

Magnetostructural transition and magnetocaloric effect in $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ single crystals

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A first order transition from a paramagnetic-austenite phase to a ferromagnetic-martensite phase occurring in off-stoichiometry single crystals of Ni_2MnGa at 313 K presents unique features due to the multifunctional character of the magnetic shape memory alloy. A remarkable magnetocaloric effect, associated with an entropy change up to $\Delta S \approx -86 \text{ J kg}^{-1} \text{ K}^{-1}$ and an adiabatic temperature change $\Delta T \approx 2.2 \text{ K}$, accompanied by mechanical strain $\Delta \epsilon \approx 3\%$ have been observed in samples subjected to changes of the applied magnetic field $\Delta H = 4 \times 10^6 \text{ A/m}$ ($\approx 5 \text{ T}$). The effects of magnetic field, temperature, and stress on the entropy variation ΔS are quantified and compared.

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INTRODUCTION

In recent years there has been a great interest in the possibility of using solid state materials for cooling applications, an interest justified by energy savings and by environmental concerns arising from current gas-based refrigeration technologies. The magnetocaloric effect (MCE) derived from materials with first-order magnetic phase transitions may be employed in the future to operate air conditioners and refrigerators on the macroscale, and for thermal sensing or localized heating/cooling on the microscale or nanoscale in micro/nanoelectromechanical systems.

Magnetostructural transitions leading to a “giant” MCE at room temperature have been directly observed in $\text{Gd}_5(\text{Si}_{1-x}\text{Ge}_x)_4$ (Refs. 1 and 2) with a ΔT_{ad} of the order of 8 K under a magnetic field variation $\Delta H = 4 \times 10^6 \text{ A/m}$ (5 T), while other ferromagnetic transition-metal alloys like Ni_2MnGa ,^{3,4} $\text{MnFeP}_{0.45}\text{As}_{0.55}$,⁵ and La(FeSi) (Ref. 6) have only been indicated as likely candidates. All these alloys are currently under scrutiny for their potential in magnetocaloric applications.^{6–8}

Ni_2MnGa Heusler alloys have two main structural phases, a cubic austenite which is stable at a temperature $T > A_f$ and a tetragonal martensite that is stable for $T < M_f$. Each phase can be ferromagnetic or paramagnetic at room temperature, depending on composition.^{3,9} In the specific case of $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$, $A_f = 320 \text{ K}$ and $M_f = 294 \text{ K}$. The transition from an austenite cubic lattice single crystal with $\{100\}$ faces to a single-variant martensite is associated with a macroscopic contraction up to 6% due to the appearance of a shorter “c” axis, also carrying the magnetic anisotropy when the alloy is ferromagnetic.

This work is directed to the study of the magnetic, mechanical, and magnetocaloric response of $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ oriented single crystals (SC) with $\{100\}$ faces, devoid of internal stresses and important structural inhomogeneities such as grain and variant boundaries. A very large entropy change, up to $|\Delta S| \approx 86 \text{ J kg}^{-1} \text{ K}^{-1}$, and an adiabatic temperature change $\Delta T_{\text{ad}} \approx 2.2 \text{ K}$ are observed for a magnetic field change $\Delta H = 4 \times 10^6 \text{ A/m}$ (5 T) as the SC undergoes the

first-order phase transition close to RT in an interval from $T = 309$ to 312 K .

If the entropy change is estimated from the latent heat of transformation measured by differential scanning calorimetry or from the Clausius-Clapeyron equation [Eq. (4)] a much lower value $|\Delta S| \approx 22\text{--}29 \text{ J kg}^{-1} \text{ K}^{-1}$ is obtained.² The peak $|\Delta S|$ and ΔT_{ad} values obtained in $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ SCs are comparable with those reported for $\text{Gd}_5\text{Si}_2\text{Ge}_2$,⁴ $\text{MnFeP}_{0.45}\text{As}_{0.55}$,⁵ and La(FeSi) (Ref. 6) in similar conditions.

EXPERIMENTAL PROCEDURES AND ANALYTICAL METHODS

$\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ SCs were prepared using the Bridgman method with a process described in detail in Ref. 10. The sample density $\rho = 8285 \text{ kg/m}^3$ was determined with an helium pycnometer. Differential scanning calorimetry (DSC) curves, dQ/dt , were measured with heating rates $dT/dt = 5\text{--}10 \text{ K/min}$ in flowing argon to define the start, peak, and finish temperatures of the austenite-to-martensite (A-M) (start M_s , peak M_p , finish M_f) and martensite-to-austenite (M-A) phase transitions (start A_s , peak A_p , finish A_f). The ΔS and latent heat ΔL connected to the transformation were calculated using

$$\Delta L = \int_{A_s}^{A_f} \frac{dQ}{dT} dT; \quad \Delta S = \int_{A_s}^{A_f} \frac{dQ}{T dT} dT. \quad (1)$$

The DSC measurements show that the A-M and M-A temperatures are $A_s = 306 \text{ K}$, $A_p = 314 \text{ K}$, $A_f = 320$; $M_s = 305 \text{ K}$, $M_p = 300 \text{ K}$, $M_f = 294 \text{ K}$. $\Delta L = -7.4 \text{ kJ/kg}$ corresponds to a $\Delta S = -24 \text{ J kg}^{-1} \text{ K}^{-1}$, a value three times lower than the ΔS obtained with a field-induced phase transformation and the Maxwell relation [Eq. (2)].

The temperature dependence of $M(T)_H$ under a magnetic field H with no applied stress, is shown in Fig. 1. At temperatures $T \leq A_f$ (heating) a first-order structural phase transition occurs around $A_f = 313 \text{ K}$. Comparing the $M(T)_H$ magnetization curves measured with an applied field $H_a = 8$

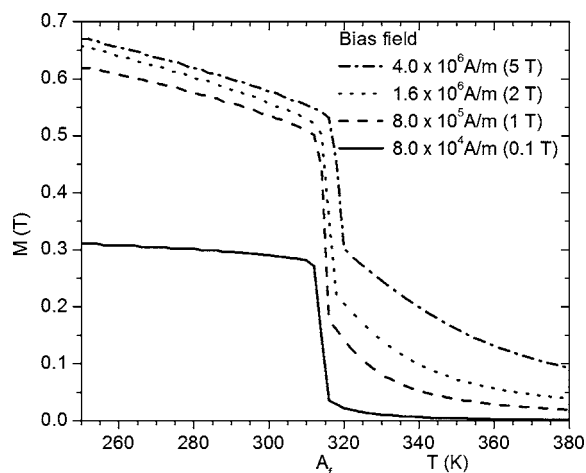


FIG. 1. Temperature dependence of the magnetization $M(T)_H$ for $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ for different values of applied field bias H . Curves measured during heating, with $H=8 \times 10^4$ A/m, 8×10^5 A/m, 1.6×10^6 A/m, 4×10^6 A/m (0.1, 1, 2, 5 T).

$\times 10^4$ A/m, 8×10^5 A/m, 1.6×10^6 A/m, 4×10^6 A/m (0.1–1–2–5 T) it can be noted that the phase transition shifts to higher T with increasing H_a , at a rate $\Delta T/\Delta H_a \approx 1$ K/T, a shift attributed to the additional Zeeman energy term $M \cdot H$ which stabilizes the martensite phase with respect to heating, a phenomenon also occurring under a compressive mechanical stress along [100], see Fig. 4 and Ref. 11.

Magnetization isotherms $M(H)_T$ were measured with a vibrating sample magnetometer (VSM) and a superconducting quantum interference device (SQUID) magnetometer. The samples were characterized after a zero-field cooling (ZFC) from the temperature of 380 K $\gg A_f$ down to 250 K $\ll M_f$. For a given composition, the martensite and austenite phases possess different saturation magnetization, initial susceptibility and magnetization curves.^{7,13} First quadrant $M(H)_T$ branches measured in the (M, H) plane at temperatures T close to the A - M transition show a nonmonotonic behavior connected to the magnetic-field-induced transition, see Fig. 2. The analysis of Arrott plots¹² indicates that in $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ the Curie temperature $T_c=312.6$ K falls within the M - A transition region between $A_s=306$ K and $A_f=320$ K.

Under the assumption that equilibrium thermodynamics can be applied, the entropy change ΔS can be estimated from the $M(H)_T$ isothermal curves using the Maxwell relation^{1,14}

$$\left[\frac{\partial S(T, H)}{\partial H} \right]_T = \left[\frac{\partial M(T, H)}{\partial T} \right]_H. \quad (2)$$

Integration of the right hand term with respect to field, in the field interval ΔH allows the estimation of ΔS , and for $\Delta H = H_2 - H_1$ if $H_1 = 0$ we have

$$\Delta S \left(\frac{T_1 + T_2}{2} \right) = \frac{1}{T_2 - T_1} \left[\int_0^{H_2} M(T_2, H) dH - \int_0^{H_2} M(T_1, H) dH \right], \quad (3)$$

where T_1 and T_2 are the respective temperatures of two ad-

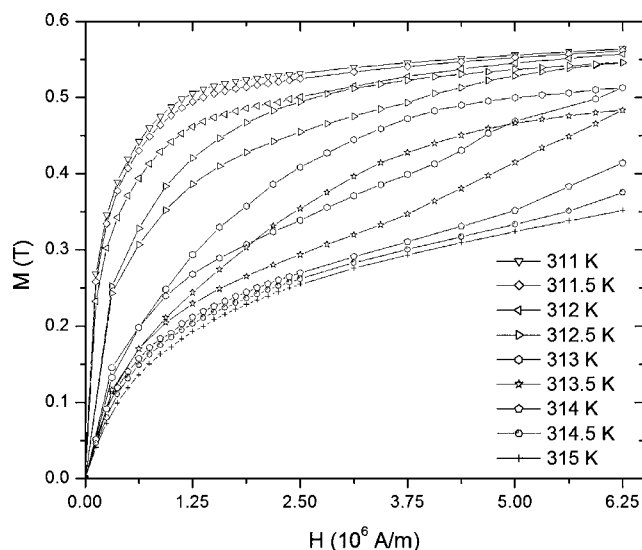


FIG. 2. Isothermal $M(H)_T$ curves showing a field induced austenite to martensite phase transition in the temperature interval between 312 and 314 K.

jacent magnetization curves (see Fig. 2). A summary of the ΔS values obtained from Eq. (3) is presented in Fig. 3.¹⁵ The Clausius-Clapeyron equation can also be used to determine the entropy variation

$$\frac{\Delta H}{\Delta T} = - \frac{Q}{T_M \Delta M}, \quad \Delta S = - \frac{Q}{T_M}, \quad (4)$$

where Q is the evolved heat of transformation, and T_M is the A - M temperature. The calculation requires estimates of the magnetization change ΔM associated to the first order phase transition (Figs. 1 and 2) and of the average temperature shift $\Delta T/\Delta H$ of the transition point with increasing field $[M(T)_H$

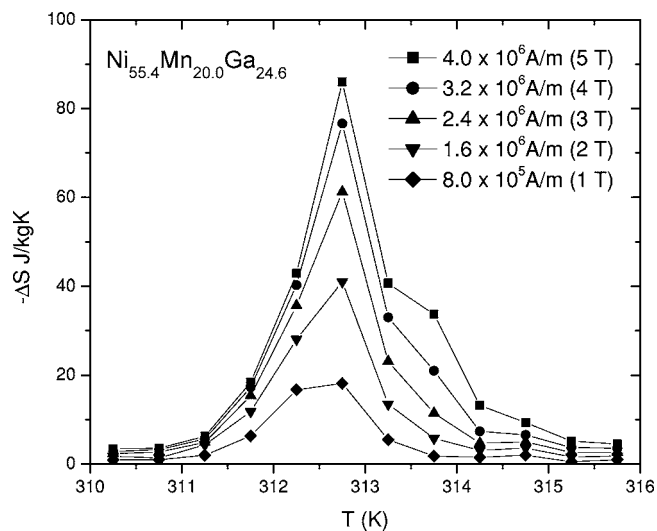


FIG. 3. Temperature dependence of the entropy variation produced by a magnetic field variation of 8×10^5 A/m to 4×10^6 A/m (1–5 T). The curves are obtained using the Maxwell relation [Eqs. (2) and (3)] and isothermal magnetization curves data (Fig. 2).

curves, see Fig. 1] or the average field shift $\Delta H/\Delta T$ of the transition point with increasing temperature [$M(H)_T$ curves, see Fig. 2].

A much more accurate and direct evaluation of the MCE potential can also be obtained either from DSC measurements under an applied field H or from the adiabatic temperature change ΔT_{ad} associated with a field variation H , a case which will be discussed in the final section.^{16,17}

The isothermal $M(H)_T$ curves (Fig. 2) measured at temperatures ranging from 311 to 315 K exhibit the following behavior: at low temperature (i.e., 311 K) $M(H)$ curves with a higher peak magnetization M_p are found, as expected from a ferromagnetic martensite phase. Lower M_p values are observed at $T > 315$ K when the sample is in the paramagnetic austenite phase. For intermediate values $312.5 \text{ K} \leq T \leq 314 \text{ K}$, associated with the A - M transition, highly non-monotonic $M(H)$ curves are measured, with an inflection point marking the magnetostructural phase transition.^{1,13,18} The magnetic field H_T triggering the onset of the field induced A - M transition shifts with temperature from about $H_{T\alpha} = 1.6 \times 10^6 \text{ A/m}$ (2 T) at $T_\alpha = 312.0 \text{ K}$ to about $H_{T\beta} = 3.6 \times 10^6 \text{ A/m}$ (4.5 T) at $T_\beta = 314.5 \text{ K}$. The maximum entropy change estimated using the isothermal $M(H)_T$ data and the Maxwell relation Eqs. (2) and (3) is $|\Delta S| \approx 86 \text{ J kg}^{-1} \text{ K}^{-1}$ at 312.75 K for a field change $\Delta H = 4 \times 10^6 \text{ A/m}$ (5 T), with an estimated 10% total error.¹⁹ This peak value becomes $\approx 41 \text{ J kg}^{-1} \text{ K}^{-1}$ at $\Delta H = 1.56 \times 10^6 \text{ A/m}$ (2 T) and $\approx 18 \text{ J kg}^{-1} \text{ K}^{-1}$ at $\Delta H = 8 \times 10^5 \text{ A/m}$ (1 T) (see Fig. 3).

Using the Clausius-Clapeyron equation [Eq. (4)] a much smaller value $|\Delta S| \approx 24\text{--}29 \text{ J kg}^{-1} \text{ K}^{-1}$, comparable to the DSC results, can be derived from magnetization curves (Figs. 1 and 2), when a value $\Delta M = 0.25\text{--}0.3 \text{ T}$, associated with the abrupt magnetization change at the transition, is assumed. The $\Delta T/\Delta H$ values are obtained from $\Delta T = 4 \text{ K}$ with a $\Delta H_a = 4 \text{ T}$ from the $M(T)$ curves in Fig. 1, and $\Delta H = H_{T\beta} - H_{T\alpha}$ and $\Delta T = T_\beta - T_\alpha$ in the case of $M(H)$ curves in Fig. 2. In the case of Eq. (4) the estimated error on $\Delta H/\Delta T$ may be much larger than 10% due to the limited number of available $M(T)$ and $M(H)$ curves and uncertainties in the ΔM value.

Among other possible sources of error the effect of magnetic hysteresis was also calculated from the comparison of $M(H)_T$ “forward and return” magnetization branches. The results show that hysteresis losses only contribute with $\sim 2 \text{ kJ/kg}$, a value at least one order of magnitude lower than the total heat exchanged during the transformation (of the order of 20 kJ/kg).²⁰

The entropy change ΔS can also be derived from the stress-strain $\sigma(\epsilon)$ behavior of the $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ SCs. Mechanical testing was performed with a double column test machine fitted with an optical extensometer, a Peltier cell heater/cooler, and a Cu-Constantan thermocouple to measure T . Before each mechanical compression along [100] the SC conditions were reset by heating above A_f . No magnetic field was applied.

Isothermal $\sigma(\epsilon)_T$ curves exhibit different Young's moduli $Y = \Delta\sigma/\Delta\epsilon$, which are connected with the martensite and austenite phases, see Fig. 4 and Ref. 21. The martensite phase

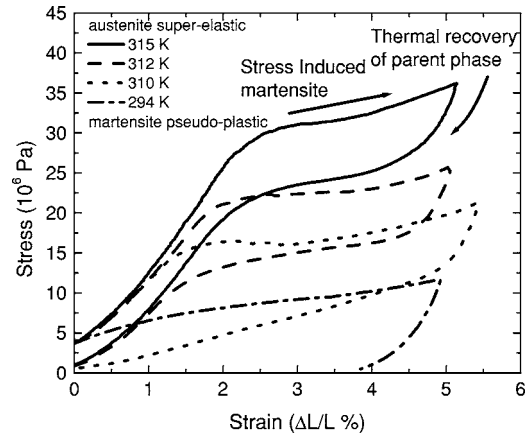


FIG. 4. [100] compressive stress-strain curves measured on the oriented single crystals at different temperatures. Below 311 K the sample in the martensite phase shows a pseudoplastic behavior with a yielding stress $\sim 5 \text{ MPa}$. In the austenite phase, at temperatures above 312 K the sample becomes superelastic.

easily accommodates stress through the process of detwinning and twin boundary motion, with values of $Y < 500 \text{ MPa}$, while the austenite phase results mechanically stiffer with $Y \approx 1 \text{ GPa}$. In Fig. 4 we observe that: (a) at $T = 294 \text{ K}$ a large strain variation $\Delta\epsilon \sim 5\%$ can be achieved with a small stress increase $\Delta\sigma < 10 \text{ MPa}$, with an almost constant modulus $Y \approx 200 \text{ MPa}$. Upon stress removal only a limited strain recovery occurs, indicating a pseudoplastic behavior; (b) At $T = 310 \text{ K}$ close to the M - A transition, Y increases to $\approx 700 \text{ MPa}$ but the behavior is still pseudoplastic, with a well defined yielding point at $\epsilon = 2\%$, where Y decreases to $\approx 150 \text{ MPa}$. Again, a very limited strain recovery is found upon unloading; (c)–(d) at $T = 315 \text{ K}$ and above, the material is in the austenite phase, the $\sigma(\epsilon)_T$ curve has a much steeper initial slope $Y \approx 1.2 \text{ GPa}$ up to $\epsilon = 2.5\%$. Beyond this threshold a lower slope $Y \approx 150 \text{ MPa}$ is found up to 5% strain, indicating that the sample has undergone a complete stress-induced A - M transformation. An almost complete strain recovery is achieved upon stress removal through a reverse M - A transformation (superelastic behavior).

In the case of a stress-induced phase transition, under the assumption of a small volume change $\Delta V < 1\%$,²² it is possible to estimate ΔS using again the anisotropic expression for the Clausius-Clapeyron equation $d\sigma/dT = -Q/T_M \epsilon_X$ where σ is the magnitude of the stress, and ϵ_X is the lattice contraction along the applied stress σ direction.^{20,23} Using the yielding points obtained from Fig. 4 we can estimate that $d\sigma/dT \approx 2.9 \text{ MPa/K}$ and $\epsilon_X \approx 6\%$ corresponds to a complete A - M transformation. In this case we obtain a $|\Delta S| \approx 22 \text{ J kg}^{-1} \text{ K}^{-1}$, in agreement with the $|\Delta S| \approx 24 \text{ J kg}^{-1} \text{ K}^{-1}$ value obtained for a temperature-induced phase transformation.

In order to better characterize the magnetocaloric potential of $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ SCs, the extremely large ΔS values obtained using the Maxwell relation [Eqs. (2) and (3)], which make this alloy a promising MCE material, were compared with the direct measurement of the adiabatic temperature rise $\Delta T_{ad}(T_s)_{\Delta H}$ associated with a magnetic field variation ΔH . ΔT_{ad} values were measured using an adiabatic cell inserted

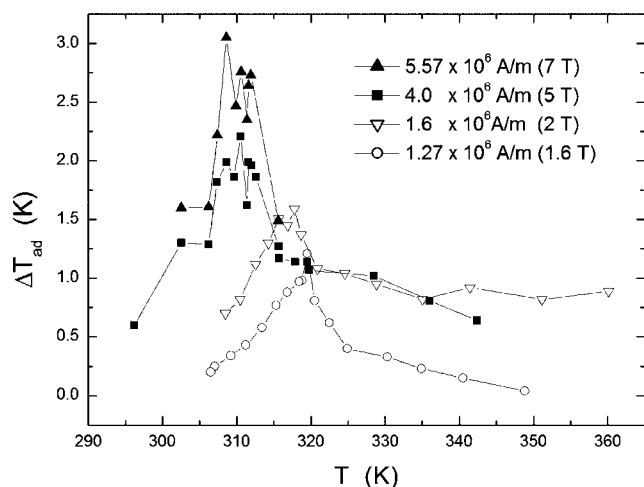


FIG. 5. Summary of the adiabatic temperature changes $\Delta T_{ad}(T)_{\Delta H}$ induced by a variable magnetic field change ΔH . The temperature of the sample is first stabilized at $T(\Delta T/\Delta t \approx 0.05 \text{ K/min})$ and then an increasing/decreasing field ramp ΔH is applied, with peak values up to $4\text{--}5.57 \times 10^6 \text{ A/m}$ (5–7 T).

in a 7 T cryomagnet. After stabilizing the sample temperature at a reference point T_s with a $\Delta T/\Delta t$ drift less than $\pm 0.05 \text{ K/min}$, in the vicinity of the phase transition, an increasing (then decreasing) magnetic field ΔH was applied in a [100] sample direction at a constant rate of $\Delta H/\Delta T = 1 \text{ T/min}$ from 0 up to $H_{\max} = 1.27, 1.56, 4, 5.56 \times 10^6 \text{ A/m}$ (1.6, 2, 5, 7 T) and then back to 0. The field increase (decrease) is associated with an almost linear T increase (decrease) up to a peak value $T \approx T_s + \Delta T_{ad}$ and then back to $T_s \pm 0.1\text{--}0.2 \text{ K}$. In the case of an adiabatic transformation, the temperature of the lattice must change as the total entropy of the body during an A - M transformation is conserved. The experimental uncertainties of the order of $\pm 0.1\text{--}0.2 \text{ K}$, measured in direct contact with the sample, are connected to the nonideal adiabatic conditions, magnetic hysteresis and eddy currents. Figure 5 shows a plot of the ΔT_{ad} values measured at different temperatures and for different field variations ΔH during cooling from $T > 345 \text{ K}$ $> A_f$. The ΔT_{ad} peak is centered on the A - M transition and its amplitude increases with ΔH increasing from $1.27 \times 10^6 \text{ A/m}$ to $5.57 \times 10^6 \text{ A/m}$ (1.6–7 T). For a $\Delta H = 4 \times 10^6 \text{ A/m}$ (5 T), $\Delta T_{ad} \approx 2.2 \text{ K}$, while for $\Delta H = 5.56 \times 10^6 \text{ A/m}$ (7 T), $\Delta T_{ad} \approx 3 \text{ K}$. For $\Delta H > 1.56 \times 10^6 \text{ A/m}$ (2 T) the ΔT_{ad} curves show a plateau up to 360 K, a behavior connected to the field (or stress)-stabilization of the martensite phase at high temperature, and which is also found in the

$M(T)_H$ curves for $H > 8 \times 10^5 \text{ A/m}$ (1 T) (Fig. 1), where long tails of $M(T)_H$ are observed up to 360 K, due to an additional Zeeman energy term $M \cdot H$ which tends to stabilize the martensite phase well above A_f . The ΔT_{ad} peak shift from 317 to 310 K observed when ΔH increases, is partly reflected in the ΔS curves (Fig. 3). The ΔS curves also exhibit secondary features between $T = 313$ and 315 K, but their lower resolution and indirect derivation does not allow for a close comparison with the ΔT_{ad} curves.

CONCLUSIONS

Different isothermal and adiabatic experimental procedures were used in order to characterize the magnetostructural transition of $\text{Ni}_{55}\text{Mn}_{20}\text{Ga}_{25}$ oriented single crystals and also to evaluate its MCE potential. A good agreement was found between $|\Delta S|$ values connected to the first order phase transition, obtained with temperature-induced ($24 \text{ J kg}^{-1} \text{ K}^{-1}$), stress-induced ($22 \text{ J kg}^{-1} \text{ K}^{-1}$) and field-induced transformations ($24\text{--}29 \text{ J kg}^{-1} \text{ K}^{-1}$ using the Clausius-Clapeyron equation and a proper ΔM value). The Maxwell approach [Eqs. (2) and (3)] was used to evaluate the entropy change in the whole 0–5 T applied field range, yielding a much larger value $|\Delta S| = 86 \text{ J kg}^{-1} \text{ K}^{-1}$, connected to the temperature dependence of the magnetization $M(T)$ within the two structural phases and at the transition point as depicted in Fig. 1.²

The great disparity between the very large isothermal $|\Delta S|$ values and the adiabatic temperature change $\Delta T \sim 2.2 \text{ K}$ is connected to the large heat capacity C_p and its variation within the transition interval,²⁴ and future investigations should help clarify the temperature dependence of C_p under intense applied fields. These results indicate that direct ΔT_{ad} measurements are the most reliable method for the evaluation of the MCE potential of a material, and this is particularly true in the case of transition metal alloys where, due to the rather high C_p with respect to rare earth systems,^{24,25} important differences can be found between the values of isothermal entropy and adiabatic temperature changes.

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