# Damping and decoherence of a nanomechanical resonator due to a few two-level systems

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We consider a quantum model of a nanomechanical flexing beam resonator interacting with a bath comprising a few damped tunneling two-level systems. In contrast with a resonator interacting bilinearly with an ohmic free oscillator bath (modeling clamping loss, for example), the mechanical resonator damping is amplitude dependent, while the decoherence of quantum superpositions of mechanical position states depends only weakly on their spatial separation.

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## I. INTRODUCTION

The past few years have seen dramatic progress toward achieving the necessary conditions for demonstrating macroscopic quantum behavior in mechanical systems. Schemes under investigation typically consider either micronscale mechanical resonators that are electrostatically coupled to superconducting qubits (quantum electromechanical systems)<sup>2-5</sup> or larger mechanical mirror resonators that couple via radiation pressure to light trapped in an optical cavity (optomechanical systems). One of the prime motivations for demonstrating quantum behavior is to deepen our understanding of the so-called quantum-classical divide. In particular we would like to understand how classical dynamics emerges from the underlying quantum dynamics as system sizes (i.e., mass/energy content) increase.<sup>6</sup> It is commonly accepted that the environmental degrees of freedom with which the mechanical resonator's mode of interest interacts are responsible for the emergence of classicality.<sup>7,8</sup> In particular, the environment is thought to cause the rapid decoherence of initial quantum superposition states of the mechanical mode, resulting in an apparent classical mixture of the states. There is a considerable body of theoretical work investigating the effective quantum dynamics of open, single particle systems. 9,10 Largely for reasons of calculational convenience, however, much of the effort has been devoted to the solvable model of an environment comprising noninteracting oscillators that are bilinearly coupled to a single oscillator system. 11,12 In light of the experimental progress mentioned above, an important issue is the actual nature of the dominant mechanical resonator mode environments. At the very low (i.e., cryogenic) temperatures to which the resonators must be cooled in order to observe quantum effects, it is not a priori obvious that the resonator mode dynamics can be mapped onto that of the oscillator system-oscillator bath model. In the present paper, we focus on a type of environment degree of freedom that is known to be relevant at low temperatures, namely the tunneling two-level system. 13,14

Tunneling two-level system (TLS) defects were first invoked in the early seventies in order to account for the observed thermodynamic properties of amorphous, dielectric materials at low temperatures. <sup>15,16</sup> Further, convincing evi-

dence for their presence was provided by acoustic phonon pulse decay and phonon pulse echo experiments. 17-19 In particular, these experiments verified the characteristic saturation of TLS's with increasing acoustic pulse intensity for resonant phonon absorption and also measured TLS relaxation and dephasing times. TLS's have recently received renewed interest as one of the main decay/decoherence mechanisms for superconducting qubits.<sup>20-27</sup> Signatures include resonant splittings induced in the qubit energy level spectra, 20,21,26 and saturation of microwave power absorption by the dielectric oxide layer of the qubit tunnel junctions. 21,25 In contrast to the bulk amorphous dielectric materials involved in earlier investigations, the much smaller, micronscale superconducting qubits have gigahertz frequency energy level separations exceeding the dilution fridge  $k_BT$ thermal energies. This characteristic points to a distinct and less explored regime in which the system qubit resonantly couples strongly to only a few TLS defects, as opposed to a dense spectrum. Similarly, it may be the case that, given the much smaller volumes ( $\sim 10^{-18}$  m<sup>3</sup>) of the micronscale mechanical resonators currently under investigation, the relevant system-environment model is an oscillator interacting with only a few TLS's. In the following sections we shall analyze such a system.

In Sec. II we give some simple estimates based on existing bulk system TLS theory in order to motivate our mechanical resonator mode-few TLS model, as well as to anticipate some of the consequences of TLS-dominated mechanical damping/decoherence. In Sec. III we derive the model closed system resonator-TLS Hamiltonian, and in Sec. IV we present the open system master equation with further details of the derivation given in the Appendix. Section V focuses on the effect of a few TLS's on the resonator damping, while Sec. VI describes the consequences for the decoherence of mechanical resonator superposition states. Section VII provides a few concluding remarks.

Although the present paper focuses on the role of TLS's in micronscale mechanical oscillator damping and decoherence, we do not completely neglect other mechanisms. In the spirit of keeping our model as simple as possible, we lump together all other relevant damping and decoherence mechanisms, such as clamping loss, <sup>28–31</sup> as an additional oscillator

bath to which the mechanical system mode couples. This will allow us to gauge somewhat the extent to which other baths "interfere" with the TLS bath in their damping and decoherence effects on the oscillator system. For example, the system oscillator's net damping rate need not be the sum of the damping rates due to the individual baths. One point that should be emphasized in this context is the highly nonlinear, quantum nature of the coupled oscillator-TLS (equivalently spin-1/2) dynamics. Exact analytical or even simpler approximate equations are hard to come by and so we will resort to solving for the full dynamics using numerical methods. We will be limited computationally to considering only a few TLS's—three to be precise. In future work we plan to find ways to analyze the effects of larger numbers of TLS's on mechanical damping/decoherence.

Another source of nanomechanical damping and decoherence that we do not explicitly take into account is the measurement process itself.<sup>32–34</sup> The resonator damping described in Sec. V can be probed using, for example, continuous in time position detection with a single electron transistor.<sup>2,4</sup> We shall assume that the resulting back reaction on the resonator due to the position detector can be simply modeled by the same additional oscillator bath at some finite temperature.<sup>35,36</sup> The resonator superposition state decoherence described in Sec. VI can be probed using, for example, the microwave cavity-superconducting qubit scheme outlined in Refs. 37 and 38.

In the present paper we neglect mechanical strain (i.e., phonon) mediated coupling between TLS's, assuming the latter to couple directly only to the oscillator system mode. We treat the TLS's damping phenomenologically, characterized by a decay time  $T_1$ . Given our current, almost complete lack of theoretical understanding of the role of TLS's for damping and decoherence in nano-to-mesoscale mechanical resonators, we feel that it is worthwhile to start with this simpler, noninteracting TLS model. The low-temperature acoustic pulse probe investigations of bulk amorphous solids 17,19 and the mechanical quality factor and resonant frequency measurements of much larger resonators<sup>39,40</sup> point to the likely importance of interactions between TLS's. 41-43 For example, phonon echo experiments yield TLS dephasing times that are much shorter than their  $T_1$  lifetimes, thought to be due to TLS spectral diffusion arising from the phonon mediated interaction between nonresonant TLS's. 41 With the significantly reduced volumes of nano-to-mesoscale mechanical resonators, these strain interactions may in fact be considerably enhanced. We plan to analyze the effects of such TLS interactions on nanomechanical damping/decoherence in a future work.

## II. SOME ESTIMATES

In this section we adopt various results from earlier analyses of bulk, amorphous systems to try to gain some initial idea of expected consequences for damping/decoherence of nano-to-mesoscale mechanical resonators due to TLS's. We begin by estimating the number magnitude of TLS's that are near resonance with the mechanical mode frequency of interest, which we shall in this paper assume to be the lowest,

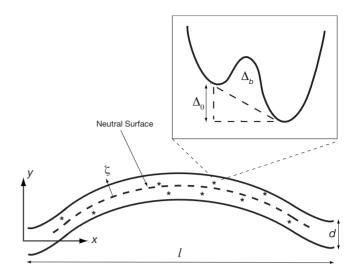


FIG. 1. Flexing doubly-clamped beam (exaggerated for clarity). Inset: TLS double well potential.

flexural mode. For a range of bulk, amorphous solids, experiments are consistent with a TLS distribution of the form<sup>14</sup>

$$dN = V \frac{\overline{P}}{\Delta_b} d\Delta_0 d\Delta_b, \tag{1}$$

where V is the mechanical resonator volume,  $\Delta_0$  and  $\Delta_b$  are the asymmetry and tunnel splitting energies of the TLS's potential double well (see Fig. 1), and  $\bar{P}$  is the approximately constant spectral density that can be expressed as

$$\bar{P} = C \frac{\rho v^2}{v^2}.$$
 (2)

Here,  $\rho$  is the mass density,  $\nu$  is the (isotropic) deformation potential, and v is the (isotropic and polarization independent) speed of sound. The dimensionless constant  $C \sim 10^{-4}-10^{-3}$  is approximately universal. 44,45 Of course, the nanomechanical resonator may not be fashioned out of one of the amorphous materials surveyed in Ref. 45, but instead out of a crystalline material. In such a case we view Eq. (1) and the estimates we shall now derive for the total TLS number as providing an upper bound. The energy eigenvalues of a given TLS are  $\pm \frac{1}{2} \sqrt{\Delta_0^2 + \Delta_b^2}$  [see Eq. (18)], so that the energy level separation of the TLS is  $E = \sqrt{\Delta_0^2 + \Delta_b^2}$ . Integrating the distribution Eq. (1) to obtain the total number of TLS's in energy width  $\delta E$  about a given TLS energy level separation  $E = \sqrt{\Delta_0^2 + \Delta_b^2}$ , we obtain:

$$\delta N = \frac{1}{2} V \bar{P} \ln \left[ \frac{1 + \sqrt{1 - (E_{\text{min}}/E)^2}}{1 - \sqrt{1 - (E_{\text{min}}/E)^2}} \right] \delta E, \tag{3}$$

where  $E_{\rm min}$  is the low-energy cutoff in the TLS distribution. <sup>46</sup> Taking the typical ballpark values  $\rho v^2 \sim 10^{11}~{\rm kg~m^{-1}~s^{-2}}$  and  $v \sim 1~{\rm eV}$ , Eq. (2) gives for the spectral density  $\bar{P} \sim 10^{44} - 10^{45}~{\rm J^{-1}~m^{-3}}$ . Substituting this into Eq. (3) and taking  $E = \hbar \omega$  (i.e., in resonance with the oscillator mode  $\omega$ ),  $\delta E = \hbar \omega/Q$ , where Q is the oscillator mode quality factor, and  $E_{\rm min}/k_B = 1~{\rm mK}$ , we obtain for our total TLS number

close to resonance expressed in natural units:

$$\delta N \sim 0.1 - 1 \frac{(V/\mu \text{m}^3)(f/\text{GHz})}{(O/10^4)}.$$
 (4)

Thus, according to this estimate, micron scale, radio frequency mechanical resonators are on the borderline between being unlikely to have a single TLS close to resonance and being very likely with a moderate increase in size.

We next estimate the nanomechanical fundamental mode displacement amplitudes that saturate the TLS's. Observation of quantum effects in the mechanical dynamics will require cooling the resonator such that  $k_BT \lesssim \hbar \omega$ . In this regime, resonant absorption damping is expected to dominate. Theory of resonant TLS mechanical damping and acoustic pulse decay in large amorphous resonators and bulk solids gives for the energy damping rate<sup>47</sup>

$$\Gamma_{\text{damp}} \approx \frac{\pi C \omega}{\sqrt{1 + (\epsilon \nu / \hbar)^2 T_1 T_2}} \tanh\left(\frac{\hbar \omega}{2k_B T}\right),$$
(5)

where C is the same dimensionless constant as introduced above,  $\epsilon$  is the elastic strain amplitude (approximated as isotropic),  $\nu$  is the deformation potential,  $T_1$  is the TLS damping time, and  $T_2$  is the TLS transverse relaxation time, related to the dephasing time  $T_{\phi}$  as  $T_2^{-1} = (2T_1)^{-1} + T_{\phi}^{-1}$ . From Eq. (5), we see that the damping rate decreases for increasing strain  $\epsilon$ , a consequence of the mechanical motion exciting the TLS's so that they cannot subsequently absorb additional vibrational energy, otherwise known as TLS saturation. The strain dependence of the damping rate becomes noticeable when  $(\epsilon \nu/\hbar)^2 T_1 T_2 \gtrsim 1$ , so that the saturation threshold strain can be defined as

$$\epsilon \sim \frac{\hbar}{\nu \sqrt{T_1 T_2}}.$$
 (6)

For the example of a doubly-clamped beam mechanical resonator of length l, thickness d, and midpoint transverse displacement amplitude Y (see Sec. III), the volume averaged rms strain is  $\bar{\epsilon} \sim dY/l^2$ . Substituting this into Eq. (6) and expressing it in terms of natural units, we obtain for the saturation threshold amplitude

$$(Y/\text{Å}) \sim 10^{-6} \frac{(l^2/\mu\text{m}^2)}{(\nu/\text{eV})(d/\mu\text{m})\sqrt{(T_1T_2/\mu\text{sec}^2)}}.$$
 (7)

Earlier phonon echo experiments in fused silica glass found TLS damping and transverse relaxation times  $T_2 \sim 10 \mu \text{sec}$ ,  $\sim 100 \mu sec$ and respectively,  $T \approx 20$  mK.<sup>19</sup> Thus, the transverse relaxation is dominated by dephasing:  $T_2 \approx T_{\phi}$ . The quantum zero-point displacement uncertainties of micron-scale mechanical resonators are  $\sim 10^{-4} - 10^{-3} \text{ Å}.^2$  Substituting into Eq. (7) the micronscale resonator dimensions, a typical magnitude deformation potential  $\nu$  of an eV, and the above relaxation times, we get a saturation displacement amplitude that is considerably smaller than the zero-point displacement uncertainty. Based on these estimates, we thus expect that experiments which measure damping and decoherence of such resonators will operate well within the saturation regime.

One important consequence of TLS saturation for the mechanical resonator damping rate can be seen from the dependence of  $\Gamma_{\rm damp}$  on the elastic strain  $\epsilon$  in Eq. (5). Given that  $\epsilon$  scales with the resonator's transverse displacement amplitude Y, the resonant TLS-dominated mechanical resonator damping rate will in turn be amplitude dependent. Thus, the effective mechanical oscillator equation of motion will experience a nonlinear damping force that depends on both the position and velocity coordinates of the oscillator.

Our final estimate concerns the decoherence of mechanical superposition states. For weak mechanical damping (i.e.,  $Q \gg 1$ ) and provided temperatures are not too low (i.e.,  $k_BT \gg \hbar\omega/Q$ ), the effective dynamics of an oscillator bilinearly interacting with a bath of free oscillators satisfies a quantum fluctuation-dissipation relation between the system oscillator's damping and decoherence rates:

$$\Gamma_{\text{decohere}} = \frac{1}{2} \Gamma_{\text{damp}} \left( \frac{\Delta Y}{Y_{zp}} \right)^2 \coth \left( \frac{\hbar \omega}{2k_B T} \right), \tag{8}$$

where  $\Delta Y$  is the uncertainty in the oscillator's position and  $Y_{zp} = \sqrt{\hbar/(2m\omega)}$  is the oscillator's quantum zero-point position uncertainty. Ref. 8 gives the high temperature limit of this relation. Assuming that this fluctuation-dissipation relation applies also to the bulk oscillator with the TLS bath, we can substitute in expression (5) for the damping rate to obtain the decoherence rate. The first thing to notice is the cancellation of the hyperbolic temperature functions. Below the saturation threshold we would therefore conclude that the decoherence rate is temperature independent while the damping rate is temperature dependent for an oscillator coupled to a TLS bath. In this respect, the oscillator system-TLS bath is "dual" to the oscillator system-oscillator bath in the sense that the decoherence rate of the latter has the inverse temperature dependence of the damping rate of the former, while the damping rate of the latter and decoherence rate of the former are both temperature independent.<sup>48</sup> However, this duality is to a certain extent academic since the above saturation estimates suggest that nano-to-mesoscale mechanical resonators will be well within the saturation regime for quantum superpositions of distinct position states that must necessarily be larger than the zero-point position uncertainty. As a consequence, the temperature dependences of the TLS  $T_1$ and  $T_2$  dependent terms must also be taken into account. Since a good understanding of the relaxation mechanisms of TLS's is lacking in nano-to-mesoscale mechanical resonators, 49 we will not attempt to make predictions for the temperature dependences of various observable quantities in the present paper.

Leaving aside temperature dependencies, another notable consequence of applying the quantum fluctuation-dissipation relation Eq. (8) to the oscillator system-TLS bath is the weaker (i.e., linear) dependence of the decoherence rate on oscillator position uncertainty. Plugging  $\Gamma_{\rm damp}$  from Eq. (5) into Eq. (8), we see that the Y dependence of the strain  $\epsilon$  cancels one factor of  $\Delta Y$  in Eq. (8), resulting in a linear dependence on position uncertainty. Thus, at low temperatures the decoherence rate should increase more gradually as the position separation in the quantum superposition state is

increased, as compared with the quadratic separation dependence for the oscillator bath. Of course, other decoherence mechanisms, e.g., due to clamping loss, will then be expected to eventually dominate if they have the stronger quadratic dependence.

Summarizing the findings of this section, we expect that a relevant model for a nano-to-micronscale mechanical resonator interacting with TLS's is a single oscillator coupled to a bath of a few TLS's. Furthermore, we expect that mechanical damping will show an amplitude dependence, while the decoherence of mechanical superposition states will depend weakly on their position separation. The following sections will bear out these expectations.

#### III. RESONATOR-TLS HAMILTONIAN

In this section we will derive the Hamiltonian describing the dynamics of the lowest, fundamental flexural mode of a doubly-clamped beam mechanical resonator interacting with TLS's that are located randomly throughout the beam volume. Related analyses are given in Refs. 49 and 50. We shall assume a long, thin, elastically isotropic beam with length l, width w, and thickness d satisfying  $l \gg w > d$ , mass density  $\rho$ , and bulk modulus K (Fig. 1).

The equation of motion for small transverse displacements y(x,t), 0 < x < l, of the beam is<sup>51</sup>

$$\rho \frac{\partial^2 y}{\partial t^2} + Kb^2 \frac{\partial^4 y}{\partial x^4} = 0, \tag{9}$$

where  $b=d/\sqrt{12}$  is the bending moment and we assume zero applied longitudinal strain. The total energy of the beam is

$$E = \frac{1}{2}\rho w d \int_0^l dx (\dot{y})^2 + \frac{1}{2}Kw db^2 \int_0^l dx (y'')^2.$$
 (10)

Solving Eq. (9) with clamped boundary conditions y(0) = y(l) = y'(0) = y'(l) = 0, we obtain for the lowest-frequency (fundamental) eigenmode:

$$y(x,t) = Y(t)\frac{\phi(x)}{\phi(l/2)},\tag{11}$$

where the normalized eigenfunction is

$$\phi(x) = A \left\{ \left[ \sin\left(\frac{\pi \alpha x}{l}\right) - \sinh\left(\frac{\pi \alpha x}{l}\right) \right] + \beta \left[ \cos\left(\frac{\pi \alpha x}{l}\right) - \cosh\left(\frac{\pi \alpha x}{l}\right) \right] \right\}, \quad (12)$$

with  $\alpha \approx 1.51$  obtained from the clamped boundary condition expression  $\cos(\pi\alpha)\cosh(\pi\alpha)=1$  and  $\beta=[\cos(\pi\alpha)-\cosh(\pi\alpha)]/[\sin(\pi\alpha)+\sinh(\pi\alpha)]\approx-1.02$ . The constant  $A\approx 0.983$  is fixed by requiring that  $\phi(x)$  be normalized as follows:

$$l^{-1} \int_0^l dx \, \phi^2(x) = 1. \tag{13}$$

The time-dependent part of the solution (11) is  $Y(t) = \text{Re}(Y_0 e^{i\omega t})$ , where the fundamental mode frequency is

$$\omega = b \left(\frac{\pi \alpha}{l}\right)^2 \sqrt{\frac{K}{\rho}} \approx 6.46 \frac{d}{l^2} \sqrt{\frac{K}{\rho}}.$$
 (14)

The solution (11) is expressed such that Y(t) gives the transverse displacement of the beam at its midpoint x=l/2. Substituting Eq. (11) into the total energy Eq. (10) and employing the normalization condition (13), we obtain

$$E = \frac{1}{2}m\phi^{-2}(l/2)\dot{Y}^2 + \frac{1}{2}m\phi^{-2}(l/2)\omega^2Y^2,$$
 (15)

where  $m=\rho wdl$  is the mass of the resonator. Thus, the fundamental mode dynamics is that of a harmonic oscillator with effective mass

$$m_{\text{eff}} = \frac{m}{\phi^2(l/2)} \approx \frac{m}{2.52},\tag{16}$$

where, from Eq. (12), we have used  $\phi(l/2) \approx 1.59$ .

Quantizing the fundamental mode, we introduce mode raising and lowering operators  $\hat{a}^+$ ,  $\hat{a}$ ;  $[\hat{a}, \hat{a}^+]=1$ , with

$$\hat{Y} = Y_{7p}(\hat{a} + \hat{a}^{+}),$$
 (17)

where  $Y_{zp} = \sqrt{\hbar/(2m_{\rm eff}\omega)}$  is the quantum zero-point displacement uncertainty. The free beam, fundamental mode Hamiltonian is then simply  $\hat{H}_m = \hbar \omega (\hat{a}^{\dagger} \hat{a} + 1/2)$ .

Moving now to the TLS Hamiltonian, we have

$$\hat{H}_{TLS} = \sum_{i=1}^{N} \left[ \frac{1}{2} \Delta_0^{(j)} \sigma_z^{(j)} + \frac{1}{2} \Delta_b^{(j)} \sigma_x^{(j)} \right], \tag{18}$$

where  $j=1,2,\ldots,N$  labels the TLS,  $\Delta_0^{(j)}$  is the asymmetry of the jth TLS's potential well, and  $\Delta_b^{(j)}$  is the TLS tunnel splitting which depends on the well barrier height and width (see Fig. 1). Mechanical resonator motion couples to a TLS largely through the strain dependence of the asymmetry energy:

$$\Delta_0^{(j)}[\epsilon_{kl}] \approx \Delta_0^{(j)} + 2\sum_{k,l=1}^3 \nu_{kl} \epsilon_{kl}^{(j)}, \tag{19}$$

where  $v_{kl}$  is the deformation potential and  $\epsilon_{kl}$  is the elastic strain tensor. For small amplitude, transverse y(x,t) flexural displacements of long, thin beams, the nonvanishing strain tensor components for a defect located at x and a distance  $-d/2 \le \zeta \le d/2$  normal to the neutral (i.e., strain-free) surface (see Fig. 1) are  $\epsilon_{xx} \approx -\zeta d^2 y/dx^2$  and  $\epsilon_{yy} = \epsilon_{zz} \approx \sigma \zeta d^2 y/dx^2$ . Here  $\sigma$  is Poisson's ratio, the relation of compressional strain normal to the axis of stretching to extension strain along the axis of stretching. From Eqs. (11) and (17), the transverse displacement field operator is

$$\hat{y}(x) = \frac{\phi(x)}{\phi(l/2)} Y_{zp}(\hat{a} + \hat{a}^{+}). \tag{20}$$

Substituting Eq. (20) into Eq. (19), we obtain for the mechanical resonator-TLS defect interaction Hamiltonian

$$\hat{H}_{\text{int}} = \sum_{i=1}^{N} \lambda^{(i)} (\hat{a} + \hat{a}^{+}) \sigma_{z}^{(j)}, \qquad (21)$$

where the resonator-TLS strain coupling strength for defect j located at  $(x_i, \zeta_i)$  in the beam takes the form

$$\lambda^{(j)} = -Y_{zp}\nu(1 - 2\sigma)\zeta_j \frac{\phi''(x_j)}{\phi(l/2)}$$
 (22)

and we have assumed for simplicity an isotropic deformation potential coupling  $\nu$ . Finally, writing out the full resonator-TLS system Hamiltonian, we have

$$\hat{H}_{S} = \hbar \omega (\hat{a}^{+} \hat{a} + 1/2) + \sum_{j=1}^{N} \left[ \frac{1}{2} \Delta_{0}^{(j)} \sigma_{z}^{(j)} + \frac{1}{2} \Delta_{b}^{(j)} \sigma_{x}^{(j)} + \lambda^{(j)} (\hat{a} + \hat{a}^{+}) \sigma_{z}^{(j)} \right].$$
(23)

The strength of the coupling  $\lambda^{(j)}$  depends on the location of the TLS defect. In particular, the coupling is strongest for a defect on the surface at the beam ends, i.e.,  $\zeta_j = \pm d/2$  and  $x_j = 0$ , l. In order to gain a sense of the expected magnitudes of the coupling, it is convenient to express the various beam material constants and dimensions in natural units. We obtain for the dimensionless coupling strength:

$$\frac{\lambda^{(j)}}{\hbar\omega} \approx -10^{-3} \left(\frac{\zeta_j}{d}\right) \left(\frac{\phi''(x_j)}{\phi''(0)}\right) \\
\times \left(\frac{\rho}{10^3 \text{ kg m}^{-3}}\right)^{1/4} \left(\frac{K}{10^{11} \text{ N m}^{-2}}\right)^{-3/4} \left(\frac{\nu(1-2\sigma)}{\text{eV}}\right) \\
\times \left(\frac{l}{\mu\text{m}}\right)^{1/2} \left(\frac{w}{\mu\text{m}}\right)^{-1/2} \left(\frac{d}{\mu\text{m}}\right)^{-1}, \tag{24}$$

while the fundamental flexural mode frequency  $\omega$  expressed in natural units is:

$$\left(\frac{\omega}{\text{GHz}}\right) \approx 8.2 \left(\frac{\rho}{10^3 \text{ kg m}^{-3}}\right)^{-1/2} \left(\frac{K}{10^{11} \text{ N m}^{-2}}\right)^{1/2} \\
\times \left(\frac{l}{\mu \text{m}}\right)^{-2} \left(\frac{d}{\mu \text{m}}\right).$$
(25)

## IV. OPEN SYSTEM MASTER EQUATION

In this section we derive the master equation for the coupled resonator-TLS system, taking into account the environment of the system. In an actual beam mechanical resonator, the fundamental flexural mode will couple not only to the TLS defects, but also to the other, higher-frequency resonator modes via anharmonic interaction terms. The fundamental mode will also couple to bulk, substrate modes at the beam supports. Furthermore, the TLS's will couple to the higher-frequency resonator modes through the strain dependence of the TLS's asymmetry energies. The latter will not only cause damping of the TLS's, <sup>49</sup> but will also induce interactions between the TLS's. <sup>41,43,52</sup> However, our goal in the present investigation is not to accurately model the respec-

tive environments of the fundamental mode and TLS's, but rather as a first step to consider the simplest possible idealized model environments in order to gain an idea of the quantum dissipation and decoherence dynamics of the mechanical resonator interacting with damped TLS's.

As idealized model environments, we consider baths of noninteracting harmonic oscillators. Hamiltonian Eq. (23) is then augmented by the environment Hamiltonian and coupling term:

$$H_{\text{env}} + H_{S-\text{env}} = \sum_{n} \hbar \omega_{n} b_{n}^{+} b_{n} + \sum_{j=1}^{N} \sum_{n} \hbar \omega_{n} c_{n}^{(j)+} c_{n}^{(j)}$$

$$+ Y \sum_{n} \kappa_{n} (b_{n}^{+} + b_{n})$$

$$+ \sum_{j=1}^{N} \sigma_{z}^{(j)} \sum_{n} \widetilde{\kappa}_{n}^{(j)} (c_{n}^{(j)+} + c_{n}^{(j)}), \qquad (26)$$

where recall  $Y=Y_{zp}(a+a^+)$  and for notational convenience we have dropped the hats on the operators and have also neglected the bath zero-point contributions. In our model each TLS is assumed to couple with strength  $\widetilde{\kappa}_n^{(j)}$  to an independent, noninteracting oscillator bath, characterized by environment mode operators  $c_n^{(j)}$ ,  $j=1,2,\ldots,N$ . The environment mode operators  $b_n$  couple directly to the resonator with strength  $\kappa_n$ , collectively modeling all energy loss mechanisms other than those involving the TLS's, such as clamping loss and anharmonic processes. Combining Hamiltonians Eqs. (23) and (26), we have the total system-environment Hamiltonian  $H=H_S+H_{\rm env}+H_{S-\rm env}$ .

In the Appendix we apply the self-consistent Born approximation together with a Markov approximation to obtain the following master equation describing the dissipative dynamics of the coupled resonator-TLS system:

$$\dot{\rho}_{S}(t) = -\frac{i}{\hbar} [H_{S}, \rho_{S}(t)] - \frac{i\gamma}{2\hbar} [Y, \{P_{Y}, \rho_{S}(t)\}] - \frac{m\omega\gamma}{2\hbar} \coth\left(\frac{\hbar\omega}{2k_{B}T}\right) \\ \times [Y, [Y, \rho_{S}(t)]] - \sum_{j=1}^{N} \frac{1}{4T_{1}^{(j)}} \left(\frac{E^{(j)}}{\Delta_{b}^{(j)}}\right)^{2} [\sigma_{z}^{(j)}, [\sigma_{z}^{(j)}, \rho_{S}(t)]] \\ - \sum_{j=1}^{N} \frac{i}{4T_{1}^{(j)}} \left(\frac{E^{(j)}}{\Delta_{b}^{(j)}}\right) \tanh\left(\frac{E^{(j)}}{2k_{B}T}\right) [\sigma_{z}^{(j)}, \{\sigma_{y}^{(j)}, \rho_{S}(t)\}], \quad (27)$$

where  $\rho_S(t)$  is the resonator-TLS system density matrix,  $P_Y$  is the resonator momentum,  $\{\cdot,\cdot\}$  denotes the anticommutator and  $E^{(j)} = \sqrt{(\Delta_0^{(j)})^2 + (\Delta_b^{(j)})^2}$  is the jth TLS energy level separation. The parameter  $\gamma$  gives the energy damping rate of the resonator in the absence of the TLS, while  $T_1^{(j)}$  gives the jth TLS relaxation time from its excited energy eigenstate in the absence of the resonator.

One potential advantage of the damping time/rate parameterization used in Eq. (27) is that it does not in fact depend explicitly on the microscopic nature of the environment and how it couples to the system. As long as the Markov approximation can be made and the fluctuation-dissipation theorem holds, then the damping and diffusion terms are uniquely related so that Eq. (27) can be assumed to apply for other system-environment interactions as well. This then allows

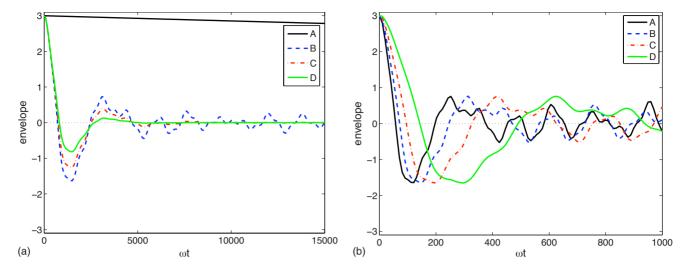


FIG. 2. (Color online) (a) Envelope of the motion of the resonator coupled to an on-resonance TLS for  $T_1 \approx 6.5 \times 10^4$  (B),  $T_1 \approx 1.6 \times 10^4$  (C), and  $T_1 \approx 6.5 \times 10^2$  (D). The solid black curve (A) shows the damping of the resonator with no TLS coupling. For all curves  $\lambda = 10^{-2}$ ,  $\Delta_0 = 0$ ,  $\Delta_b = 1$ ,  $\gamma = 10^{-5}$ , T = 2.02. (b) Dependence of the resonator ensemble-averaged amplitude vs time for different resonator-TLS coupling constants  $\lambda$ . Parameters are the same as (a), with  $T_1 \approx 6.5 \times 10^4$ ,  $\lambda = 0.125$  (A),  $\lambda = 0.1$  (B),  $\lambda = 0.075$  (C), and  $\lambda = 0.05$  (D).

environment model-independent predictions for the open system dynamics provided that they are expressed in terms of the damping parameters  $\gamma$  and  $T_1^{(j)}$ , as opposed to predictions concerning the explicit temperature dependence, which depend on the nature of the TLS environment.

## V. DAMPING

In this and the following section, we present the results of numerically solving the master Eq. (27) using the quantum optics toolbox.<sup>53</sup> Most of the results are for the mechanical resonator mode subsystem only with the TLS sector of state space traced over; we assume that it is the resonator mode which is directly probed in experiment.

We begin this section with a focus on the damping of the mechanical resonator coupled to a single TLS. Both the resonator and the TLS are coupled to independent Ohmic oscillator baths. We assume that the system is initially in a product state,  $\rho_S(0) = \rho_{\rm res}(0) \otimes \rho_{\rm TLS}(0)$ , where the TLS is initially in a thermal state  $\rho_{\rm TLS}(0) = \exp[-H_{\rm TLS}/k_BT]/Z$  with  $H_{\rm TLS}$  defined in Eq. (18) and  $Z = {\rm Tr}(\exp[-H_{\rm TLS}/k_BT])$ . Similarly, the initial resonator state is a thermal state with  $H_m = \hbar \omega (a^\dagger a + 1/2)$  that has been displaced using the operator  $d = \exp[x_0(a^\dagger - a)/2]$ , where  $x_0$  is the initial displacement of the thermal state from equilibrium in units of the quantum zeropoint displacement uncertainty  $Y_{zp}$  defined in Eq. (17); from now on we use x to denote the mechanical resonator fundamental mode displacement in units of the zero-point uncertainty.

We use Eqs. (24) and (25) to determine the resonator-TLS coupling constant  $\lambda$  and the fundamental flexural mode frequency  $\omega$ . For  $l=10~\mu\text{m}$ ,  $w=1~\mu\text{m}$ ,  $d=0.1~\mu\text{m}$ , we find  $\lambda/\hbar\omega\approx10^{-2}$  and  $\omega\approx2\,\pi\times100~\text{MHz}$ . Where convenient, we shall use dimensionless time units,  $t\!\rightarrow\!\omega t$ , with  $T_1$  and  $\gamma$  expressed as  $\omega T_1$  and  $\gamma/\omega$ , respectively, and  $\lambda$ ,  $\Delta_i$ , and temperature T expressed as  $\lambda/\hbar\omega$ ,  $\Delta_i/\hbar\omega$ , and  $k_BT/\hbar\omega$ , respectively.

We begin with a symmetric TLS ( $\Delta_0$ =0) that is on resonance with the mechanical oscillator ( $\Delta_b = 1$ ). In Fig. 2(a), we plot the envelope of the resonator's ensemble-averaged position versus time, corresponding to the so-called interaction picture or rotating frame, where the resonator and TLS's rapid free evolution are factored out. We give the resonator an initial displacement  $x_0=3$  and assume a range of experimentally realistic values for the TLS relaxation time that are relevant at mK temperatures, 1  $\mu \sec \lesssim T_1 \lesssim 100 \ \mu \sec^{20} \text{We}$ also assume that the resonator's energy damping rate due solely to its Ohmic bath (i.e., in the absence of the TLS) to be  $\gamma = 10^{-5}$ . Comparing the envelope of the resonator's motion at T=10 mK (=2.02 in dimensionless units) for  $T_1$ = 100  $\mu$ sec (=6.5 × 10<sup>4</sup> in dimensionless units) (curve B) to the envelope of the resonator in the absence of the TLS (curve A), we see that the TLS and its bath cause significant amplitude damping of the resonator, even for large values of  $T_1$ . Figure 2(a) also shows an increase in the damping of the resonator for decreasing values of  $T_1$ ; for shorter TLS damping times, energy exchanged between the resonator and the TLS is more quickly dissipated through the TLS bath.

Note also from Fig. 2(a) that the resonator's average position damps out and then revives on time scales much less than the TLS relaxation time,  $T_1$ , appearing to indicate a complete transfer of energy from the mechanical resonator to the TLS. However, the on-resonance TLS can only absorb a maximum of one quantum (phonon) of vibrational energy, while the energy stored in the resonator for the considered initial displacement  $x_0$ =3 corresponds to more than one phonon on average. This apparent paradox is resolved by noting that the quantum resonator's average energy depends on the average of the position squared, not the square of the average; not all of the energy is transferred to the TLS when the average position completely damps out. This can be seen in Fig. 3, where the individual resonator and TLS energies, as well as the total TLS+resonator energy, are plotted over time.

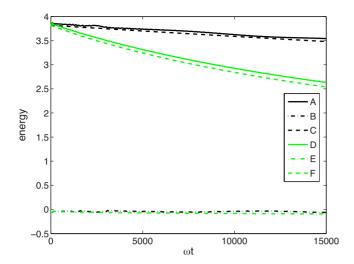


FIG. 3. (Color online) Dependence of resonator and TLS average energy vs time for the same parameters as those used in Fig. 2(a), with  $T_1 \approx 6.5 \times 10^4$  (black) and  $T_1 \approx 6.5 \times 10^2$  (gray). (A, D) Resonator energy; (B, E) TLS energy; (C, F) Resonator+TLS energy.

Energy is able to be transferred between the oscillator and the TLS because of the long TLS  $T_1$  times. If  $T_1$  is shorter then the energy transferred to the TLS dissipates to its bath more rapidly, with the result that less energy returns to the oscillator. The effect of a shorter  $T_1$  on the oscillator and oscillator+TLS energy is shown in Fig. 3. Figure 2(b) demonstrates the dependence of the resonator dynamics on the oscillator-TLS coupling constant  $\lambda$ . For weaker couplings the damping out and revival of the oscillator's motion occurs at later times.

Because a TLS absorbs only a finite amount of energy  $E = \sqrt{\Delta_0^2 + \Delta_b^2}$ , it can become saturated, affecting its influence on the resonator damping rate. In Fig. 4 we plot the resonator amplitude decay rate  $\gamma_A$  versus time for a range of initial displacements  $x_0$ , where  $\gamma_A$  is defined as follows:

$$\gamma_A = -\frac{\partial}{\partial(\omega t)} \ln(\langle x(\omega t) \rangle).$$
(28)

In order to display trends in damping more clearly we have increased the values for  $\gamma$ ,  $\lambda$ , and  $T_1^{-1}$ , shortening the time over which the damping takes place. We see in Fig. 4 that as  $x_0$  increases, the initial decay rate of the resonator decreases.

For a large initial displacement,  $x_0=10$  (D), the initial decay rate approaches that of the resonator in the absence of the TLS (E), suggesting near total saturation of the TLS. For later times, however, when the resonator amplitude has decaved to a value near the zero-point displacement, the decay rates for all four initial displacements approach a common, constant value. For  $x_0=5$  this value is reached at  $\omega t \approx 250$ , while for  $x_0 = 10$  this value is reached at  $\omega t \approx 375$ . We know that the oscillator bath's contribution to damping is constant at all times [Fig. 4(E)], whereas the resonator coupled to the TLS shows amplitude-dependent damping initially, and amplitude-independent damping at later times [Fig. 4(A)-4(D)]. These two distinct behaviors indicate that the TLS is indeed saturated at higher resonator amplitudes, while for lower amplitudes the TLS is unsaturated and its contribution to damping is therefore uniform. On the right-hand side of Fig. 4 we investigate the  $T_1$  dependence of the amplitude at which the crossover from amplitude-dependent to amplitude-independent damping occurs. The crossover amplitude  $x_{CO}$  is plotted as a function of  $T_1$ , showing a nearly linear relationship.

Figure 5 shows the damping of a resonator with initial displacement  $x_0$ =5 coupled to both an oscillator bath and a TLS (A), and coupled to the TLS (B), and oscillator bath (C) individually. Curve D is the sum of curves B and C. The substantial difference between curves A and D demonstrates that one cannot simply add the individual damping rates to obtain the net TLS+oscillator bath damping rate when both these sources are present.

So far we have considered just the special case of a symmetric ( $\Delta_0$ =0) and resonant ( $\Delta_b$ =1) TLS. In an actual me-

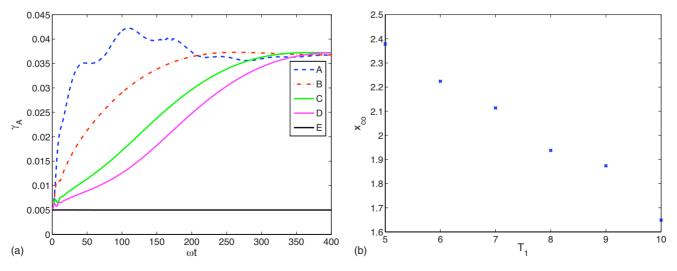


FIG. 4. (Color online) (a): Amplitude decay rate of resonator coupled to TLS with  $T_1$ =10 for  $x_0$ =3 (A),  $x_0$ =5 (B),  $x_0$ =8 (C),  $x_0$ =10 (D) and without TLS (E) as a function of time. (b): Dependence of crossover amplitude  $x_{CO}$  on  $T_1$  for  $x_0$ =8. For all curves  $\lambda$ =0.1,  $\Delta_0$ =0,  $\Delta_b$ =1,  $\gamma$ =0.01 and T=1.

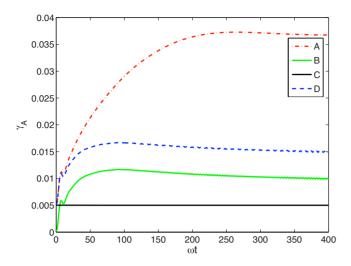


FIG. 5. (Color online) Decay rate of resonator for  $x_0$ =5 with TLS and oscillator bath (A), with TLS only (B), with oscillator bath only (C), and sum of curves B and C (D). For all curves  $\lambda = 0.1$ ,  $\lambda_0 = 0$ ,  $\lambda_b = 1$ ,  $\gamma = 0.01$ , T = 1, and  $T_1 = 10$ .

chanical resonator there will be a distribution of TLS's, not necessarily symmetric or on resonance [see Eq. (1)]. In Fig. 6, we show the resonator's amplitude damping rate  $\gamma_A$  for a range of TLS  $\Delta_0$  and  $\Delta_b$  values. In the absence of a TLS,  $\gamma_A$  is equal to half the energy damping rate,  $\gamma$ , due to the oscillator bath. Figure 6 shows that  $\gamma_A$  is greatest for  $\Delta_0$ =0 and  $\Delta_b$ =1, and sharply decreases to  $\gamma/2$  as  $\Delta_b$  is moved off resonance. The resonator's damping rate decreases more gradually as the TLS is made more asymmetric ( $\Delta_0 \neq 0$ ). The damping rates in this figure were extracted from an oscillator with small initial displacements in the range of constant values shown in Fig. 4, and therefore showed no time or amplitude dependence.

We now consider the damping of the resonator coupled to three TLS's, which have energies close to the resonator energy. The TLS's  $\Delta_i$  values are indicated by the diamond, circle, and triangle symbols in Fig. 7. The TLS energies were selected randomly from within the range  $0.75 \le E \le 1.25$  using the distribution Eq. (1).

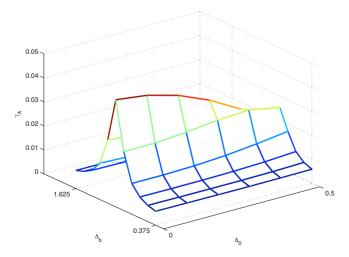


FIG. 6. (Color online) Resonator damping rate for various values of  $\Delta_0$  and  $\Delta_b$ . The parameter values  $\lambda$ ,  $\gamma$ , T, and  $T_1$  are the same as those used in Fig. 4.

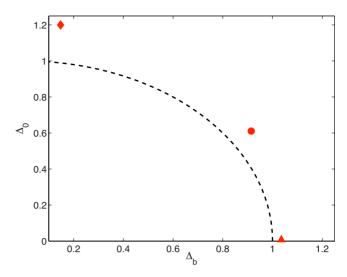


FIG. 7. (Color online) Considered distribution of TLS's. The energies of the TLS's are  $\Delta_0$ =1.2002 and  $\Delta_b$ =0.1475 (diamond),  $\Delta_0$ =0.6108 and  $\Delta_b$ =.9145 (circle),  $\Delta_0$ =0.0070 and  $\Delta_b$ =1.0354 (triangle). The dashed line denotes the TLS energy on resonance with the mechanical oscillator.

As is the case for a single TLS, we expect the damping of the resonator when coupled to multiple TLS's to show amplitude dependence for early times due to TLS saturation. Figure 8 shows the decay in the presence of the three TLS's and the oscillator bath for three different initial displacements  $x_0$  (curves A, B, C). As expected, the resonator decays more quickly for smaller initial displacements, while for larger initial displacements the decay rate approaches that due to the oscillator bath only, indicating saturation. Unexpectedly, at later times there is a crossover to a much slower, constant decay rate that is even less than that of the resonator in the absence of the TLS's, i.e., due to the oscillator bath only. The amplitude of the envelope at which the crossover occurs appears to be different for each of the curves in Fig. 8, which are normalized to allow comparison of resonator

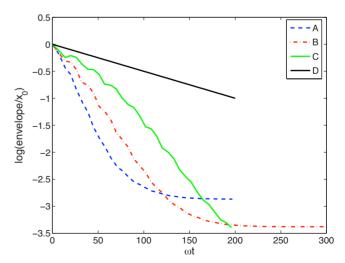


FIG. 8. (Color online) Damping of the oscillator coupled to three TLS's with initial displacements  $x_0$ =3 (A),  $x_0$ =5 (B), and  $x_0$ =8 (C). For all curves  $\lambda$ =0.1,  $\gamma$ =0.01, T=1, and  $T_1$ =10. (D) shows the damping of the oscillator in the absence of the TLS's.

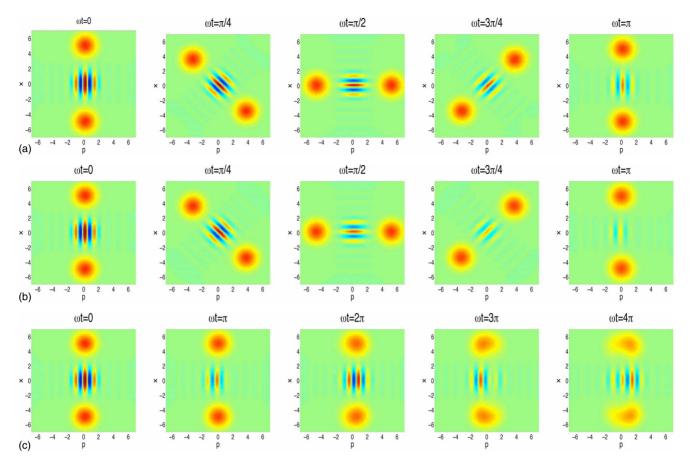


FIG. 9. (Color online) (a) Wigner function of the resonator density matrix in the absence of the TLS, where  $x_0$ =5,  $\gamma$ =0.01, T=1, and  $T_1$ =10. (b) Wigner function for the resonator coupled to the TLS, where  $x_0$ =5,  $\lambda$ =0.1,  $\Delta_0$ =0,  $\Delta_b$ =1,  $\gamma$ =0.01, T=1, and  $T_1$ =10. (c) Wigner function for the resonator coupled to the TLS, but without the resonator's independent Ohmic bath, where  $x_0$ =5,  $\lambda$ =0.1,  $\Delta_0$ =0,  $\Delta_b$ =1, T=1, and  $T_1$ =10. Note: time steps for (c) are larger than for (a) and (b).

states with different initial amplitudes. However, the actual (unnormalized) amplitudes at which the crossover occurs are the same for each curve, independent of the state's initial  $x_0$  displacement. We have also found similar crossover behavior in amplitude decay rates assuming other randomly selected distributions of three TLS's with energies close to the resonator energy. The bumps in curves B and C are a result of numerical approximation and are not a product of the system's behavior.

## VI. DECOHERENCE

In this section we investigate the contribution of the TLS's to the decoherence of a mechanical resonator Schrödinger cat state. The resonator's initial state consists of a superposition of two coherent states:  $|\psi\rangle = N^{-1}(|+x_0\rangle + |-x_0\rangle)$ , where  $|\pm x_0\rangle = \exp[\pm x_0(\hat{a}^\dagger - \hat{a})/2]|0\rangle$  with initial displacement  $\pm x_0$  and N is a normalization factor. The parameter choices are  $\gamma = 0.01$ ,  $\lambda = 0.1$ , and  $T_1 = 10$ , the same as those used for showing the trends in damping in Sec. V. In order to study the evolution of the decoherence of the cat state, we evaluate the Wigner function of the resonator density matrix  $\rho$ . Figure 9(a) shows the Wigner function in the absence of TLS's, i.e., with only the ohmic oscillator bath, at five equal time step increments. Within a single period of the

oscillator's motion, the interference fringes between the two cat states decay substantially for the assumed parameter choices. Figure 9(b) shows the evolution of the Wigner function for the same initial resonator state but with a single, on-resonance TLS coupled to the resonator in addition to the Ohmic bath. The interference fringes decay more rapidly due to the presence of the TLS. Figure 9(c) shows the Wigner function for the resonator coupled to a single TLS, but in the absence of the resonator's independent Ohmic bath. The decoherence time in this case is longer than the resonator's oscillation period.

In order to obtain a more quantitative understanding of the TLS-induced decoherence, we take the average amplitude of the interference fringes in a small, disklike region centered between the two peaks. We then define the interference amplitude  $A_{\rm int}$  using the equation

$$\exp(-A_{\text{int}}) = |W_{\text{fringes}}(x, p)|, \tag{29}$$

which is related to the "fringe visibility function" used in Ref. 54 to define a quantity similar to our  $A_{\rm int}$ . The authors of Ref. 54 show that the decoherence rate of a harmonic oscillator cat state coupled to an ohmic oscillator bath is proportional to the slope of  $A_{\rm int}$ . Figure 10 shows  $A_{\rm int}$  as a function of time for the resonator in the absence of the TLS. As pre-

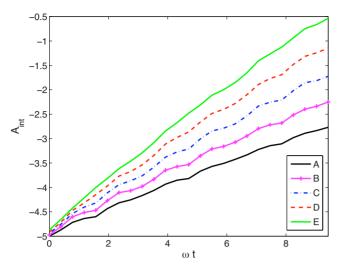


FIG. 10. (Color online)  $A_{\rm int}$  vs  $\omega t$  for the resonator in the absence of TLS's. Initial displacements are  $x_0$ =5 (A),  $x_0$ =5.5 (B),  $x_0$ =6 (C),  $x_0$ =6.5 (D),  $x_0$ =7 (E), with  $\Delta_0$ =0,  $\Delta_b$ =1,  $\gamma$ =0.01, T=1, and  $T_1$ =10.

dicted by theory, we can extract a decoherence rate from the constant increase in  $A_{\rm int}(\omega t)$ . We find that the decoherence rate, or the slope of  $A_{\rm int}(\omega t)$ , goes as the square of the initial displacement, as expected. Fig. 11 shows  $A_{\rm int}$  as a function of time for the resonator interacting with an on-resonance TLS, but without the resonator's independent Ohmic bath. The decoherence due to the TLS does not show the same dependence on the initial displacement as the oscillator bath-induced decoherence; in fact, there is no apparent systematic dependence on initial displacement. In particular, increasing the initial displacement does not result in an overall increase in the decoherence rate.

In the Wigner function plot Fig. 9(c) for the resonator coupled to the damped TLS only, the interference fringes in the center region partially decay away and then return after a

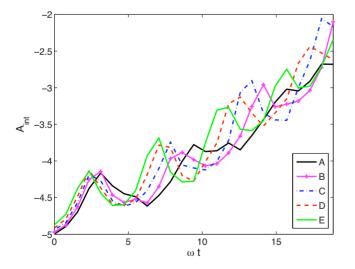


FIG. 11. (Color online)  $A_{\rm int}$  vs  $\omega t$  for the resonator coupled to a single, on-resonance TLS, but not to the resonator's independent ohmic oscillator bath. Initial displacements are  $x_0$ =5 (A),  $x_0$ =5.5 (B),  $x_0$ =6 (C),  $x_0$ =6.5 (D),  $x_0$ =7 (E), with  $\lambda$ =0.1,  $\Delta_0$ =0,  $\Delta_b$ =1, T=1, and  $T_1$ =10.

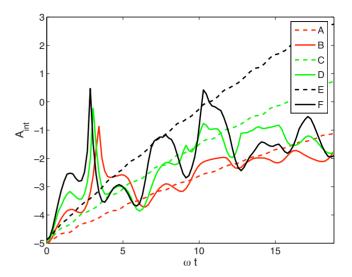


FIG. 12. (Color online) Displacement dependence of  $A_{\rm int}$  vs  $\omega t$  for the resonator coupled to the independent ohmic oscillator bath (A, C, and E) and to the three TLS's with energies indicated in Fig. 7 without the oscillator's ohmic bath (B, D, and F). The initial displacements are  $x_0$ =5 (A, B),  $x_0$ =6 (C, D), and  $x_0$ =7 (E, F). The parameter values are  $\lambda$ =0.1,  $\Delta_0$ =0,  $\Delta_b$ =1, T=1, and  $T_1$ =10.

full mechanical period. These interference oscillations, which can also be seen in Fig. 10, are a consequence of the on-resonance TLS behaving like a position measuring device. As the resonator interacts with the TLS, the two distinct position states in the superposition cause the TLS state to evolve in different ways, resulting in an entangled resonator-TLS state; the resonator partially decoheres. However, because the coupling between the TLS and its environment as parameterized by the  $T_1$  time is relatively weak, subsequent evolution almost completely undoes the entanglement; the resonator partially recoheres, restoring the interference between the two position states.

In Fig. 12 we plot the decoherence of the resonator coupled to three TLS's for three initial displacements (B, D, and F), as well as the decoherence of the resonator coupled only to the oscillator bath for comparison. The decoherence due to the presence of the three TLS's is greater than that due to a single TLS, while the decoherence due to the oscillator bath shows a systematic dependence on displacement that the TLS-induced decoherence does not exhibit. Decoherences and partial recoherences on the shorter, mechanical period time scales can be clearly seen, due to the mechanical resonator-TLS's entangling-disentangling dynamics as discussed above for the single TLS case. Similar behavior was found for other randomly selected sets of three TLS's with energies near the resonator energy. Finally, in Fig. 13 we plot  $A_{\rm int}$  vs.  $\omega t$  for the resonator coupled only to the ohmic bath (A), coupled only to the three TLS's (B), and coupled to both the ohmic bath and the three TLS's (C). As expected, we find that decoherence occurs more rapidly when the oscillator is coupled to both the ohmic bath and to the three TLS's.

## VII. CONCLUSION

In the present paper we have investigated the damping and decoherence dynamics of the flexural mode of a nano-

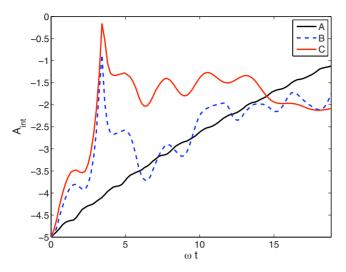


FIG. 13. (Color online)  $A_{\rm int}$  vs  $\omega t$  for the resonator coupled to the independent ohmic oscillator bath only (A), to three TLS's only (B), and to the ohmic oscillator bath and the three TLS's (C). The TLS  $\Delta_i$  values are the same as those in Fig. 12. The initial displacement is  $x_0$ =5, and the parameter values are  $\lambda$ =0.1,  $\gamma$ =0.01, T=1, and  $T_1$ =10.

mechanical beam resonator interacting with a few damped TLS's. It was found that the resulting damping rate is amplitude dependent, while the decoherence rate for superpositions of position states depends only weakly on their separation. This is to be contrasted with the damping and decoherence trends of the more commonly considered resonator interacting bilinearly with an ohmic bath of free oscillators. In the latter case, the resulting damping is amplitude independent, while the decoherence rate scales with the square of the position separation in the initial superposition state.

In our model, strain-mediated interactions between the TLS's were neglected. It will be interesting to take such interactions into account; the reduced volume of a suspended, nanoscale resonator may result in a significant enhancement of the strain-mediated TLS-TLS interaction as compared with the TLS-TLS interaction in the bulk. It is also important to try to increase the number of TLS's in our numerical experiments and compare the obtained damping and decoherence trends with approximate analytic results derived for the model system of a resonator interacting weakly with a dense spectrum of TLS's. This will then enable a test of the analytical approximations, as well as help shed light on the role of TLS's in the larger, optomechanical resonator experiments.

## **ACKNOWLEDGMENTS**

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# APPENDIX: DERIVATION OF THE OSCILLATOR-TLS DISSIPATIVE MASTER EQUATION

In terms of the system-environment density matrix  $\rho$  and Liouvillian superoperator L defined by  $L\rho = [H, \rho]$  where H is the total system-environment Hamiltonian, the time-dependent Schrödinger equation is

$$\dot{\rho} = -\frac{i}{\hbar} L \rho. \tag{A1}$$

We wish to derive a master equation for the system density matrix comprising the oscillator and TLS only:  $\rho_S$ =Tr<sub>env</sub>  $\rho$ , where the trace is performed over the oscillator-TLS environment. Following the Nakajima-Zwanzig projection operator method<sup>55,56</sup> along the lines of Ref. 57, we present projectors

$$P(\,\cdot\,) = \rho_{\rm env} \otimes \operatorname{Tr}_{\rm env}(\,\cdot\,) \tag{A2}$$

and

$$Q(\cdot) = (1 - \rho_{\text{env}} \otimes \text{Tr}_{\text{env}})(\cdot), \tag{A3}$$

where  $\rho_{\rm env} = e^{-\beta H_{\rm env}}/Z$ , with  $\beta = 1/k_B T$ , for environment temperature T. Suppose that at the initial time t = 0, the system and environment are in a product state  $\rho(0) = \rho_S(0) \otimes \rho_{\rm env}$ . Then  $P\rho(0) = \rho(0)$  and  $Q\rho(0) = 0$ . Now partition the density matrix  $\rho$  and Schrödinger equation using the projectors P and Q:

$$\dot{\rho}_1 = -\frac{i}{\hbar} PL(\rho_1 + \rho_2) \tag{A4}$$

$$\dot{\rho}_2 = -\frac{i}{\hbar}(1 - P)L(\rho_1 + \rho_2),$$
 (A5)

where  $\rho_1 = P\rho = \rho_{\text{env}} \otimes \rho_S$  and  $\rho_2 = Q\rho$ . Solving formally for  $\rho_2$ , we have

$$\rho_2(t) = -\frac{i}{\hbar} \int_0^t dt' \exp\left[-\frac{it'}{\hbar} (1 - P)L\right] (1 - P)L\rho_1(t - t'),$$
(A6)

where we have used the fact that  $\rho_2(0) = Q\rho(0) = 0$ . Substituting Eq. (A6) into Eq. (A4), we obtain

$$\dot{\rho}_1 = -\frac{i}{\hbar} P L \rho_1 - \frac{1}{\hbar^2} \int_0^t dt' P L$$

$$\times \exp \left[ -\frac{i}{\hbar} (t - t') (1 - P) L \right] (1 - P) L \rho_1(t'). \quad (A7)$$

Using the definition for the Liouvillian superoperator L given above and assuming

$$\operatorname{Tr}_{\text{env}}(b_n \rho_{\text{env}}) = \operatorname{Tr}_{\text{env}}(c_n^{(j)} \rho_{\text{env}}) = 0, \tag{A8}$$

Equation (A7) simplifies to

$$\dot{\rho}_S = -\frac{i}{\hbar} L_S \rho_S - \frac{1}{\hbar^2} \int_0^t dt' \Sigma_S(t - t') \rho_S(t'), \qquad (A9)$$

where the self-energy superoperator kernel is

$$\Sigma_{\rm S}(t) = \text{Tr}_{\rm env} \left[ L_{\rm S-env} \exp(-iQLt/\hbar) L_{\rm S-env} \rho_{\rm env} \right] \quad (A10)$$

and where  $L_S$  is the system part and  $L_{S-env}$  the systemenvironment part of the full Liouvillian superoperator L.

We now make the Born approximation, which amounts to dropping the interaction part  $L_{S-\text{env}}$  from the full L appearing in the exponential term of the kernel:

$$\Sigma_{S}(t) \approx \text{Tr}_{\text{env}} [L_{S-\text{env}} e^{-iQ(L_{S} + L_{\text{env}})t/\hbar} L_{S-\text{env}} \rho_{\text{env}}]$$

$$= \text{Tr}_{\text{env}} [L_{S-\text{env}} e^{-i(L_{S} + L_{\text{env}})t/\hbar} L_{S-\text{env}} \rho_{\text{env}}], \quad (A11)$$

where we can drop the Q projector as in the last line, a consequence of Eq. (A8). We assume that the system-environment interaction is sufficiently weak to justify making this Born approximation.

Given the bilinear in operators form of the systemenvironment interaction Hamiltonian  $H_{S-\text{env}}$  [third and fourth terms in Eq. (26)] and using the following identity for any two operators A and B

$$Tr(AB) = \frac{1}{2} \sum_{\nu=0}^{3} Tr(A\sigma_{\nu}) Tr(B\sigma_{\nu}), \qquad (A12)$$

where  $\sigma_i$ , i=1,2,3 are the Pauli matrices and  $\sigma_0$  is the identity matrix, the Born approximation to the master Eq. (A9) can be rewritten after some algebra as follows:

$$\dot{\rho}_{S}(t) = -\frac{i}{\hbar} [H_{S}, \rho_{S}(t)] - \frac{1}{\hbar^{2}} \int_{0}^{t} dt' \operatorname{Tr}_{env} [BB(-t')\rho_{env}]$$

$$\times [Y, Y(-t')e^{-iH_{S}t'/\hbar}\rho_{S}(t-t')e^{+iH_{S}t'/\hbar}]$$

$$-\frac{1}{\hbar^{2}} \sum_{j=1}^{N} \int_{0}^{t} dt' \operatorname{Tr}_{env} [C^{(j)}C^{(j)}(-t')\rho_{env}]$$

$$\times [\sigma_{z}^{(j)}, \sigma_{z}^{(j)}(-t')e^{-iH_{S}t'/\hbar}\rho_{S}(t-t')e^{+iH_{S}t'/\hbar}] + \text{h.c.}.$$
(A13)

In this expression,  $O(t) = e^{iH_S t/\hbar} O e^{-iH_S t/\hbar}$  for some operator O, "h.c." denotes the hermitian conjugate of the preceding integral terms, and we have used the shorthand notations  $B = \sum_n \kappa_n (b_n^+ + b_n)$  and  $C^{(j)} = \sum_n \widetilde{\kappa}_n^{(j)} (c_n^{(j)+} + c_n^{(j)})$ . Using the fact that the environment is in a thermal state to work out the environment correlation functions, we obtain

$$\operatorname{Tr}_{\text{env}}[BB(t)\rho_{\text{env}}] = \int_0^\infty d\omega J(\omega) [\coth(\beta \hbar \omega/2)\cos(\omega t) + i\sin(\omega t)], \tag{A14}$$

where the bath spectral density is

$$J(\omega) = \sum_{n} \kappa_n^2 \delta(\omega - \omega_n). \tag{A15}$$

We have a similar equation for the correlation function involving  $C^{(j)}$ :

$$\operatorname{Tr}_{\text{env}}[C^{(j)}C^{(j)}(t)\rho_{\text{env}}] = \int_{0}^{\infty} d\omega \widetilde{J}^{(j)}(\omega) \left[ \operatorname{coth}(\beta \hbar \omega/2) \cos(\omega t) + i \sin(\omega t) \right], \tag{A16}$$

with

$$\widetilde{J}^{(j)}(\omega) = \sum_{n} (\widetilde{\kappa}_{n}^{(i)})^{2} \delta(\omega - \omega_{n}). \tag{A17}$$

For simplicity, we assume an "Ohmic" spectral density with power law cutoff:

$$J(\omega) = \alpha \omega \frac{\Lambda^2}{\omega^2 + \Lambda^2},\tag{A18}$$

where  $\Lambda$  is the ultraviolet cutoff frequency. Substituting Eq. (A18) into Eq. (A14) and using contour integration to solve for the integral, we obtain:

$$\operatorname{Tr}_{\text{env}}[BB(t)\rho_{\text{env}}] = \frac{\pi\alpha\Lambda^{2}}{2} \left[ e^{-\Lambda t} \cot(\beta\hbar\Lambda/2) + \frac{4}{\beta\hbar^{2}} \sum_{n=1}^{\infty} \frac{(2\pi n/\beta)e^{-2\pi nt/\beta\hbar}}{(2\pi n/\beta\hbar)^{2} - \Lambda^{2}} + ie^{-\Lambda t} \right],$$
(A19)

with a similar expression for the correlation function Eq. (A16).

From the form of the environment correlation function Eq. (A19), we see that it decays rapidly to zero relative to the oscillator and TLS dynamical time scales, provided we assume that the environment temperature satisfies  $k_BT \gg \hbar \omega$ ,  $E^{(j)}$ , where  $E^{(j)} = \sqrt{(\Delta_0^{(j)})^2 + (\Delta_b^{(j)})^2}$  is the jth TLS energy level separation. Subject to this condition on the temperature, we can make a Markov approximation in master Eq. (A13) by setting  $t \to \infty$  in the upper integration limit and expanding to first order in time the system's t'-dependent unitary evolution operator wherever it appears, i.e.,  $e^{\pm iH_S t'}$ . The resulting Born-Markov master equation is

$$\begin{split} \dot{\rho}_{S}(t) &= -\frac{i}{\hbar} [H_{S}, \rho_{S}(t)] + \frac{iI_{1}}{\hbar^{2}} [Y^{2}, \rho_{S}(t)] - \frac{iI_{2}}{\hbar^{2}m} [Y, \{P_{Y}, \rho_{S}(t)\}] \\ &- \frac{R_{1}}{\hbar^{2}} [Y, [Y, \rho_{S}(t)]] + \frac{R_{2}}{\hbar^{2}m} [Y, [P_{Y}, \rho_{S}(t)]] - \frac{1}{\hbar^{2}} \sum_{j=1}^{N} \widetilde{R}_{1}^{(j)} \\ &\times [\sigma_{z}^{(j)}, [\sigma_{z}^{(j)}, \rho_{S}(t)]] - \frac{i}{\hbar^{3}} \sum_{j=1}^{N} \Delta_{b}^{(j)} \widetilde{I}_{2}^{(j)} [\sigma_{z}^{(j)}, \{\sigma_{y}^{(j)}, \rho_{S}(t)\}] \\ &+ \frac{1}{\hbar^{3}} \sum_{j=1}^{N} \Delta_{b}^{(j)} \widetilde{R}_{2}^{(j)} [\sigma_{z}^{(j)}, [\sigma_{y}^{(j)}, \rho_{S}(t)]], \end{split} \tag{A20}$$

where  $P_Y$  is the oscillator momentum,  $\{\cdot,\cdot\}$  denotes the anticommutator, and the R and I coefficients are the real and imaginary parts of the environment correlation function time integrals:

$$R_1 = \text{Re} \int_0^\infty dt \, \text{Tr}_{\text{env}} [BB(t)\rho_{\text{env}}], \qquad (A21)$$

$$R_2 = \text{Re} \int_0^\infty dtt \, \text{Tr}_{\text{env}} [BB(t)\rho_{\text{env}}], \qquad (A22)$$

$$\widetilde{R}_{1}^{(j)} = \operatorname{Re} \int_{0}^{\infty} dt \operatorname{Tr}_{\text{env}} [C^{(j)}C^{(j)}(t)\rho_{\text{env}}], \qquad (A23)$$

$$\widetilde{R}_{2}^{(j)} = \operatorname{Re} \int_{0}^{\infty} dt t \operatorname{Tr}_{\text{env}} [C^{(j)} C^{(j)}(t) \rho_{\text{env}}]$$
 (A24)

and analogously for the imaginary parts. In the Born-Markov master Eq. (A20), the  $I_1$  term renormalizes the frequency of the oscillator, while the  $R_2$  term is the so-called "anomalous diffusion" contribution. We shall neglect both terms, justified by the assumed weak system-environment coupling and the above condition on the environment temperature. The remaining oscillator environment terms involving the  $I_2$  and  $R_1$  cause damping and thermal diffusion of the oscillator, respectively. It is convenient to parametrize  $I_2$  in terms of the energy damping rate  $\gamma$  of the oscillator in the absence of the TLS:  $I_2 = \hbar m \gamma/2$ . The diffusion coefficient then becomes  $R_1 = m \gamma k_B T$ , the expected form that follows from the fluctuation-dissipation theorem.

The effect of the remaining three TLS environment terms are most straightforwardly understood by considering the coupled moment equations of the three Pauli matrices in the absence of the oscillator:

$$\begin{split} \frac{d\langle\sigma_{x}^{(j)}\rangle}{dt} &= -\frac{\Delta_{0}^{(j)}}{\hbar}\langle\sigma_{y}^{(j)}\rangle - \frac{4\widetilde{R}_{1}^{(j)}}{\hbar^{2}}\langle\sigma_{x}^{(j)}\rangle - \frac{4\Delta_{b}^{(j)}}{\hbar^{3}}\widetilde{I}_{2}^{(j)},\\ \frac{d\langle\sigma_{y}^{(j)}\rangle}{dt} &= \frac{\Delta_{0}^{(j)}}{\hbar}\langle\sigma_{x}^{(j)}\rangle - \frac{4\widetilde{R}_{1}^{(j)}}{\hbar^{2}}\langle\sigma_{y}^{(j)}\rangle - \left(1 + \frac{4\widetilde{R}_{2}^{(j)}}{\hbar^{2}}\right)\frac{\Delta_{b}^{(j)}}{\hbar}\langle\sigma_{z}^{(j)}\rangle,\\ \frac{d\langle\sigma_{z}^{(j)}\rangle}{dt} &= \frac{\Delta_{b}^{(j)}}{\hbar}\langle\sigma_{y}^{(j)}\rangle. \end{split} \tag{A25}$$

One finds for weak system-environment coupling that the  $\widetilde{R}_2^{(j)}$  term can be neglected, while the  $\widetilde{R}_1^{(j)}$  term causes damping/dephasing of the TLS and the  $\widetilde{I}_2^{(j)}$  diffusion term ensures that the moments decay to the thermal equilibrium state. Again, it is convenient to parametrize  $\widetilde{R}_1^{(j)}$  in terms of the relaxation time  $T_1^{(j)}$  of the jth TLS excited eigenstate in the absence of the oscillator. From the moment equations, we obtain  $\widetilde{R}_1^{(j)} = \hbar^2 (E^{(j)}/\Delta_b^{(j)})^2 (4T_1^{(j)})^{-1}$  and  $\widetilde{I}_2^{(j)} = \hbar/(2k_BT)\widetilde{R}_1^{(j)}$ , as follows from the fluctuation-dissipation theorem. In terms of these parametrizations, master Eq. (A20) becomes

$$\begin{split} \dot{\rho}_{S}(t) &= -\frac{i}{\hbar} [H_{S}, \rho_{S}(t)] - \frac{i\gamma}{2\hbar} [Y, \{P_{Y}, \rho_{S}(t)\}] \\ &- \frac{m\gamma k_{B}T}{\hbar^{2}} [Y, [Y, \rho_{S}(t)]] \\ &- \sum_{j=1}^{N} \frac{1}{4T_{1}^{(j)}} \left(\frac{E^{(j)}}{\Delta_{b}^{(j)}}\right)^{2} [\sigma_{z}^{(j)}, [\sigma_{z}^{(j)}, \rho_{S}(t)]] \\ &- \sum_{j=1}^{N} \frac{i}{8T_{1}^{(j)}} \left(\frac{(E^{(j)})^{2}}{\Delta_{b}^{(j)} k_{B}T}\right) [\sigma_{z}^{(j)}, \{\sigma_{y}^{(j)}, \rho_{S}(t)\}], \quad (A26) \end{split}$$

where we recognize in the first line the familiar master equation for a quantum Brownian oscillator in the large temperature limit.

While the master Eq. (A26) is valid in the large temperature limit  $k_B T \gg \hbar \omega$ ,  $E^{(j)}$ , it is desirable to investigate the system dynamics at low temperatures as well, such that  $k_B T \lesssim \hbar \omega$ ,  $\Delta^{(j)}$ . In principle, a more involved analysis of Eq. (A13) with correlation relation expressions Eq. (A19) can yield a Markovian approximation that is valid at lower temperatures. However, a more direct way is simply to invoke the quantum version of the fluctuation-dissipation theorem, which for a Brownian oscillator amounts to making the following replacement in the diffusion term in Eq. (A26):

$$\frac{\hbar\omega}{2k_BT} \to \tanh\left(\frac{\hbar\omega}{2k_BT}\right). \tag{A27}$$

The resulting Born-Markov master equation describing the quantum Brownian motion of the oscillator alone is valid for temperatures  $k_BT\gg\gamma\hbar$ . Given the assumed weak systemenvironment coupling, i.e., a large quality factor  $Q=\omega/\gamma\gg1$ , oscillator dynamics can now be investigated at low temperatures such that  $k_BT\lesssim\hbar\omega$ . Analogously, we can make the replacement

$$\frac{E^{(j)}}{2k_BT} \to \tanh\left(\frac{E^{(j)}}{2k_BT}\right) \tag{A28}$$

in the second TLS (diffusion) term of the master Eq. (A26). The resulting moments for the three Pauli matrices in the absence of the oscillator then decay to the correct quantum thermal equilibrium state as required. We shall assume that making the replacements Eqs. (A27) and (A28) in Eq. (A26) yield the Born-Markov master equation that is valid for temperatures  $k_BT\gg\gamma\hbar$ ,  $\hbar/T_1$ , provided the interactions between the oscillator and TLS, as well as between the oscillator-TLS system and environment are weak, i.e.,  $\lambda^{(j)} \ll \hbar \omega$ ,  $E^{(j)}$ ;  $Q \gg 1$  and  $E^{(j)}T_1/\hbar \gg 1$ .

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