Noise correlations in a flux qubit with tunable tunnel coupling

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We have measured flux-noise correlations in a tunable superconducting flux qubit. The device consists of two loops that independently control the qubit's energy splitting and tunnel coupling. Low-frequency flux noise in the loops causes fluctuations of the qubit frequency and leads to dephasing. Since the noises in the two loops couple to different terms of the qubit Hamiltonian, a measurement of the dephasing rate at different bias points provides a way to extract both the amplitude and the sign of the noise correlations. We find that the flux fluctuations in the two loops are anticorrelated, consistent with a model where the flux noise is generated by randomly oriented unpaired spins on the metal surface.

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I. INTRODUCTION

The performance of qubits based on superconducting circuits is affected by the ubiquitous low-frequency flux noise present in such devices. Early measurements on superconducting quantum interference devices (SQUIDs) showed the existence of flux noise with a 1/f-like power spectrum. The noise was found to be universal in the sense that it depended only weakly on materials and sample dimensions. In more recent years, it has become clear that the same excess flux noise limits the phase coherence of superconducting qubits. A slowly varying flux leads to fluctuations of the qubit energy levels, which has been shown to be the dominant dephasing mechanism in both flux and phase qubits. Finding the origin and a possible remedy for the excess flux noise is therefore of importance to facilitate further improvements of intrinsic coherence times in these devices.

Theories have been developed to explain the microscopic origins of the noise, involving the existence of real or effective unpaired spins in the vicinity of the superconducting structures. The Various experiments have shown the presence of a large number of localized spins on the surface of thin films of normal and superconducting metals, well as in Si/SiO2 interfaces. Sendelbach et al. measured correlations between flux and inductance noise in SQUIDs, possibly suggesting the formation of spin clusters. The results suggest that the flux noise is related to the nonequilibrium dynamics of the spin system, possibly described by spin glass models or fractal spin clusters. Recent measurements on qubits with different geometries indicate that the flux noise scales as (l/w), in agreement with the surface spin model (l) is the length and (l) is the width of the superconducting wires).

Flux noise correlations have been studied in a system of coupled qubits sharing parts of their loops. ¹⁸ It was found that the flux fluctuations originating from the shared branch lead to correlations in the noise of the two qubits. In this work, we use a single, two-loop qubit to investigate flux noise correlations between different parts within a single qubit [Fig. 1(b)]. The fluxes in the two loops couple to the longitudinal and transverse components of the qubit's Hamiltonian, respectively. The

ability to control both parameters of the Hamiltonian allows us to investigate qubit coherence properties at different frequencies while remaining at the optimal bias point. ¹⁹ By measuring the qubit dephasing rate as a function of the flux bias, we can extract the correlations between the flux fluctuations in the two loops. Knowing that the two fluxes couple differently to the qubit energy allows us to determine the sign of the correlations. We find the flux noise to be strongly anticorrelated, in agreement with a model where the noise is generated by spins on the superconductor surface.

II. SETUP

The standard flux qubit consists of a superconducting loop with three or more Josephson junctions [Fig. 1(a)]. The diabatic states correspond to clockwise and counterclockwise circulating currents, respectively. ^{20,21} When the flux in the loop is close to half a flux quantum, $\Phi = 0.5\Phi_0$, the Hamiltonian is $H = -(\frac{\Delta}{2}\sigma_x + \frac{\varepsilon}{2}\sigma_z)$ within a two-level approximation. Here, $\varepsilon = 2I_{\rm P}(\bar{\Phi} - 0.5\bar{\Phi}_0)$, where $I_{\rm P}$ is the persistent current and $\Phi_0 = h/2e$. The tunnel coupling Δ is fixed by fabrication and determined by the size of the smallest Josephson junction. By replacing the smallest junction with a second loop, the tunnel coupling Δ can be tuned in situ by the flux $\Phi_2 = f_2 \Phi_0$ in the second loop [Fig. 1(b)]. 19,22 Due to the device geometry, the detuning ε is controlled by the combined flux $(f_1 + f_2/2)\Phi_0$, where $f_1 = \Phi_1/\Phi_0$ is the normalized flux in loop 1.²¹ To clarify the relation between the qubit parameters and the two fluxes, we introduce the effective fluxes

$$f_z = (f_1 + f_2/2) - 1/2, \quad f_x = f_2.$$
 (1)

The energy separation of the qubit is then given by

$$E_{01}/h = \sqrt{\varepsilon^2 + \Delta^2}$$
, with $\varepsilon = \varepsilon(f_z)$, $\Delta = \Delta(f_x)$. (2)

The qubit is embedded in a dc SQUID for reading out the qubit state. The readout is implemented by applying a short current pulse to the SQUID; due to the inductive coupling between the SQUID and the qubit, the SQUID switching probability will vary depending on the qubit state.²³

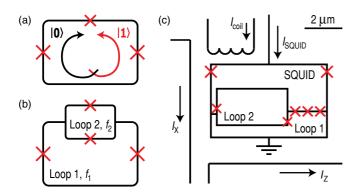


FIG. 1. (Color online) (a) A standard flux qubit. The two diabatic states correspond to clockwise and counterclockwise circulating currents. (b) A tunable flux qubit. The smallest junction has been replaced by an additional loop. (c) The actual sample design. The qubit is embedded in a SQUID used for readout of the qubit state. The line widths are not drawn to scale; a detailed drawing can be found in Appendix A.

The design of the actual device is shown in Fig. 1(c). The structure is made of aluminum and is fabricated using ebeam lithography and standard two-angle shadow evaporation techniques (see Appendix A for a detailed drawing). There are two local current-bias lines, which, together with the global external field, allow us to control the fluxes in the two qubit loops and in the readout SQUID independently. Due to the close proximity of the loops and the bias lines, there is substantial cross-coupling between the different elements. The measured inductive couplings are given in Appendix B. During the experiments, we applied appropriate compensation currents to the bias lines to compensate the unwanted couplings. The residual unwanted coupling is less than 1%.

III. RESULTS

Figure 2(a) shows two qubit spectra measured for two values of f_x . The measurement was done by applying a long microwave pulse (3 μ s) to saturate the qubit before reading out its state. The spectra have the form expected from Eq. (2), but with different values of Δ . The horizontal feature around 3.2 GHz is due to the plasma mode of the readout SQUID. In Fig. 2(b) we plot the measured Δ as a function of f_x . The tunnel coupling Δ is symmetric around $f_x = 0$ and can be tuned experimentally from 1.5 to 15 GHz. The dashed line shows the results of a numerical simulation of the qubit energy levels for realistic fabrication parameters. To quantify the relation between Δ and f_x we plot the numerical derivative of the data for a region around $f_x = 0.39$ [Fig. 2(c)]. We have marked the positions of the two operating points with $\Delta = 2.5$ GHz and $\Delta = 3.5$ GHz, where we perform coherence measurements. The sensitivity $\partial \Delta / \partial f_x$ is different for those two points.

The results in Fig. 2 show that our device behaves as expected and that we can tune the qubit parameters Δ and ε independently by applying fluxes in the two loops. To characterize the qubit coherence as a function of those parameters, we perform energy-relaxation (T_1) , free-induction decay (FID), and Hahn-echo measurements. T_1 is measured by applying a π pulse to the qubit and delaying the read-out. Figure 3(a) shows the extracted T_1 decay times as a

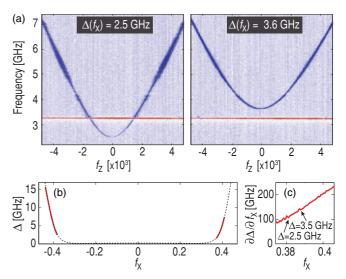


FIG. 2. (Color online) (a) Qubit spectra, measured for two values of f_x . The features at 3.2 GHz are due to the SQUID plasma frequency. Note that the scale for f_z is magnified by a factor of 1000. (b) Qubit tunnel coupling Δ measured as a function of f_x . The dashed line is the result of a numerical simulation. (c) Numerical derivative $\partial \Delta/\partial f_x$ of the data in (b).

function of detuning f_z , measured for the two values of Δ stated in Fig. 2(c). T_1 is fairly independent of f_z . The difference in T_1 for the two values of Δ can be attributed to differences in detuning from the SQUID plasma mode at $f_{\rm plasma} = 3.2$ GHz.

The FID sequence consists of two $\pi/2$ pulses separated by a time t. The FID is sensitive to low-frequency noise

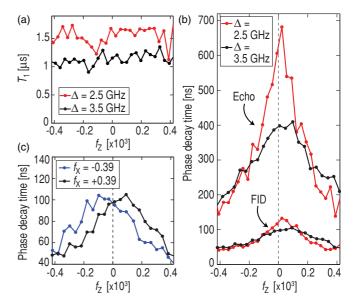


FIG. 3. (Color online) (a) Energy decay time T_1 . The decay does not depend strongly on the flux detuning. (b) Echo and free-induction decay times versus flux detuning. The position of the longest decay times is shifted to positive flux detuning. (c) Free-induction decay measured at $f_x = \pm 0.39$. Depending on the sign of f_x , the position of the longest decay time shifts in different directions. All measurements were done by sweeping f_z while keeping f_x constant.

that causes adiabatic fluctuations in the qubit energy splitting E_{01} . The Hahn echo contains an extra π pulse in the middle of the sequence to refocus low-frequency fluctuations. For Gaussian-distributed noise with a 1/f-type spectrum, the decay of both the FID and the Hahn echo has the form $p(t) = e^{-t/2T_1} e^{-(t/T_{\varphi(F/E)})^2}$. By first measuring T_1 , we can extract the pure dephasing times $T_{\varphi F}$ and $T_{\varphi E}$ for the FID and the Hahn-echo sequences, respectively.³

In Fig. 3(b) we plot $T_{\varphi F}$ and $T_{\varphi E}$ as a function of f_z for the two values of Δ . We make a few observations: (i) Time $T_{\varphi E}$ is 4–5 times longer than $T_{\varphi F}$, consistent with the 1/f-type spectrum.²⁴ (ii) Both $T_{\varphi F}$ and $T_{\varphi E}$ fall off as $|f_z|$ is increased; this is because $\partial E_{01}/\partial f_z$ is 0 only at $f_z = 0$ and increases approximately linearly with $|f_z|$ over this range of f_z . However, contrary to Refs. 3 and 25, the echo dephasing times are considerably shorter than the limit set by energy relaxation $(2T_1)$ even close to $f_z = 0$. This is a result of our device having an extra loop that controls Δ : fluctuations in f_x will couple to Δ , which will couple to E_{01} even when $f_z = 0$. (iii) Close to $f_z = 0$, the dephasing times are longer for $\Delta = 2.5 \text{ GHz}$ than for $\Delta = 3.5$ GHz: this is because the sensitivity $\partial \Delta / \partial f_x$ to noise in f_x is stronger at $\Delta = 3.5$ GHz [see Fig. 2(c)]. (iv) The longest dephasing times do not occur at $f_z = 0$ but are slightly shifted to positive f_z . The effect is visible for both values of Δ , but the shift is larger for $\Delta = 3.5$ GHz.

We investigate the shift in more detail by measuring the FID at $\Delta = 3.5$ GHz for positive and negative values of f_x . The results are shown in Fig. 3(c); at $f_x = -0.39$, the longest dephasing times are shifted toward negative f_z . Even though Δ is the same at both $f_x = 0.39$ and $f_x = -0.39$, the sensitivity $\partial \Delta / \partial f_x$ is negative for $f_x < 0$ and positive for $f_x > 0$. The fact that the shift depends on the sign of $\partial \Delta / \partial f_x$ leads us to suspect that there are correlations between f_x and f_z . We have checked that the shift does not depend on the SQUID bias current for small excursions from the operating point.26 Residual unwanted coupling between the bias lines and the loops may induce a small flux in f_x when sweeping f_z , which will cause uncertainty when determining the point of $f_z = 0$. However, having residual unwanted couplings of less than 1% gives an upper bound of $0.01 \times \Delta \times (\partial \Delta/\partial f_x)/(\partial \varepsilon/\partial f_z)^2 \sim 3 \times 10^{-6}$ for the uncertainty in f_z , which is considerably smaller than the shifts shown in Fig. 3(c).

IV. CORRELATIONS

The phase decay rate $\Gamma_{\varphi F}=1/T_{\varphi F}$ is due to a combination of noise in both f_x and f_z . To calculate $\Gamma_{\varphi F}$ in the presence of correlations, we assume that the fluctuations δf_x and δf_z are described by noise spectra of the form $S_{f_x}(\omega)=(A_x\Phi_0^{-2})/|\omega|$ and $S_{f_z}(\omega)=(A_x\Phi_0^{-2})/|\omega|$. In addition, we introduce the correlation spectrum $S_{f_zf_x}(\omega)=(A_{zx}\Phi_0^{-2})/|\omega|^{18,27}$ and the correlation coefficient $c_{zx}=\langle \delta f_z \delta f_x \rangle/\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_x^2 \rangle}=A_{zx}/\sqrt{A_xA_z}$. The correlation spectrum is thus assumed to have the same form as the individual noise spectra S_{f_x} and S_{f_z} . The total decay rate is²⁴

$$\Gamma_{\varphi F} = \frac{\ln(1/\omega_{\text{low}}t)}{\hbar \,\Phi_0^2} \left[A_x \left(\frac{\partial E_{01}}{\partial f_x} \right)^2 + A_z \left(\frac{\partial E_{01}}{\partial f_z} \right)^2 + 2 \, c_{zx} \sqrt{A_x A_z} \left(\frac{\partial E_{01}}{\partial f_x} \right) \left(\frac{\partial E_{01}}{\partial f_z} \right) \right]^{1/2}.$$
(3)

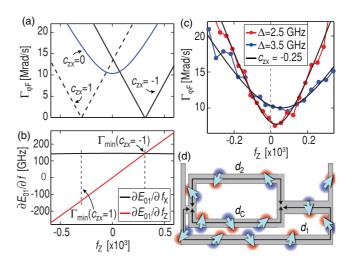


FIG. 4. (Color online) (a) Phase decay rate $\Gamma_{\varphi F}$ expected from the sensitivities shown in (b), with $A_z = A_x = (3 \,\mu \Phi_0^2)$. (b) Sensitivity of the qubit energy to flux fluctuations. For perfectly correlated noise $(c_{zx}=\pm 1)$, the fluctuations cancel out when $\partial E_{01}/\partial f_x = \mp \partial E_{01}/\partial f_z$. (c) Measured decay rate $\Gamma_{\varphi F}$. The fit gives a correlation factor of $c_{zx}=-0.25$. (d) Schematic picture of the surface-spin model. Spins located on the shared line labeled d_c induce fields pointing in opposite directions in the two loops.

The low-frequency cutoff $\omega_{\text{low}}/2\pi=1$ Hz is imposed by the measurement protocol. Figure 4(a) shows the result of Eq. (3), plotted for $A_z=A_x$ and three values of the correlation coefficient c_{zx} . Without any correlations ($c_{zx}=0$), the decay rate increases with $|f_z|$, and the value at $f_z=0$ is set by the noise in f_x . However, if we assume perfectly correlated ($c_{zx}=1$) or anticorrelated ($c_{zx}=-1$) noise, the point of minimal decay shifts to negative and positive values of f_z , respectively. In addition, the decay rate goes to 0 in those points.

To understand how correlations can lead to shifts of the dephasing times, we consider how the fluctuations in f_x and f_z couple to the energy splitting E_{01} . Figure 4(b) shows the sensitivities $\partial E_{01}/\partial f_x$ and $\partial E_{01}/\partial f_z$ for $\Delta=3.5$ GHz, extracted from the data in Fig. 2. If the noise is completely correlated, the fluctuations in E_{01} will perfectly cancel when $\partial E_{01}/\partial f_x = -\partial E_{01}/\partial f_z$. This happens at the point labeled $\Gamma_{\min}(c_{zx}=1)$ in Fig. 4(b). On the other hand, if the noise is perfectly anticorrelated, the fluctuations in E_{01} will cancel when $\partial E_{01}/\partial f_x = \partial E_{01}/\partial f_z$. This also explains why the phase decay data taken at $f_x = -0.39$ shift in the opposite direction [Fig. 3(c)]. Here, the derivative $\partial \Delta/\partial f_x$ is negative, which gives $\partial E_{01}/\partial f_x$ a minus sign and makes the points $\Gamma_{\min}(c_{zx}=1)$ and $\Gamma_{\min}(c_{zx}=-1)$ trade places.

We can fit the measured decay rate to Eq. (3) in order to extract the flux-noise amplitude and the correlation coefficient in our sample. The results are shown in Fig. 4(c), giving $A_z = (3.9 \, \mu \Phi_0)^2$, $A_x = (3.1 \, \mu \Phi_0)^2$, and $c = -0.25 \pm 0.05$. We stress that the same fitting parameters are used for both values of Δ . The reason why the data for $\Delta = 2.5$ GHz show a less dramatic shift in f_z is because $\partial E_{01}/\partial f_x$ is smaller at this value of Δ . The values for $\partial E_{01}/\partial f_x$ and $\partial E_{01}/\partial f_z$ used in the fits were extracted from Fig. 2, giving $\partial \varepsilon/\partial f_z = 1.37$ THz, $\partial \Delta/\partial f_x = 110$ GHz for $\Delta = 2.5$ GHz

and $\partial \varepsilon / \partial f_z = 1.28$ THz, $\partial \Delta / \partial f_x = 142$ GHz for $\Delta = 3.5$ GHz.

It is important to point out that the correlations discussed so far have been between fluctuations δf_z , δf_x in the *effective* fluxes defined by Eq. (1). The fluctuations and the correlations in the *geometric* fluxes f_1 , f_2 can be found by inverting Eq. (1). Assuming that the fluctuations δf_1 , δf_2 are described by spectra $S_{f_1}(\omega) = (A_1\Phi_0^{-2})/|\omega|$ and $S_{f_2}(\omega) = (A_2\Phi_0^{-2})/|\omega|$, we find (see Appendix C for a derivation)

$$A_{1} = A_{z} + A_{x}/4 - c_{zx}\sqrt{A_{z}A_{x}} = (4.5 \,\mu\Phi_{0})^{2},$$

$$A_{2} = A_{x} = (3.1 \,\mu\Phi_{0})^{2},$$

$$c_{12} = c_{zx}\sqrt{\frac{A_{z}}{A_{1}}} - \frac{1}{2}\sqrt{\frac{A_{x}}{A_{1}}} = -0.55.$$
(4)

Fabrication imperfections may cause deviations in the sizes of the two junctions in loop 2, which will affect Eq. (4). From the results in Fig. 2(b), we know that the junction asymmetry is less than $\pm 10\%$, which will lead to an uncertainty of the correlation coefficient c_{12} of about ± 0.1 . Note that the measurement is sensitive to correlations in the frequency range 1 Hz to ~ 1 MHz, as set by the FID weighting function. To exclude the influence from room-temperature electronics, we note that the noise from the current source has an A_i/f type noise spectrum with $A_i \sim (1 \text{ nA})^2.^{28}$ This will create $A_1 \sim (0.3 \, \mu \Phi_0)^2$ of flux noise in loop 1, which is an order of magnitude lower than the extracted noise amplitudes.

The results of Eq. (4) show that the flux fluctuations in the two loops of the sample are anticorrelated. This is clear evidence that the noise is not due to a global fluctuating magnetic field, since such fluctuations would give positive correlations. Instead, we consider a model where the noise is due to a large number of randomly oriented spins distributed over the metal surface [see Fig. 4(d)]. The spins will generate local magnetic fields that are picked up by the loops, and fluctuations of the spin orientations will give rise to flux noise. In our sample, spins that are located on the line that is shared by the loops [labeled d_c in Fig. 4(d)] will induce fields of opposite directions in loop 1 and loop 2. This will give rise to negative correlations between the fluxes in the loops.

To get an estimate of the expected correlations, we assume (i) that the field of a single spin only couples to a loop if it is sitting on that loop's circumference, (ii) that the width of the sample wires is constant, and (iii) that the amount of flux that a loop picks up from a single spin is independent of the spin's position along the width of the wire. The assumptions seem reasonable based on numerical simulations of the coupling between a SQUID and the magnetic moment of a single spin. Under these conditions the flux fluctuations generated by an ensemble of randomly oriented spins will scale as $\delta f \propto \sqrt{\rho \ d}$, where ρ is the spin density and d the length of the loop. The correlation coefficient becomes

$$c_{12} = \frac{\langle \delta f_1 \, \delta f_2 \rangle}{\sqrt{\langle \delta f_1^2 \rangle \langle \delta f_2^2 \rangle}} = \frac{-d_c}{\sqrt{(d_1 + d_c)(d_2 + d_c)}}.$$
 (5)

Here d_c is the length of the line segment shared by both loops, and d_1 , d_2 are the lengths of the remaining sections of the two

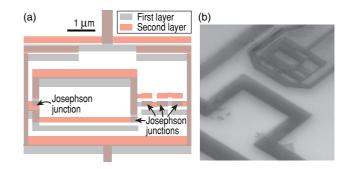


FIG. 5. (Color online) (a) Drawing of the device, showing the location of metal from the two evaporation stages. (b) SEM picture of a device with the same geometry as the one used in the experiments.

loops [Fig. 4(d)]. With values relevant for our sample $(d_1 = 10.8 \ \mu\text{m}, d_2 = 6.0 \ \mu\text{m}, d_c = 4.8 \ \mu\text{m})$, we find $c_{12} = -0.37$. This is smaller than the value extracted experimentally, but the agreement is reasonable considering the simplicity of the model. Further work is needed to develop a more realistic model of the device (see Appendix A) and to describe the correlations when spin interactions are taken into account. ^{15,16} We also note that the noise ratio A_1/A_2 roughly agrees with the ratio $(d_1 + d_c)/(d_2 + d_c)$ of the circumferences of the two loops, as expected from the surface spin model.

To conclude, we have investigated flux noise correlations by measuring dephasing rates in a tunable flux qubit. We find the flux fluctuations in neighboring loops to be anticorrelated, in agreement with predictions from models where the flux noise is generated by randomly oriented spins on the metal surface. The ability to extract noise correlations provides important information about the microscopic origin of the flux noise. The method presented here is general and can be extended to samples with different geometries. Combining this method with recent improvements in multipulse noise spectroscopy²⁵ opens up the possibility of measuring correlations at different frequencies and thereby probing the dynamics of the surface spin system.

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APPENDIX A: SAMPLE DETAILS

Figure 5(a) shows a drawing of the qubit, indicating the displacement of the two superconducting layers and the overlapping regions where Josephson junctions are formed. In Fig. 5(b), we show an SEM picture of a device with the same geometry as the one used in the experiments. The qubit and the readout SQUID are shown at the upper right in the figure. The two lines next to the qubit are the local flux bias lines, while the thicker line at the lower left is the microwave drive line.

APPENDIX B: INDUCTANCE MATRIX

The fluxes and currents are related by the inductance matrix

$$\begin{bmatrix} f_{SQ} \\ f_z \\ f_x \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} & M_{13} \\ M_{21} & M_{22} & M_{23} \\ M_{31} & M_{32} & M_{33} \end{bmatrix} \begin{bmatrix} I_{coil} \\ I_z \\ I_x \end{bmatrix}.$$

The matrix elements were determined by measuring ε , Δ , and the SQUID switching current as a function of the three bias currents, giving

$$M = \begin{bmatrix} \frac{1}{1.1648 \text{ mA}} (1 & 0.247 & 0.248) \\ \frac{1}{3.0055 \text{ mA}} (1 & 0.303 & 0.232) \\ \frac{1}{3.7817 \text{ mA}} (1 & 0.244 & 0.285) \end{bmatrix}.$$

APPENDIX C: DERIVATION OF FLUX CORRELATIONS

We start by defining the normalized fluxes $f_1 = \Phi_1/\Phi_0$ and $f_2 = \Phi_2/\Phi_0$ in the two qubit loops. Correlations between fluctuations δf_1 and δf_2 in these parameters are characterized by the correlation coefficient c_{12} , defined as

$$c_{12} = \frac{\langle \delta f_1 \, \delta f_2 \rangle}{\sqrt{\langle \delta f_1^2 \rangle \langle \delta f_2^2 \rangle}}.$$
 (C1)

The qubit parameters $\varepsilon = \varepsilon(f_z)$ and $\Delta = \Delta(f_x)$ are controlled by the effective fluxes

$$f_z = (f_1 + f_2/2) - 1/2,$$

 $f_x = f_2.$ (C2)

The coefficient for describing correlations between fluctuations δf_z and δf_x in the effective fluxes is given by

$$c_{zx} = \frac{\langle \delta f_z \, \delta f_x \rangle}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_x^2 \rangle}} = \frac{\langle (\delta f_1 + \delta f_2/2) \, \delta f_2 \rangle}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle}}$$
$$= \frac{\langle \delta f_1 \, \delta f_2 \rangle}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle}} + \frac{\langle \delta f_2^2 \rangle/2}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle}}.$$
 (C3)

We want to be able to extract c_{12} from the measured correlations c_{zx} between the effective fluxes. We start by inserting the expression for $\langle \delta f_1 \delta f_2 \rangle$ from Eq. (C1) into Eq. (C3). This

gives

$$c_{zx} = \frac{c_{12}\sqrt{\langle \delta f_1^2 \rangle \langle \delta f_2^2 \rangle}}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle}} + \frac{\langle \delta f_2^2 \rangle / 2}{\sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle}}$$
$$= c_{12}\sqrt{\frac{\langle \delta f_1^2 \rangle}{\langle \delta f_z^2 \rangle}} + \frac{1}{2}\sqrt{\frac{\langle \delta f_2^2 \rangle}{\langle \delta f_z^2 \rangle}}. \tag{C4}$$

Solving for c_{12} gives

$$c_{12} = c_{zx} \sqrt{\frac{\langle \delta f_z^2 \rangle}{\langle \delta f_1^2 \rangle}} - \frac{1}{2} \sqrt{\frac{\langle \delta f_2^2 \rangle}{\langle \delta f_1^2 \rangle}} = c_{zx} \sqrt{\frac{\langle \delta f_z^2 \rangle}{\langle \delta f_1^2 \rangle}} - \frac{1}{2} \sqrt{\frac{\langle \delta f_x^2 \rangle}{\langle \delta f_1^2 \rangle}}.$$
(C5)

In addition, we need to express the fluctuations $\langle \delta f_1^2 \rangle$ in terms of the effective fluctuations c_{zx} , $\langle \delta f_x^2 \rangle$, and $\langle \delta f_z^2 \rangle$. From the definition in Eq. (C2), we have

$$\langle \delta f_z^2 \rangle = \langle (\delta f_1 + \delta f_2/2)^2 \rangle = \langle \delta f_1^2 \rangle + \langle \delta f_1 \, \delta f_2 \rangle + \langle \delta f_2^2 \rangle / 4.$$
(C6)

Using the expression for $\langle \delta f_1 \, \delta f_2 \rangle$ from Eq. (C1), we get

$$\langle \delta f_z^2 \rangle = \langle \delta f_1^2 \rangle + c_{12} \sqrt{\langle \delta f_1^2 \rangle \langle \delta f_2^2 \rangle} + \langle \delta f_2^2 \rangle / 4.$$
 (C7)

Inserting the expression for c_{12} from Eq. (C5) gives

$$\langle \delta f_z^2 \rangle = \langle \delta f_1^2 \rangle + c_{zx} \sqrt{\langle \delta f_z^2 \rangle \langle \delta f_2^2 \rangle} - \frac{1}{2} \sqrt{\langle \delta f_x^2 \rangle \langle \delta f_2^2 \rangle} + \langle \delta f_2^2 \rangle / 4.$$
(C8)

Noting that $\langle \delta f_2^2 \rangle = \langle \delta f_x^2 \rangle$, we have

$$\langle \delta f_z^2 \rangle = \langle \delta f_1^2 \rangle + c_{zx} \sqrt{\langle \delta f_z^2 \rangle \langle \delta f_x^2 \rangle} - \langle \delta f_x^2 \rangle / 4.$$
 (C9)

Finally, solving for $\langle \delta f_1^2 \rangle$ gives

$$\langle \delta f_1^2 \rangle = \langle \delta f_z^2 \rangle + \langle \delta f_x^2 \rangle / 4 - c_{zx} \sqrt{\langle \delta f_z^2 \rangle \langle \delta f_z^2 \rangle}. \tag{C10}$$

We assume that the fluctuations δf_1 , δf_2 , δf_z , and δf_x are all described by noise spectra of the form $S_{f_1}(\omega) = A_1/|\omega|$, $S_{f_2}(\omega) = A_2/|\omega|$, $S_{f_z}(\omega) = A_z/|\omega|$, and $S_{f_x}(\omega) = A_x/|\omega|$. Using this and summarizing the results of Eq. (C5) and Eq. (C10), we get

$$A_{1} = A_{z} + A_{x}/4 - c_{zx}\sqrt{A_{z}A_{x}},$$

$$A_{2} = A_{x},$$

$$c_{12} = c_{zx}\sqrt{\frac{A_{z}}{A_{1}}} - \frac{1}{2}\sqrt{\frac{A_{x}}{A_{1}}}.$$
(C11)

This is Eq. (4) above.

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