

Elastic constants and volume changes associated with two high-pressure rhombohedral phase transformations in vanadium

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We present results from *ab initio* calculations of the mechanical properties of the rhombohedral phase (β) of vanadium metal reported in recent experiments, and other predicted high-pressure phases (γ and bcc), focusing on properties relevant to dynamic experiments. We find that the volume change associated with these transitions is small: no more than 0.15% (for β - γ). Calculations of the single crystal and polycrystal elastic moduli (stress-strain coefficients) reveal a remarkably small discontinuity in the shear modulus and other elastic properties across the phase transitions even at zero temperature where the transitions are first order.

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I. INTRODUCTION

The existence of a high-pressure rhombohedral phase of pure crystalline vanadium has been the focus of an intense research effort recently. The first indication of a phase transition came from the theoretical observation that the C_{44} shear modulus of bcc vanadium decreases and becomes negative at pressures greater than ~ 1.3 Mbar,^{1,2} pressures that are experimentally accessible. A negative shear modulus means that the material is mechanically unstable under trigonal (prismatic) shear, suggesting a phase transition. At that time, the experimental evidence showed no phase transition up to 1.54 Mbar.³ Then recently, Ding *et al.*⁴ conducted x-ray diffraction experiments in the diamond anvil cell (DAC) up to 1.5 Mbar and found features in the diffraction peaks that were consistent with a second-order phase transformation to a rhombohedral structure with an $R\bar{3}m$ point group symmetry at pressures above 0.69 Mbar. It was soon confirmed that density functional theory (DFT) finds the rhombohedral phase to be the ground state at zero temperature and pressures above 0.8 Mbar, which is in reasonably good agreement with experiment.⁵ In fact, it was shown that DFT predicts additional phase transformations that had not been found in experiment, i.e., a first-order transformation to a different rhombohedral structure at 1.2 Mbar and a third transformation back to the bcc structure at 2.8 Mbar.⁵ The prediction of the existence of the two high-pressure phase transformations has been supported further by DFT phonon calculations.⁶

Alternative techniques may provide the pressures needed to observe the second rhombohedral phase and the reentrant bcc phase. Dynamic experiments do not rely on the mechanical integrity of anvils and are able to reach multimegabar pressures. They have been used to study similar transformations such as the diffusionless α - ϵ transition in iron.⁷ There are several challenges specific to vanadium, however. The softening of the shear modulus and the rhombohedral phase transition are related to subtle electronic effects,² which are likely to be weakened by increased temperature. Recent

ramp wave techniques based on Z,⁸ laser,^{9,10} and graded-density impactor¹¹ drives are able to generate high pressure without the entropy generation of shockwave techniques and are, therefore, preferable in the present context. Another challenge is that the subtle rhombohedral distortion ($<1^\circ$) detected by x-ray diffraction in the DAC is probably too small for *in situ* x-ray diffraction in dynamic experiments.¹² Indirect techniques are an alternative to detect the transition. For example, Velocity Interferometer System for Any Reflector (VISAR) free-surface velocity measurements can detect changes in the density due to a volume change, and they can be used to infer the longitudinal stress and, hence, the change in strength if the equation of state is known.^{10,13} Rayleigh-Taylor growth rate is another way to probe strength.⁹

In this paper, we use DFT to make predictions about the properties of high-pressure vanadium relevant to dynamic experiments. We compute the magnitude of the volume change associated with the three phase transitions related to the rhombohedral structure in Sec. III. We also compute the elastic properties and calculate bounds on, and an explicit estimate of, the polycrystalline shear modulus in Secs. IV and V, respectively. Since the strength is typically assumed to vary with the shear modulus,¹⁴ any anomalies in the shear modulus are likely to provide a signature in the VISAR trace. Indeed, an important motivation for the present work is to assess whether the bcc shear modulus C_{44} going to zero is likely to produce a strong signature. The shear modulus also affects defect energetics and may have a measurable effect on transition kinetics. We consider the implications of our results for dynamic experiments to detect the high-pressure phases.

II. THEORETICAL BACKGROUND

The rhombohedral crystal structure of vanadium at high pressure results from a slight distortion of the bcc structure. Specifically, the distortion is a uniaxial strain along $\langle 111 \rangle$, which remains a threefold symmetry axis of the crystal. This structure is known as the β -Po structure (*Strukturbericht* A_7 ,

Pearson *hR1*). It still has a single atom per unit cell, so the rhombohedral transition may be expected to be diffusionless (martensitic) and likely rapid despite the small energy difference. There are four independent threefold axes, so there are four variants of the rhombohedral crystal that are degenerate in energy.

The ground state of the single-crystal rhombohedral phase has been determined from first principles using a volume-conserving rhombohedral shear path,⁵

$$T(\delta) = \begin{pmatrix} k & \delta & \delta \\ \delta & k & \delta \\ \delta & \delta & k \end{pmatrix} \quad (1)$$

in the usual bcc crystal frame, where k is determined from the real positive solution of $\det(T)=1$ to ensure constant volume. The approach is to use DFT in combination with a gradient-corrected exchange and correlation energy functional¹⁵ as implemented in the Vienna *ab initio* simulation package (VASP) code along with the projector augmented-wave (PAW) method.¹⁶ Specifically, the PAW potentials with 13 valence electrons ($3s$, $3p$, $3d$, and $4s$ states) are used. The plane wave cutoff energy is 66.15 Ry and an unshifted $60 \times 60 \times 60$ uniform mesh is used for the k -point sampling; this results in 5216 and 18 941 k points in the irreducible Brillouin zone of the unstrained bcc and rhombohedral lattices, and up to 18 941 and 54 932 k points for the strained bcc and rhombohedral lattices, respectively. For all of the calculations, we use a primitive cell.

III. VOLUME CHANGE DUE TO TRANSFORMATION

In Ref. 5, we calculated the enthalpy and pressure as functions of strain along the rhombohedral deformation path and used the enthalpy to find any stable or metastable crystal structures. We noted that the equations of state (EOS) for the bcc and rhombohedral structures are nearly identical, so their bulk moduli are essentially equal (differing by no more than 3%), and reported the EOS of the ground state up to 2 Mbar. We now use those data together with additional data on the EOS of the metastable structures to calculate the volume change associated with the phase transformations in a readily accessible form.

By using the EOS $P_i(V)$ for the stable and metastable structures ($i=bcc, \beta, \gamma$), we have calculated the associated volume change ΔV according to

$$P_j(V_i + \Delta V) = P_i(V_i) \quad (2)$$

for pairs of structures i and j . In practice, we have calculated the pressure at a set of volumes and used piecewise quadratic interpolation to solve the equal pressure condition (2) between those points, equivalent to the common tangent construction at the phase boundaries. The EOS data are tabulated in Table I. A comparison of the ground-state equation of state with experimental data⁴ was presented in Fig. 3. of Ref. 5. The theoretical equation of state values compare well with the experimental data, with perhaps a very slight overbinding in the generalized gradient approximation. The relative volume change with respect to the bcc phase, $\Delta V/V_{bcc}$, is plotted in Fig. 1.

TABLE I. Equations of state for the bcc, β , and γ phases and metastable structures. Pressures are in Mbar and volumes are in units of the ambient volume $V_o=13.518 \text{ \AA}^3$.

Volume	Pressure		
	bcc	β	γ
1.000	0.000		
0.831	0.479		
0.804	0.596		
0.779	0.726	0.724	
0.759	0.840	0.838	
0.754	0.870	0.869	
0.729	1.031	1.030	
0.717	1.118	1.117	1.110
0.707	1.191	1.190	1.183
0.705	1.210	1.209	1.202
0.681	1.408	1.407	1.399
0.659	1.627	1.627	1.620
0.636	1.869	1.870	1.866
0.614	2.136	2.138	2.140
0.593	2.430	2.433	2.445
0.588	2.494		2.510
0.572	2.769		2.782
0.568	2.841		2.852
0.551	3.149		

In principle, there is a volume change during the transformation from bcc (α) to the first rhombohedral phase (β), a second volume change associated with the transformation to the second rhombohedral phase (γ), and a third volume change associated with the transformation back to bcc (α) at high pressure. There is no path connecting β and γ that preserves the point group, so they must be distinct phases; the two bcc regions appear to be connected at finite

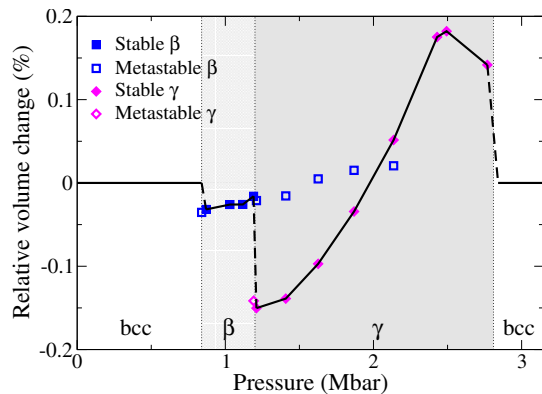


FIG. 1. (Color online) The volumetric strain $\Delta V/V$ of the ground state of single-crystal vanadium at zero temperature with respect to that of the bcc structure. Dashed lines correspond to three volume changes associated with three phase transitions. The light (dark) gray area represents the pressure range in which the β (γ) phase is the ground state. The bcc phase is stable in the other regions.

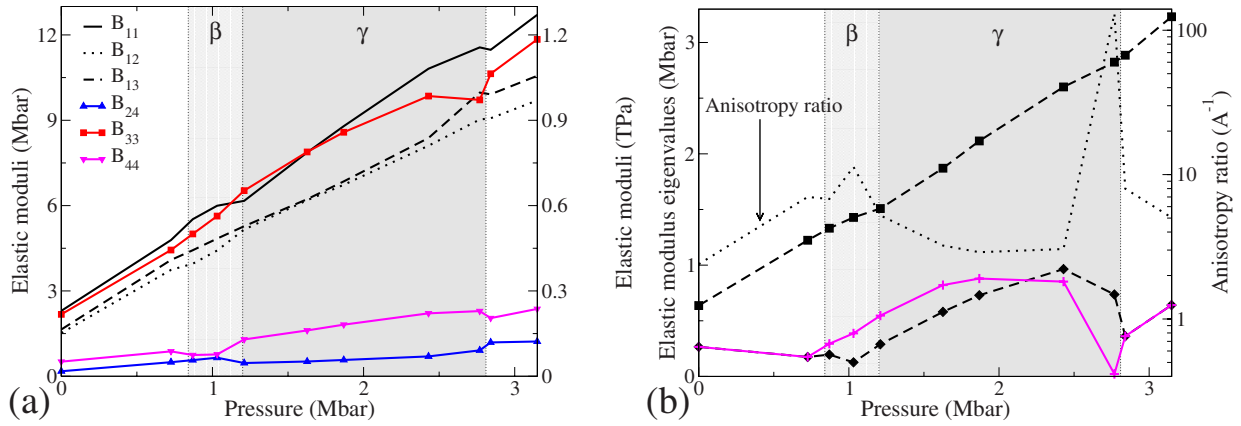


FIG. 2. (Color online) The elastic moduli (specifically, the stress-strain coefficients) of the ground-state single-crystal structure as a function of pressure. (a) B_{ijkl} written in Voigt notation in the frame of the primitive rhombohedral cell. (b) The corresponding eigenvalues of the 9×9 stress-strain coefficient matrix B_{ijkl} (see text). In the rhombohedral phase, there are six independent elastic moduli (stress-strain coefficients) (vs three for bcc) (Ref. 17) and three independent shear eigenvalues for vanadium metal (dashed curves represent doubly degenerate eigenvalues). The anisotropy ratio A^{-1} is also plotted, showing an extreme value just below the γ -bcc transition.

temperature.² In practice, the kinetics of the transformation may cause the transformation to be overdriven so that the initial phase is retained in a metastable state past the phase boundary until the new phase has a chance to nucleate and grow. For this reason, it is interesting to examine the entire curve in Fig. 1, and not just the values in between the equilibrium phase boundaries.

In each case, the initial ΔV is a volume change, so the volume is reduced following the transition. The volume change associated with the bcc to β transformation is small: 0.03% or less in magnitude. It would not be easy to detect such a small change in a dynamic experiment. The magnitude of the volume change associated with the second transformation is larger: about 0.15% for the β to γ transformation at 1.2 Mbar. The volume change would be about the same if bcc were retained to a pressure of ~ 1.2 Mbar and then transformed directly to γ . However, if the bcc or β phase persists to higher pressures, the volume change becomes progressively smaller and eventually changes sign, becoming a volume expansion near 2 Mbar. The final transition back to bcc again has a change of over 0.1% in magnitude. So the β to γ transformation has the strongest signature in terms of volume change, but it may not be large enough to detect.

IV. SINGLE-CRYSTAL ELASTIC MODULI

We next consider how the single-crystal elastic moduli change with pressure. Specifically, we calculate $B_{ijkl}(P)$, the elastic moduli with respect to a shear-stress-free reference state at pressure P (either the bcc or rhombohedral structure, as specified). The B_{ijkl} are often called the stress-strain coefficients, as we do below.¹⁷ They are directly related to sound velocities at high pressure. B_{ijkl} can be obtained from the deformation paths used for an orthorhombic lattice¹⁸ or for a trigonal lattice,¹⁹ and the details are given in the Appendix.

The six independent stress-strain coefficients, B_{11} , B_{33} , B_{12} , B_{13} , B_{44} , and B_{24} (here, given in Voigt notation in the

rhombohedral frame with directions $[\bar{1}10]_{bcc}$, $[\bar{1}\bar{1}2]_{bcc}$ and $[111]_{bcc}$ as 1, 2, and 3, respectively), are plotted in Fig. 2(a). They are discontinuous at the first-order phase transitions; however, within the domain of each stable phase, most of the stress-strain coefficients monotonically increase with pressure. The exception is B_{33} near the γ to the reentrant bcc phase boundary (roughly 2.8 Mbar). Since B_{33} is associated with uniaxial strain along the threefold axis, its anomalous behavior is suggestive, but a better presentation is needed to separate the effects of shear and compression.

Indeed, there is a remarkable approximate continuity of the elastic properties across the phase transitions that is not readily apparent from the elements of B_{ijkl} . The bulk modulus of the rhombohedral phases is within 3% of that of the bcc structure, as we already discussed. The eigenvalues of the 9×9 matrix $B_{(ij)(kl)}$ provide a description of the elasticity that is less coordinate dependent, but there is a technical

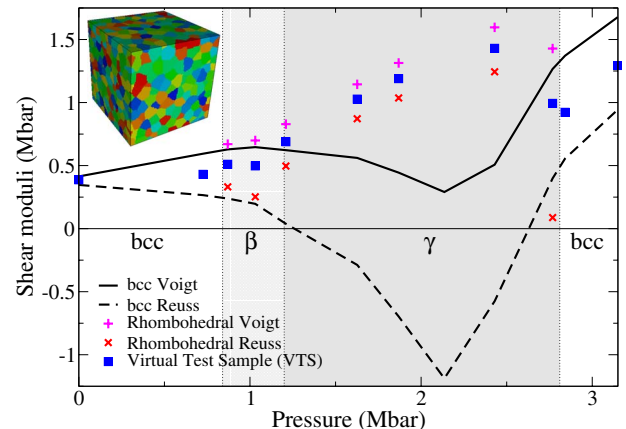


FIG. 3. (Color online) The polycrystalline shear modulus as a function of pressure, along with the Voigt and Reuss bounds for bcc, β , and γ . This shear modulus is based on the stress-strain coefficients B_{ijkl} of the single-crystal structure [see Fig. 2(a)] and calculated from the virtual test sample with a random grain orientation shown in color (inset).

TABLE II. Deformation gradients for the six independent stress-strain coefficients in the rhombohedral lattice and the corresponding strain energy relations per unit volume at pressure P .

Stress-strain coefficient	Deformation gradient	Strain energy
B_{11}	$T(\delta) = \begin{pmatrix} 1 + \delta & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$	$u(\delta, P) = -P\delta + \frac{1}{2}B_{11}\delta^2$
B_{33}	$T(\delta) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 + \delta \end{pmatrix}$	$u(\delta, P) = -P\delta + \frac{1}{2}B_{33}\delta^2$
B_{12} (and B_{66})	$T(\delta) = \begin{pmatrix} 1 + \delta & 0 & 0 \\ 0 & 1 - \delta & 0 \\ 0 & 0 & \frac{1}{1 - \delta^2} \end{pmatrix}$	$u(\delta) = (B_{11} - B_{12})\delta^2 = 2B_{66}\delta^2$
B_{13}	$T(\delta) = \begin{pmatrix} 1 + \delta & 0 & 0 \\ 0 & 1 + \delta & 0 \\ 0 & 0 & 1 + \delta \end{pmatrix}$	$u(\delta, P) = -3P(\delta + \delta^2) + \frac{1}{2}(2B_{11} + B_{33} + 2B_{12} + 4B_{13})\delta^2$
B_{44}	$T(\delta) = \begin{pmatrix} \frac{1}{1 - \delta^2} & 0 & 0 \\ 0 & 1 & \delta \\ 0 & \delta & 1 \end{pmatrix}$	$u(\delta) = 2B_{44}\delta^2$
B_{24} ($-B_{14}$)	$T(\delta) = \begin{pmatrix} 1 + \delta & 0 & 0 \\ 0 & 1 - \delta & \delta \\ 0 & 0 & \frac{1}{1 - \delta^2} \end{pmatrix}$	$u(\delta) = \frac{1}{2}(2B_{11} - 2B_{12} + B_{44} - 4B_{24})\delta^2$

issue. In the rhombohedral phase, shear and compression are mixed in the sense that a nonequaxed strain is required to produce a purely hydrostatic pressure, and the tetragonal strains to produce hydrostatic pressure and pure shear are not orthogonal. To eliminate any ambiguity, we restrict to the space of constant volume strains by using a projection matrix $\Pi_{(ij)(kl)} = \delta_{(ij)(kl)} - \frac{1}{3}\delta_{ij}\delta_{kl}$. Then the 9×9 matrix $\Pi B \Pi / 2$ has five nontrivial eigenvalues, corresponding to different shear moduli. This matrix is closely related to von Mises stresses.

The eigenvalues are plotted in Fig. 2(b). The top curve represents two degenerate eigenvalues that are equal to $B' = (B_{11} - B_{12})/2$ in the bcc phase, the usual shear modulus for tetragonal shear in the cubic crystal. It is quite smooth. The remaining three eigenvalues are degenerate in the bcc phase and equal to B_{44} , which is the shear modulus for trigonal shear in the cubic crystal (not to be confused with the B_{44} in

the rhombohedral frame). In the rhombohedral phases, two of these eigenvalues remain degenerate, but one splits off. That single eigenvalue represents a pure shear corresponding to the rhombohedral deformation. Its value is $(B_{11} + 2B_{33} + B_{12} - 4B_{13})/6$, which decreases toward zero as the pressure in the rhombohedral phases approaches the bcc phase boundary. This decrease is most pronounced approaching the high-pressure reentrant bcc phase (2.8 Mbar), but it is present at both. In the energy curves, it is clear that the width of the rhombohedral well broadens with the change in pressure as it rises above the bcc well and quickly becomes unstable. By the same token, the single eigenvalue reaches its maximum at 1.87 Mbar, which is the pressure at which the rhombohedral well is deepest and most stable against the bcc phase. The eigenvalues can also be used to study the elastic anisotropy of the crystal. The anisotropy ratio ($A = B_{44}/B'$ in bcc)

has been calculated for all four phases from the ratio of the smallest and largest eigenvalues. For an isotropic material, $A=1$; for vanadium, $1/A$ is never less than its ambient value, fluctuates throughout the entire pressure range studied, and becomes extremely high near the γ -bcc boundary ($A \sim 1/130$). For comparison, the most anisotropic cubic transition metal at ambient conditions is copper²⁰ with $A=3.21$, and among all cubic elements, recent calculations found for polonium $A=1/6-1/18$ at $T=0$ K.²¹

V. POLYCRYSTALLINE SHEAR MODULI

Polycrystalline vanadium without texture has isotropic mechanical behavior, which is described by just two independent elastic moduli: the bulk modulus K and the shear modulus G . Regardless of phase, K is within 3% of that of the bcc structure as mentioned earlier. By using the single-crystal B_{ijkl} , G may be bounded by the Voigt and Reuss approximations of constant strain and constant stress, respectively.²² Since dynamic experiments conducted at Z-pinch and laser facilities often use thin-film targets with microstructures that can vary from columnar to equiaxed depending on how they are processed, the Voigt and Reuss bounds are helpful in assessing the range of possible responses. In calculating the Voigt and Reuss bounds shown in Fig. 3 (as well as the explicit polycrystalline calculations below), we assume that the deformations are infinitesimal. With the low energy barriers, switching between variants of the rhombohedral phase may contribute to the strain with no cost in stored elastic energy, leading to a reduction in the shear modulus. At larger strains, the response to rhombohedral strains stiffens anharmonically. Both of these effects have been neglected. The homogenized shear modulus in the rhombohedral phase is positive, indicating mechanical stability. The variation in the Voigt–Reuss difference results from the changing crystalline anisotropy.

In the case of a microstructure with more equiaxed grains, we calculate the polycrystalline shear modulus by homog-

enizing the single-crystal B_{ijkl} of the ground-state structure at each pressure using a virtual test sample (VTS).²³ The procedure in Ref. 23 has been repeated: the VTS is strained in six pure shear modes (ϵ_{12} , ϵ_{23} , ϵ_{31} , $\epsilon_{11}-\epsilon_{22}$, $\epsilon_{22}-\epsilon_{33}$, and $\epsilon_{33}-\epsilon_{11}$) and the results from six calculations are averaged to reduce the effects of anisotropy. The isotropic average shear modulus (G_{VTS}) plotted in Fig. 3 has been obtained by equating the calculated elastic energy per volume to an ideal elastic solid at the same strain:

$$u = G_{VTS}(\epsilon_{11}^2 + \epsilon_{22}^2 + \epsilon_{33}^2 + \epsilon_{12}^2 + \epsilon_{23}^2 + \epsilon_{31}^2). \quad (3)$$

Only one or two of the six strains are nonzero at each run, depending on which of the six modes has been applied, and the resulting variance in six independent runs is indicative of the anisotropy. The overall VTS prediction lies between the Voigt and Reuss bounds, and the VTS values are within 5% of the Voigt–Reuss–Hill average²⁴ except at the reentrant bcc phase boundary, where the VTS value is 31% greater. The Voigt–Reuss difference at this phase boundary is quite large: 1.34 Mbar. The constant-stress Reuss average is sensitive to the most compliant orientation, whereas the Voigt average is fairly insensitive; the VTS shear modulus is closer to the Voigt value. It significantly decreases at this point of high anisotropy and may lead to an anomalous dynamic response.

VI. CONCLUSION

We have investigated the properties relevant to dynamic experiments for two high-pressure rhombohedral phases in vanadium metal. It will be challenging for dynamic experiments to detect the rhombohedral phase unambiguously. The distortion is probably too small for *in situ* x-ray diffraction, although it might be large enough in γ .⁵ We have predicted that the volume change associated with any phase transformation up to 3.15 Mbar is small and may not have a clear signature in the VISAR trace. We have also predicted values for the single-crystal and polycrystalline stress-strain coeffi-

TABLE III. Calculated stress-strain coefficients and various polycrystalline shear modulus predictions for the stable phase. All quantities are in units of Mbar except that volume has been scaled by the ambient volume $V_o=13.518 \text{ \AA}^3$.

Stable phase	Volume (V/V_o)	Pressure (P)	Bulk modulus (K)	Single-crystal stress-strain coefficients						Polycrystalline		
				B_{11}	B_{33}	B_{12}	B_{13}	B_{44}	B_{24}	VTS	Voigt	Reuss
bcc	1	0.00	1.82	2.30	2.18	1.52	1.64	0.51	0.18	0.39	0.41	0.35
	0.779	0.73	4.21	4.79	4.44	3.74	4.09	0.87	0.49	0.43	0.59	0.27
β	0.754	0.87	4.63	5.52	5.00	3.96	4.43	0.75	0.57	0.51	0.67	0.33
	0.729	1.03	5.09	6.00	5.63	4.42	4.84	0.77	0.65	0.50	0.70	0.25
γ	0.705	1.20	5.59	6.17	6.53	5.16	5.27	1.29	0.46	0.69	0.83	0.50
	0.659	1.62	6.77	7.87	7.89	6.19	6.23	1.61	0.52	1.03	1.14	0.87
	0.636	1.87	7.45	8.79	8.58	6.73	6.85	1.81	0.57	1.19	1.31	1.04
	0.593	2.45	9.02	10.81	9.85	8.11	8.38	2.21	0.70	1.43	1.60	1.24
	0.572	2.78	10.09	11.56	9.72	9.03	9.97	2.29	0.91	0.99	1.43	0.09
bcc	0.568	2.84	10.15	11.48	10.64	9.07	9.91	2.04	1.19	0.92	1.37	0.56
	0.551	3.15	10.99	12.71	11.84	9.70	10.56	2.37	1.22	1.29	1.68	0.94

cients in the rhombohedral phases at zero temperature. The β and γ phases smoothly cut off the negative values of the bcc B_{44} . The first-order transitions between the bcc and rhombohedral phases give remarkably small changes in the stress-strain coefficients, as evident from the plots of the shear modulus and the stress-strain matrix eigenvalues, apart from near the γ -bcc transition, where the crystal is highly anisotropic.

The results here were obtained by using DFT at zero temperature for pure vanadium. Since the phase transition is driven by rather subtle electronic structure effects, the elastic constants may be substantially affected by changes in temperature or impurities.^{2,5,25} It would be interesting to see whether the remarkable continuity of the moduli persists as the phase boundaries and the relative stiffness of the bcc and rhombohedral structures change.

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APPENDIX: CALCULATION OF STRESS-STRAIN COEFFICIENTS IN THE RHOMBOHEDRAL LATTICE

The high-pressure stress-strain coefficients B_{ijkl} can be obtained in many different ways, but in Table II, we summarize the deformation gradients and the corresponding strain energy relations that we used to calculate B_{ijkl} here. The pressure term is involved in some of the strain energy relations, for which the deformation gradients are not volume conserving. The stress-strain coefficients $B_{ijkl}(P)$ are equal to C_{ijkl} when the pressure vanishes, as explained in detail in Chap. 2 of Ref. 17. For a recent discussion of the stress-strain coefficients B_{ijkl} , see Ref. 26. For $P \neq 0$, the relation is¹⁷

$$B_{ijkl} = -P(\delta_{jl}\delta_{ik} + \delta_{il}\delta_{jk} - \delta_{ij}\delta_{kl}) + C_{ijkl}. \quad (\text{A1})$$

The resulting stress-strain coefficients along with the calculated polycrystalline shear moduli are tabulated in Table III.

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¹N. Suzuki and M. Otani, *J. Phys.: Condens. Matter* **14**, 10869 (2002).

²A. Landa, J. Klepeis, P. Söderlind, I. Naumov, L. Vitos, and A. Ruban, *J. Phys.: Condens. Matter* **18**, 5079 (2006); A. Landa, J. Klepeis, P. Söderlind, I. Naumov, O. Velikokhatnyi, L. Vitos, and A. Ruban, *J. Phys. Chem. Solids* **67**, 2056 (2006).

³K. Takemura, in *Science and Technology of High Pressure*, Proceedings of AIRAPT-17, edited by M. H. Manghnani, W. J. Nellis, and M. F. Nicol (University Press, Hyderabad, India, 2000), p. 443.

⁴Y. Ding, R. Ahuja, J. Shu, P. Chow, W. Luo, and H.-K. Mao, *Phys. Rev. Lett.* **98**, 085502 (2007).

⁵B. Lee, R. E. Rudd, J. E. Klepeis, P. Söderlind, and A. Landa, *Phys. Rev. B* **75**, 180101(R) (2007).

⁶W. Luo, R. Ahuja, Y. Ding, and H.-K. Mao, *Proc. Natl. Acad. Sci. U.S.A.* **104**, 16428 (2007).

⁷G. E. Duvall and R. A. Graham, *Rev. Mod. Phys.* **49**, 523 (1977).

⁸D. B. Reisman, A. Toor, R. C. Cauble, C. A. Hall, J. R. Asay, M. D. Knudson, and M. D. Furnish, *J. Appl. Phys.* **89**, 1625 (2001).

⁹B. A. Remington *et al.*, *Mater. Sci. Technol.* **22**, 474 (2006).

¹⁰R. F. Smith, J. H. Eggert, A. Jankowski, P. M. Celliers, M. J. Edwards, Y. M. Gupta, J. R. Asay, and G. W. Collins, *Phys. Rev. Lett.* **98**, 065701 (2007).

¹¹J. H. Nguyen, D. Orlikowski, F. H. Streitz, J. A. Moriarty, and N. Holmes, *J. Appl. Phys.* **100**, 023508 (2006).

¹²D. Kalantar *et al.*, *Phys. Rev. Lett.* **95**, 075502 (2005).

¹³J. B. Aidun and Y. M. Gupta, *J. Appl. Phys.* **69**, 6998 (1991).

¹⁴D. J. Steinberg, S. G. Cochran, and M. W. Guinan, *J. Appl. Phys.* **51**, 1498 (1980).

¹⁵J. P. Perdew, K. Burke, and M. Ernzerhof, *Phys. Rev. Lett.* **77**, 3865 (1996).

¹⁶P. E. Blöchl, *Phys. Rev. B* **50**, 17953 (1994); G. Kresse and D. Joubert, *ibid.* **59**, 1758 (1999).

¹⁷D. C. Wallace, *Thermodynamics of Crystals* (Dover, Mineola, 1972).

¹⁸P. Ravindran, L. Fast, P. A. Korzhavyi, B. Johansson, J. Wills, and O. Eriksson, *J. Appl. Phys.* **84**, 4891 (1998).

¹⁹J. Zhao, J. M. Winey, and Y. M. Gupta, *Phys. Rev. B* **75**, 094105 (2007).

²⁰J. P. Hirth and J. Lothe, *Theory of Dislocations*, 2nd ed. (Krieger, Malabar, FL, 1982).

²¹D. Legut, M. Friák, and M. Šob, *Phys. Rev. Lett.* **99**, 016402 (2007).

²²J. P. Watt and L. Peselnick, *J. Appl. Phys.* **51**, 1525 (1980).

²³R. Becker, *J. Comput.-Aided Mater. Des.* **9**, 145 (2002); LLNL Report No. UCRL-TR-234680, 2007 (unpublished).

²⁴R. Hill, *Proc. Phys. Soc., London, Sect. A* **65**, 349 (1952); D. H. Chung, *Philos. Mag.* **8**, 833 (1963).

²⁵X. Sha and R. E. Cohen, in *Materials Research at High Pressure*, MRS Symposia Proceedings No. 987, edited by M. R. Manaa, A. F. Goncharov, R. J. Hemley, and R. Bini, (Materials Research Society, Pittsburgh, 2007), p. 0987-PP05-08.

²⁶E. Gregoryanz, R. J. Hemley, H. K. Mao, R. E. Choen, and P. Gillet, *Phys. Rev. Lett.* **90**, 079702 (2003).