

## Exchange bias in antiferromagnetic-ferromagnetic-antiferromagnetic structures with out-of-plane magnetization

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Exchange bias effects are investigated in antiferromagnetic- (AF<sub>1</sub>-) ferromagnetic- (F-) antiferromagnetic (AF<sub>2</sub>) structures, where the F consists of a [Pt/Co] multilayer with perpendicular anisotropy and the two AF layers are composed of IrMn. The AF<sub>1</sub> and AF<sub>2</sub> thicknesses are varied so that the two IrMn layers exhibit different blocking temperatures. After field cooling, enhancements of the coercivity  $H_C$  and exchange bias field  $H_E$  are observed in the AF<sub>1</sub>-F-AF<sub>2</sub> structures with respect to the two subsystems with a single AF layer (i.e., AF<sub>1</sub>-F and F-AF<sub>2</sub>). For all systems, the magnitude and sign of  $H_E$  can be subsequently tailored by field cooling processes under fields of different sign while  $H_C$  remains constant. The net effect of having two AF-F interfaces is roughly the sum of each individual interface contribution.

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### INTRODUCTION

Exchange bias refers to the shift of the hysteresis loop, along the magnetic field axis, which is typically observed in exchange interacting ferromagnetic- (F-) antiferromagnetic (AF) materials.<sup>1-4</sup> The loop shift, denoted as  $H_E$ , is often accompanied by an enhancement of the coercivity  $H_C$  and is commonly induced by field cooling the F-AF system from above the Néel temperature of the AF. During the last decade, this phenomenon has been extensively investigated both from fundamental and technological points of view, mainly due to its applications in the development of magnetic random access memories (MRAM) and read heads based on spin valves or magnetic tunnel junction devices, where F-AF bilayers constitute an essential part.<sup>5,6</sup> The majority of F-AF bilayers where exchange bias has been studied exhibit an in-plane magnetic anisotropy. However, recently, exchange bias effects have also been induced along the perpendicular-to-film direction, both in continuous multilayers<sup>7-15</sup> or in lithographed nanostructures.<sup>16</sup> In some cases, perpendicular exchange bias is observed at room temperature, hence making these structures appealing for the implementation of spin valves or tunnel junctions with perpendicular anisotropy.<sup>9,10</sup>

In thin film form, exchange bias has been primarily investigated in F-AF bilayer structures.<sup>1-4</sup> Exchange bias effects in more complex systems such as F-AF-F trilayers or in multilayers containing several F-AF or ferrimagnetic-AF interfaces have also been reported, both in systems with in-plane<sup>17-27</sup> or with out-of-plane anisotropy.<sup>12-15</sup> In particular, it has been shown that when two or more F layers are separated by AF spacers, they can become coupled through the spacer (ferromagnetically, antiferromagnetically or at 90°), resulting in a range of interesting phenomena. In the case of F-AF multilayers with ferromagnetic coupling between the F layers, an enhancement of coercivity has been observed, which may be appealing for thin film magnets.<sup>22,23</sup> Such  $H_C$  enhancement is attributed to either an effective

magnetic surface anisotropy introduced on top of each F by the subsequent AF layer<sup>24</sup> or to the interlayer coupling between the successive F layers through the AF spacers.<sup>22</sup> Although exchange bias effects in F-AF-F and [AF-F] multilayers have been explored to some extent, the effects of the coupling in AF-F-AF trilayers (i.e., a single F surrounded by two adjacent AF layers) have been far less investigated. The few existing studies of this type concentrate mainly on the chemical or structural changes occurring at the F-AF interfaces and their effects on the strength of the coupling.<sup>28-31</sup> Comparative studies between AF-F-AF trilayers and F-AF bilayers with analogous composition have not been performed so far. Hence, the way exchange bias properties will be modified when a F layer is simultaneously coupled with two adjacent AF layers, instead of one, has not been systematically examined.

In this article, we investigate exchange bias effects in AF<sub>1</sub>-F-AF<sub>2</sub> structures, where the F is a [Pt/Co] multilayer with a perpendicular to plane effective magnetic anisotropy and the two AF layers are IrMn with different thickness, displaying different blocking temperatures (i.e., temperature at which exchange bias vanishes upon heating). For simplicity, we will refer to the AF<sub>1</sub>-F-AF<sub>2</sub> structures as the “trilayer” systems and the AF<sub>1</sub>-F and F-AF<sub>2</sub> structures as “bilayers.” Our results show that, after field cooling a given trilayer from above the blocking temperature of the two AF, both  $H_C$  and  $H_E$  are enhanced with respect to the two constituent bilayers. Actually, the  $H_C$  and  $H_E$  values in the trilayers are roughly the sum of those from each individual AF-F interface. Moreover, due to their different blocking temperatures, the relative orientation of the two AF layers composing the trilayer systems can be tuned by combining successive field cooling processes under fields of different sign. The resulting  $H_E$  is determined by the magnitude and sign of the exchange bias field induced at each interface. Conversely, the coercivity is found to remain constant, independent of the coupling direction, both in the AF<sub>1</sub>-F-AF<sub>2</sub> or in the AF<sub>1</sub>-F or F-AF<sub>2</sub> systems.

## EXPERIMENTAL

Three series of multilayers with the compositions (i) buffer(5 nm)/IrMn(7 nm)/Pt(0.4 nm)/[Co(0.4 nm)/Pt(2 nm)]<sub>4</sub>, denoted as AF<sub>1</sub>-F, (ii) Pt(0.4 nm)/[Co(0.4 nm)/Pt(2 nm)]<sub>3</sub>/Co(0.4 nm)/Pt(0.4 nm)/IrMn(*t*<sub>IrMn,top</sub>)/Pt(2 nm), denoted as F-AF<sub>2</sub>, and (iii) Cu(5 nm)/IrMn(7 nm)/Pt(0.4 nm)/[Co(0.4 nm)/Pt(2 nm)]<sub>3</sub>/Co(0.4 nm)/Pt(0.4 nm)/IrMn(*t*<sub>IrMn,top</sub>)/Pt(2 nm) denoted as AF<sub>1</sub>-F-AF<sub>2</sub> (where Cu is a buffer layer) were deposited onto thermally oxidized Si wafers by dc magnetron sputtering. For the AF<sub>1</sub>-F stack several buffer layers Cu, Ta, and Pt were preliminary tested. Although the thickness of the bottom IrMn layer AF<sub>1</sub> is kept constant to 7 nm, the AF<sub>2</sub> thickness values *t*<sub>AF<sub>2</sub></sub> range from 2 to 15 nm for both F-AF<sub>2</sub> and AF<sub>1</sub>-F-AF<sub>2</sub> structures. A thin Pt spacer was introduced between the AF and the first and/or last Co layer in the F multilayer to enhance the strength of the coupling.<sup>10</sup> The base pressure was  $5.3 \times 10^{-6}$  Pa, whereas the Ar pressure during deposition was 0.25 Pa. All depositions were performed at room temperature. The samples were then annealed at 450 K (above the blocking temperature *T*<sub>B</sub> of all systems) for 0.5 h and subsequently cooled under a field of *H*<sub>FC</sub> = -2.5 kOe, applied perpendicular to the film plane, to set the unidirectional exchange anisotropy in this direction. Hysteresis loops, applying the magnetic field perpendicular to the thin film direction, were subsequently measured at room temperature using an extraordinary Hall effect setup, a technique which is particularly sensitive to the perpendicular component of the magnetization.<sup>32</sup> Thermal activation effects on exchange bias properties were evaluated by subsequently field cooling the samples under a positive field (i.e., *H*<sub>FC</sub> = +2.5 kOe) from temperatures ranging from 300 to 450 K, after the standard (*H*<sub>FC</sub> = -2.5 kOe) cooling procedure.<sup>33</sup> Note that the top IrMn layer thickness was purposely varied in order to be able to tune the blocking temperature distribution of AF<sub>2</sub> with respect to the one of AF<sub>1</sub>.

## RESULTS AND DISCUSSION

Representative hysteresis loops for the AF<sub>1</sub>-F (with a Cu buffer layer) and F-AF<sub>2</sub> stacks, measured along the perpendicular to film direction, after perpendicular field cooling from 450 K under *H*<sub>FC</sub> = -2.5 kOe, are shown in Fig. 1. It can be seen that the loops display a rather square shape, with a remanence to saturation magnetization ratio close to 1. This indicates that the samples exhibit an effective magnetic anisotropy perpendicular to the film, which is known to arise from the hybridization between the electronic *d* states of Pt and Co at the Pt/Co interfaces.<sup>34</sup> Furthermore, the loops exhibit a shift along the magnetic field axis, i.e., a perpendicular exchange bias. It should be noted that, for the same IrMn thickness (e.g., *t*<sub>AF<sub>1</sub></sub> = *t*<sub>AF<sub>2</sub></sub> = 7 nm) the magnitude of *H*<sub>E</sub> is larger when the IrMn is deposited on top of the [Pt/Co] multilayer, i.e., F-AF<sub>2</sub>, than at the bottom, i.e., AF<sub>1</sub>-F. This difference in the exchange bias properties between top and bottom configurations is in qualitative agreement with results reported in F-AF bilayers with in-plane anisotropy. Structural differences (e.g., grain size, texture, or interface roughness)

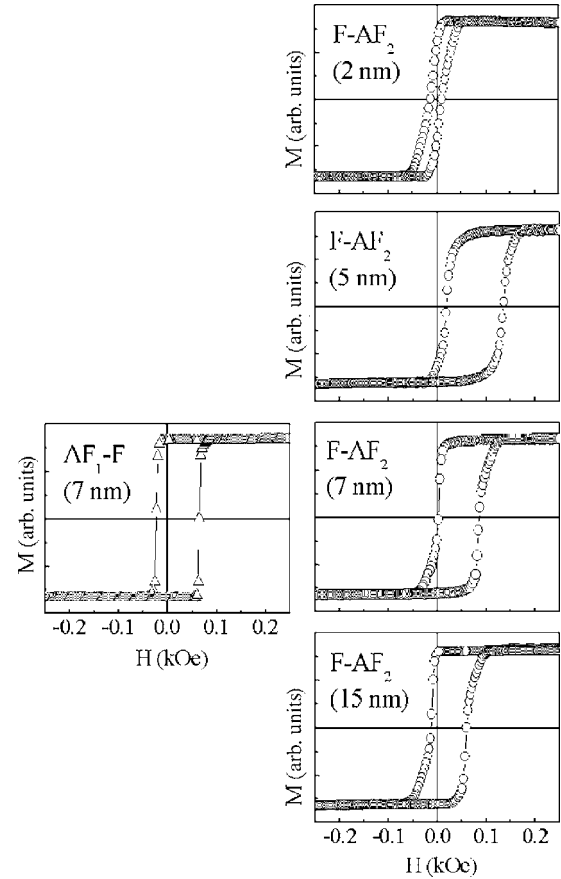


FIG. 1. Hysteresis loops corresponding to the AF<sub>1</sub>-F (with *t*<sub>AF<sub>1</sub></sub> = 7 nm) and F-AF<sub>2</sub> (with *t*<sub>AF<sub>2</sub></sub> = 2, 5, 7, and 15 nm) bilayers measured by extraordinary Hall effect along the perpendicular to film direction, after field cooling (*H*<sub>FC</sub> = -2.5 kOe) along the same direction from *T* = 450 K.

between the two configurations have been proposed as the most reasonable explanations for this effect.<sup>35,36</sup> Changes in the microstructure could also explain the slight decrease in the squareness ratio (i.e., remanence to saturation ratio) in the F-AF<sub>2</sub> system with respect to AF<sub>1</sub>-F. Other effects of the microstructure can be seen in the role of the buffer layer, where Cu maximizes the exchange bias properties for AF<sub>1</sub>-F, compared to Ta or Pt buffers. Actually, Cu is often used as buffer for the growth of IrMn,<sup>35,37</sup> although perpendicular exchange bias in IrMn—[Pt/Co]<sub>*n*</sub> multilayers where the IrMn is deposited onto other buffer layers, such as Pt, has also been reported.<sup>38</sup> In the following, only results on structures with Cu buffer layer will be presented.

Shown in Fig. 2 are the dependences of *H*<sub>E</sub> and *H*<sub>C</sub> on *t*<sub>AF<sub>2</sub></sub> for the F-AF<sub>2</sub> bilayers. It is observed that *H*<sub>C</sub> and *H*<sub>E</sub> follow the same behavior as observed for many in-plane systems using IrMn as AF.<sup>39–41</sup> Namely, both *H*<sub>E</sub>(*t*<sub>AF</sub>) and *H*<sub>C</sub>(*t*<sub>AF</sub>) exhibit a peak for relatively thin AF layers. In the F-AF<sub>2</sub> sample with *t*<sub>AF<sub>2</sub></sub> = 2 nm virtually no exchange bias is observed because the AF thickness is so small that the IrMn spin lattice is not sufficiently pinned, so that it is dragged by the magnetization of the adjacent [Pt/Co] multilayer when it switches. The inverse relationship between *H*<sub>E</sub> and *t*<sub>IrMn</sub> ob-

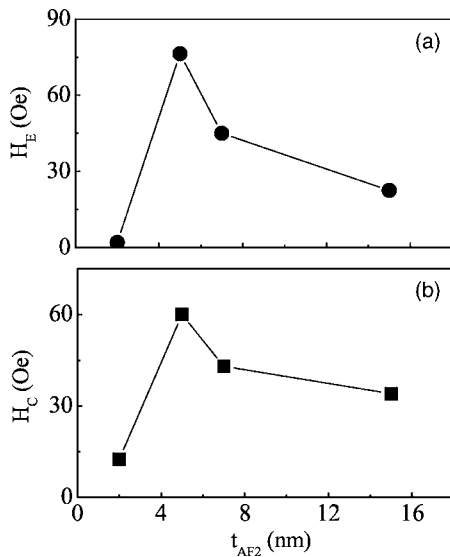


FIG. 2. Dependence of (a) the exchange bias field  $H_E$  and (b) the coercivity  $H_C$  on the  $AF_2$  thickness  $t_{AF_2}$  for the F- $AF_2$  systems. The lines are guides to the eye.

served for  $t_{IrMn} > 5$  nm can be understood within the framework of Malozemoff's model, where it is predicted that  $H_E$  is inversely proportional to the AF domain size (closely related to the AF thickness).<sup>42</sup> The domain state model can also account for this relationship between  $H_E$  and  $t_{IrMn}$  since it predicts a reduced number of AF domain walls for thick layers, which should result in a  $H_E$  decrease.<sup>39</sup>

Shown in Fig. 3 are some hysteresis loops for the  $AF_1$ -F- $AF_2$  structures for  $t_{AF_1} = 7$  nm and  $t_{AF_2} = 2, 5, 7,$  and  $15$  nm. When comparing these loops with those of the  $AF_1$ -F and F- $AF_2$  bilayers, it can be seen that the loop shape is more square in the trilayers than in the F- $AF_2$  systems. This indicates that the presence of the bottom IrMn layer in the full  $AF_1$ -F- $AF_2$  structures improves the out-of-plane anisotropy. This effect might have a magnetic, rather than structural, origin. Specifically, the presence of two, instead of one, AF layers induces an extra out-of-plane anisotropy when the trilayer is field cooled along the perpendicular to film direction, consequently improving the squareness of  $AF_1$ -F- $AF_2$  structure. A similar effect has been observed in some F-AF multilayers, where it is possible to induce exchange bias effects along the perpendicular to film direction even when the F layers exhibit, intrinsically (i.e., without the presence of the AF), an in-plane magnetic anisotropy.<sup>13,15</sup> In these systems, the hysteresis loops, measured along the perpendicular to film direction, also become more square and the appearance of perpendicular exchange bias is accompanied with an enhancement of coercivity. Remarkably, the improvement of the out-of-plane anisotropy induced by an AF has been proposed as a way to extend the temperature range of out-of-plane behavior in multilayers.<sup>43</sup>

Apart from the squareness improvement, in Fig. 3 it can be also seen that both  $H_E$  and  $H_C$  for the  $AF_1$ -F- $AF_2$  structure are significantly larger than in the corresponding  $AF_1$ -F and F- $AF_2$  constituent bilayers. Closer inspection of the loops reveals that the  $H_E$  for the  $AF_1$ -F- $AF_2$  structure is

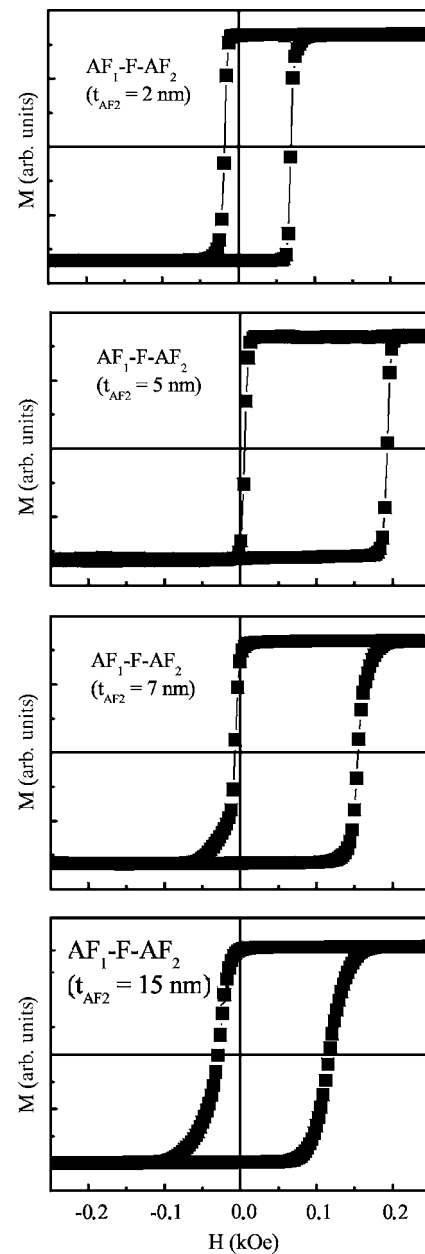


FIG. 3. Hysteresis loops corresponding to the  $AF_1$ -F- $AF_2$  system (with  $t_{AF_1} = 7$  nm and  $t_{AF_2} = 2, 5, 7,$  and  $15$  nm) systems measured by extraordinary Hall effect along the perpendicular to film direction, after field cooling ( $H_{FC} = -2.5$  kOe) along the same direction from  $T = 450$  K.

actually the sum of the loop shifts of the two constituent  $AF_1$ -F and F- $AF_2$  stacks after field cooling. This is indicated in Fig. 4, where the dependences of  $H_E$  and  $H_C$  in the  $AF_1$ -F- $AF_2$  trilayers are plotted as a function of  $t_{AF_2}$ . The discontinuous line in Fig. 4(a) is the arithmetic sum of exchange bias fields of the  $AF_1$ -F and F- $AF_2$  bilayers, which virtually overlaps with the experimental values obtained for the  $AF_1$ -F- $AF_2$  trilayers. Conversely, the sum of the coercivities of  $AF_1$ -F and F- $AF_2$  [discontinuous line in Fig. 4(b)] is slightly larger than  $H_C(AF_1$ -F- $AF_2)$ . This is because part of the measured  $H_C$  does not originate from the coupling with

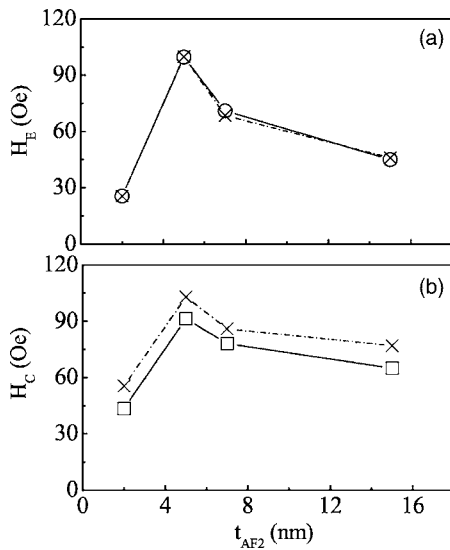


FIG. 4. Dependence of (a) the exchange bias field  $H_E$  and (b) the coercivity  $H_C$  on the  $AF_2$  thickness  $t_{AF_2}$  for the  $AF_1$ -F- $AF_2$  systems. Note that the continuous lines are guides to the eye. The crosses and discontinuous lines indicate the calculated  $H_E$  and  $H_C$  values that would be obtained for the  $AF_1$ -F- $AF_2$  systems if they were the arithmetic sum of the  $H_E$  and  $H_C$  values of the two  $AF_1$ -F and F- $AF_2$  counterparts.

the AF layers but it is the intrinsic  $H_C$  of the [Pt/Co] multilayer, which is of the order of a 12 Oe, similar to the  $H_C$  of the F- $AF_2$  system with  $t_{IrMn2}=2$  nm, where exchange bias effects are almost inexistent. In fact, if one takes into account that  $H_C([Pt/Co]) \sim 12$  Oe then, again, the coercivity enhancement (i.e., due to the coupling with the AF layers) of the  $AF_1$ -F- $AF_2$  stack is essentially the sum of coercivities of the corresponding  $AF_1$ -F and F- $AF_2$  structures. This additive character of the exchange bias properties of the two F-AF interfaces is maintained for all the investigated  $t_{AF_2}$ . In particular, the maximum in  $H_E$  and  $H_C$  for  $t_{AF_2}=5$  nm, observed for F- $AF_2$ , is mimicked in the  $AF_1$ -F- $AF_2$  structure. This additive behavior arises because, during magnetization reversal, the magnetization of the [Pt/Co] multilayer is simultaneously pinned, along *the same direction*, by the two adjacent AF layers and, consequently, the F-AF contact area increases, thus enhancing the total energy necessary to overcome by the F layer during reversal. This is of particular interest for the case of  $H_C$ , since some authors reporting  $H_C$  enhancements in F-AF multilayers with more than one F layer attribute such effect to the interlayer coupling between the several F layers,<sup>22,23</sup> hence neglecting that  $H_C$  can also be enhanced simply because of the simultaneous coupling of each F with the two adjacent AF layers. Furthermore, it should be noted that the results of our work might shed light to the origin of the  $H_C$  enhancement, typically observed in F-AF powder mixtures, where the F particles are surrounded by several AF grains, thus resulting in multiple F-AF interfaces.<sup>44</sup>

The effect of varying the relative orientation of the coupling between the F layer and each of the AF layers has also been investigated. For this purpose, all the samples ( $AF_1$ -F, F- $AF_2$  and  $AF_1$ -F- $AF_2$  multilayers), which had al-

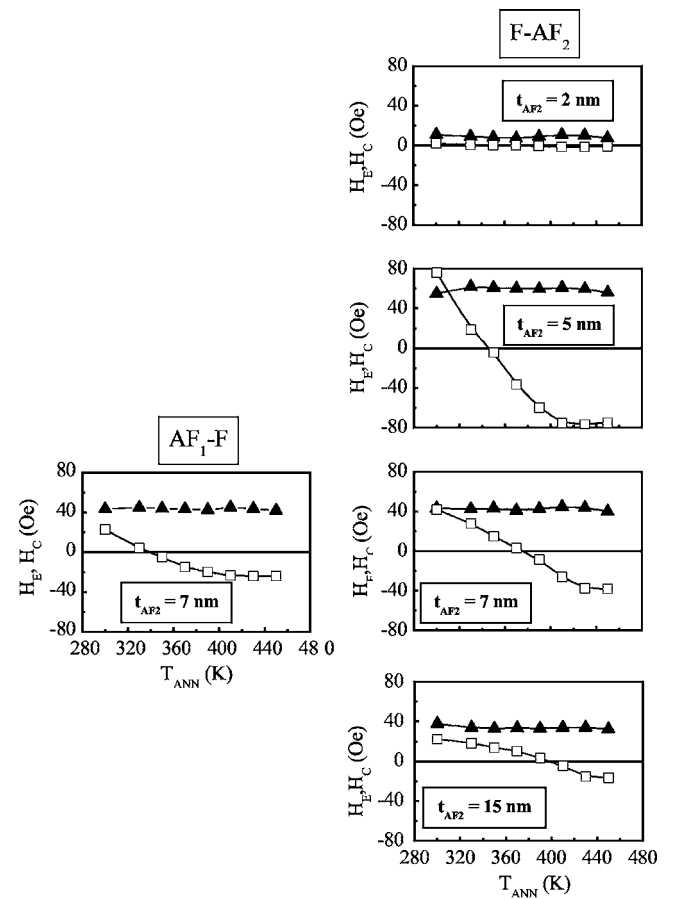


FIG. 5. Dependence of the exchange bias field  $H_E$  ( $\square$ ) and the coercivity  $H_C$  ( $\blacktriangle$ ) of the  $AF_1$ -F (with  $t_{AF_2}=7$  nm) and the F- $AF_2$  (with  $t_{AF_2}=2, 5, 7,$  and  $15$  nm) bilayers on the annealing temperature  $T_{ann}$  from which the samples are field cooled in positive field ( $H_{FC}=2.5$  kOe) after the standard field cooling process from  $T=450$  K, using a negative field ( $H_{FC}=-2.5$  kOe). The lines are guides to the eye.

ready been field cooled from  $T=450$  K in a negative field,  $H_{FC}=-2.5$  kOe, were again field cooled under a *positive* field,  $H_{FC}=+2.5$  kOe, from several annealing temperatures  $T_{ann}$ , located between room temperature and 450 K. Shown in fig. 5 are the dependencies of  $H_E$  and  $H_C$  on  $T_{ann}$  for different  $t_{AF_2}$  for the  $AF_1$ -F and F- $AF_2$  systems. It can be seen that  $H_E$  tends to decrease, changing sign, when increasing  $T_{ann}$ . Actually, the combination of two consecutive field cooling processes under fields of different sign, allows probing thermal activation effects in exchange bias systems.<sup>33</sup> Namely, if thermal activation effects are present at  $T=T_{ann}$ , the initially induced (i.e., with cooling in negative field) exchange bias will be reduced to some extent due to some loss of the AF pinning strength, i.e., some grains in the AF layer can become superparamagnetic if their local blocking temperature is below  $T_{ann}$ . Since the samples are subsequently cooled again using a positive field, the AF grains affected by the thermal activation at  $T_{ann}$  will be then realigned but in the opposite direction, leading to an overall reduction of  $H_E$  when measured at room temperature. It can be seen in Fig. 5 that for the F- $AF_2$  systems, the average blocking temperature



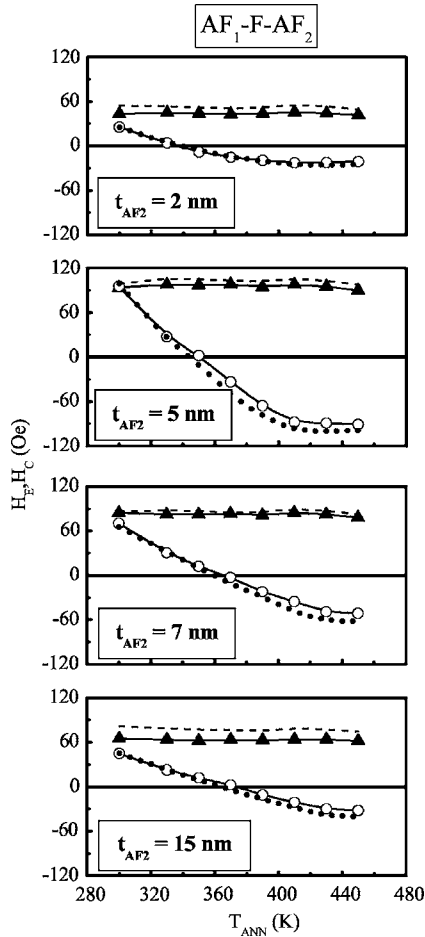


FIG. 6. Dependence of the exchange bias field  $H_E$  (—○—) and the coercivity  $H_C$  (—▲—) of the  $AF_1$ -F- $AF_2$  trilayers on the annealing temperature  $T_{ann}$  from which the samples are field cooled in positive field ( $H_{FC}=2.5$  kOe) after the standard field cooling process, from  $T=450$  K, using a negative field ( $H_{FC}=-2.5$  kOe). The continuous lines are guides to the eye, whereas the dashed and dotted lines are, respectively, the calculated  $H_C$  and  $H_E$  values that are obtained from the arithmetic sum of the  $H_E$  and  $H_C$  measured in the two constituent bilayers  $AF_1$ -F and F- $AF_2$  after field cooling from  $T_{ann}$ .

(temperature at which  $H_E$  crosses zero)  $T_{B,ave}$  increases for larger  $t_{AF_2}$  values, from  $T_{B,ave} \sim 340$  K for  $t_{AF_2}=5$  nm to  $T_{B,ave} \sim 410$  K for  $t_{AF_2}=15$  nm (for  $t_{AF_2}=2$  nm  $T_{B,ave}$  is below room temperature). This reduction of  $T_{B,ave}$  with decreasing  $t_{AF}$  is in agreement with many exchange bias systems.<sup>1</sup> Additionally, it should be noted that for the same thickness of the  $AF_1$  and  $AF_2$  layers,  $t_{AF}=7$  nm,  $T_{B,ave}$  of  $AF_1$ -F systems is substantially lower,  $T_{B,ave}(AF_1-F) \sim 340$  K, than for the F- $AF_2$  system [ $T_{B,ave}(F-AF_2) \sim 380$  K]. This has probably a microstructural origin. For example, differences in crystallite size, roughness or defects between  $AF_1$  and  $AF_2$  can account for this different blocking temperature. It should be noted that, for all bilayer systems, although  $H_E$  decreases with  $T_{ann}$ ,  $H_C$  remains insensitive to the coupling direction.

Plotted in Fig. 6 are the dependencies of  $H_E$  and  $H_C$  on  $T_{ann}$  for different  $t_{AF_2}$  for the  $AF_1$ -F- $AF_2$  systems. For

comparison,  $H_E(AF_1-F)+H_E(F-AF_2)$ , and  $H_C(AF_1-F)+H_C(F-AF_2)$  (obtained from the data in Fig. 5) are also given in Fig. 6 as dotted and dashed lines, respectively. Similar to the results obtained after the standard field cooled process,  $H_C$  and  $H_E$  of the  $AF_1$ -F- $AF_2$  systems after the second field cooling process are also roughly the sum of the two  $H_E$  and  $H_C$  values of the  $AF_1$ -F and F- $AF_2$  counterparts. The slight difference in measured and calculated  $H_C$  is due, as before, to the intrinsic  $H_C$  of the [Pt/Co] multilayer. Moreover, Figs. 5 and 6 reveal some effects which are worth mentioning. For example, for  $T_{ann}=360$  K, the  $AF_1$  layer in the  $AF_1$ -F system has essentially reversed its orientation due to the field cooling in negative field (see left panel in Fig. 5). However, for the same  $T_{ann}=360$  K and for  $t_{AF_2}=15$  nm, the  $AF_2$  layer in F- $AF_2$  system is still mainly oriented in the upwards direction (bottom panel in Fig. 5). As a result, one can infer that in the corresponding  $AF_1$ -F- $AF_2$  multilayer, the two AF layers will be roughly antiparallel to each other. As a result, one would expect this sample to exhibit virtually no exchange bias at this temperature. Interestingly, this is indeed what is observed in Fig. 6. In addition, the  $T_{B,ave}$  of the  $AF_1$ -F- $AF_2$  trilayers is lower than for the F- $AF_2$  bilayers for the same  $t_{AF_2}$ . This is best seen for large  $t_{AF_2}$ , e.g., comparing the lower panels of Figs. 5 and 6. For example,  $T_{B,ave}(F-AF_2) \sim 400$  K for  $t_{AF_2}=15$  nm for F- $AF_2$ , while  $T_{B,ave}(AF_1-F-AF_2) \sim 370$  K for the trilayer with the same thickness. This arises because the trilayer has thermal activation effects at both F-AF interfaces. Hence,  $T_{B,ave}$  in the trilayers is somewhat an average of the  $T_{B,ave}$  of the two interfaces. Finally, it is worth mentioning that, as it occurs for the bilayers,  $H_C$  in the trilayers is also roughly constant for whatever the orientation of the coupling in the two F-AF interfaces. This is because  $H_C$  depends on the irreversible dragging of AF spins, which enhances the Zeeman energy required for the reversal of the F layer and this does not depend on the coupling direction but only on its strength. These results, apart from their fundamental importance, are of particular technological interest both for the processing of thin film permanent magnets and for advancement in the implementation of novel types of magnetoelectronic devices.

## CONCLUSIONS

In summary, the exchange bias effects in  $AF_1$ -F- $AF_2$  structures have been investigated and compared to those in  $AF_1$ -F and F- $AF_2$  constituent substructures. It was observed that the exchange bias energy in the  $AF_1$ -F- $AF_2$  sandwich is approximately given by the algebraic sum of the two exchange bias coupling energies separately measured in  $AF_1$ -F and F- $AF_2$  bilayers. The sign in this algebraic sum can be modified by different annealing conditions (parallel or antiparallel annealing). In contrast, the coercivity of the F layer in  $AF_1$ -F- $AF_2$  is roughly given by the sum of the coercivity of the  $AF_1$ -F and F- $AF_2$  bilayers minus the coercivity of the F layer alone. In some particular cases it is thus possible to obtain  $H_E \sim 0$  in the  $AF_1$ -F- $AF_2$ , while having nonzero  $H_E$  values of opposite sign in the two  $AF_1$ -F and F- $AF_2$  counterparts. Our results demonstrate that the coerciv-

ity enhancement typically observed in F-AF multilayers containing more than one F film does not necessarily originate uniquely from interlayer coupling between the several F layers but also from the additive exchange coupling effects of each F with its neighboring AF layers.

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