Near-field radiative heat transfer for structured surfaces

Svend-Age Biehs, Oliver Huth, and Felix Rüting

Institut für Physik, Carl von Ossietzky Universität, D-26111 Oldenburg, Germany (Received 16 May 2008; published 12 August 2008)

We apply an analytical approach for determining the near-field radiative heat transfer between a metallic nanosphere and a planar semi-infinite medium with some given surface structure. This approach is based on a perturbative expansion, and evaluated to first order in the surface profile. With the help of numerical results obtained for some simple model geometries we discuss typical signatures that should be obtainable with a near-field scanning thermal microscope operated in either constant-height or constant-distance mode.

DOI: [10.1103/PhysRevB.78.085414](http://dx.doi.org/10.1103/PhysRevB.78.085414)

: $44.40.+a$, $78.66.-w$, $05.40.-a$, $41.20.Jb$

I. INTRODUCTION

Recent progress in the fabrication of a near-field scanning thermal microscope (NSThM) enables one to measure the radiative heat transfer between a cooled sample and a hot probe directly in the near-field regime, i.e., for distances in the nanometer range. $1,2$ $1,2$ Due to thermally excited evanescent waves, in this regime one expects an energy transfer several orders of magnitude greater than the black body value.³ For estimating the heat current in such a device several theoretical models are available, which describe the probe as a dielectric sphere, and the sample as a semi-infinite dielectric body with a flat surface. $4-10$ $4-10$ These models can now be tested against the data provided by the NSThM.

In the literature, the near-field radiative heat transfer between a sphere and a structured surface has not been studied so far, although such a geometry is of considerable practical relevance and theoretical interest. Therefore, in the present paper we analyze the near-field radiative heat transfer between a spherical probe and planar samples with surface structures such as depicted in Fig. [1.](#page-0-0) In particular, we discuss numerical results obtained for a planar surface structured by an infinite bar and a square pad, respectively.

In this work, we use the general formulation of the nearfield radiative heat transfer between a probe described as a spherical metallic nanoparticle within the dipole approximation and a second material as developed in Refs. [8](#page-8-5)[–10,](#page-8-4) which is based on Rytov's fluctuational electrodynamics.¹¹ This formulation allows one to take the material's properties of the probe into account in terms of its electric and magnetic dipole moments, and the properties of the sample material, which is assumed to be a semi-infinite body with a given surface structure, through the local density of states 12 above that medium. Since the dipole moments of the probe or nanoparticle are known it remains to calculate the local density of states (LDOS) above the sample material. This is done within a perturbative approximation employing the Ewald-Oseen extinction theorem, as described in detail in Ref. [13.](#page-8-8) It should be mentioned that our work is closely related to Ref. [14,](#page-8-9) where the changes of linewidth and the line shift for a molecule near a structured surface were calculated, since the electric LDOS can in principle be read off from the Green's function calculated therein. However, in our work not only the electric but also the magnetic fields are determined, since it is known^{10[,15](#page-8-10)} that for metallic nanoparticles these magnetic

fields can cause a heat transfer much greater than that due to the electric fields, as a result of the induction of Foucault's currents.

This paper is organized as follows: In Sec. II we introduce the dipole model for the radiative heat transfer between a metallic nanoparticle and an arbitrary second material, and outline the strategy of the following calculations. In order to determine the electromagnetic LDOS, we deduce the appropriate dyadic Green's functions in Sec. III by means of a perturbative expansion due to Agarwal, 13 which we terminate after the first order. Within this approach, the LDOS itself is calculated and numerically evaluated for different surface profiles in Sec. IV, where we also deduce tentative criteria justifying the restriction to the lowest-order contributions. In Sec. V we then present some numerical results for the nearfield heat transfer between a metallic nanosphere and a structured surface, and predict signatures that should be observable with a NSThM operated in either constant-height or constant-distance mode.

II. HEAT TRANSFER BETWEEN A NANOPARTICLE AND A SECOND MEDIUM

It has recently been shown^{8[–10](#page-8-4)} that the near-field radiative heat transfer between a metallic nanoparticle with radius *R* and temperature T_p and a dielectric material with temperature T_S can be described within the dipole model for particle-

FIG. 1. Sketch of a probe-sample configuration with a square pad on a flat surface.

sample distances $a \ge R$. In this model the electric polarizability α_p and the magnetic polarizability μ_p of the particle are given $by¹⁶$

$$
\alpha_P(\omega, R) = 4\pi R^3 \frac{\epsilon_P(\omega) - 1}{\epsilon_P(\omega) + 2}
$$
 (1)

and

$$
\mu_P(\omega, R) = -\frac{R^3}{2} \left\{ 1 - 3 \frac{d_s^{\prime 2}(\omega)}{R^2} + 3 \frac{d_s^{\prime}(\omega)}{R} \cot \left[\frac{R}{d_s^{\prime}(\omega)} \right] \right\}
$$
(2)

with the permittivity of the probe $\epsilon_p(\omega)$ and $d'_s(\omega)$ $\overline{e} = c(\omega \sqrt{\epsilon_P(\omega) - 1})^{-1}$; as usual, *c* denotes the velocity of light in vacuum. Assuming that the two bodies are in local thermal equilibrium, the mean energy rate *P* flowing from the hot to the cold body is given by the relation

$$
P = \int_0^\infty d\omega [\Theta(\omega, T_P) - \Theta(\omega, T_S)] 2\omega [\alpha_p''(\omega, R) D^E(\omega, \mathbf{r})
$$

+ $\mu_p''(\omega, R) D^H(\omega, \mathbf{r})].$ (3)

Here, the sign of the mean energy rate *P* is determined by the difference of the Bose-Einstein functions $\Theta(\omega, T)$ $\mathcal{L} := \hbar \omega[\exp(\hbar \omega \beta) - 1]^{-1}$ with the temperature $\beta^{-1} := k_B T$ so that the sign is positive for $T_P > T_S$ and negative otherwise. The material's properties of the nanoparticle are taken into account in Eq. (3) (3) (3) by means of the imaginary part (as indicated by the double prime) of the electric and magnetic polarizabilities, $\alpha_p''(\omega, R)$ and $\mu_p''(\omega, R)$, whereas the material's and geometrical properties of the second medium enter into this expression via the electric and magnetic local density of states $D^{E}(\omega, \mathbf{r})$ and $D^{H}(\omega, \mathbf{r})$ at the point **r** above this medium, where the probe is located. Therefore, the thermal radiative heat transfer between a nanoparticle and an arbitrary second medium can be calculated if the electromagnetic local density of states above that medium is known. We point out that in the opposite limit $a \ll R$ the dipole model discussed here is not valid, whereas the so called "proximity approximation" should prove to be useful then. 17

Now the local density of states can be calculated with the help of the relations¹⁸

$$
D^{E}(\omega, \mathbf{r}) = \frac{\omega}{\pi c^2} \epsilon_{S}^{"}(\omega) \int d^3 r' \operatorname{Tr}[\mathbf{G}^{E}(\mathbf{r}, \mathbf{r}') \mathbf{G}^{E}(\mathbf{r}, \mathbf{r}')^{\dagger}] \quad (4)
$$

and

$$
D^{H}(\omega, \mathbf{r}) = \frac{\omega}{\pi c^2} \frac{\epsilon_{S}^{\prime\prime}(\omega)}{\omega^2 \mu_0^2} \int d^3 r^{\prime}
$$

× Tr{ ∇ × $\mathbb{G}^{E}(\mathbf{r}, \mathbf{r}^{\prime}) [\nabla \times \mathbb{G}^{E}(\mathbf{r}, \mathbf{r}^{\prime})]^{\dagger}$ }, (5)

in the case of local equilibrium inside a heat-radiating local medium surrounded by vacuum. Here μ_0 is the magnetic permeability of the vacuum, and $\epsilon_{S}(\omega)$ is the relative permittivity of the material considered. These relations can in principle be evaluated by determining the electric dyadic Green's function $G^E(\mathbf{r}, \mathbf{r}')$ with the source points **r**' inside the medium and the observation point **r** outside the medium, implementing the tensor product with its hermitian conjugate and integrating over the volume of the medium. Since, here only a local equilibrium inside the medium is assumed, one can use these relations to investigate for example the heat transfer between bodies kept at different temperatures.

Considering a medium surrounded by vacuum, the nonequilibrium expressions in Eqs. (4) (4) (4) and (5) (5) (5) can be decomposed into an evanescent and a propagating part by transforming the volume integral into a surface integral.¹⁷ This evanescent part of the local density of states coincides with the equilibrium expression, since the evanescent modes are bound to the surface of the medium and are therefore not relevant for preserving a global equilibrium situation. Thus, the evanescent part of the local density of states above a material surrounded by vacuum can also be calculated by means of the equilibrium expressions $17,18$ $17,18$

$$
D^{E}(\omega, \mathbf{r}) = \frac{\omega}{\pi c^2} \text{Im Tr } G_R^{E}(\mathbf{r}, \mathbf{r})
$$
 (6)

and

$$
D^{H}(\omega, \mathbf{r}) = \frac{\omega}{\pi c^2} \text{Im Tr } G_R^H(\mathbf{r}, \mathbf{r}), \qquad (7)
$$

which state that the electric and magnetic local density of states at the point **r** is given by the imaginary part of the trace of the renormalized Green's functions $G_R^E(\mathbf{r}, \mathbf{r})$ and $G_R^H(\mathbf{r}, \mathbf{r})$, where the renormalization procedure is defined as¹⁹

$$
\mathbb{G}_R^{EH}(\mathbf{r}, \mathbf{r}) = \lim_{\mathbf{r} \to \mathbf{r}'} \left[\mathbb{G}^{EH}(\mathbf{r}, \mathbf{r}') - \mathbb{G}_0^{EH}(\mathbf{r}, \mathbf{r}') \right] \tag{8}
$$

with $G_0^{E/H}(\mathbf{r}, \mathbf{r}')$ denoting the Green's function of the vacuum. Since the Green's function with the observation and source point located above the medium consists of an incident and a reflected part, with the incident part coinciding with $G_0^{E/H}(\mathbf{r}, \mathbf{r}')$, the renormalized dyadic Green's function coincides with the reflected Green's function so that the index "*R*" can be understood as both "renormalized" and "reflected."

Obviously, the relations in Eqs. (6) (6) (6) and (7) (7) (7) are much easier to evaluate than the expressions in Eqs. (4) (4) (4) and (5) (5) (5) , giving reliable results for such distances above the material, at which the evanescent modes dominate the local density of states. Since we are especially interested in the evanescent regime, we focus on the equilibrium relations in order to determine the radiative heat transfer between a nanoparticle and a structured surface, keeping in mind that the results hold in the evanescent regime only. Thus, it is necessary to calculate the reflected electric and magnetic Green's function with observation points **r** and source points **r**' located outside the material of interest. For an electric source current \mathbf{j}_{e0} and a magnetic source current \mathbf{j}_{m0} located at the point **r**', the reflected fields and reflected dyadic Green's functions are connected by the relations

$$
\mathbf{E}_R(\omega, \mathbf{r}) = i\omega\mu_0 \mathbf{G}_R^E(\mathbf{r}, \mathbf{r}') \mathbf{j}_{e0}
$$
 (9)

and

FIG. 2. Sketch of an example structure, showing a particular value of the surface profile $hf(x, y)$ at $x = x_0$ and $y = 0$.

$$
\mathbf{H}_R(\omega, \mathbf{r}) = \mathrm{i}\,\omega\mu_0 \mathbb{G}_R^H(\mathbf{r}, \mathbf{r}')\mathbf{j}_{m0} \tag{10}
$$

Furthermore, in vacuum the electric and magnetic dyadic Green's functions are related by 20

$$
G_R^H(\mathbf{r}, \mathbf{r}') = -\frac{1}{k_0^2} \nabla \times G_R^E(\mathbf{r}, \mathbf{r}') \times \nabla'
$$
 (11)

with $k_0 := \omega/c$.

In the following, we will therefore perturbatively evaluate the reflected electric field generated by an electric current **j***^e*⁰ located at the source point **r**' above a semi-infinite medium with a structured surface, determine the electric dyadic Green's function by means of Eq. (9) (9) (9) , and from this result deduce the magnetic dyadic Green's function from Eq. ([11](#page-2-0)). Finally, we calculate the local densities of states above the structured surface with Eqs. (6) (6) (6) and (7) (7) (7) . These densities, in their turn, then allow us to determine the near-field radiative heat transfer between a metallic nanoparticle and a semiinfinite medium with a structured surface.

III. GREEN'S FUNCTION ABOVE A STRUCTURED SURFACE

In order to calculate the electromagnetic fields above a structured surface, we assume that the surface profile is given by an expression $hf(x, y)$, where the dimensionless function $f(x, y)$ varies between zero and unity, and *h* is the characteristic scale of the profile variation, as sketched in Fig. [2.](#page-2-1) Moreover, we assume that *h* be small compared to all other relevant length scales of the problem so that we can apply a perturbation expansion. This approach has been worked out in great detail by Agarwal¹³ so that it suffices here to mention only those elements that are indispensable to follow our line of reasoning.

Within this approach the so-called Ewald-Oseen extinc-tion theorem^{21,[22](#page-8-17)} is employed, allowing us to restate the boundary conditions of the electromagnetic fields in the given geometry as integral equations. For the case of a nonmagnetic, isotropic, local, and linear material this theorem states that for observation points **r** outside that material, i.e., $\mathbf{r} \notin V$ (see Fig. [2](#page-2-1)), one has

$$
\mathbf{E}(\mathbf{r}) = \mathbf{E}_{I}(\mathbf{r}) + \mathbf{E}_{R}(\mathbf{r}) = \mathbf{E}_{I} + \frac{1}{k_{0}^{2}} \nabla \times \nabla \times
$$
\n
$$
\int_{\partial V} dS' \left[\mathbf{E}_{T}(\mathbf{r}') \frac{\partial g(\mathbf{r} - \mathbf{r}')}{\partial \mathbf{n}'} - g(\mathbf{r} - \mathbf{r}') \frac{\partial \mathbf{E}_{T}(\mathbf{r}')}{\partial \mathbf{n}'} \right].
$$
\n(12)

Here, the field $E(r)$ outside the medium is simply the sum of the incident field $\mathbf{E}_I(\mathbf{r})$ and the reflected field $\mathbf{E}_R(\mathbf{r})$. The latter is described by the surface integral in Eq. (12) (12) (12) so that the reflected field $\mathbf{E}_R(\mathbf{r})$ can be calculated by means of the free Green's function

$$
g(\mathbf{r} - \mathbf{r}') = \frac{e^{ik_0|\mathbf{r} - \mathbf{r}'|}}{4\pi|\mathbf{r} - \mathbf{r}'|}
$$
(13)

and the transmitted field $\mathbf{E}_T(\mathbf{r})$. In addition, $\partial/\partial \mathbf{n}'$ symbolizes the normal derivative, taken in the direction of the unit normal of the surface,

$$
\mathbf{n}' = -\frac{\mathbf{e}_z + h \nabla'_{\parallel} f(x', y')}{\sqrt{1 + h^2 |\nabla'_{\parallel} f(x', y')|^2}},\tag{14}
$$

with $\nabla'_{\parallel} := (\partial_{x'}, \partial_{y'}, 0)^t$ and \mathbf{e}_z the unit vector in *z* direction.

On the other hand, for observation points **r** within the medium, i.e., $\mathbf{r} \in V$, the Ewald-Oseen theorem gives

$$
0 = \mathbf{E}_I + \frac{1}{k_0^2} \nabla \times \nabla \times
$$

$$
\int_{\partial V} dS' \left[\mathbf{E}_T(\mathbf{r}') \frac{\partial g(\mathbf{r} - \mathbf{r}')}{\partial \mathbf{n}'} - g(\mathbf{r} - \mathbf{r}') \frac{\partial \mathbf{E}_T(\mathbf{r}')}{\partial \mathbf{n}'} \right].
$$
(15)

In fact, the surface integrals in Eqs. (12) (12) (12) and (15) (15) (15) have the same structure, but one has to keep in mind that $\mathbf{r} \notin V$ in Eq. (12) (12) (12) , whereas $\mathbf{r} \in V$ in Eq. (15) (15) (15) , so that both integrals give different results. By means of Eq. (15) (15) (15) the transmitted field $\mathbf{E}_T(\mathbf{r})$ can be computed if the incident field $\mathbf{E}_I(\mathbf{r})$ is given so that the sought-after reflected field $\mathbf{E}_R(\mathbf{r})$ can then be determined with the surface integral in Eq. (12) (12) (12) .

Now the transmitted and reflected fields in Eqs. (12) (12) (12) and (15) (15) (15) are expanded in a power series

$$
\mathbf{E}_{T/R}(\mathbf{r}) = \sum_{n=0}^{\infty} \mathbf{E}_{T/R}^{(n)} h^n.
$$
 (16)

Furthermore, all quantities in the Ewald-Oseen extinction theorem are expanded in a Taylor series with respect to the small quantity $hf(x, y)$, giving

$$
\mathbf{E}_T(\mathbf{r}') = \mathbf{E}_T^{(0)}(x', y', z' = 0)
$$

- $hf(x', y') \frac{\partial \mathbf{E}_T^{(0)}}{\partial z'}(x', y', z' = 0) + \mathcal{O}(h^2)$ (17)

for the transmitted field and

$$
g(\mathbf{r} - \mathbf{r}') = g(\mathbf{r} - \mathbf{r}') \Big|_{z'=0} - h f(x', y') \frac{\partial}{\partial z'} g(\mathbf{r} - \mathbf{r}') \Big|_{z'=0}
$$

+ $\mathcal{O}(h^2)$ (18)

for the Green's function. The normal derivative times the surface element dS' yields

$$
dS'\frac{\partial}{\partial \mathbf{n}'} = -dx'dy'[\mathbf{e}_z + \nabla'_\parallel hf(x',y')] \cdot \nabla'. \qquad (19)
$$

Substituting these expressions into Eqs. (12) (12) (12) and (15) (15) (15) and comparing coefficients yields constitutive equations for the fields in different orders of *h*.

Next, it is useful to expand the fields in plane waves according to

$$
\mathbf{E}_{T}(\mathbf{r}) = \int \frac{d^{2}\kappa}{(2\pi)^{2}} e^{i(\kappa \mathbf{x} + k_{z} z)} \mathcal{E}_{T}(\kappa),
$$

$$
\mathbf{E}_{R}(\mathbf{r}) = \int \frac{d^{2}\kappa}{(2\pi)^{2}} e^{i(\kappa \mathbf{x} - k_{z0} z)} \mathcal{E}_{R}(\kappa),
$$

$$
\mathbf{E}_{I}(\mathbf{r}) = \int \frac{d^{2}\kappa}{(2\pi)^{2}} e^{i(\kappa \mathbf{x} + k_{z0} z)} \mathcal{E}_{I}(\kappa),
$$
(20)

and to utilize the Weyl expansion

$$
g(\mathbf{r} - \mathbf{r}') = \int \frac{d^2 \kappa}{(2\pi)^2} \frac{i}{2k_{z0}} e^{i[\kappa(\mathbf{x} - \mathbf{x}') + k_{z0}|z - z']}
$$
(21)

for the Green's function, having introduced the notation k_{z0}^2 $=k_0^2 - \kappa^2$, $k_z^2 = k_0^2 \epsilon_r - \kappa^2$, $\mathbf{x} = (x, y)^t$, and $\kappa = (k_x, k_y)^t$. It has to be emphasized that the use of these expansions down to the surface relies on the Rayleigh hypothesis, as discussed in Ref. [21.](#page-8-16)

With the help of the plane-wave expansions the relations for the Fourier components of the reflected fields in terms of the incident field are easily calculated; for details we refer again to the work by Agarwal.¹³ For the zeroth-order field one obtains the expression

$$
\mathcal{E}_R^{(0)}(\kappa) = -\left[\frac{k_z - k_{z0}}{k_z + k_{z0}}\right] + \frac{2k_{z0}(k_z - k_{z0})}{k_0^2(k_{z0}\varepsilon_r + k_z)}(\kappa - k_z k_{z0}\mathbf{e}_z)\right] \mathcal{E}_I(\kappa),
$$
\n(22)

and for the first-order field

$$
\mathcal{E}_R^{(1)}(\mathbf{\kappa}) = \mathbf{i}(\varepsilon_S - 1) \int \frac{d^2 \kappa'}{(2\pi)^2} F(\mathbf{\kappa} - \mathbf{\kappa'}) \mathbb{L}(\mathbf{\kappa})
$$

$$
\times \left[\frac{2k'_{z0}}{k'_z + k'_{z0}} \mathbb{1} + \frac{2k'_{z0}}{k_0^2 (k'_{z0} \varepsilon_S + k'_z)} \mathbf{K}'_0 \otimes \mathbf{K}' \right] \mathcal{E}_I(\mathbf{\kappa'}), \tag{23}
$$

with $\mathbf{K}' := (\kappa', k_z')^t$, $\mathbf{K}_0' := (\kappa', k_z')^t$, and the dyadic operator

$$
\mathbb{L}(\kappa) := \frac{1}{k_{z0}\varepsilon_{S} - k_{z}} [(\kappa^{2} + k_{z}k_{z0})(1 - \mathbf{e}_{z} \otimes \mathbf{e}_{z}) - \kappa \otimes \kappa + k_{z}\mathbf{e}_{z} \otimes \kappa + \varepsilon_{r}\kappa^{2}\mathbf{e}_{z} \otimes \mathbf{e}_{z} + \varepsilon_{r}k_{z0}\kappa \otimes \mathbf{e}_{z}].
$$
 (24)

Here \otimes symbolizes the dyadic product of two vectors, and 1 the unit dyad. Of course, also higher orders can be calculated within this approach, 13 but the higher-order contributions become increasingly cumbersome. Thus, this approach is particularly useful if meaningful results can already be obtained to first order. Hence, we restrict ourselves here to these firstorder fields and try to give approximate criteria justifying this termination of the series later on.

From Eq. ([9](#page-1-5)) it is clear that the Fourier component of the electric dyadic Green's function for the reflected fields given in Eqs. (22) (22) (22) and (23) (23) (23) can be read off if we consider the incident electric fields \mathcal{E}_I generated by a delta-like source current \mathbf{j}_{e0} located at $\mathbf{r}^{\prime\prime}$ and put the Fourier component of the result into Eqs. (22) (22) (22) and (23) (23) (23) . According to Eq. (9) (9) (9) , this field can be stated as

$$
\mathbf{E}_I(\omega, \mathbf{r}) = i\omega\mu_0 C_0^E(\mathbf{r}, \mathbf{r}'') \cdot \mathbf{j}_{e0},\tag{25}
$$

where here G_0^E is the free dyadic Green's function, which can directly be obtained from the relation

$$
\mathbb{G}_0^E(\mathbf{r}, \mathbf{r''}) = \left(1 + \frac{\nabla \otimes \nabla}{k_0^2}\right)g(\mathbf{r} - \mathbf{r''}).\tag{26}
$$

Inserting the Weyl expansion from Eq. (21) (21) (21) for the Green's function $g(\mathbf{r} - \mathbf{r}'')$, such that $z'' \leq z$, yields

$$
C_0^E(\mathbf{r}, \mathbf{r''}) = \int \frac{d^2 \kappa}{(2\pi)^2} \frac{ie^{i[\kappa \cdot (\mathbf{x} - \mathbf{x''}) + k_{z0}(z - z'')]}}{2k_{z0}} [\mathbf{e}_\perp \otimes \mathbf{e}_\perp
$$

$$
+ \mathbf{e}_{\parallel}(-k_{z0}) \otimes \mathbf{e}_{\parallel}(-k_{z0})].
$$
 (27)

Here we have defined the unit vectors in vacuum for the transverse electric (TE) and transverse magnetic (TM) modes as

$$
\mathbf{e}_{\perp} := \frac{1}{\kappa} (k_{y}, -k_{x}, 0)^{t} \tag{28}
$$

and

$$
\mathbf{e}_{\parallel}(k) := \frac{1}{\kappa k_0} (k_x k_y k_y k_z \kappa^2)^t. \tag{29}
$$

Using this expression for the free Green's function in Eq. (25) (25) (25) allows us to identify the Fourier component of the incident field, which is

$$
\mathcal{E}_{I}(\kappa) = -\omega \mu_0 \frac{e^{-i(\kappa \cdot x'' + k_{z0} z'')}}{2k_{z0}} \times [\mathbf{e}_{\perp} \otimes \mathbf{e}_{\perp} + \mathbf{e}_{\parallel}(-k_{z0}) \otimes \mathbf{e}_{\parallel}(-k_{z0})] \cdot \mathbf{j}_{e0}. \quad (30)
$$

Now, it is a straightforward exercise to calculate the reflected fields. Substituting Eq. (30) (30) (30) into Eq. (22) (22) (22) gives the zerothorder field

$$
\mathcal{E}_R^{(0)}(\kappa) = -\omega \mu_0 \frac{e^{-i(\kappa \cdot x'' - k_{z0} z'')}}{2k_{z0}} \times [r_\perp \mathbf{e}_\perp \otimes \mathbf{e}_\perp + r_\parallel \mathbf{e}_\parallel(k_{z0}) \otimes \mathbf{e}_\parallel(-k_{z0})] \cdot \mathbf{j}_{e0},
$$
\n(31)

where we have introduced the usual Fresnel reflection coefficients for the TE and TM modes, defined as

$$
r_{\perp} := \frac{k_{z0} - k_z}{k_{z0} + k_z} \tag{32}
$$

and

$$
r_{\parallel} := \frac{\varepsilon_{S} k_{z0} - k_{z}}{\varepsilon_{S} k_{z0} + k_{z}}.\tag{33}
$$

The first-order field can be calculated by substituting Eq. (30) (30) (30) in Eq. (23) (23) (23) , giving

$$
\mathcal{E}_R^{(1)}(\mathbf{\kappa}) = -\mathrm{i}(\varepsilon_S - 1) \int \frac{d^2 \kappa'}{(2\pi)^2} F(\mathbf{\kappa} - \mathbf{\kappa}') \mathbb{L}(\mathbf{\kappa}') \frac{\omega \mu_0}{2k_{z0}} e^{-\mathrm{i}(\mathbf{\kappa} \cdot \mathbf{x}'' + k_{z0}z'')}
$$

$$
\times [t'_{\perp} \mathbf{e}'_{\perp} \otimes \mathbf{e}'_{\perp} + t'_{\parallel} \mathbf{e}'_{\parallel}(-k'_z) \otimes \mathbf{e}_{\parallel}(-k'_z)] \cdot \mathbf{j}_{e0}, \qquad (34)
$$

with the transmission coefficients for the TE and the TM modes defined as

$$
t_{\perp} := \frac{2k_{z0}}{k_{z0} + k_z} \tag{35}
$$

and

$$
t_{\parallel} := \frac{2k_{z0}}{\varepsilon_{\rm S}k_{z0} + k_z}.
$$
 (36)

Due to the definition of the vector \mathbf{e}_{\parallel} for the TM modes in Eq. ([29](#page-3-5)) the TM-mode transmission coefficient defined here does not coincide with the standard formulation of the transmission coefficient. Finally, the reflected electric dyadic Green's function can be read off, giving the zeroth-order expression

$$
C_R^{E,0}(\mathbf{r}, \mathbf{r}'') = \int \frac{d^2 \kappa}{(2\pi)^2} \frac{\mathrm{i} e^{\mathrm{i}[\kappa(\mathbf{x} - \mathbf{x}'') - k_{z0}(z + z'')]}}{2k_{z0}}
$$

$$
\times [r_\perp \mathbf{e}_\perp \otimes \mathbf{e}_\perp + r_\parallel \mathbf{e}_\parallel(k_{z0}) \otimes \mathbf{e}_\parallel(-k_{z0})], \quad (37)
$$

and the first-order expression

$$
G_R^{E,1}(\mathbf{r}, \mathbf{r''}) = (1 - \varepsilon_S) \int \frac{d^2 \kappa}{(2\pi)^2} \int \frac{d^2 \kappa'}{(2\pi)^2} F(\kappa - \kappa') L(\kappa')
$$

$$
\times \frac{1}{2k'_{z0}} e^{i(\kappa x - k_{z0}z)} e^{-i(\kappa' \cdot x + k'_{z0}z)}
$$

$$
\times [t'_1 e'_1 \otimes e'_1 + t'_1 e'_1(-k'_z) \otimes e_1(-k'_z)]. \quad (38)
$$

Since the magnetic dyadic Green's function is linked with the electric one by means of Eq. (11) (11) (11) , we now have all ingredients to calculate the LDOS above a structured surface up to first order.

IV. LOCAL DENSITY OF STATES ABOVE A STRUCTURED SURFACE

The zeroth- and first-order Green's functions in Eqs. (37) (37) (37) and (38) (38) (38) can now be used to calculate the electric and magnetic local density of states

$$
D^{E/H}(\omega, \mathbf{r}) \approx D_0^{E/H}(\omega, \mathbf{r}) + D_1^{E/H}(\omega, \mathbf{r})
$$

$$
:= \frac{\omega}{\pi c^2} \text{Im Tr} G_R^{E/H,0} + h \frac{\omega}{\pi c^2} \text{Im Tr} G_R^{E/H,1} \quad (39)
$$

by means of the equilibrium relations in Eqs. (6) (6) (6) and (7) (7) (7) . As expected, and as a confirmation of the validity of the approach, to zeroth order we obtain the well-known expressions 12

$$
D_0^E(\omega, a) = \frac{\omega}{4\pi^2 c^2} \text{Im} \int_0^\infty dk_x \frac{k_x e^{-2\gamma a}}{2\gamma} \left(r_\perp + \frac{2k_x^2 - k_0^2}{k_0^2} r_\parallel \right)
$$
(40)

and

$$
D_0^H(\omega, a) = \frac{\omega}{4\pi^2 c^2} \text{Im} \int_0^\infty dk_x \frac{k_x e^{-2\gamma a}}{2\gamma} \left(r_\parallel + \frac{2k_x^2 - k_0^2}{k_0^2} r_\perp \right)
$$
\n(41)

for the LDOS at the distance *a*=−*z* above a semi-infinite body, with $\gamma = \sqrt{k_x^2 - k_0^2}$. The first-order contributions are

$$
D_1^{E}(\omega, a) = h \operatorname{Im} \left[\frac{1 - \epsilon_S}{\omega \pi} \int \frac{d^2 \kappa}{4 \pi^2} \int \frac{d^2 \kappa'}{4 \pi^2} F(\kappa - \kappa') e^{i(\kappa - \kappa') \cdot x} e^{i(k_{z0} + k'_{z0})a} \frac{t'_{\parallel}}{2k'_{z0}} \frac{t_{\parallel}}{2k_{z0}} \{k_z k_{z0}(\kappa'^2 + k'_z k'_{z0}) + k'_z k'_{z0}(\kappa^2 + k_z k_{z0}) - (\kappa \cdot \kappa')(k_z k'_z + \epsilon_S k_{z0} k'_{z0}) + \epsilon_S \kappa^2 \kappa'^2 + (\kappa \cdot \kappa')^2 \}
$$

\n
$$
= h \operatorname{Im} \left[\frac{1 - \epsilon_S}{\omega \pi} \int \frac{d^2 \kappa}{4 \pi^2} \int \frac{d^2 \kappa'}{4 \pi^2} F(\kappa - \kappa') e^{i(\kappa - \kappa') \cdot x} I_E(\kappa, \kappa') \right]
$$
(42)

and

$$
D_{1}^{H}(\omega, a) = h \operatorname{Im} \left[\frac{\epsilon_{S} - 1}{\omega \pi} \int \frac{d^{2} \kappa}{4 \pi^{2}} \int \frac{d^{2} \kappa'}{4 \pi^{2}} F(\boldsymbol{\kappa} - \boldsymbol{\kappa}') e^{i(\boldsymbol{\kappa} - \boldsymbol{\kappa}') \cdot x} e^{i(k_{z0} + k_{z0}')a} \frac{t_{\parallel}'}{2k_{z0}'} \frac{t_{\parallel}}{2k_{z0}} \left\{ \left[\frac{\kappa'^{2} + k_{z}' k_{z0}'}{k_{0}^{2}} (k_{z0} k_{z0}' - \boldsymbol{\kappa} \cdot \boldsymbol{\kappa}') + k_{z0} k_{z} \right] (\kappa^{2} + k_{z0} k_{z}) \right\} + k_{z0}' (k_{z} - k_{z0}) \frac{(\boldsymbol{\kappa} \times \boldsymbol{\kappa}')^{2}}{\kappa'^{2}} \frac{\kappa'^{2} + k_{z0}' k_{z}'}{k_{0}^{2}} + k_{z}' (k_{z} - k_{z0}) \frac{(\boldsymbol{\kappa} \cdot \boldsymbol{\kappa}')^{2}}{\kappa'^{2}} - \epsilon_{S} k_{0}^{2} \boldsymbol{\kappa} \cdot \boldsymbol{\kappa}' \right\}
$$
\n
$$
\equiv h \operatorname{Im} \left[\frac{\epsilon_{S} - 1}{\omega \pi} \int \frac{d^{2} \kappa}{4 \pi^{2}} \int \frac{d^{2} \kappa'}{4 \pi^{2}} F(\boldsymbol{\kappa} - \boldsymbol{\kappa}') e^{i(\boldsymbol{\kappa} - \boldsymbol{\kappa}') \cdot x} I_{H}(\boldsymbol{\kappa}, \boldsymbol{\kappa}') \right]. \tag{43}
$$

From Eqs. (42) (42) (42) and (43) (43) (43) it can be seen that in first order the electric and magnetic local density of states are given by an integral of the Fourier transform

$$
F(\mathbf{\kappa} - \mathbf{\kappa}') = \int dx \int dy f(x, y) e^{-i\mathbf{x} \cdot (\mathbf{\kappa} - \mathbf{\kappa}')}
$$
(44)

of the profile $f(x, y)$, multiplied by the exponential factor $\exp[i(\kappa - \kappa') \cdot x]$ and the function $I_E(\kappa, \kappa')$ or $I_H(\kappa, \kappa')$, respectively. Due to the factor $exp[i(k_{z0}+k_{z0}^{\prime})a]$, these two functions are exponentially damped for κ and κ' with modulus much greater than the inverse observation distance *a*−1 in the near field, since in the evanescent regime $k_{z0} \approx i \kappa$ and $k'_{z0} \approx i \kappa'$. Therefore, the smaller the observation distance the more Fourier components contribute to the integral. Hence, from the structure of the first-order integrals it can be expected that for distances smaller than the characteristic width of the surface profile function, the electric and magnetic local density of states resembles the surface profile.

This behavior is confirmed in Fig. [3,](#page-5-1) where the numerical

evaluation of the electric density of states from Eq. ([39](#page-4-3)) above a square pad with a height *h*=5 nm and width *w* =15 nm on a plane surface is plotted. Here, we have used the frequency ω =10¹⁴ s⁻¹ and the Drude permittivity ϵ_s of gold. Obviously, at an observation distance of *a*=40 nm the values of the local density of states resemble a two dimensional bell-shaped function, whereas at an observation distance of $a=5.5$ nm, being much smaller than the width of the square pad, the values of the local density mimic the underlying structure, apart from softened edges.

In the following, we discuss the magnitude of the contributions of the zeroth and first order of the electric and magnetic local density of states. For that purpose, we assume an infinitely extended bar with a width *w* on a plane surface modeled by the profile function

$$
f(x,y) = \frac{1}{\exp[a(|x| - \frac{w}{2})] + 1},
$$
\n(45)

assuming $d=10^9$ m⁻¹ and $w=30$ nm. The height of the bar (see Fig. [4](#page-5-2)) is chosen to be $h=5$ nm.

The numerical values of the local density of states at a constant observation distance $a=10$ nm above the base plane are shown in Fig. [5,](#page-6-0) using again the frequency ω $=10^{14}$ s⁻¹ and the Drude permittivity for gold. First, one observes that the values of the magnetic LDOS are much greater than the values of its electric counterpart, which is typical for metals, whereas for polar dielectric bodies the electric LDOS usually gives greater values than the magnetic one. Second, at the given observation distance we find values

FIG. 3. Electric LDOS from Eq. ([39](#page-4-3)) above a square pad with an edge length of 15 nm and a height of *h*=5 nm for two different observation distances $\left[\text{(a) } a = 40 \text{ nm} \text{ and } \text{(b) } a = 5.5 \text{ nm} \right]$ from the base plane. The frequency considered is $\omega = 10^{14} \text{ s}^{-1}$.

FIG. 4. Plot of $hf(x, y)$ with the profile function defined by Eq. (45) (45) (45) with $d=10^9$ m⁻¹, $w=30$ nm, and $h=5$ nm.

FIG. 5. LDOS of a gold half space structured by a gold bar (see Fig. [4](#page-5-2)). The frequency used is $\omega = 10^{14} \text{ s}^{-1}$ and the observation distance 10 nm. Observe the different scales for the electric LDOS (a) and the magnetic LDOS (b).

for the first-order contribution to the electric LDOS, which are of the same order of magnitude as the zeroth-order contribution. On the other hand, the values of the first-order magnetic LDOS are significantly smaller than the zerothorder values for all lateral positions. Third, the values of D_1^E and D_1^H give an equally good image of the bar on the plane surface, the width of the two bell-shaped curves being approximately the same. Therefore, in this case both first-order contributions give qualitatively similar results.

In Fig. [6](#page-6-1) we plot the ratio of the first- and zeroth-order LDOS D_1/D_0 for the same surface profile directly above the

FIG. 6. Dependence of the ratio of the first and zeroth order of the LDOS on the observation distance *a* calculated above the profile shown in Fig. [4](#page-5-2) for $x=0$ and frequency $\omega=10^{14} \text{ s}^{-1}$.

FIG. 7. Electric local density of states $(D_0^E$: dash-dotted line; D_1^E : dashed line; $D_0^E + D_1^E$: solid line) above the structured surface as depicted in Fig. [4](#page-5-2) at a frequency of ω =10¹⁴ s⁻¹ and a constant separation of 10 nm between observation point and surface.

bar, i.e., at $x=0$, for observation distances ranging from 6 to 100 nm. As expected, this ratio increases for decreasing observation distance, suggesting that for small distances higherorder terms have to be considered. These higher-order terms can in principle be calculated by an iterative scheme deduced by Greffet. 23 We suggest that it might be sufficient to consider only D_0 and D_1 as long as the ratio D_1/D_0 does not exceed the ten percent level. This means that the numerical results depicted in Figs. $5(a)$ $5(a)$ and $5(b)$ refer to distances where higher-order terms should be taken into account. Furthermore, it is evident from Fig. [6](#page-6-1) that for all distances the ratio of the leading two contributions to the magnetic LDOS gives much smaller values than the corresponding ratio for the electric LDOS. Therefore, it can be concluded that the approximation committed when considering only the zerothand first-order terms holds for the magnetic part for much smaller distances than for the electric part. This also means that the underlying structure becomes important in the electric LDOS for much greater distances than in the magnetic LDOS.

So far we have determined the LDOS at a constant height above the base plane of the structured surface. A very common operation mode in near-field microscopy is the constantdistance mode, where the separation between the tip and the individual features of the sample is kept constant. $²$ In order</sup> to calculate the LDOS relevant for this mode, we use the observation distance $a + hf(x, y)$ instead of $a = const.$ in Eq. ([39](#page-4-3)). Figure [7](#page-6-2) shows the LDOS obtained for this constantdistance mode above the structured half space depicted in Fig. [4.](#page-5-2)

In the constant-height mode [see Fig. $5(a)$ $5(a)$ and $5(b)$] the first-order term D_1 gives a rough image of the underlying surface structure, while the zeroth-order term D_0 is constant. However, in the constant-distance mode (see Fig. [7](#page-6-2)) the qualitative behavior of the two contributions is more complex due to the variation of the observation distance. Here, the zeroth-order term D_0 coincides more or less with the inverse of the underlying structure, and the first-order term *D*¹ gives relatively large values near the edge of the bar due to the variation in observation distance. Therefore, at least two regimes of observation distances can be distinguished: At large distances, where D_1/D_0 is small, the LDOS is dominated by the zeroth-order term, giving values which coincide approximately with the inverse of the surface structure. At distances where at least the first-order term has to be taken into account, the variation in distance leads to a rather complex pattern of the LDOS.

V. CONSEQUENCES FOR THE NEAR-FIELD SCANNING THERMAL MICROSCOPE

Up to this point, only the LDOS at a frequency corresponding to 300 K have been calculated. Before we discuss some numerical results for the full near-field radiative heat transfer between a metallic nanosphere and a structured surface, we emphasize the restrictions of the model: First, due to the dipole approximation this model is only valid for distances *a* significantly greater than the radius of the sphere *R*. Second, for distances and sphere radii smaller than the mean free path of the conduction electrons, nonlocal and quantum mechanical effects become important and have to be implemented. Third, due to the perturbative approach the results apply under the condition that the height *h* of the profile is the smallest length scale, i.e., $h \leq \min\{a, \lambda_{th}, w\}$ with the width of the surface structure *w* and the thermal wavelength $\lambda_{\text{th}} \approx \hbar \beta c$. In particular this means that the perturbative approach is not valid for distances $a \ll R$; in this limit the "proximity approximation" can be utilized.¹⁷ Nonetheless, it is reasonable to explore the perturbative predictions in some detail.

To this end, we evaluate the near-field radiative heat transfer between a gold nanoparticle and a gold sample as given by Eq. (3) (3) (3) , using the polarizabilities (1) and (2) of the sphere with the Drude permittivities ϵ_P and ϵ_S for gold. As surface profile we employ the infinitely extended bar from Eq. (45) (45) (45) with parameters as in Fig. [4.](#page-5-2) In order to relate the results for the energy flow *P* to the numerical results for the LDOS, we evaluate Eq. ([3](#page-1-0)) for a constant height, $a=10$ nm, and a constant distance, $a = 10$ nm+ $hf(x, y)$, where a nanoparticle radius of $R=10$ nm has been chosen. As shown in Fig. [8,](#page-7-0) in both cases the near-field radiative heat transfer is dominated by the magnetic contribution, this being a typical feature for good metals such as gold (at the given distance). Apart from this the curves displayed in Fig. [8](#page-7-0) reflect the corresponding plots of the LDOS at a frequency near the thermal frequency ω_{th} . This is a consequence of Eq. ([3](#page-1-0)) since the main contributions to the frequency integral stem from frequencies near the thermal frequency as long as there are no resonances in the thermally accessible frequency regime. We also implemented the proximity approximation for the given geometry numerically (with the same parameters as in Fig. [8](#page-7-0)), obtaining qualitatively similar results for the near-field radiative heat transfer as those given by the dipole model.

Hence, the conclusions deduced in the last section for the local density of states can be transferred to the near-field radiative heat transfer between a sphere and a structured surface, modeling a NSThM tip and a structured sample. Thus, for example we conclude that the lateral resolution of a NSThM increases for decreasing distances, as long as this microscope can be described within the dipole model. The

FIG. 8. Near-field radiative heat transfer between the structured sample depicted in Fig. [4](#page-5-2) ($T_S=100$ K) and a spherical probe (T_P $=300$ K) with a radius of 10 nm in each case $\left[\text{(a)} \right]$ constant-height mode and (b) constant-distance mode].

lateral resolution is comparably good for the electric part P_E and the magnetic part P_H , with the topology of the surface profile being well resolvable for distances much smaller than the width of the surface pattern. On the other hand, for nonmetallic materials, i.e., in a situation with $P_E \gg P_H$, the underlying structure becomes important for much greater distances than for metallic materials, as can be concluded from Fig. [6.](#page-6-1)

Furthermore, a NSThM gives very different images of the underlying structure when either the constant-height or the constant-distance mode is used. In particular, for distances where $D_0 \ge D_1$ the values for *P* should resemble the inverse surface structure in constant-distance mode, whereas for distances where D_1 becomes important, the measured signal can be rather complex in that mode. On the other hand, in constant-height mode the signal should approximately resemble the topology of the underlying structure at distances where D_1 becomes important. These are strong predictions that are amenable to immediate verification in current experiments,² and may help to correctly interpret the various types of signals obtainable with a NSThM.²⁴

ACKNOWLEDGMENTS

This work was supported in part by the Deutsche Forschungsgemeinschaft through Grant No. KI 438/8-1. We also thank M. Holthaus for useful comments on the text.

- ¹A. Kittel, W. Müller-Hirsch, J. Parisi, S.-A. Biehs, D. Reddig, and M. Holthaus, Phys. Rev. Lett. **95**, 224301 (2005).
- 2U. F. Wischnath, J. Welker, M. Munzel, and A. Kittel, Rev. Sci. Instrum. **79**, 073708 (2008).
- $3D.$ Polder and M. van Hove, Phys. Rev. B 4, 3303 (1971).
- ⁴ I. A. Dorofeyev, J. Phys. D **31**, 600 (1998).
- ⁵ J. B. Pendry, J. Phys.: Condens. Matter 11, 6621 (1999).
- ⁶ J.-P. Mulet, K. Joulain, R. Carminati, and J.-J. Greffet, Appl. Phys. Lett. **78**, 2931 (2001).
- 7A. I. Volokitin and B. N. J. Persson, Phys. Rev. B **63**, 205404 $(2001).$
- 8G. V. Dedkov and A. A. Kyasov, Tech. Phys. Lett. **33**, 305 $(2007).$
- ⁹I. Dorofeyev, Phys. Lett. A **372**, 1341 (2008).
- 10P.-O. Chapuis, M. Laroche, S. Volz, and J.-J. Greffet, Phys. Rev. B 77, 125402 (2008).
- 11S. M. Rytov, Y. A. Kravtsov, and V. I. Tatarskii, *Principles of* Statistical Radiophysics (Springer, New York, 1989), Vol. 3.
- 12K. Joulain, R. Carminati, J.-P. Mulet, and J.-J. Greffet, Phys. Rev. B 68, 245405 (2003).
- ¹³G. S. Agarwal, Phys. Rev. B **15**, 2371 (1977).
- ¹⁴ C. Henkel and V. Sandoghdar, Opt. Commun. **158**, 250 (1998).
- 15Yu. V. Martynenko and L. I. Ognev, Tech. Phys. **50**, 1522 $(2005).$
- 16L. D. Landau and E. M. Lifshitz, *Electrodynamics of Continuous Media* (Pergamon, Oxford, 1960).
- 17A. I. Volokitin and B. N. J. Persson, Rev. Mod. Phys. **79**, 1291 $(2007).$
- 18K. Joulain, J.-P. Mulet, F. Marquier, R. Carminati, and J.-J. Greffet, Surf. Sci. Rep. **57**, 59 (2005).
- ¹⁹L. D. Landau and E. M. Lifshitz, *Statistical Physics Part 2* (Butterworth, Oxford, 2002).
- 20L. B. Felsen and N. Marcuvitz, *Radiation and Scattering of Waves* (IEEE, New York, 1994).
- 21M. Nieto-Vesperinas, *Scattering and Diffraction in Physical Op*tics (World Scientific, Singapore, 2006).
- $2²²$ D. N. Pattanayak and E. Wolf, Opt. Commun. **6**, 217 (1972).
- ²³ J.-J. Greffet, Phys. Rev. B **37**, 6436 (1988).
- 24A. Kittel, U.-F. Wischnath, J. Welker, O. Huth, F. Rüting, and S.-A. Biehs (unpublished).