhibit the effects reported in this paper. Thus annealing a resonator is beneficial in two respects. Due to the increased active ion population it will exhibit a higher maser output power, leading to a reduction in the Schawlow-Townes thermal noise limit,<sup>4</sup> as well as leading to a potential improvement in the curvature of the frequency-temperature dependence as is reported in this section.

For the crystal C2, the maser operation is very different as the concentration of the active ions is higher, resulting in a higher maser output power of  $-40$  dB m, compared to  $-56$  dB m for C1. In addition, maser signals are observed not only at the WGH<sub>17,0,0</sub> frequency, but also at different modes whose frequencies are within the ESR bandwidth.<sup>5</sup> Like C1, all the pump modes for which a maser signal can be excited in C2 have a temperature turnover point independent of the applied power. Characterizing the turnover point for this crystal reveals more complex effects than C1.

Figure 8 shows the signal at 12.037 GHz, oscillating for a pump applied at 31.349 GHz. Each curve represents the maser frequency dependence as a function of temperature for

TABLE II. Summary of the calculated concentrations.

$\nu_{\text{pump}}$ (GHz)	$T_{\text{inv}}$ (K)	Power (dB m) <sup>a</sup>	$N_{\text{int}}$ (ppb) <sup>b</sup>	$\zeta$	$N_{\text{maser}}$ (ppb) <sup>c</sup>	$\xi$
31.320	9.834	$-62.59$	13.46	0.0135	7.74	0.6180
31.337	8.656	$-60.50$	7.11	0.0071	11.09	1.0000
31.339	8.169	$-65.50$	5.32	0.0053	3.57	0.3162
31.347	–	$-69.00^d$	–	–	1.90	0.1412

<sup>a</sup>Measured at the resonator output.

<sup>b</sup>Calculated from Eq. (3).

<sup>c</sup>Calculated from Eq. (5).

<sup>d</sup>At 9 K.

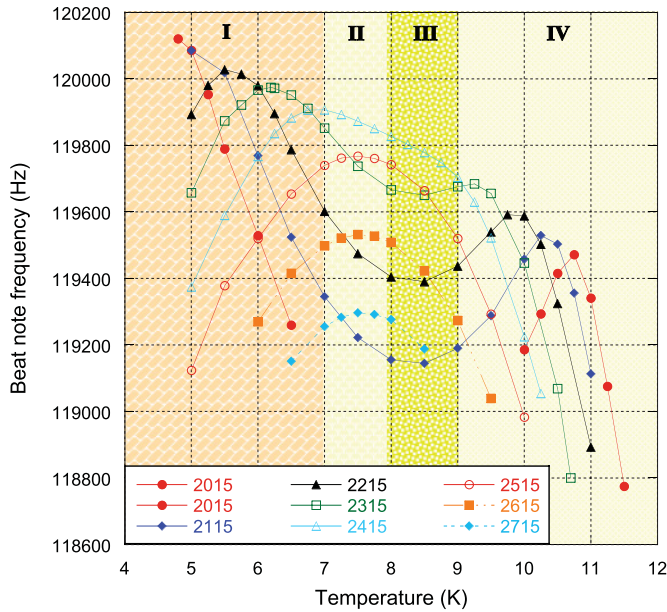


FIG. 8. (Color online) Evolution of the maser signal frequency at 12.037 GHz with temperature for different values of the same pump at offsets (in Hertz) from 31.349 780 000 GHz.

different pump frequencies. Here, the maser frequency shows a strong dependence on the pump tuning. We note that when the frequency  $\nu_{\text{pump}} \leq 31.349782315$  GHz, there are three  $T_{\text{inv}}$ —one near 6 K, the second around 8 K, and the third at 10.5 K. When  $\nu_{\text{pump}} \geq 31.349782415$  GHz, there is only one  $T_{\text{inv}}$  at around 8 K, and the system behaves in the same classical fashion as the first crystal.

We can also divide the figure into four zones, with each zone defining a turnover temperature. From the results shown in Fig. 8, we can draw the evolution of the different turning point with the pump frequency (cf. Fig. 9).

The annulment exists for multiple temperatures only for crystal C2 with high  $\text{Fe}^{3+}$  concentration. This effect appears to be nonlinear, showing that a variation in the active ion population is induced as the temperature is varied, which in turn changes the turning point temperature as the temperature is varied.

The annulment temperature depends on the distribution of the ions and the population difference between their levels. When the annulment temperature for the  $\text{WGH}_{17,0,0}$  mode is measured using a network analyzer, no change is seen due to the small population difference at this frequency (5% of the total active population). However, when the maser is operating, i.e., being pumped, the configuration of the ions is completely different: population inversion exists between the  $|1/2\rangle$  and  $|3/2\rangle$  levels, and saturation is seen at 31 GHz where the populations of states  $|1/2\rangle$  and  $|5/2\rangle$  are equal. The population inversion rate is determined by the choice of pump mode near 31 GHz. For each pump mode the strength of the maser signal depends on its coupling and spatial field distribution in the crystal. Strong coupling allows an optimum exchange of energy with the ions, and field distributions occupying more volume in the crystal increase the interactions with different classes of ions. Considering the inhomogeneous broadening of the line at 31 GHz in addition to these factors,

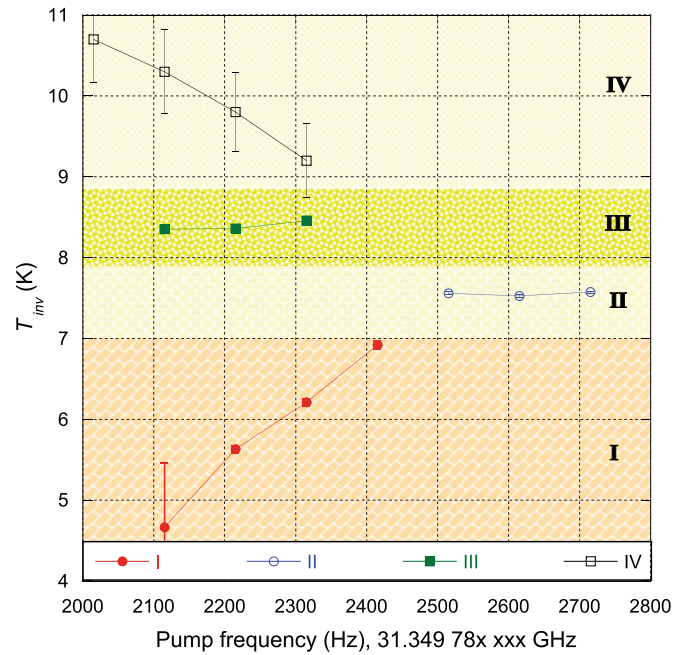


FIG. 9. (Color online) Evolution of the turnover temperature at 12.037 GHz with different values of the same pump at offsets (in Hertz) from 31.349 780 000 GHz.

we can understand why  $T_{\text{inv}}$  is different from one pump to another. The  $\text{Fe}^{3+}$  spins act as individual packets selected by the corresponding pump WG mode. Thus the pump signal selects a different quantity of ions among the broadened ESR frequency.

For C2 the case is more complex because  $T_{\text{inv}}$  is not only different from one pump to another for the same maser signal, but is different for the same pump mode when the frequency is tuned. The maser frequency shows more than one temperature turnover point for some pump frequencies and no annulment

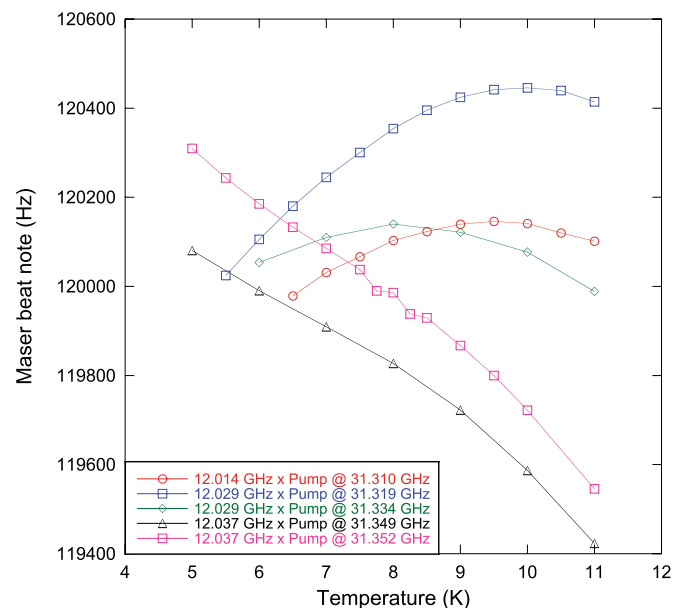


FIG. 10. (Color online) Evolution of the maser signal frequency with temperature for different pumps.

TABLE III. Different annulment and operation limit temperatures for optimal operation of the maser

$\nu_{\text{pump}}$ (GHz)	$\nu_{\text{maser}}$ (GHz)	$T_{\text{inv}}$ (K)	$T_{\text{operation}}$ (K)
31.310	12.014	9.407	15
31.319	12.029	9.910	26
31.334	12.029	8.140	23
31.349	12.037	–	28
31.352	12.037	–	30

for others. In the case where there is more than one, the curvature of annulment is significantly reduced, which has the potential to improve stability and reduce the temperature control requirements of the maser.

### 1. Optimum Operation

Characterization of the maser frequency with temperature was performed at a fixed pump frequency. However, the pump WG mode is temperature dependent, as well as the WG modes near 12.04 GHz. To optimize the maser operation, it is necessary to tune the pump frequency for each operating temperature. This optimum frequency corresponds to maxima or minima of the maser frequency, depending on the  $T_{\text{inv}}$  being measured. Figure 10 shows how the maser frequency varies with temperature for different pump modes. The signal at 12.014 GHz has a turnover point at 10 K, the one at 12.029 GHz is at 10.3 K, and the one at 12.037 GHz shows no turnover temperature at all. The measurements were performed at different power levels, which were found to have no effect on the turnover temperature.

## IV. MASER TEMPERATURE OPERATION LIMIT

In order to characterize the upper temperature limit  $T_{\text{operation}}$  for maser operation, we adjust the pump frequency for each measurement as per the last section. The results are summarized in Table III. The 12.037-GHz maser signal oscillates until 28 K when pumped at 31.349 GHz and 30 K when pumped at 31.352 GHz. The power of the maser signal is observed to decrease as the temperature is raised. This is due to the fact that the populations of the  $\text{Fe}^{3+}$  energy levels follow

a Boltzmann distribution at thermal equilibrium. At higher temperatures, the difference in population between levels is reduced, resulting in less efficient masing. At high temperature (20–30 K) the number of ions pumped at 31.3 GHz is lower than at 4.2 K, leading to a smaller population inversion ratio. This directly affects the maser power and causes it to drop as temperature rises. In addition, the absorption at 31.3 GHz is a result of a mixing between the  $|1/2\rangle$  and  $|5/2\rangle$  spin states of the  $\text{Fe}^{3+}$  ion, which occurs with very small probability.<sup>26,31,32</sup> The population difference at 31.3 GHz is high enough to excite the maser signal with this probability at low temperatures ( $<30$  K) but not at high temperatures ( $>30$  K). At higher temperatures still, characterization of the WG modes around 12.04 GHz showed absorption effects up to 140 K. The strength of the absorption decreases when the temperature is increased; however, no maser operation has been observed at these temperatures.

## V. CONCLUSION

We have demonstrated how  $\text{Fe}^{3+}$  ions in a sapphire maser influence the frequency-temperature turnover point of the maser signal. We compared the behavior of two crystals, one with a low active ion concentration and the other with a high concentration. The first crystal showed classical behavior where  $T_{\text{inv}}$  is independent of the pump power and frequency, but was different between pump modes due to different packets of ions being excited for each pump. The population of ions that creates the maser causes a change in the intrinsic annulment temperature  $T_{\text{inv}}$  for the mode. The crystal with higher  $\text{Fe}^{3+}$  concentration showed a more complex behavior, where  $T_{\text{inv}}$  was different not only from one pump mode to another, but showed many turnover points for some choices of pump, and in some cases none at all. Thus the curvature of the annulment point in some cases could be reduced, which would also reduce the requirements for temperature control when generating a stable frequency.

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