Thermoelectric efficiency at maximum power in low-dimensional systems

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Low-dimensional electronic systems in thermoelectrics have the potential to achieve high thermal-to-electric energy conversion efficiency. A key measure of performance is the efficiency when the device is operated under maximum power conditions. Here we study the efficiency at maximum power, in the absence of phononmediated heat flow, of three low-dimensional, thermoelectric systems: a zero-dimensional quantum dot with a Lorentzian transmission resonance of finite width, a one-dimensional (1D) ballistic conductor, and a thermionic TI- power generator formed by a two-dimensional energy barrier. In all three systems, the efficiency at maximum power is independent of temperature, and in each case a careful tuning of relevant energies is required to achieve maximal performance. We find that quantum dots perform relatively poorly under maximum power conditions, with relatively low efficiency and small power throughput. Ideal one-dimensional conductors offer the highest efficiency at maximum power (36% of the Carnot efficiency). Whether 1D or TI systems achieve the larger maximum power output depends on temperature and area filling factor. These results are also discussed in the context of the traditional figure of merit *ZT*.

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I. INTRODUCTION

There is broad, current interest in developing highperformance thermoelectric (TE) materials for the generation of electric power from heat sources such as waste heat. Of particular interest are nanostructured materials for two primary reasons: first, a high density of interfaces, on a length scale comparable to the phonon mean-free path, can be used to reduce parasitic heat flow carried by the crystal lattice. $1-3$ Second, a reduced dimensionality of the electronic system, achieved by band engineering or by nanostructuring on the scale of the electron wavelength, can be used, in principle, to optimize a material's electronic properties. Specifically, sharp features of the electronic density of states (DOS) can increase the thermopower (Seebeck coefficient) S, which is a measure of the average kinetic energy of mobile electrons relative to the chemical potential, and can thus increase the power factor^{4-[8](#page-7-4)} $S^2 \sigma$, where σ is the electric conductivity.

To characterize a TE material, one commonly uses the figure of merit $ZT = S^2 \sigma T / (\kappa_e + \kappa_l)$ which is a function of the power factor and of the electron's (κ_e) and lattice's (κ_l) contributions to the parasitic thermal conductivity. *ZT* is closely related to the achievable efficiency of thermal-to-electric energy conversion. A delta-function-shaped DOS maximizes *ZT*, [6](#page-7-5) and can be used to establish reversible thermal-toelectric energy conversion at the thermodynamically maximal Carnot efficiency $\eta_C = \Delta T/T_H$,^{[9–](#page-7-6)[12](#page-7-7)} where $\Delta T = T_H - T_C$ is the temperature difference between a hot (H) and cold (C) electron reservoir at temperatures T_H and T_C , respectively (Fig. [1](#page-0-0)). The development of strategies to realize operation near η_C (Refs. [11](#page-7-8) and [13](#page-7-9)) helps understanding the sources of irreversible conversion losses and is thus of both fundamental and practical interest. However, efficiency near η_c requires near-reversible operation, a limit where the power output necessarily goes to zero. For practical applications it is thus of greater interest to understand the relationship between efficiency and power production. The relevant fundamental efficiency limit in this context is the Curzon-Ahlborn (CA) limit

$$
\eta_{CA} = 1 - \sqrt{T_C/T_H} \approx \frac{\eta_C}{2} + \frac{\eta_C^2}{8} + \mathcal{O}(\eta_C^3) + \cdots, \qquad (1)
$$

which is the thermodynamically maximum efficiency of a heat engine operating under conditions where the maximum power output is maximized[.14](#page-7-10) Esposito *et al.*[12,](#page-7-7)[15](#page-7-11) recently showed that zero-dimensional quantum dots (QDs) with a deltalike transmission function, tuned to produce maximum power, have a TE conversion efficiency that matches the CA limit up to quadratic terms in η_c . However, limiting the analysis to a deltalike transmission function sets the QDs power output to negligible values. Finite broadening of the transmission function is needed to reach full maximum

FIG. 1. (Color online) The basic setup considered here consists of a device described by its transmission function $\tau(E)$ (τ_{QD} and τ_{1D}) are sketched as examples), with contact leads that act as the hot and cold electron reservoirs. A bias voltage, *V*, is applied symmetrically with respect to the average chemical potential μ , which can be tuned relative to the transmission function, using a gate voltage.

power but is associated with a reduction in efficiency[.9](#page-7-6) Prior work has explored electron energy filters with a digital (on-off) energy dependence as a function of filter width.^{9[,16](#page-7-12)} The role of finite broadening of a single-energy level has also been considered for the nonlinear thermoelectric performance of a molecular junction.¹⁷ The properties of a realistic quantum-dot energy filter based on resonant tunneling have not yet been explored.

Here we ask: which low-dimensional electronic system yields the highest TE efficiency under maximum power conditions? Specifically, we address three idealized systems: first, a zero-dimensional QD with finite, Lorentzian broadening of the transmission resonances, allowing for maximized power production; second, an idealized quantum wire [onedimensional (1D)], and third, a two-dimensional (2D), TI energy barrier embedded into a bulk material with a lower band gap. Our goal is to establish which of these electronic systems fundamentally offers the best trade-off between thermoelectric power and efficiency. For this purpose, we assume ideal electronic properties such that our conclusions become independent of specific material parameters, such as mean-free paths, with the only exception of the effective mass in TI system. For the TI system, we also focus on the properties of the barrier itself, and do not consider the TE properties of the three-dimensional (3D) host material. In addition, we do not include the phonon contribution to heat flow in our calculations: it is external to the electronic system and can be added to the analysis by considering the associated parasitic heat flow.

Our work is complementary to recent work by Kim *et al.*[8](#page-7-4) who compared Seebeck coefficient *S* and power factor in generic 1D, 2D, and 3D electronic systems. That study found that, when tuning each system to its maximum power factor, $S_{1D} > S_{2D} > S_{3D}$, and that 1D systems also have the highest power factor per mode. Here, we add the QD and TI systems to the comparison, and do not focus on the power factor, which is evaluated under open-circuit conditions. Efficiency at maximum power, in contrast, is achieved under finite current conditions at a specific operating point, and we evaluate the actual power and efficiency at that operating point.

In the following, in Sec. [II,](#page-1-0) we will first describe our technical approach, and calculate for each system the operating conditions (in terms of bias voltage and position of the chemical potential) that produce, at given ΔT , maximum power, maximum efficiency (η_{max}) as well as maximum efficiency at maximum power $(\eta_{\text{max }P})$, and we discuss the mechanism that reduces η_{max} below the CA value for each system. For all three systems $\eta_{\max P}$ is found to be independent of temperature. We then compare our results across the three systems and place our results into the context of the traditional figure of merit, *ZT*.

II. MODELING DETAILS

Figure [1](#page-0-0) shows the generic device configuration considered here. A cold (C) and hot (H) electron reservoir each obey a Fermi-Dirac contribution,

$$
f_{H/C} = \left[1 + \exp\left(\frac{E - \mu_{H/C}}{k_B T_{H/C}}\right)\right]^{-1}.
$$
 (2)

For simplicity in the calculations, we assume that the voltage difference *V* is applied symmetrically across the device

 $(\pm V/2)$ such that the electrochemical potentials in the hot and cold electron reservoirs are given by $\mu_{H/C} = \mu \pm eV/2$, where μ is the chemical potential of the system at equilibrium (*V*=0).

The two reservoirs are connected by a device that acts as an energy-selective filter described by its transmission function $\tau(E)$, which depends on the dimensionality of the device. In an experiment, a gate can be used to tune μ relative to the device's transmission function, which we here assume to be independent of the gate voltage.

To generate thermoelectric power, the transmission function must be positioned such that high-energy electrons from the hot side can move, against applied bias voltage, into empty states on the cold side, but (ideally) not vice versa. Power is increased by large net electron flow from hot to cold, regardless of electron energy. Efficiency is optimized when this is achieved at minimal heat transport, for example, by suppressing the flow of electrons with relatively large kinetic energy (energy filtering).

In the following, we explore this balance of power and efficiency optimization, as a function of μ and *V*, for our three different low-dimensional systems. All numerical calculations are performed for a fixed ratio of $\Delta T/T_c$ =0.1. Note that, in general, nonlinear effects are important, and results will depend on ΔT for large $\Delta T/T$.^{[18](#page-7-14)}

A. Quantum dot

A quantum dot is a zero-dimensional system with welldefined energy levels defined by a combination of size quantization and Coulomb-repulsion effects. One implementation is a double-barrier resonant tunneling quantum dot embedded in a nanowire, $11,19$ $11,19$ with the leads corresponding to the electron reservoirs in Fig. [1.](#page-0-0)

Here we consider the use of a dot's discrete energy spectrum as an energy filter: the dot transmits electrons with energy corresponding to an energy level E_0 inside the dot via resonant tunneling. We assume that transport through the dot is elastic, and that the energy-level separation ΔE is much larger than the thermal energy *kT*, such that only the resonance located at E_0 contributes to electron transport.

Thermoelectric transport through a quantum dot with onedimensional leads can be described by the Landauer formalism,

$$
I = \frac{2e}{h} \int (f_H - f_C) \tau_{\text{QD}}(E) dE.
$$
 (3)

The transmission function τ_{QD} of a single energy level at energy E_0 is approximated by a Lorentzian function²⁰ as

$$
\tau_{\rm QD}(E) = \frac{(\Gamma/2)^2}{(E - E_0)^2 + (\Gamma/2)^2},\tag{4}
$$

where Γ is the full width at half maximum of the transmission function.

The net heat flux (\dot{Q}_H) out of the hot reservoir is given by,

FIG. 2. (Color online) (a) Power and (b) efficiency normalized by Carnot efficiency, of a QD as a function of bias voltage *V* and average chemical potential μ , for $T_C = 300 \text{ K}$, $T_H = 330 \text{ K}$ $(\Delta T/T_C=0.1)$, and Γ = 0.01*kT*. The open-circuit voltage, V_{oc} is highlighted in (red) dashed line (peak V_{oc} corresponds to *S* \approx 2 meV/K). The system works as a generator when the bias is between zero and V_{oc} . The vertical green line indicates the μ where maximum power occurs. (c) Current through a QD is the integral over the product of τ_{QD} (green) [Eq. ([3](#page-1-1))] and $\Delta f = (f_H - f_C)$, shown here in blue, using the μ and *V* that result in P_{max} . Two transmission widths, $\Gamma = 0.5kT$ and $5kT$ are plotted here in the approximate position where maximum power would be achieved.

$$
\dot{Q}_H = \frac{2}{h} \int (E - \mu_H)(f_H - f_C)\tau(E)dE, \tag{5}
$$

and electric power output and thermoelectric efficiency are given by $P = IV$ and $\eta = P/\dot{Q}_H$, respectively. In Figs. [2](#page-2-0)(a) and $2(b)$ $2(b)$, we show calculations of each of these quantities as a function of V and μ . Data are shown only where electric power is produced by the dot, and efficiency is normalized by η_c . The (red) dashed line, where the current driven by the temperature gradient is canceled by that driven by the voltage difference, represents the open-circuit voltage (V_{oc}) as a function of $(\mu - E_0)$. The line shape of V_{oc} is determined by the shape and width of the transmission function, 21 which results from the coupling strength to the leads, contributing tunneling processes,²² as well as by ΔE when $\Delta E \approx kT$ (Ref. [21](#page-7-17)) (this case is not considered here). Inside the pocket defined by V_{oc} , the system acts as a power generator. For ex-

FIG. 3. (Color online) Power versus normalized efficiency of a quantum dot for various Γ as indicated. The left vertical axis shows data for T_C = 300 K and T_H = 330 K whereas the right vertical axis shows the power for $T_C=1$ K and $T_H=1.1$ K. The shape of the curves does not depend on temperature.

ample, when μ is located within a few kT below a resonance of τ_{QD} (Fig. [1](#page-0-0)) at E_0 , hot electrons move from occupied states on the hot side to empty states on the cold side, even in the presence of a small counter bias.

Figures $2(a)$ $2(a)$ and $2(b)$ can be used to read out the operating points for maximum power and maximum efficiency, which occur at different sets of μ and *V*: efficiency is highest near $V \approx V_{oc}$, whereas power is optimized closer to $\mu \approx E_0$, and at intermediate *V*. This can be easiest understood by considering a narrow transmission function $(\Gamma \ll kT)$: in this case, the efficiency is maximal when the resonance is positioned at the energy where $(f_H - f_C) = 0$ [see Fig. [2](#page-2-0)(c)], because here transport is reversible, 9 and this equilibrium condition also defines V_{oc} . Power is maximized (i) when μ_H is lined up within a kT or so below E_0 , such that current is maximized, and (ii) when $V \approx V_{oc} / 2$, in order to optimize the product *P*=*IV*.

Note that the quantitative results presented here are for T_c = 300 K and T_H = 330 K. Whereas these are very high temperatures in the context of quantum-dot transport experiments, which are typically performed around 1 K, quantitative data at this temperature are easier to interpret in the context of thermoelectric applications. The results are valid as long as $kT \leq (\mu, \Delta E)$ and in the absence of electronphonon interactions, and for a QD we find that the thermoelectric properties scale as Γ/kT .

We now discuss the influence of the resonant level width Γ on the QD power and efficiency. We begin by tracing both power and efficiency along constant μ , that is, along a vertical line in Figs. $2(a)$ $2(a)$ and $2(b)$. For each operating point (μ, V) , we then graph the power at that point as function of the corresponding efficiency. The result is a loop, and all loops for all μ fill up a region in (η, P) space, whose shape and position depend on Γ , as shown in Fig. [3.](#page-2-1)

For a very small Γ (see $\Gamma = 0.01kT$ in Fig. [3](#page-2-1)), $\tau_{\text{QD}}(E)$ approaches a delta function, and the maximum efficiency approaches the Carnot limit, as expected 9 but the maximum power is very small. A larger Γ allows more electrons to contribute to power generation, and power increases until it reaches a peak value at $\Gamma \approx 2.25kT$, whereas the maximum efficiency monotonically decreases with increasing Γ (Fig. [4](#page-3-0)). To understand this behavior, consider Fig. $2(c)$ $2(c)$, which

FIG. 4. (Color online) η_{max} *p* (red, crosses) and η_{max} (blue, open dots), both normalized by Carnot efficiency, and maximum power (green, full dots) of a quantum dot as a function of Γ/kT for T_C = 300 K and T_H = 330 K. Maximum power peaks around Γ/kT = 2.25. Efficiency at maximum power $\eta_{\text{max }P}$ approaches η_{CA} = 51% for small Γ and is always smaller than η_{max} .

shows examples for $\tau_{\text{QD}}(E)$ overlayed onto $\Delta f = (f_H - f_C)$ at finite bias voltage. The integral over the product of both functions determines the current $[Eq. (3)]$ $[Eq. (3)]$ $[Eq. (3)]$. Electron transport is reversible (a requirement for Carnot efficiency) only where $\Delta f = 0.9$ $\Delta f = 0.9$ Away from this energy, electrons either travel in the wrong direction [where $\mu < E_n$ in Fig. [2](#page-2-0)(c)], or they carry excessive kinetic energy, wasting heat in electricity production. This explains the drop in efficiency for increasing Γ . As Γ increases, the Lorentzian-shaped $\tau_{\text{QD}}(E)$ samples over a wide energy range, and at some point it is not possible to increase Γ without also substantially sampling regions where Δf < 0, such that power decreases beyond an optimal value for Γ .

B. Nanowire

Here we consider an ideal 1D-electronic system with a width comparable to the Fermi wavelength (λ_F) , and with a length shorter than the electron mean-free path, such as a quantum point contact defined in a two-dimensional electron gas[.23](#page-7-19)[,24](#page-7-20) As a result of confinement, the electron energy is quantized in the two lateral dimensions but can assume any value along the transport direction *x*,

$$
E(x, y, z) = E_n(y, z) + \frac{\hbar^2 k_x^2}{2m^*},
$$
\n(6)

where $n \ge 1$ is the integer subband number and m^* is the electron effective mass.

Using a step-function shaped transmission function

$$
\tau_{1D}(E) = \sum_{n=1}^{\infty} \Theta(E - E_n)
$$
 (7)

in the Landauer formalism, we can calculate the current and heat flux out of the hot side using Eqs. (3) (3) (3) and (5) (5) (5) , respectively.²⁵ For a more realistic description of a quantumpoint contact, one can use the analytic transmission function of a saddle-point potential, $\tau(E) = \sum_{n=1}^{\infty} \left[1 + \exp\left(\frac{2\pi(E_n - E)}{\hbar \omega_x}\right)\right]^{-1}$ with $E_n = V_0 + (n - \frac{1}{2})\hbar \omega_y$, where V_0 is the height of the saddle, and the longitudinal and lateral curvatures of the saddle-point potential are characterized by the angular fre-

TABLE I. Comparing the maximum power and normalized efficiency at maximum power for step function and saddle-point transmission function. $\hbar \omega_v = 5$ meV, $T_C = 1$ K, and $T_H = 1.1$ K.

τ	p_{max} (fW)	Normalized EMP $(\%)$	ω_x/ω_v
Step fn.	1.8180	36.21	
$\hbar \omega_r = 0.01 kT$	1.8176	36.21	1.7×10^{-4}
$\hbar \omega_r = 0.1 kT$	1.8172	36.21	1.7×10^{-3}
$\hbar\omega_r = kT$	1.7746	35.66	1.7×10^{-2}

quencies, ω_x and ω_y , respectively. Note that as $\omega_x/\omega_y \rightarrow 0$, the saddle-point transmission approaches the step-function transmission. Maximum power and efficiency from the two transmission functions, for $\hbar \omega_v \gg kT$, agree within 2% for $\hbar \omega_x \le kT$ (Table [I](#page-3-1)), and in the following we use Eq. ([7](#page-3-2)).

The thermopower of a quantum-point contact is known to strongly depend on the number of occupied subbands, $25-27$ and as one may expect, we find the same for power and normalized efficiency as shown in Figs. $5(a)$ $5(a)$ and $5(b)$. The reason for why a wire with one occupied subband $(n=1)$ performs comparatively much better than the one with two occupied subbands $(n=2)$ is indicated in Fig. $5(c)$ $5(c)$: because transmission below the first subband is zero, it is possible to tune μ to a value just below E_1 , such that Δf (solid green line) allows electron flow only from hot to cold. This is not possible near the onset of the second subband (E_2) where Δf (solid brown line) will always allow parasitic electron backflow carried by the first subband, reducing current, power and efficiency. In the following, we therefore focus on wires with μ in the vicinity of E_1 and $(E_2 - E_1) \ge kT$.

Similar to the QD case, the power of a 1D power generator is largest within a few kT of E_1 [indicated in Fig. [5](#page-4-0)(a)], allowing significant thermal excitation from μ ^{μ} into the first 1D subband, and for $V \approx 0.5V_{oc}$, where the product *IV* is maximized.

C. Thermionic power generator

A thermionic refrigerator or power generator is based on an energy barrier that preferentially transmits electrons with high kinetic energy. Whereas the original concept²⁸ considered use of a vacuum diode, Shakouri and Bowers 29 introduced the use of semiconductor heterostructures with energy band-offsets more suitable for room temperature operation with high power density. It is important to note that a 2D energy barrier embedded into a 3D bulk material filters electrons with respect to their cross-plane momentum, and not actually with respect to their total energy. $10,30$ $10,30$ Here we assume conservation of in-plane momentum and a sufficiently thick barrier such that tunneling is suppressed, 31 and we assume ballistic and elastic transport across the barrier.

Using the Tsu-Esaki formula, 32 the current density is given by

$$
J = \frac{m^*e}{2\pi^2\hbar^3} \int \left[\zeta_H - \zeta_C \right] \tau(E_x) dE_x, \tag{8}
$$

where

FIG. 5. (Color online) Thermoelectric performance of a 1D conductor. (a) Power (nW) and (b) normalized efficiency, η/η_C , near the first (E_1) and second (E_2) subband edges for T_H = 330 K and T_c = 300 K. The full green line indicates the μ for maximum power output. (c) Transmission function τ_{1D} [Eq. ([7](#page-3-2)), blue line] and Δf $=f_H-f_C$ near the onset of the lowest (green) and second subbands (brown) with *V*=−2 mV and $(E_2 - E_1) = 0.5$ eV.

$$
\zeta_{H/C} = kT_{H/C} \log \left[1 + \exp \left(-\frac{E_x - \mu_{H/C}}{kT_{H/C}} \right) \right],\tag{9}
$$

and m^* is the effective mass of electrons. Disregarding tunneling, the transmission function [Fig. $6(c)$ $6(c)$] is given by

$$
\tau_{\rm TI}(E_x) = \Theta(E_x - E_b) \tag{10}
$$

with $E_b = (\hbar k'_x)^2 / 2m^*$ and $\hbar k'_x$ is the minimal cross-plane momentum needed to cross the barrier.

The heat flux out of the hot side per unit area is given by

$$
\dot{q}_H = \frac{m^*}{2\pi^2 \hbar^3} \int \left[\phi_H \zeta_H - \phi_C \zeta_C \right] \tau(E_x) dE_x, \tag{11}
$$

where $\phi_{H/C} = (E_x + kT_{H/C} - \mu_H)$ and power density (per unit area) and efficiency are obtained from $\mathcal{P}_{\text{TI}}=JV$ and η $=$ P/ \dot{q}_H , respectively, and are shown in Figs. [6](#page-4-1)(a) and 6(b) using the effective mass of GaAs, $m^* = 0.07m_e$. Because of the similarity in transmission functions, the TI results are qualitatively similar to those obtained in the 1D case, except that the maximum power for the TI system occurs for μ $>E_1$ (Ref. [8](#page-7-4)) [see also Fig. [6](#page-4-1)(c)].

FIG. 6. (Color online) (a) Power density (in MW/m^2) and (b) normalized efficiency η/η_C for a thermionic (TI) energy barrier as a function of *V* and μ for T_H =330 K and T_C =300 K. (c) Transmission function $\tau_{\text{TI}}(E)$ [Eq. ([10](#page-4-2))] and $\Delta \zeta = \zeta_H - \zeta_C > 0$ [Eq. ([9](#page-4-3))] for *V*=0 (green) and for *V*=−2 mV (brown) and for μ −*E*₁=0.05 eV where maximum power is produced. The choice of $\mu > E_1$ ensures that all of the region where $\Delta \zeta = \zeta_H - \zeta_C > 0$ contributes to current flow.

III. COMPARISON AND DISCUSSION

We now turn to a comparison of the three lowdimensional systems in terms of their performance under maximum power conditions. Care must be taken in a quantitative comparison of power numbers because the QD and 1D systems produce a certain amount of power per mode (or per device) whereas the TI system has a per-area power density. Here we choose to assume a specific cross section A_0 for a single 1D or QD device, and express the total power output of a TI device with area A_0 as

$$
P_{\rm TI} = \mathcal{P}_{\rm TI} A_0. \tag{12}
$$

In the following we choose $A_0 = (10 \text{ nm})^2$, that is, we consider, for example, an array of nanowires with one singlemode nanowire every 10 nm (a very high density³³). Note that no such scaling is needed for efficiency comparisons, where cross sections drop out.

A. Maximum power and efficiency at maximum power

In Fig. [7](#page-5-0) we show loop graphs in (η, P) space for the value of μ that yields maximum power in each system. The

FIG. 7. (Color online) (a)–(d) Loops along constant μ chosen at P_{max} of each system [i.e., along the green line of Figs. [2](#page-2-0)(b), [5](#page-4-0)(b), and $6(b)$ $6(b)$ show that efficiency at maximum power is independent of temperature. Note that the power values of the TI system depend on A_0 (see main text), whereas the efficiency values are independent of this choice. The QDs values depend on Γ .

horizontal position of the peak of each loop then corresponds to $\eta_{\text{max }P}/\eta_C$, the normalized efficiency at maximum power. We find that, under our assumptions, $\eta_{\text{max }P}$ is independent of temperature in each system (for constant Γ/kT in the case of QD). Analytically, this is because the parameters $(V, \mu, \text{ and})$ E) in the argument of Fermi-Dirac distribution are each scaled by thermal energy, and the integrand in the Landauer equation [Eq. ([3](#page-1-1))] is constant when Γ is also scaled with thermal energy. Note that $\eta_{\text{max }P}$ will certainly depend on temperature when, for example, temperature-dependent elastic or inelastic scattering rates are taken into account.

Quantitatively, we find that $\eta_{\text{max }P}/\eta_C$ approaches the Curzon-Ahlborn value 51% for a QD system with $\Gamma \ll kT$ [Fig. $7(a)$ $7(a)$], as expected¹² (see also Fig. [4](#page-3-0)). For $\Gamma = 2.25kT$ [Fig. $7(b)$ $7(b)$], where a QD system produces maximum power (see Fig. [4](#page-3-0)), we find a drastically reduced $\eta_{\text{max}} p / \eta_c = 17\%$. The corresponding values for the 1D and TI systems are 36% and 24%, respectively [Figs. $7(c)$ $7(c)$ and $7(d)$].

The first key finding of our paper is thus that the efficiency at maximum power of a 1D system exceeds that of both the QD $\left[$ at $\Gamma = 2.25kT$ where maximum power is reached, see Fig. $7(b)$ $7(b)$ and TI systems. Intuitively one may have expected this result: the main disadvantage of a QD system with finite Γ is the low-energy tail of the transmission function, which leads to parasitic backflow of electrons. 1D systems with their sharp onset of the transmission function at E_1 do not have this problem. TI systems, on the other hand, also have a sharp onset but are not actually energy filters, but filters for cross-plane momentum. Electrons with sufficient momentum to cross the barrier carry, on average, additional kinetic energy in their lateral degrees of freedom, wasting heat in the power-generation process[.10,](#page-7-25)[30](#page-7-26)[,34](#page-8-0)[,35](#page-8-1)

It should be noted that strategies exist that can improve the performance of a TI barrier by focusing electrons into the cross-plane direction, $30,34$ $30,34$ using processes that lead to nonconservation of electron momentum[.36](#page-8-2) In the interest of a transparent comparison of existing low-dimensional systems,

FIG. 8. (Color online) Maximum power as a function of temperature with $m^* = 0.7m_e$ and $\Delta T/T_C = 0.1$. T_\times is the temperature where 1D and TI systems yield the same power. T_{\times} depends on A_0 (see main text) and on the electron effective mass $[Eq. (8)$ $[Eq. (8)$ $[Eq. (8)$. see also Fig. [9](#page-5-2)].

such additional effects are not considered here.

Turning now to a comparison of the absolute power val-ues, we show in Fig. [8](#page-5-1) that maximum power scales with T^2 in the QD and 1D cases, and with T^3 for TI system. Note that this result is specific for a TI barrier that filters forward momentum only, and would likely be different for an "ideal" barrier that acts as a true energy barrier.^{10,[30,](#page-7-26)[34](#page-8-0)[,35](#page-8-1)} Overall, OD systems have the lowest power output per mode or per area. Comparing 1D and TI systems, there exists a crossover temperature (T_{\times}) , above which the TI system has the higher total power output. The value of T_{\times} decreases with m^* (because the TI power is proportional to m^*) and decreases with A_0 because a smaller A_0 corresponds to a higher power density in 1D systems (Fig. 9).

B. Relation to the figure of merit

In this section we wish to place our results into the context of the traditional figure of merit for thermoelectric systems,

$$
ZT = \frac{S^2 \sigma}{\kappa_e + \kappa_l} T = \frac{S^2 \sigma T}{\kappa_e} \left(\frac{\kappa_e}{\kappa_l + \kappa_e} \right) = (ZT)_{el} \left(\frac{\kappa_e}{\kappa_l + \kappa_e} \right),
$$
\n(13)

where *T* needs to be taken as the average temperature (T_C) $+T_H$ /2. In the following we focus on $(TT)_{el}$, the electronic

FIG. 9. (Color online) T_{\times} as defined in Fig. [8](#page-5-1) as a function of effective area A_0 of a 1D system for different effective mass: InAs (0.023 m_e), GaAs (0.07 m_e), and PbTe (0.17 m_e).

FIG. 10. (Color online) (a) Power factor S^2G (blue) and thermal conductance (green), (b) $(TT)_{el}$ (brown) and P_{max} (cyan) as a function of $\mu - E_0$ for a quantum dot with $\Gamma = 0.01kT$ and $T_C = 300$ K and T_H = 330 K.

part of ZT as defined in Eq. (13) (13) (13) , that is, we continue to assume $\kappa_l = 0$.

Unlike P_{max} and η_{max} , $(ZT)_{el}$ is not evaluated at a specific working point with finite power output. Specifically, *S* and κ are defined at the open-circuit condition (*I*=0), and σ is evaluated at $\Delta T = 0$ in the linear-response limit $(V \rightarrow 0)$. We therefore evaluate κ_e along the open-circuit curve, e.g., the red line in Fig. [2](#page-2-0)(b). It is the ratio of σ and κ_e that enters *ZT*, and it can be written as

$$
\frac{\sigma}{\kappa_e} = \frac{G}{K} = \frac{(dI/dV)_{\Delta T=0}}{(Q_H/\Delta T)_{I=0}}.
$$
\n(14)

where G is the electrical conductance and K is the electronic thermal conductance.

Figure [10](#page-6-0) shows the power factor (S^2G) , *K*, $(ZT)_{el}$, and P_{max} for a QD with a small Γ =0.01*kT* at T_C =300 K and T_H =330 K. The power factor has a characteristic doublepeak structure³⁸ which results from the line shape of a QDs Seebeck coefficient [Figs. $2(a)$ $2(a)$ and $2(b)$]. For small Γ , $(ZT)_{el}$ can reach enormously high values. 37

Based on *ZT*, one can predict a thermoelectric system's maximum efficiency from Ref. [39](#page-8-5) by

$$
\eta = \frac{M-1}{M + T_C/T_H} \eta_C,\tag{15}
$$

where $M = \sqrt{1+ZT}$. In Fig. [11](#page-6-1) we show a comparison of this equation (full line) with the exact calculations of η_{max} [extracted from Fig. $2(b)$ $2(b)$, graphed as a function of the maximum $(ZT)_{el}$ (Fig. [10](#page-6-0)) for many different values of Γ , and confirm the figure of merit *ZT* is an excellent predictor of the maximum efficiency, also in QDs. By comparison to Fig. [4,](#page-3-0) we also find that η_{max} (predicted by *ZT*) and η_{max} *p* agree

FIG. 11. (Color online) Plot of η/η_c vs $(ZT)_{el}$ for various values of Γ as indicated in the legend. The blue solid line is Eq. ([15](#page-6-3)).

quite well except for very small Γ , where the highest efficiency is achieved. However, $(ZT)_{el}$ alone is clearly not a good predictor of maximum power: P_{max} peaks at a value for Γ where $(ZT)_{el}$ is well below its maximum value.

Figure [12](#page-6-2) show S^2G , *K*, $(ZT)_{el}$, and P_{max} , for the 1D and TI systems. Note that *G* and *K* for the TI system have been obtained by multiplying σ and κ_e with $A_0 = 100$ nm². In each case, the behavior of $(ZT)_{el}$ as a function of $(\mu - E_1)/kT$ results from that of the Seebeck coefficients, gradually increasing for μ below the band edge, and $(ZT)_{el}$ as a function of $(\mu - E_1)/kT$ is independent of temperature. Note that our value for S^2G of 1D system is identical with the result in Ref. [8.](#page-7-4) Like in the case of a QD, the divergence of $(ZT)_{el}$ for small μ is misleading as the power peaks for a finite value of μ .

ZT-*el* is much higher than experimental results *ZT* $\approx 0.1-1$ for thermoelectric systems in general. However, if one includes the lattice (phonon) contribution to calculate the full *ZT*, the modeling results would reduce substantially, to those practically observed, since κ_l is usually much higher than κ_e in semiconductor materials. In the interest of generality, we here do not include the material-dependent κ_l into our comparison.

FIG. 12. (Color online) (a) Power factor and thermal conductance, (b) $(ZT)_{el}$ and P_{max} of 1D, as a function of $(\mu - E_1)/kT$ with T_C =300 K and T_H =330 K. (c) and (d) power factor, thermal conductance, $(ZT)_{el}$, and P_{max} of the same condition for TI system. Note that *G* and *K* are obtained by assuming the effective area to be 100 nm². $(ZT)_{el}$ of 1D is independent of temperature.

IV. CONCLUSIONS

We compared thermoelectric efficiency in the maximum power regime for a quantum dot, a one-dimensional ballistic wire, and a thermionic power generator, each tuned to produce maximum thermoelectric power. Specifically, we considered finite Γ for the QD system, and found that maximum power is produced for $\Gamma = 2.25kT$. Out of these three systems, the 1D system offers the highest achievable efficiency at maximum power, whereas above a crossover temperature *T* a thermionic energy barrier produces the higher power per area. In our analysis we neglected the influence of parasitic heat flow carried by phonons which, in all cases, will reduce the efficiency by a factor $Q_H/(\dot{Q}_{ph} + \dot{Q}_H)$. In a comparison between a 1D system realized using nanowires and TI systems, the influence of phonons may be to the advantage of nanowires, as surface scattering in nanowires strongly suppresses lattice heat conductivity in nanowires to a value significantly below the bulk value. $40-45$ $40-45$ However, a full comparison for a specific application certainly needs to be material specific, and should take into account the influence of a finite mean-free path,⁸ possible momentum nonconser-

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vation for electron flow across a TI barrier, which can be used to enhance the TI system's performance, $30,36$ $30,36$ and the thermoelectric properties of the material in which a TI barrier is embedded. 18 In order to place our results into context we also calculated the traditional figures of merit for each system, finding that the electronic $(ZT)_{el}$ is indeed a good predictor of the maximum electronic efficiency, but not generally for $\eta_{\text{max }P}$. More importantly, $(ZT)_{el}$, which theoretically can be made arbitrarily large for each of the three systems studied, does not predict the working point where maximum power is achieved.

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